

Calculation Report: «1750 OX Residences - 1750 N Oxford Ave. - Eau Claire, WI»

XC structural engineering

August 7, 2019

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CALCULATION REPORT

1 Introduction and scope

This report describes the calculation procedure and data considered in order to design the structure of a new apartment building in Eau Claire, Wisconsin.

The construction consists in a three-story apartment building with a first-floor footprint of about 19,500 square feet, a below-grade parking garage with a footprint of about 27,200 square feet, perimeter retaining walls, a slab-on-grade, and a conventional foundation system.

The first floor system is precast hollow core concrete plank on precast beams and columns. For the upper floors and roof, the system is wood-framed. Retaining walls and slab on grade are comprised of cast in place concrete, except for three reinforced CMU walls next to the garage aisles, that will be demolished during the second phase of construction.

The foundation uses conventional cast in place concrete footings to transfer axial compression and lateral loads to the ground.

2 Building codes

The following building and material codes were used for the design:

- Building code
 - International Building Code, 2018 Edition (IBC 2018) with reference to Minimum Design Loads for Buildings and Other Structures by the American Society of Civil Engineers, 2016 Edition (ASCE 7).
- Material codes
 - Reinforced Concrete: Building Code Requirements for Structural Concrete and Commentary by the American Concrete Institute, 2019 Edition (ACI 318).
 - Masonry: Building Code Requirements and Specification for Masonry Structures and Companion Commentaries, 2013 Edition (ACI 530/530).

3 Loading criteria

A summary of the project-specific loading criteria follows (see appendix A for a detailed list of load values).

3.1 Gravity loading

The gravity loads listed in Table 1 are in addition to the self weight of the structure. The minimum loading requirements were taken from ASCE 7 as well as the loading criteria supplied by the engineer of record. Loads are given in pounds per square foot (psf).

In addition to these uniform slab loads, a perimeter dead load of 12 psf was applied to the structure to account for the weight of the cladding system.

3.2 Wind design criteria

Wind loading is in accordance with the IBC and ASCE 7 requirements as shown in Table 2.

3.3 Snow loading

Wind loading is in accordance with the ASCE 7 requirements as shown in Table 3.

Table 1: Gravity Loads

Use	Live Loading	Superimposed Dead Loading
Parking Garage	40	3
Storage/HVAC	125	28
Stairways, exits	100	28
Level 1 residential	40	28
Level 1 corridors	100	28
Level 1 office, recreational	100	28
Level 1 courtyard (footprint)	150	150
Elevated levels residential	40	28
Elevated levels corridors	40	28
Cornices	60	-
Balconies	40	28
Roof	20	28

Table 2: Wind Design Criteria

Parameter	Value
Basic Wind Speed, 3-second gust (ultimate)	115 mph
Basic Wind Speed, 3-second gust (nominal)	90 mph
Exposure	B
Occupancy Category	II
Importance Factor (I_w)	1.0
Topographic Factor (K_{zt})	1.0
Enclosure Classification	Enclosed
Mean Roof Height (h)	33'

Table 3: Snow Design Criteria

Parameter	Value
Ground snow load p_g	60 psf
Terrain category	B
Exposure factor C_e	1.0
Thermal factor C_t	1.0
Occupancy Category	II
Snow load importance factor I_s	1.0
Snow load flat roof	42 psf

4 Seismic design criteria

Seismic loads are in accordance with the IBC requirements as shown in Table 4.

Table 4: **Seismic Design Criteria**

Parameter	Value
Building Latitude/Longitude	44°49'01.8"N 91°30'34.8"W
Occupancy Category	II
Importance Factor I_e	1.0
Mapped Spectral Acceleration	$S_s = 0.045$; $S_1 = 0.038$
Site Class	B
Site Class Coefficients	$F_a = 1.0$; $F_v = 1.0$
Spectral Response Coefficients	$S_{DS} = 0.03$; $S_{D1} = 0.025$
Seismic Design Category	A

5 Materials

The material properties used for the design are summarized in Tables 5 and 6.

Table 5: **Concrete properties**

Member	Nominal f'_c
Footings	3.0 ksi
Basement Walls	4.0 ksi
Foundation frost walls	4.0 ksi
Stair landings and treads	4.0 ksi
Slab on grade	4.0 ksi

Table 6: **Reinforcement properties**

Standard	Nominal f_y
All ASTM A615 Grade 60	60 ksi

6 Design and analysis software

The computer software employed for the analysis of the structure is the Finite Element Program called **XC** (see program description at http://xcengineering.xyz/html_files/software.html).

7 Load combinations

The load combinations shown in tables 7 and 8 follow the strength design load combinations listed in IBC, section 1605.

Table 7: Combinations Ultimate Limit States

Identifier	Load Combination
ULS01:	1.4*D
ULS02_a:	1.2*D + 1.6*Lru + Lpu + 0.5*S
ULS02_b:	1.2*D + 1.6*Lrs + Lps + 0.5*S
ULS03_a:	1.2*D + 1.6*S + 0.5*Lru + Lpu
ULS03_b:	1.2*D + 1.6*S + 0.5*Lrs + Lps
ULS04_b:	1.2*D + 1.6*S + 0.5*W_NS
ULS04_a:	1.2*D + 1.6*S + 0.5*W_WE
ULS05_a:	1.2*D + W_WE + 0.5*Lru + Lpu
ULS05_b:	1.2*D + W_NS + 0.5*Lru + Lpu
ULS05_c:	1.2*D + W_WE + 0.5*Lrs + Lps
ULS05_d:	1.2*D + W_NS + 0.5*Lrs + Lps
ULS06_a:	1.2*D + 0.5*Lru + Lpu + 0.2*S
ULS06_b:	1.2*D + 0.5*Lrs + Lps + 0.2*S
ULS07_a:	0.9*D + W_WE
ULS07_b:	0.9*D + W_NS

Where:

D = dead load

Lru = live load (uniform on rooms)

Lrs = live load (staggered pattern on rooms)

Lpu = live load (uniform on patios)

Lps = live load (staggered pattern on patios)

S = snow load

W_WE = Wind West-East

W_NS = Wind North-South

Table 8: Combinations Serviceability Limit States

Identifier	Load Combination
SLS01:	1.0*D
SLS02_a:	1.0*D + 1.0*Lru + Lpu + 0.3*S
SLS02_b:	1.0*D + 1.0*Lrs + Lps + 0.3*S
SLS03_a:	1.0*D + 1.0*S + 0.3*Lru + 0.3*Lpu
SLS03_b:	1.0*D + 1.0*S + 0.3*Lrs + 0.3*Lps
SLS04_a:	1.0*D + W_WE + 1.0*Lru + Lpu
SLS04_b:	1.0*D + W_NS + 1.0*Lru + Lpu
SLS04_c:	1.0*D + W_WE + 1.0*Lrs + Lps
SLS04_d:	1.0*D + W_NS + 1.0*Lrs + Lps
SLS05_a:	1.0*D + W_WE
SLS05_b:	1.0*D + W_NS

Where:

- D = dead load
- Lru = live load (uniform on rooms)
- Lrs = live load (staggered pattern on rooms)
- Lpu = live load (uniform on patios)
- Lps = live load (staggered pattern on patios)
- S = snow load
- W_WE = Wind West-East
- W_NS = Wind North-South

8 Wood framing

9 Basement

9.1 Structural model

A three-dimensional elastic computer model of the substructure is analyzed using XC. The model includes first floor frame and columns (see figure 1). The hollow core planks are modelled using shell elements, while beams and columns are modelled using frame elements. Loads transmitted by 2nd, 3rd floors and roof are applied to the 1st. Load layout is shown in figure 10. See in figures 2 to 9 load distribution for each load case.

Linear loads are expressed in kN/m and surface loads in kN/m², where:

$$\begin{aligned}1 \text{ kN/m} &= 68.52178 \text{ lb/ft} \\1 \text{ kN/m}^2 &= 20.885434 \text{ psf}\end{aligned}$$

9. BASEMENT

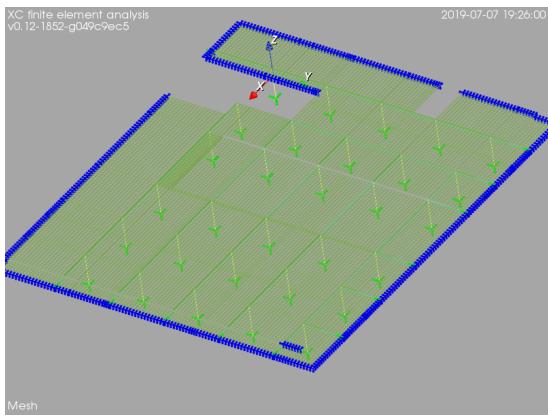


Figure 1: Elastic model, mesh.

