# Foundation Calculation Report: «1750 OX Residences - 1750 N Oxford Ave. - Eau Claire, WI»

#### XC structural engineering

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## 1 Building codes

The following building and material codes were used for the design:

 $\bullet\;$  Building code

 International Building Code, 2018 Edition (IBC 2018) with reference to Minimum Design Loads for Buildings and Other Structures by the American Society of Civil Engineers, 2016 Edition (ASCE 7).

#### Material codes

- Reinforced Concrete: Building Code Requirements for Structural Concrete and Commentary by the American Concrete Institute, 2019 Edition (ACI 318).
- Masonry: Building Code Requirements and Specification for Masonry Structures and Companion Commentaries, 2013 Edition (ACI 530/530).

## 2 Loading criteria

A summary of the project-specific loading criteria follows (see appendix A for a detailed list of load values).

#### 2.1 Gravity loading

The gravity loads listed in Table 1 are in addition to the self weight of the structure. The minimum loading requirements were taken from ASCE 7 as well as the loading criteria supplied by the engineer of record. Loads are given in pounds per square foot (psf).

Use Superimposed Live Loading Dead Loading Parking Garage 40 3 125 28 Storage/HVAC Stairways, exits 100 28 Level 1 residential 40 28 Level 1 corridors 100 28 Level 1 office, recreational 100 28 Level 1 courtyard (footprint) 150 150 Elevated levels residential 40 28 Elevated levels corridors 40 28 Cornices 60 28 Balconies 40 Roof 20 28

Table 1: Gravity Loads

In addition to these uniform slab loads, a perimeter dead load of 12 psf was applied to the structure to account for the weight of the cladding system.

#### 2.2 Wind design criteria

Wind loading is in accordance with the IBC and ASCE 7 requirements as shown in Table 2.

#### 2.3 Snow loading

Wind loading is in accordance with the ASCE 7 requirements as shown in Table 3.

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Table 2: Wind Design Criteria

Parameter	Value
Basic Wind Speed, 3-second gust (ultimate)	115 mph
Basic Wind Speed, 3-second gust (nominal)	90 mph
Exposure	В
Occupancy Category	II
Importance Factor $(I_w)$	1.0
Topographic Factor $(K_{zt})$	1.0
Enclosure Classification	Enclosed
Mean Roof Height (h)	33'

Table 3: Snow Design Criteria

Parameter	Value
Ground snow load $p_g$	60  psf
Terrain category	В
Exposure factor $C_e$	1.0
Thermal factor $C_t$	1.0
Occupancy Category	II
Snow load importance factor $I_s$	1.0
Snow load flat roof	42 psf

# 3 Seismic design criteria

Seismic loads are in accordance with the IBC requirements as shown in Table 4.

Table 4: Seismic Design Criteria

Parameter	Value
Building Latitude/Longitude	44°49'01.8"N 91°30'34.8"W
Occupancy Category	II
Importance Factor $I_e$	1.0
Mapped Spectral Acceleration	$S_s = 0.045; S_1 = 0.038$
Site Class	В
Site Class Coefficients	$F_a = 1.0; F_v = 1.0$
Spectral Response Coefficients	$S_{DS} = 0.03; S_{D1} = 0.025$
Seismic Design Category	A

## 4 Materials

The material properties used for the design are summarized in Tables 5 and 6.

Table 5: Concrete properties

Member	Nominal $\mathbf{f}'_c$
Footings	3.0 ksi
Basement Walls	4.0 ksi
Foundation frost walls	4.0 ksi
Stair landings and treads	4.0 ksi
Slab on grade	4.0 ksi

Table 6: Reinforcement properties

Standard	Nominal $f_y$
All ASTM A615 Grade 60	60 ksi

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# A Appendix A. Loading criteria