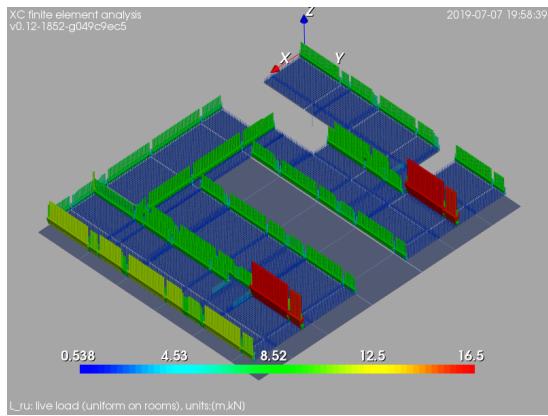


Figure 4: Load case L_{rs}: live load (staggered pattern on rooms) [units: kN,m].

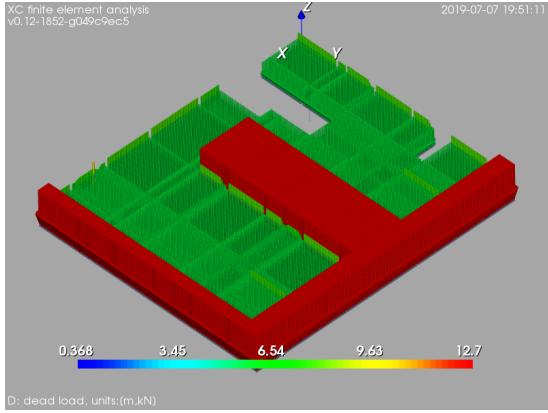


Figure 2: Load case D: dead load (include slab self-weight) [units: kN,m].

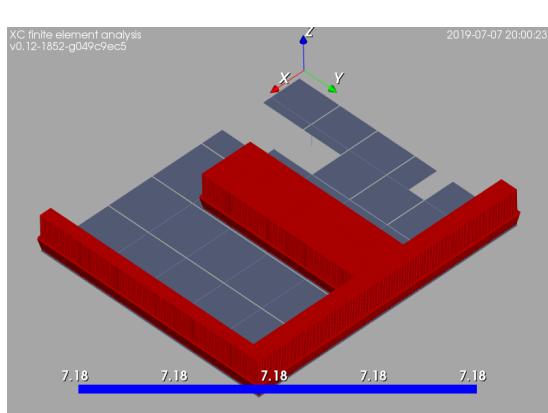


Figure 5: Load case L_{pu}: live load (uniform on patios) [units: kN,m].

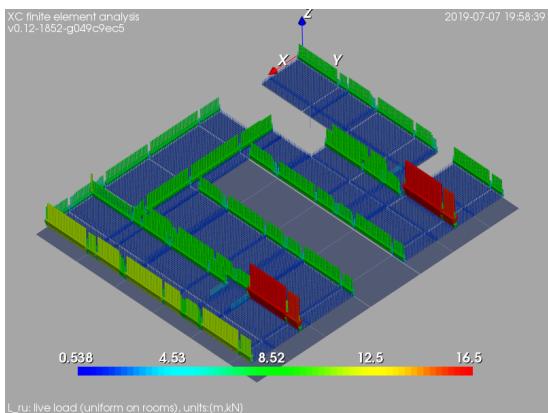


Figure 3: Load case L_{ru}: live load (uniform on rooms) [units: kN,m].

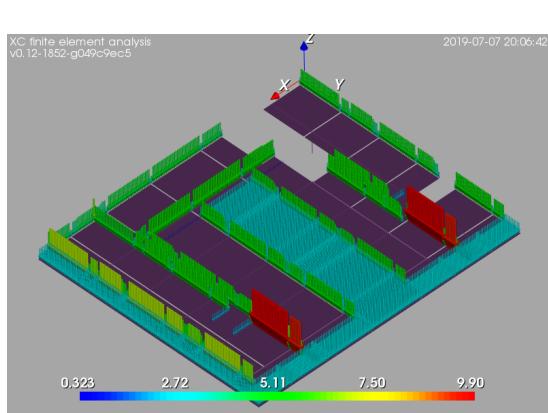


Figure 6: Load case S: snow [units: kN,m].

CALCULATION REPORT

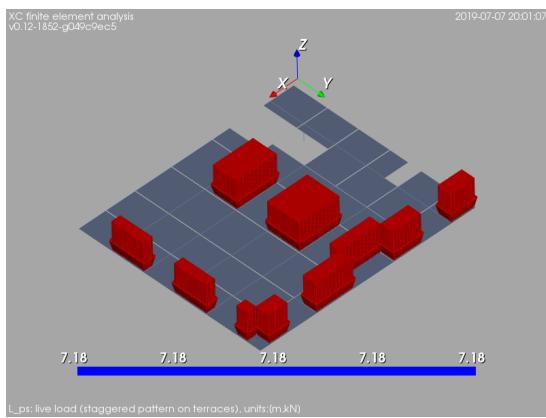


Figure 7: Load case Lps: live load (staggered pattern on patios) [units: kN,m].

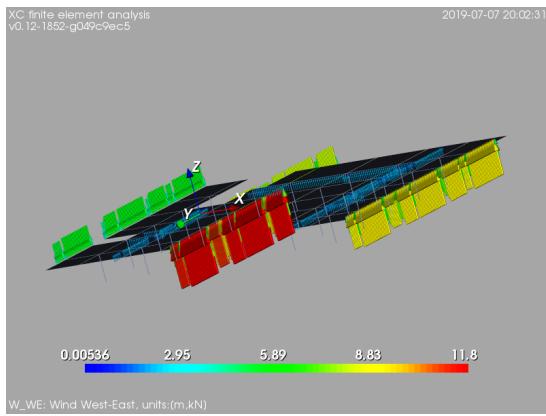


Figure 8: Load case W_WE: wind West-East [units: kN,m].

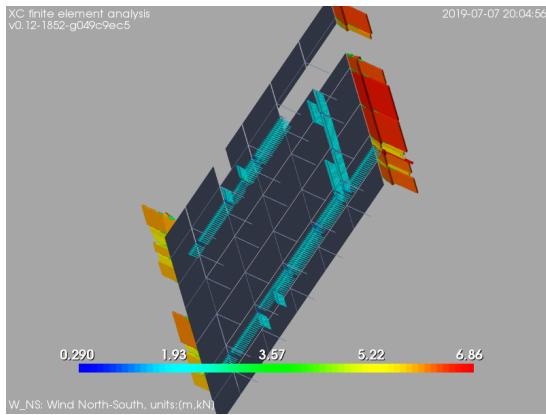


Figure 9: Load case W_NS: wind North-South [units: kN,m].

9. BASEMENT

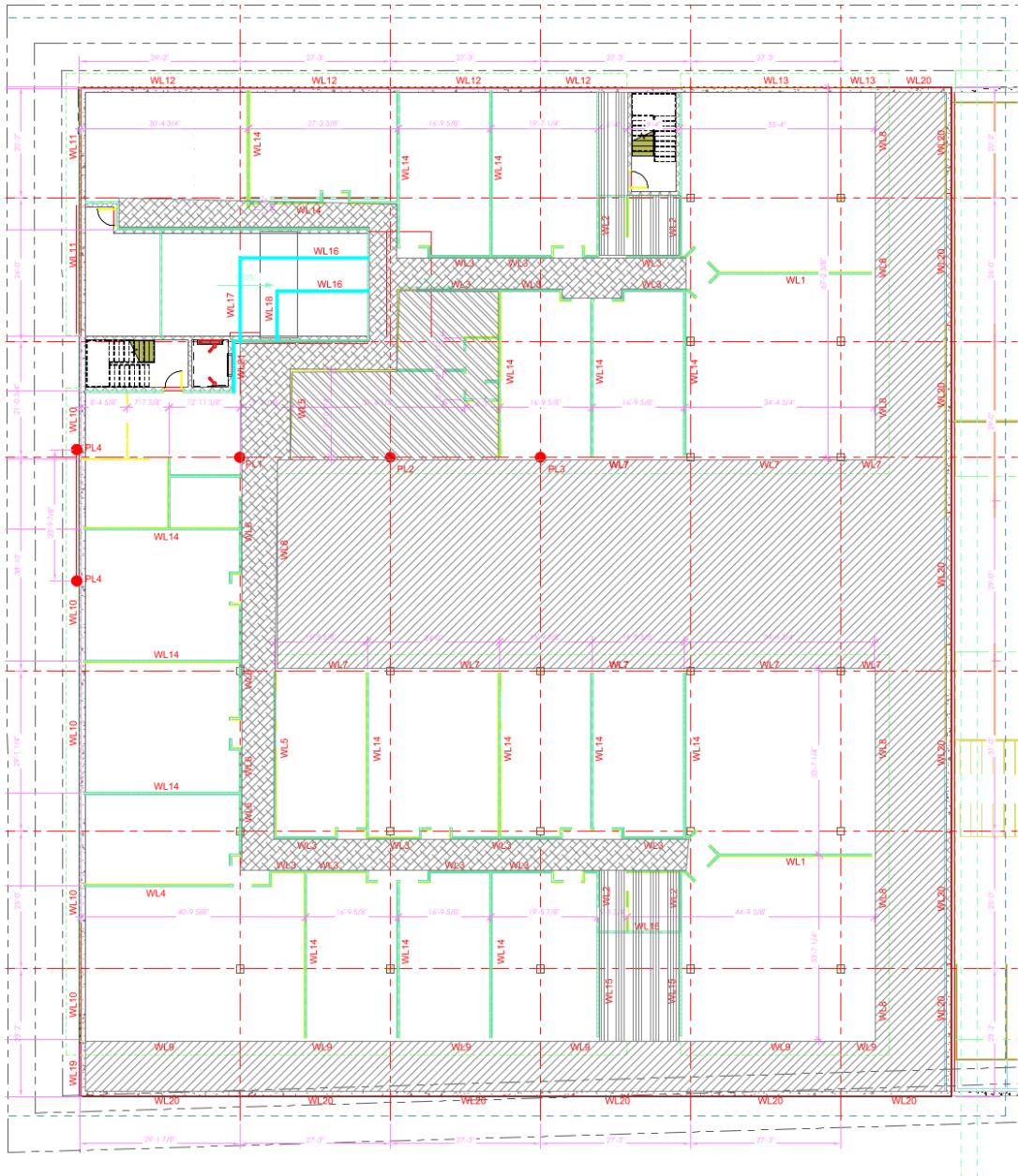


Figure 10: Load layout on first floor.

WALL LOAD SCHEDULE										
MARK	ELEV.	DEAD LOAD Kips/ft ²	LIVE LOAD Kips/ft ²	SNOW LOAD Kips/ft ²	WEATHER WIND LOAD Kips/ft ²	WIND LOAD Kips/ft ²	N/S WIND LOAD Kips/ft ²	EARTH PRESS. Kips/ft ²	CHORD LOAD Kips/ft ²	CHORD LOAD Kips/ft ²
WL1	0'-0"	1.51	0.11	0.40	N/A	0.40	N/A	0.15	N/A	N/A
WL2	0'-0"	0.83	0.74	0.44	0.40	N/A	0.40	N/A	N/A	N/A
WL3	0'-0"	1.12	1.84	1.10	0.40	N/A	0.40	0.15	N/A	N/A
WL4	0'-0"	1.05	1.57	0.76	0.40	N/A	0.40	0.15	N/A	N/A
WL5	0'-0"	1.11	0.73	1.07	0.40	0.40	0.40	0.15	N/A	N/A
WL6	0'-0"	1.58	1.67	1.00	1.61	2.39	N/A	0.15	N/A	N/A
WL8	0'-0"	0.50	N/A	N/A	N/A	0.39	1.20	N/A	N/A	N/A
WL9	0'-0"	1.73	2.26	1.36	1.84	N/A	N/A	0.15	N/A	N/A
WL10	0'-0"	0.50	N/A	N/A	N/A	0.39	0.39	0.20	2.50	N/A
WL11	0'-0"	0.50	N/A	N/A	N/A	0.39	1.26	N/A	2.50	N/A
WL12	0'-0"	1.55	1.57	0.54	N/A	1.08	N/A	0.15	2.50	N/A
WL13	0'-0"	1.58	1.67	1.00	N/A	1.08	N/A	0.15	2.50	N/A
WL14	0'-0"	0.27	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
WL15	1'-0"	1.07	1.03	1.48	0.40	N/A	0.40	0.15	N/A	N/A
WL16	1'-0"	0.95	1.10	0.40	N/A	0.40	0.40	0.15	N/A	N/A
WL17	1'-0"	0.94	1.07	1.07	0.40	N/A	0.39	0.40	N/A	N/A
WL18	1'-0"	0.69	0.20	0.20	0.40	N/A	0.39	0.40	N/A	N/A
WL19	1'-0"	N/A	N/A	N/A	N/A	N/A	N/A	N/A	2.50	N/A
WL20	1'-0"	N/A	N/A	N/A	N/A	N/A	N/A	N/A	2.50	N/A
WL21	1'-0"	N/A	N/A	N/A	N/A	N/A	N/A	N/A	2.50	N/A

POINT LOAD SCHEDULE			
MARK	DEAD LOAD Klb	LIVE LOAD Klb	SNOW LOAD Klb
PL1	15.24	25.01	15.01
PL2	30.47	50.02	30.02
PL3	15.24	25.01	15.01
PL4	15.24	32.01	15.01

SUPERIMPOSED UNIFORM LOAD SCHEDULE				
MARK	DEAD LOAD PSF	LIVE LOAD PSF	SNOW LOAD PSF	COMMENTS
	15.00	150.00	42.00	YARDS AND TERRACES PEDESTRIAN
	20.00	100.00	N/A	CORRIDORS FIRST FLOOR
	20.00	100.00	N/A	STAIRS AND EXITS
	20.00	100.00	N/A	STORE FIRST FLOOR
	20.00	40.00	N/A	PRIVATE ROOMS KITCHEN, BATH, ETC.

MARK	DIMENSIONS			BOTTOM REINFORCING		COLUMNS
	W	L	D	LONG	SHORT	
FT90a	9'-0"	9'-0"	1'-8"	(10)-#7	(10)-#7	A1 A2
FT90b	9'-0"	9'-0"	1'-8"	(10)-#8	(10)-#8	A3 A4 A5
FT96a	9'-6"	9'-6"	1'-8"	(10)-#7	(10)-#7	B2
FT96b	9'-6"	9'-6"	1'-8"	(10)-#8	(10)-#8	B3 B4 B5
FT100	10'-0"	10'-0"	2'-1"	(11)-#8	(11)-#8	F1 F2 F3 F4 F5
FT106	10'-6"	10'-6"	2'-3"	(11)-#8	(11)-#8	C1
FT110a	11'-0"	11'-0"	2'-1"	(12)-#8	(12)-#8	G2 G3 G4 G5
FT110b	11'-0"	11'-0"	2'-3"	(12)-#8	(12)-#8	D1 G1
FT116	11'-6"	11'-6"	2'-1"	(12)-#8	(12)-#8	C2 C3 C4 C5
FT120	12'-0"	12'-0"	2'-3"	(13)-#8	(13)-#8	D2 D3 D4 D5

COLUMN FOOTING SCHEDULE
1. REFER TO STRUCTURAL NOTES SHEET FOR LAPS IN STEEL REINFORCEMENT.
2. REFER TO FUNDATION PLAN FOR TOP OF FOOTING ELEVATIONS.
3. ALL FOOTING EXCAVATIONS SHALL BE INSPECTED AND APPROVED BY THE GEOTECHNICAL ENGINEER PRIOR TO PLACING CONCRETE

Table 9: Column footing schedule.

9.2 Footings

9.2.1 Loads

The loads acting on the footings are shown in §B.

9.2.2 Load combinations

The load combinations are shown in tables 7 and 8.

9.2.3 Footing dimensions and reinforcement

The dimensions and the reinforcement of the footings are indicated in the table 9. The position of the footing in the building grid is indicated at the last column.

9.2.4 Limit state checking

Allowable soil-bearing pressures. The results obtained for the verification of the soil-bearing capacity are shown in the table 10.

Flexure design. The capacity factor for the bending in the longitudinal and transverse directions are shown in figures 11 and 12.

Shear design. The results of the shear strength verification are shown in the table 11. The results of the punching shear strength verification are shown in table 12.

9.3 Basement walls

9.3.1 Introduction

The design is based in the following assumptions:

- Design wall with pinned base and pinned top.
- Neglect corner regions (wall spans one-way only).
- Top slab is in place and has achieved full strength prior to back-filling.
- Vehicular traffic around the building is represented by a uniform load of 250 psf (11.97 kN/m^2).