## A.1 Dead loads

Materials			
Wood structural panel	$36.0 \text{ pcf} = 5655 \frac{\text{newton}}{\text{meter}^3}$		
Concrete reinforced stone (including gravel)	$150.0 \text{ pcf} = 23563 \frac{\text{newton}}{\text{meter}^3}$		
Steel	$489.0 \text{ pcf} = 76816 \frac{\text{newton}}{\text{meter}^3}$		
Gypsum crete	$115.0 \text{ pcf} = 18065 \frac{\text{newton}}{\text{meter}^3}$		
Gypsum,loose	$70.0 \text{ pcf} = 10996 \frac{\text{newton}}{\text{meter}^3}$		
Earth (not submerged) sand and gravel (wet)	$120.0 \text{ pcf} = 18850 \frac{\text{newton}}{\text{meter}^3}$		
Water	$62.4 \text{ pcf} = 9802 \frac{\text{newton}}{\text{meter}^3}$		
Frame partitions Wood or steel studs, $\frac{1}{2}$ in gypsum board inside Wood studs, 2x4 unplastered Wood studs, 2x4 plastered one side Wood studs, 2x4 plastered two sides Movable steel partitions Frame walls Exterior stud wall 2x4 @ 16in, $\frac{5}{8}$ gypsum insulated, $\frac{3}{8}$ in siding Exterior stud wall 2x6 @ 16in, $\frac{5}{8}$ gypsum insulated,	8 psf = 383 pascal 4 psf = 192 pascal 12 psf = 575 pascal 20 psf = 958 pascal 4 psf = 192 pascal 11 psf = 526 pascal		
$\frac{3}{8}$ in siding Exterior stud wall with brick veneer CMU wall 8in Window, glass, frame and sash Cladding Fiber cement panels, large format $38.4$ in $\times$ $102$ in Fiber cement panels, small scale $9.6$ in $\times$ $102$ in Perforated metal panel at exterior HVAC location	48 psf = 2298 pascal 60 psf = 9425 pascal 8 psf = 383 pascal 3.2 psf = 153 pascal 3.2 psf = 153 pascal		
Floor truss Single chord @ 24in o.c. spacing Double chord @ 24in o.c. spacing Sheating Roof sheating Floor sheating Ceilings	3.2  psf = 153  pascal 4.25  psf = 203  pascal 3.5  psf = 167  pascal 2.5  psf = 120  pascal 2.5  psf = 120  pascal		
Deck composite sleeperes (3in)	9.00  psf = 431  pascal		

## A.2 Live loads

Occupancy or use	Uniform	Concentrated	Notes
Private rooms and corridors	40.0  psf =	-	IBC-2018 Table 1607.1
serving them in multifamily	1915 pascal		
dwelling			
Stairs and exits	100.0  psf =	300  pound =	IBC-2018 Table 1607.1.
	4788 pascal	1334 newton	Concentrated load on stair
			treads applied on an area
			of 2 inches by 2 inches
Balconies and decks	same as occu-	-	IBC-2018 Table 1607.1
	pancy served		
Garages (passenger vehicles	40.0  psf  =	-	IBC-2018 Table 1607.1
only)	1915 pascal		
Cornices	$60.0  ext{ psf} =$	-	IBC-2018 Table 1607.1
	2873 pascal		
Elevator machine room and con-	-	300  pound =	IBC-2018 Table 1607.1.
trol room grating		1334 newton	Concentrated load applied
			on an area of 2 inches by
			2 inches
Flat roof (not occupiable) +	20.0  psf =	300  pound =	IBC-2018 Table 1607.1
maintenace	958 pascal	1334 newton	
Yards and terraces, pedestrians	100.0  psf =	-	IBC-2018 Table 1607.1
	4788 pascal		
Sidewalks, vehicular driveways	250.0  psf =	8000  pound =	IBC-2018 Table 1607.1
and yards, subject to trucking	11970 pascal	35586 newton	
Corridors first floor	100.0  psf =	-	IBC-2018 Table 1607.1
	4788 pascal		
Store first floor	100.0  psf =	-	IBC-2018 Table 1607.1
	4788 pascal		