Foundation	Worst combination	Vertical load (kN)	Capacity factor
A1	SLS04_a	-356.20	0.33
A2	SLS02_a	-644.78	0.60
A3	SLS02_a	-950.92	0.88
A4	SLS02_a	-881.82	0.82
A5	SLS04_b	-933.03	0.86
B2	SLS02_a	-670.79	0.56
B3	SLS02_a	-1,030.65	0.86
B4	SLS02_a	-968.24	0.80
B5	SLS04_b	-972.32	0.81
C1	SLS02_a	-1,460.67	0.99
C2	SLS02_a	-1,742.45	0.99
C3	SLS02_a	-1,750.31	0.99
C4	SLS02_a	-1,751.62	0.99
C5	SLS02_a	-1,660.02	0.94
D1	SLS02_a	-1,648.12	1.02
D2	SLS04_a	-1,950.01	1.01
D3	SLS04_a	-1,959.12	1.02
D4	SLS04_a	-1,960.14	1.02
D5	SLS04_a	-1,838.69	0.96
F1	SLS02_a	-1,090.88	0.82
F2	SLS02_a	-997.32	0.75
F3	SLS02_a	-1,011.87	0.76
F4	SLS02_a	-1,005.30	0.75
F5	SLS04_b	-741.90	0.56
G1	SLS02_a	-1,496.86	0.93
G2	SLS02_a	-1,256.06	0.78
G3	SLS02_a	-1,227.94	0.76
G4	SLS02_a	-1,137.75	0.70
G5	SLS04_b	-1,167.26	0.72

Table 10: Soil bearing pressures. Capacity factors

Footing	Worst combination	Vertical load (kN)	thickness (m)	l (m)	d (m)	c (m)	Vd/l kN/m	Vu kN/m	CF
A1	SLS04_a	-356.20	0.51	2.74	0.46	0.41	33.66	280.00	0.12
A2	SLS02_a	-644.78	0.51	2.74	0.46	0.41	60.94	280.00	0.22
A3	SLS02_a	-950.92	0.51	2.74	0.46	0.41	89.87	280.00	0.32
A4	SLS02_a	-881.82	0.51	2.74	0.46	0.41	83.34	280.00	0.30
A5	SLS04_b	-933.03	0.51	2.74	0.46	0.41	88.18	280.00	0.31
B2	SLS02_a	-670.79	0.51	2.90	0.46	0.41	63.00	280.00	0.22
B3	SLS02_a	-1,030.65	0.51	2.90	0.46	0.41	96.79	280.00	0.35
B4	SLS02_a	-968.24	0.51	2.90	0.46	0.41	90.93	280.00	0.32
B5	SLS04_b	-972.32	0.51	2.90	0.46	0.41	91.31	280.00	0.33
C1	SLS02_a	-1,460.67	0.69	3.20	0.62	0.41	111.20	378.00	0.29
C2	SLS02_a	-1,742.45	0.64	3.51	0.57	0.41	138.68	350.00	0.40
C3	SLS02_a	-1,750.31	0.64	3.51	0.57	0.41	139.31	350.00	0.40
C4	SLS02_a	-1,751.62	0.64	3.51	0.57	0.41	139.42	350.00	0.40
C5	SLS02_a	-1,660.02	0.64	3.51	0.57	0.41	132.12	350.00	0.38
D1	SLS02_a	-1,648.12	0.69	3.35	0.62	0.41	125.50	378.00	0.33
D2	SLS04_a	-1,950.01	0.64	3.66	0.57	0.41	153.65	350.00	0.44
D3	SLS04_a	-1,959.12	0.64	3.66	0.57	0.41	154.37	350.00	0.44
D4	SLS04_a	-1,960.14	0.64	3.66	0.57	0.41	154.45	350.00	0.44
D5	SLS04_a	-1,838.69	0.64	3.66	0.57	0.41	144.88	350.00	0.41
F1	SLS02_a	-1,090.88	0.64	3.05	0.57	0.41	87.98	350.00	0.25
F2	SLS02_a	-997.32	0.64	3.05	0.57	0.41	80.44	350.00	0.23
F3	SLS02_a	-1,011.87	0.64	3.05	0.57	0.41	81.61	350.00	0.23
F4	SLS02_a	-1,005.30	0.64	3.05	0.57	0.41	81.08	350.00	0.23
F5	SLS04_b	-741.90	0.64	3.05	0.57	0.41	59.84	350.00	0.17
G1	SLS02_a	-1,496.86	0.69	3.35	0.62	0.41	113.98	378.00	0.30
G2	SLS02_a	-1,256.06	0.64	3.35	0.57	0.41	100.75	350.00	0.29
G3	SLS02_a	-1,227.94	0.64	3.35	0.57	0.41	98.50	350.00	0.28
G4	SLS02_a	-1,137.75	0.64	3.35	0.57	0.41	91.26	350.00	0.26
G5	SLS04_b	-1,167.26	0.64	3.35	0.57	0.41	93.63	350.00	0.27

Table 11: Shear design. Capacity factors

Footing	Worst combination	Vertical load (kN)	thickness (m)	L (m)	d (m)	c (m)	Vd/l kN/m	Vu kN/m	CF
A1	SLS04.a	-356.20	0.51	2.74	0.46	0.41	92.90	517.97	0.18
A2	SLS02.a	-644.78	0.51	2.74	0.46	0.41	168.16	517.97	0.32
A3	SLS02.a	-950.92	0.51	2.74	0.46	0.41	248.00	517.97	0.48
A4	SLS02.a	-881.82	0.51	2.74	0.46	0.41	229.98	517.97	0.44
A5	SLS04.b	-933.03	0.51	2.74	0.46	0.41	243.33	517.97	0.47
B1	SLS02.a	-429.53	0.51	2.90	0.46	0.41	113.28	517.97	0.22
B2	SLS02.a	-670.79	0.51	2.90	0.46	0.41	176.91	517.97	0.34
B3	SLS02.a	-1,030.65	0.51	2.90	0.46	0.41	271.82	517.97	0.52
B4	SLS02.a	-968.24	0.51	2.90	0.46	0.41	255.36	517.97	0.49
B5	SLS04.b	-972.32	0.51	2.90	0.46	0.41	256.43	517.97	0.50
C1	SLS02.a	-1,460.67	0.69	3.20	0.62	0.41	320.25	699.26	0.46
C2	SLS02.a	-1,742.45	0.64	3.51	0.57	0.41	410.79	647.47	0.63
C3	SLS02.a	-1,750.31	0.64	3.51	0.57	0.41	412.64	647.47	0.64
C4	SLS02.a	-1,751.62	0.64	3.51	0.57	0.41	412.95	647.47	0.64
C5	SLS02.a	-1,660.02	0.64	3.51	0.57	0.41	391.35	647.47	0.60
D1	SLS02.a	-1,648.12	0.69	3.35	0.62	0.41	365.00	699.26	0.52
D2	SLS04.a	-1,950.01	0.64	3.66	0.57	0.41	462.88	647.47	0.71
D3	SLS04.a	-1,959.12	0.64	3.66	0.57	0.41	465.05	647.47	0.72
D4	SLS04.a	-1,960.14	0.64	3.66	0.57	0.41	465.29	647.47	0.72
D5	SLS04.a	-1,838.69	0.64	3.66	0.57	0.41	436.46	647.47	0.67
F1	SLS02.a	-1,090.88	0.64	3.05	0.57	0.41	250.18	647.47	0.39
F2	SLS02.a	-997.32	0.64	3.05	0.57	0.41	228.72	647.47	0.35
F3	SLS02.a	-1,011.87	0.64	3.05	0.57	0.41	232.06	647.47	0.36
F4	SLS02.a	-1,005.30	0.64	3.05	0.57	0.41	230.55	647.47	0.36
F5	SLS04.b	-741.90	0.64	3.05	0.57	0.41	170.14	647.47	0.26
G1	SLS02.a	-1,496.86	0.69	3.35	0.62	0.41	331.50	699.26	0.47
G2	SLS02.a	-1,256.06	0.64	3.35	0.57	0.41	293.79	647.47	0.45
G3	SLS02.a	-1,227.94	0.64	3.35	0.57	0.41	287.22	647.47	0.44
G4	SLS02.a	-1,137.75	0.64	3.35	0.57	0.41	266.12	647.47	0.41
G5	SLS04.b	-1,167.26	0.64	3.35	0.57	0.41	273.02	647.47	0.42

Table 12: Two-way shear design. Capacity factors

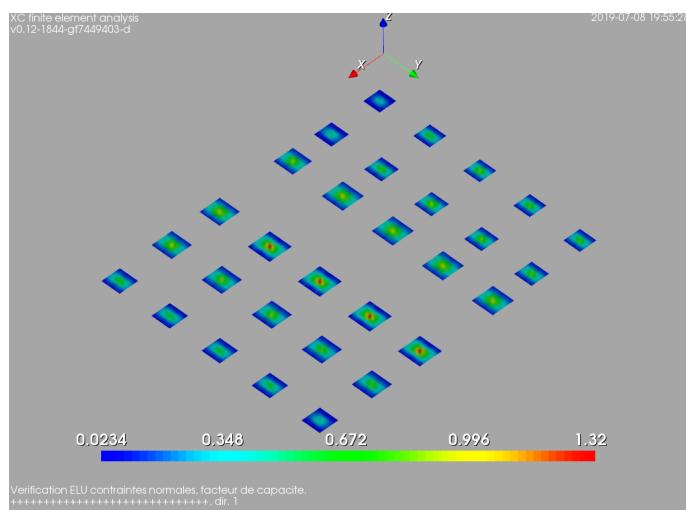


Figure 11: Flexure in the longitudinal direction. Capacity factor.