## A.3 Snow loads

Ground snow load	$p_q = 60.0 \text{ psf} = 2873 \text{ pascal}$	ASCE 7. Figure 7.1
Exposure factor	$\tilde{C}_e = 1.0$	ASCE 7. Table 7-2. Terrain cat-
		egory B, roof partially exposed
Thermal factor	$C_t = 1.0$	ASCE 7. Table 7-3.
Snow load importance factor	$I_s = 1.0$	ASCE 7. Table 7-4. Structure
		risk category II
Snow load flat roof	$p_f = 0.7 \times C_e \times C_t \times I_s \times p_g = 0.7 \times$	ASCE 7. Sect. 7.3
	$1.0 \times 1.0 \times 1.0 \times 60.0 = 42.0 \text{ psf} =$	
	2873 pascal	

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#### A.4 Wind loads

Alternate all-heights method.

Ultimate design wind speed  $V_{ult} = 115 \frac{\text{miles}}{\text{hour}} = 51 \frac{\text{meters}}{\text{second}}$ 

Velocity pressure exposure coef-  $K_z = 0.72$ 

ficient

Topographic factor  $K_{zt} = 1.0$ 

IBC-2018, sect. 1609.6. Regularly shaped building, less than 75 feet in height, not sensitive to dynamic effects, not channeling effects or buffeting, simple diaphragm building

IBC-2018, figure 1609.3(1). Risk category II building

ASCE 7, table 27.3.1. Exposure B, height above ground level  $z \approx 33$  feet

ASCE 7, sect. 26.8

Net pressure coefficients  $C_{net}$ . Main windforceresisting frames and systems

Description	$C_{net}$ + Internal	$C_{net}$ - Internal
	pressure	presure
Windward wall	0.43	0.73
Leeward wall	-0.51	-0.21
Sidewall	-0.66	-0.35
Parapet windward wall	1.2	28
Parapet leeward wall	-0.8	85
Flat roof	-1.09	-0.79

IBC-2018, Table 1609.6.2, enclosed

**Design wind pressures**  $P_{net}$ . Main windforce-resisting frames and systems

IBC-2018, sect. 1609.6.3

 $P_{net} = 0.00256 \times V^2 \times K_z \times C_{net} \times K_{zt}$ Description  $P_{net}$  + Internal  $P_{net}$  - Internal pressure presure Windward wall 10.5 psf = 501 pascal17.8 psf = 852 pascalLeeward wall -12.4 psf = -595 pascal-5.1 psf = -245 pascalSidewall -16.1 psf = -770 pascal-8.5 psf = -409 pascalParapet windward wall 31.2 psf = 1494 pascalParapet leeward wall -20.7 psf = -992 pascalFlat roof -26.6 psf = -1272 pascal -19.3 psf = -992 pascal

# A.5 Earthquake loads

Parameter 0.2-second spectral response acceleration	$S_s = 0.045$	IBC-2018, figure 1613.3.1(1). Site class B
Parameter 1-second spectral response acceleration	$S_1 = 0.038$	IBC-2018, figure 1613.3.1(2). Site class B
Seismic design category	$S_1 \leq 0.04 \ and \ S_s \leq 0.15 \rightarrow \mathrm{SDS} \ \mathrm{A}$	IBC-2018, sect. 1613.3.1
Site coefficients	$F_a = 1.0, F_v = 1.0$	IBC-2018, $tables$
		1613.3.3(1) and
		1613.3.3(2). Site class $B$
Maximum considered earthquake spectral re- sponse acceleration for short periods	$S_{MS} = F_a \cdot S_s = 0.045$	IBC-2018, sect. 163.3.3
	$S_{M1} = F_a \cdot S_1 = 0.038$	IBC-2018, sect. 163.3.3
Design spectral response acceleration parameters	$S_{DS} = \frac{2}{3} S_{MS} = 0.03$	IBC-2018, sect. 163.3.4
	$S_{D1} = \frac{2}{3}S_{M1} = 0.025$	IBC-2018, sect. 163.3.4

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