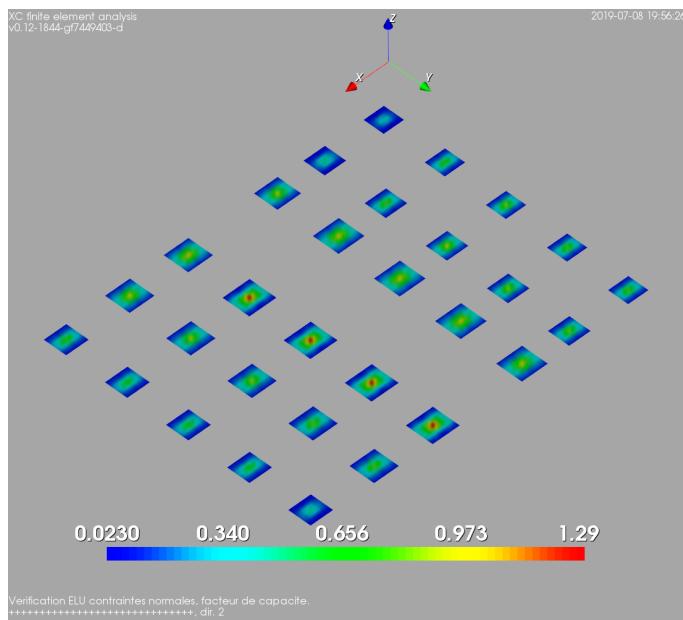


Figure 12: Flexure in the transverse direction. Capacity factor.

- The vertical response of the soil calculated using a Winkler model with a sub-grade reaction module of set of 200 pounds per cubic inch ($54.29 \times 10^6 \text{ N/m}^3$).
- Water table deep below structure.

9.3.2 Load determination

Self weight. The self weight of the reinforced concrete is calculated from its density: 2500 kg/m^3 .

Axial loads from building. The loads transferred by the top slab to the wall are as follows:

Building side	Load	Phase 1 (kN/m)	Phase 2 (kN/m)
North	SnowL	10.06	10.06
	LiveL	21.67	21.67
	Wind_NS	-15.12	-15.12
	Wind_WE	-1.33	-1.33
	DeadL	31.54	31.54
South	SnowL	8.04	16.08
	LiveL	14.22	28.44
	Wind_NS	4.97	9.95
	Wind_WE	-0.23	-0.46
	DeadL	20.58	41.15
East	SnowL	11.96	11.96
	LiveL	23.75	23.75
	Wind_NS	-0.07	-0.07
	Wind_WE	12.97	12.97
	DeadL	30.87	30.87
West	SnowL	15.02	15.02
	LiveL	27.15	27.15
	Wind_NS	-0.20	-0.20
	Wind_WE	-13.20	-13.20
	DeadL	29.81	29.81

9.3.3 Load combinations

Serviceability limit states		
Equation 16-8	EQ1608	1.0*selfWeight+1.0*deadLoad
Equation 16-9	EQ1609A	1.0*selfWeight+1.0*deadLoad+1.0*trafficLoad
Equation 16-9	EQ1609B	1.0*selfWeight+1.0*deadLoad+1.0*liveLoad
Equation 16-10	EQ1610	1.0*selfWeight+1.0*deadLoad+1.0*snowLoad
Equation 16-11	EQ1611A	1.0*selfWeight+1.0*deadLoad+0.75*trafficLoad+0.75*snowLoad
Equation 16-11	EQ1611B	1.0*selfWeight+1.0*deadLoad+0.75*liveLoad+0.75*snowLoad
Equation 16-12	EQ1612	1.0*selfWeight+1.0*deadLoad+0.6*windLoad
Equation 16-13	EQ1613A	1.0*selfWeight+1.0*deadLoad+0.45*windLoad+0.75*trafficLoad+0.75*snowLoad
Equation 16-13	EQ1613B	1.0*selfWeight+1.0*deadLoad+0.45*windLoad+0.75*liveLoad+0.75*snowLoad
Equation 16-14		doesn't apply
Equation 16-15	EQ1615	0.6*selfWeight+0.6*deadLoad+0.6*windLoad
Equation 16-16		doesn't apply

Ultimate limit states.		
Equation 16-1	EQ1601	1.4*selfWeight+1.4*deadLoad
Equation 16-2	EQ1602A	1.2*selfWeight+1.2*deadLoad+1.6*trafficLoad+0.5*snowLoad
Equation 16-2	EQ1602B	1.2*selfWeight+1.2*deadLoad+1.6*liveLoad+0.5*snowLoad
Equation 16-3	EQ1603A	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*trafficLoad
Equation 16-3	EQ1603B	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*liveLoad
Equation 16-3	EQ1603C	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*windLoad
Equation 16-4	EQ1604A	1.2*selfWeight+1.2*deadLoad+1.0*windLoad+0.5*trafficLoad+0.5*snowLoad
Equation 16-4	EQ1604B	1.2*selfWeight+1.2*deadLoad+1.0*windLoad+0.5*liveLoad+0.5*snowLoad
Equation 16-5	EQ1605A	1.2*selfWeight+1.2*deadLoad+0.5*trafficLoad+0.7*snowLoad
Equation 16-5	EQ1605B	1.2*selfWeight+1.2*deadLoad+0.5*liveLoad+0.7*snowLoad
Equation 16-6		doesn't apply
Equation 16-7		doesn't apply

Earth pressure. The soil pressure over the wall has been calculated using the lateral pressure at rest with a coefficient $K_0 = 0.5$.

CONCRETE WALL REINFORCING SCHEDULE					
MARK	TYPE	THICKNESS	REINFORCEMENT		REMARKS
			VERTICAL	HORIZONTAL	
W1	CONCRETE	10"	5#'s AT 18"o.c.	5#'s AT 12"o.c.	inside face
W2	CONCRETE	10"	5#'s AT 12"o.c.	5#'s AT 12"o.c.	inside face
W3	CONCRETE	10"	6#'s AT 12"o.c.	5#'s AT 12"o.c.	inside face
W4	CONCRETE	8"	4#'s AT 12"o.c.	3#'s AT 12"o.c.	centered in wall thickness

CONCRETE WALL REINFORCING SCHEDULE NOTES:
1. REFER TO STRUCTURAL NOTES SHEET FOR LAPS IN STEEL REINFORCEMENT.
2. COORDINATE AND VERIFY ALL DIMENSIONS WITH ARCHITECTURAL DRAWINGS AND EXIST. CONDITIONS

Table 13: Concrete walls reinforcing schedule

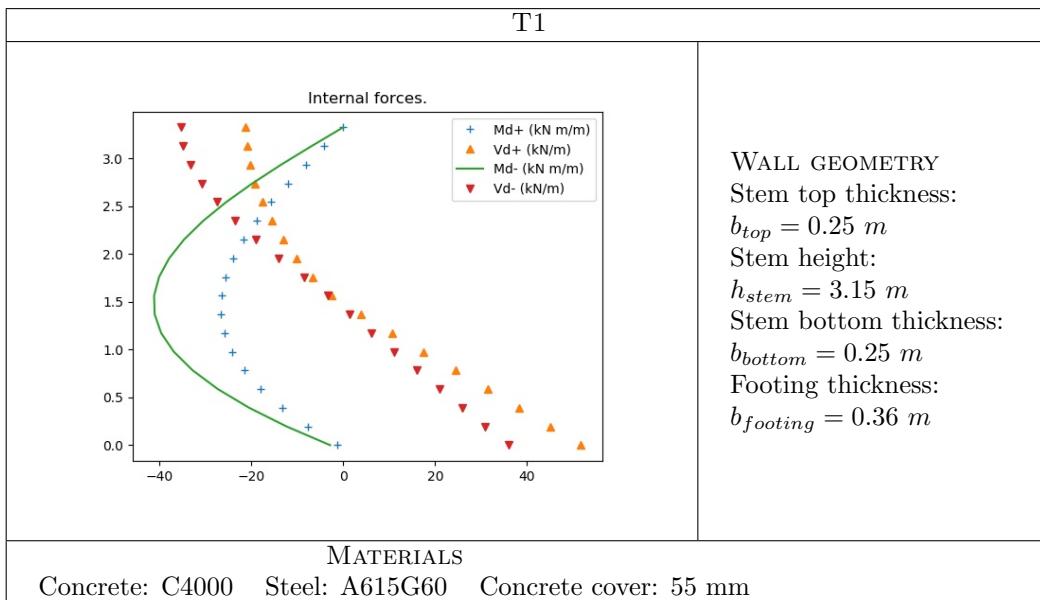


Table 14: Wall materials and dimensions T1

9.3.4 Stem dimensions and reinforcement

The thickness and the reinforcement for the walls are indicated in the table 13.

Wall types. For analysis purposes we have considered the following wall types:

Wall	Stem height (m)
T1	3.15
T2	2.74
T3	3.53
T4	3.12
T5	2.51
T6	3.43

Internal forces. The envelope of internal forces envelope for each of the walls are given in tables 14 to 19.

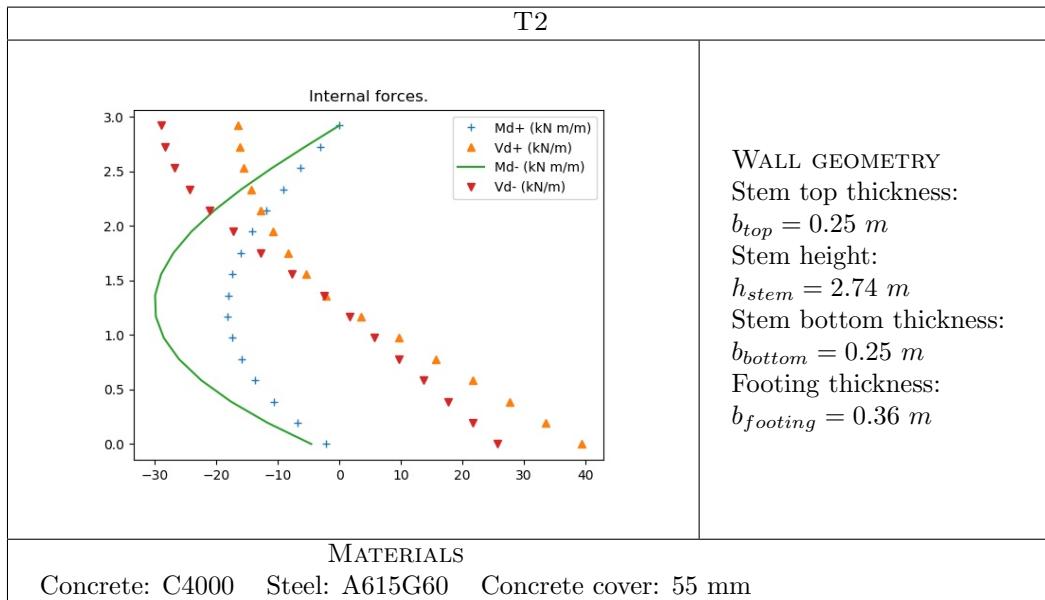


Table 15: Wall materials and dimensions T2

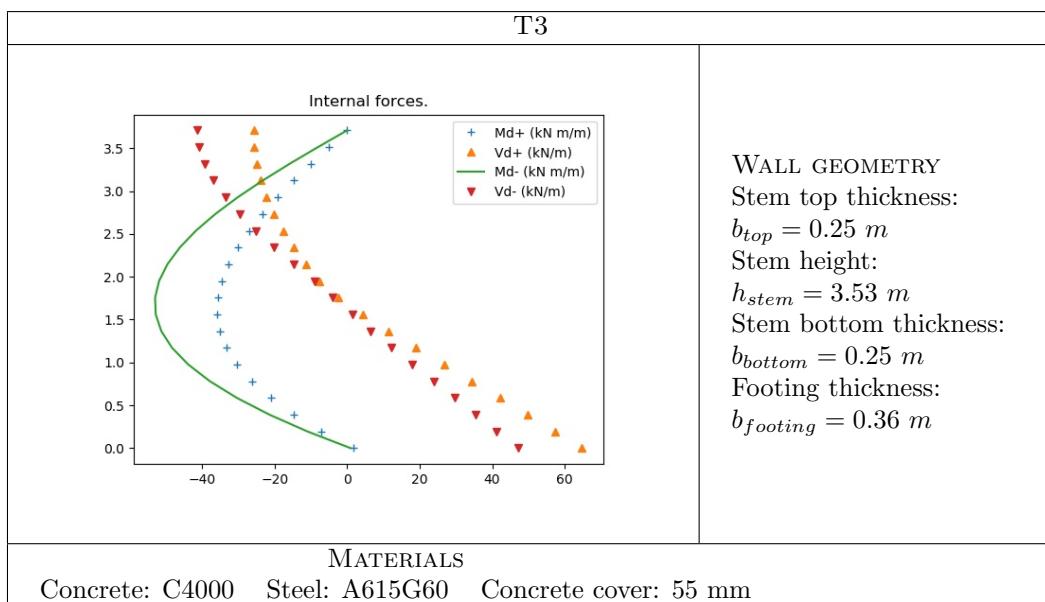


Table 16: Wall materials and dimensions T3

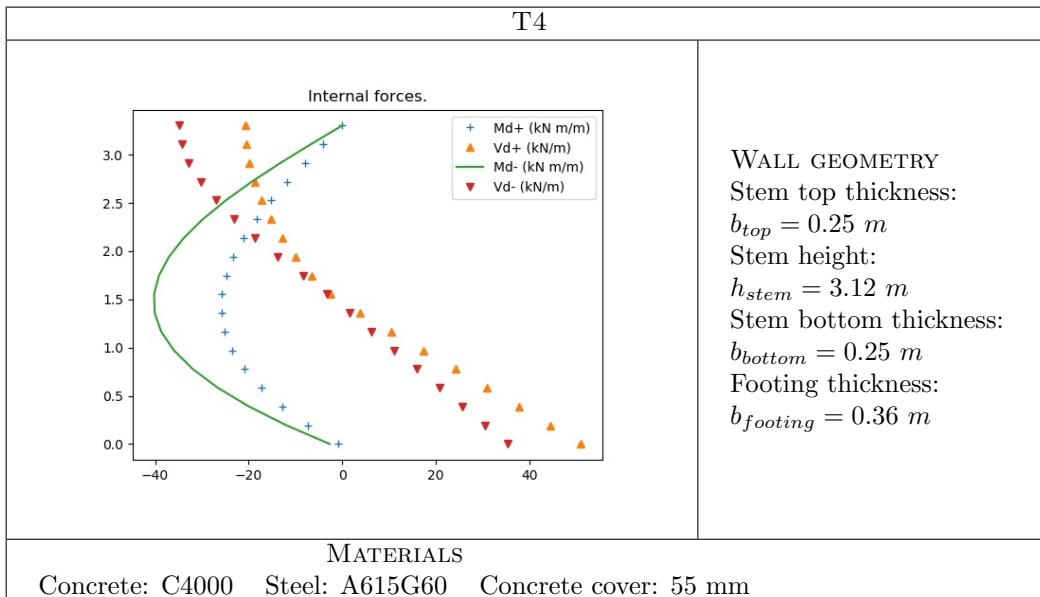


Table 17: Wall materials and dimensions T4

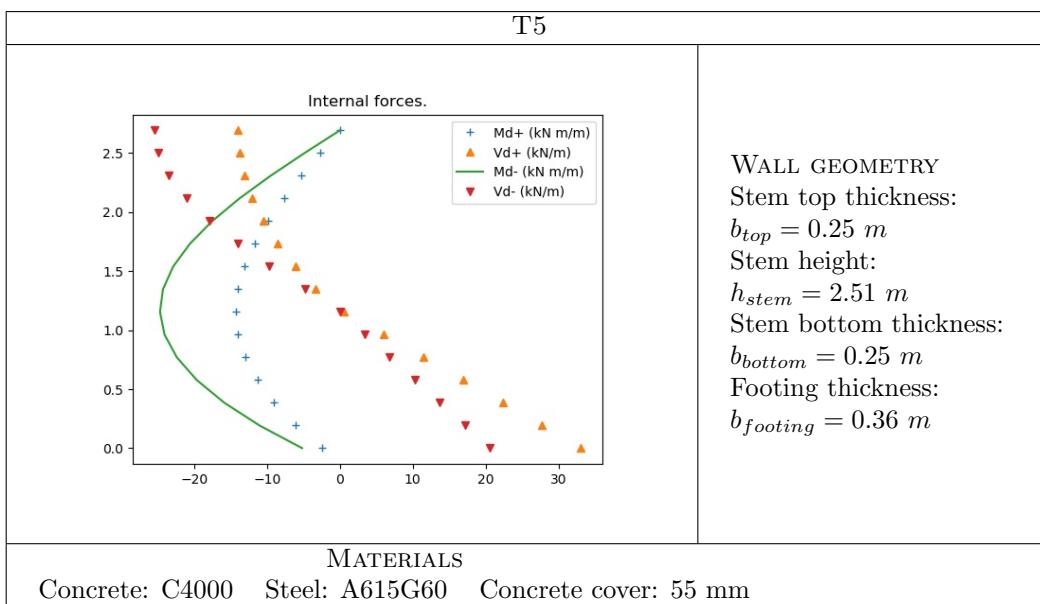


Table 18: Wall materials and dimensions T5

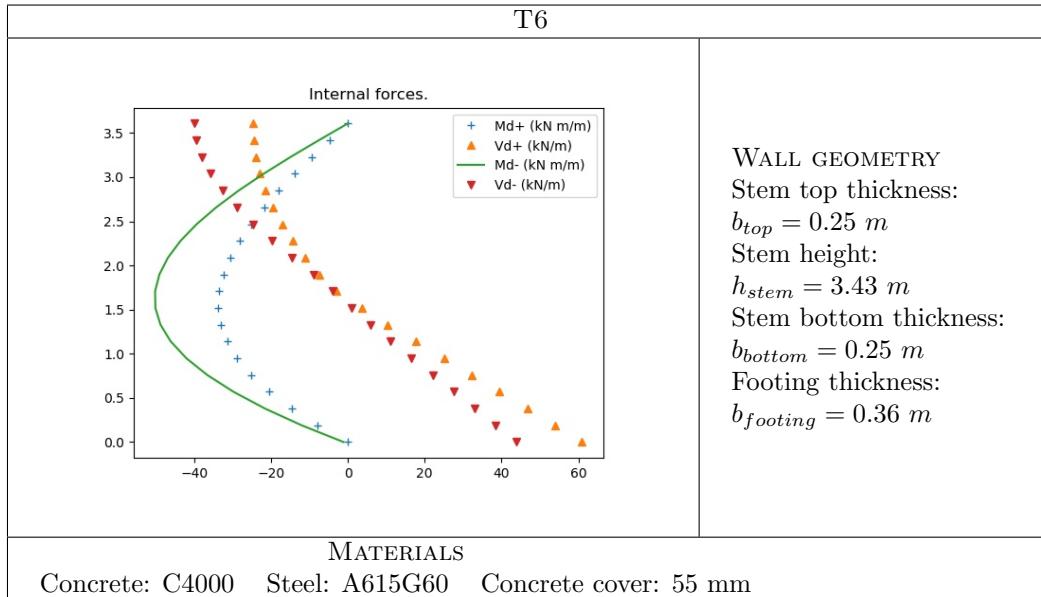


Table 19: Wall materials and dimensions T6

Reinforcement checks.

WALL VERTICAL REINFORCEMENTS	
T1 wall. Inside stem reinforcement:	RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 16 mm, spacing: 300 mm reinf. development $L=0.34 \text{ m}$ (22 diameters). area: $As = 6.67 \text{ cm}^2/\text{m}$ areaMin: $4.56 \text{ cm}^2/\text{m}$ $F(As) = 1.46 \text{ OK!}$ Bending check: $Md = 40.09 \text{ kN m}$, $MR = 41.36 \text{kN m}$ $F(M) = 1.03 \text{ OK!}$ Shear check: $Vd = 7.61 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 26.21 \text{ OK!}$
T2 wall. Inside stem reinforcement:	RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 16 mm, spacing: 400 mm reinf. development $L=0.34 \text{ m}$ (22 diameters). area: $As = 5.00 \text{ cm}^2/\text{m}$ areaMin: $4.56 \text{ cm}^2/\text{m}$ $F(As) = 1.10 \text{ OK!}$ Bending check: $Md = 29.02 \text{ kN m}$, $MR = 31.02 \text{kN m}$ $F(M) = 1.07 \text{ OK!}$ Shear check: $Vd = 6.84 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 29.15 \text{ OK!}$
T3 wall. Inside stem reinforcement:	RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 19 mm, spacing: 300 mm reinf. development $L=0.61 \text{ m}$ (32 diameters). area: $As = 9.47 \text{ cm}^2/\text{m}$ areaMin: $4.56 \text{ cm}^2/\text{m}$ $F(As) = 2.08 \text{ OK!}$ Bending check: $Md = 51.88 \text{ kN m}$, $MR = 58.26 \text{kN m}$ $F(M) = 1.12 \text{ OK!}$ Shear check: $Vd = 7.98 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 24.98 \text{ OK!}$
T4 wall. Inside stem reinforcement:	RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 16 mm, spacing: 300 mm reinf. development $L=0.34 \text{ m}$ (22 diameters). area: $As = 6.67 \text{ cm}^2/\text{m}$ areaMin: $4.56 \text{ cm}^2/\text{m}$ $F(As) = 1.46 \text{ OK!}$ Bending check: $Md = 39.19 \text{ kN m}$, $MR = 41.36 \text{kN m}$ $F(M) = 1.06 \text{ OK!}$
..../..	

WALL VERTICAL REINFORCEMENTS (CONT.)
Shear check: $V_d = 7.46 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 26.73 \text{ OK!}$
T5 wall. Inside stem reinforcement:
RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 16 mm, spacing: 400 mm reinf. development $L = 0.34 \text{ m}$ (22 diameters). area: $A_s = 5.00 \text{ cm}^2/\text{m}$ areaMin: 4.56 cm^2/m $F(A_s) = 1.10 \text{ OK!}$ Bending check: $M_d = 23.62 \text{ kN m}$, $MR = 31.02 \text{kN m}$ $F(M) = 1.31 \text{ OK!}$ Shear check: $V_d = 6.42 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 31.05 \text{ OK!}$
T6 wall. Inside stem reinforcement:
RC section dimensions; $b = 1.00 \text{ m}$, $h = 0.25 \text{ m}$ diam: 19 mm, spacing: 300 mm reinf. development $L = 0.61 \text{ m}$ (32 diameters). area: $A_s = 9.47 \text{ cm}^2/\text{m}$ areaMin: 4.56 cm^2/m $F(A_s) = 2.08 \text{ OK!}$ Bending check: $M_d = 49.02 \text{ kN m}$, $MR = 58.26 \text{kN m}$ $F(M) = 1.19 \text{ OK!}$ Shear check: $V_d = 8.13 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 24.54 \text{ OK!}$

SHEAR CHECK
T1 wall. Shear check:
Shear check: $V_d = 42.99 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 4.64 \text{ OK!}$
T2 wall. Shear check:
Shear check: $V_d = 31.78 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 6.27 \text{ OK!}$
T3 wall. Shear check:
Shear check: $V_d = 55.00 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 3.63 \text{ OK!}$
T4 wall. Shear check:
Shear check: $V_d = 42.35 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 4.71 \text{ OK!}$
T5 wall. Shear check:
Shear check: $V_d = 26.03 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 7.66 \text{ OK!}$
T6 wall. Shear check:
Shear check: $V_d = 51.43 \text{ kN}$, $VR = 199.37 \text{ kN}$ $F(V) = 3.88 \text{ OK!}$

Wall foundations The results obtained for the verifications of the footing stability and the soil-bearing capacity. According to the geotechnical report the allowable soil bearing pressure is 3000 psf (143.64 kN/m^2).

WALL FOUNDATION: T1			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.23	1.00	EQ1609A
Adm. pressure:	1.09	1.00	EQ1613B
WALL FOUNDATION: T2			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.46	1.00	EQ1609A
Adm. pressure:	1.13	1.00	EQ1613B
WALL FOUNDATION: T3			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.13	1.00	EQ1609A
Adm. pressure:	1.12	1.00	EQ1613B
WALL FOUNDATION: T4			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.45	1.00	EQ1609A
Adm. pressure:	1.08	1.00	EQ1613B
WALL FOUNDATION: T5			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.69	1.00	EQ1609A
Adm. pressure:	1.22	1.00	EQ1613B
WALL FOUNDATION: T6			
Verification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.10	1.00	EQ1609A
Adm. pressure:	1.03	1.00	EQ1613B
$F_{avail.}$: available security.			
F_{req} : required security.			

9.4 Ramp

9.4.1 Design criteria

Materials	Concrete: $f'_c = 4.0$ ksi Reinforcing steel: $f_y = 60$ ksi
Structural loads	Self weight reinforced concrete: 2500 kg/m^3 Live load garages (passenger vehicles): 40 psf Concentrated load vehicle : 3000 pound
Load cases	D: dead load (see fig. 15) Lunif: uniform live load (see fig. 16) LconcSpan1: concentrated live load on mid-span 1 (see fig. 17) LconcSpan2: concentrated live load on mid-span 2 (see fig. 18) LconcSpan3: concentrated live load on mid-span 3 (see fig. 19)
Ultim. Limit States	ULS01: $1.4*D$ ULS02: $1.2*D + 1.6*Lunif$ ULS03: $1.2*D + 1.6*LconcSpan1$ ULS04: $1.2*D + 1.6*LconcSpan2$ ULS05: $1.2*D + 1.6*LconcSpan3$
Structural model	3D elastic computer model (see fig. 14) analyzed using XC

9.4.2 Acceptance criteria

Figure 13 shows the design thickness of the ramp slab and the reinforcing layout.

The slab is checked for the load combinations summarized in section 9.4.1. The limit state checking was performed in general compliance with ACI 318, using the program XC. The representative plots for the results obtained are shown in figs. 22 to 22 for the normal stresses check, and figs. 23 to 26 for the shear check. In every case, all the elements have a demand to capacity ratio of 1.0 or less.

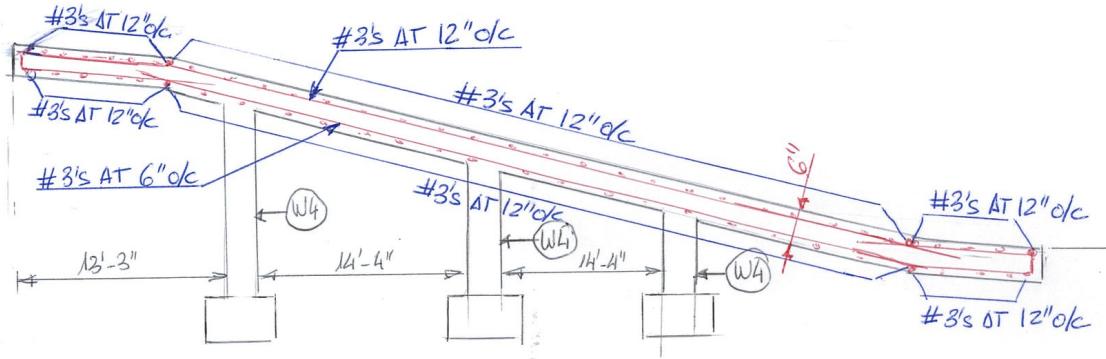


Figure 13: Ramp. Reinforcing layout.

CALCULATION REPORT

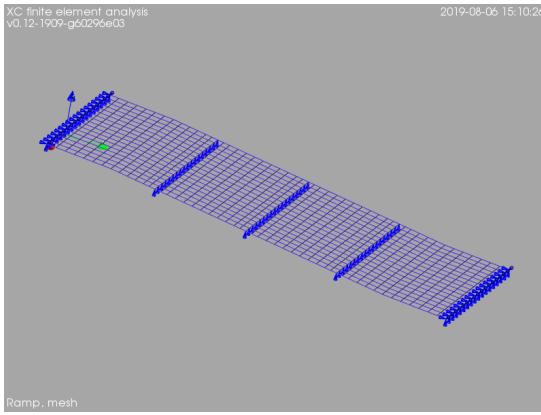


Figure 14: Ramp elastic model, mesh.

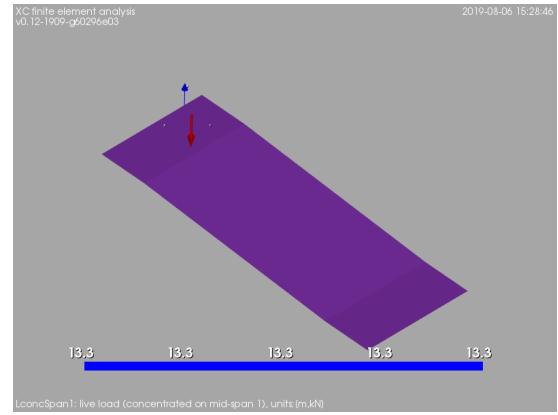


Figure 17: Load case $Lv_{conc,s1}$: concentrated live load (vehicles) on mid-span 1 [units: kN].

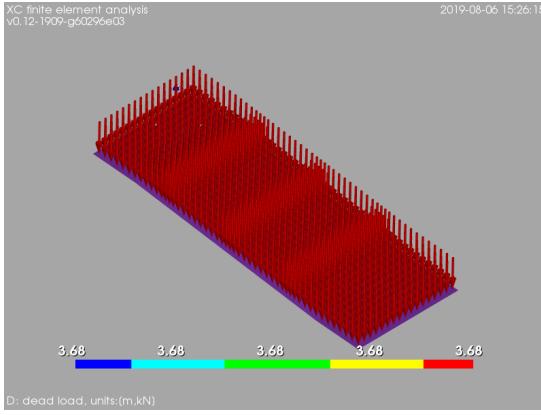


Figure 15: Load case D: dead load (include slab self-weight) [units: kN/m^2].

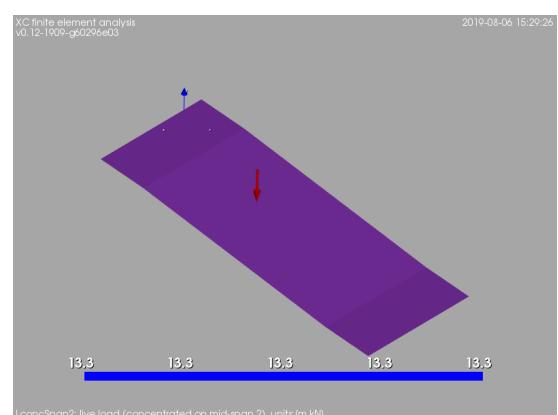


Figure 18: Load case $Lv_{conc,s2}$: concentrated live load (vehicles) on mid-span 2 [units: kN].

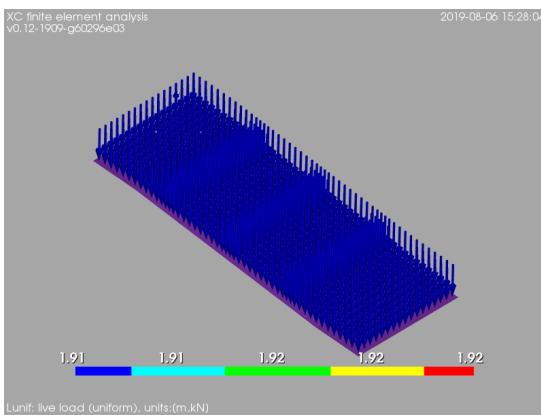


Figure 16: Load case Lv_{unif} : uniform live load (vehicles) [units: kN/m^2].

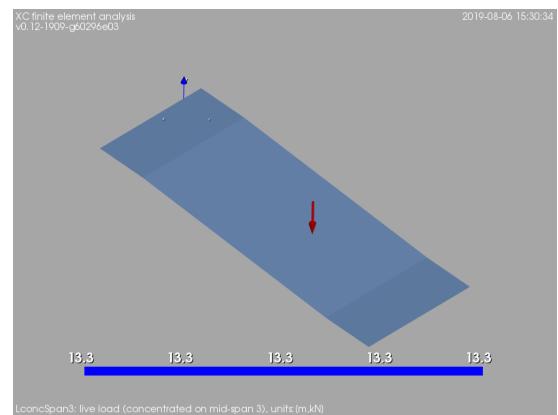


Figure 19: Load case $Lv_{conc,s3}$: concentrated live load (vehicles) on mid-span 3 [units: kN].

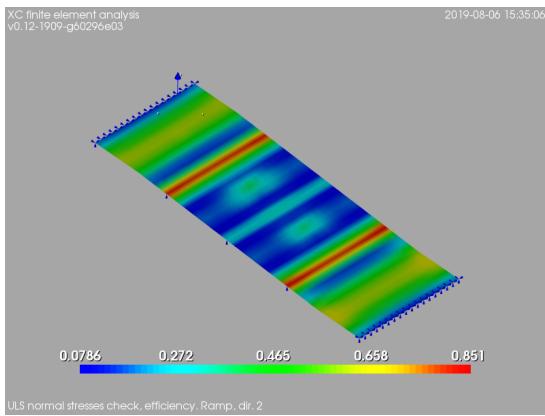


Figure 20: ULS normal stresses check. Efficiency in longitudinal direction

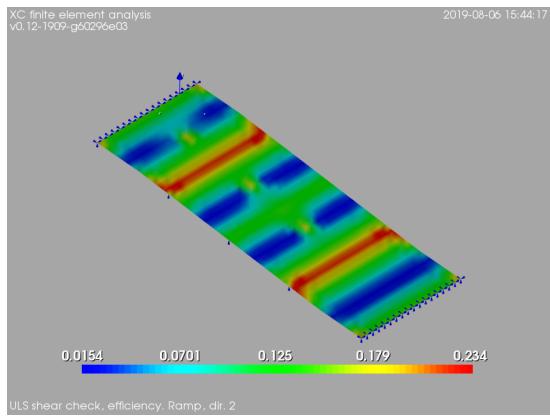


Figure 23: ULS shear check. Efficiency in longitudinal direction

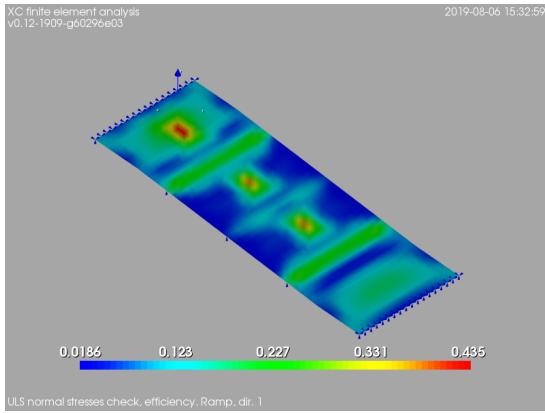


Figure 21: ULS normal stresses check. Efficiency in transversal direction

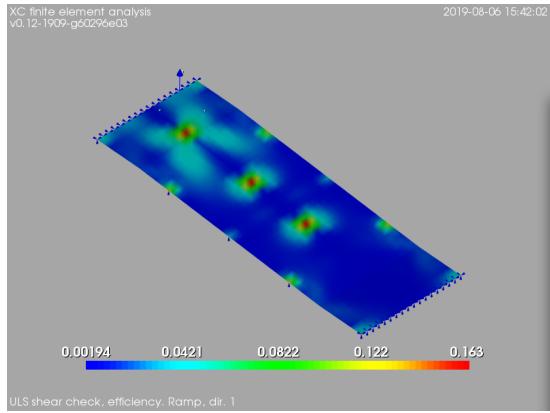


Figure 24: ULS shear check. Efficiency in transversal direction

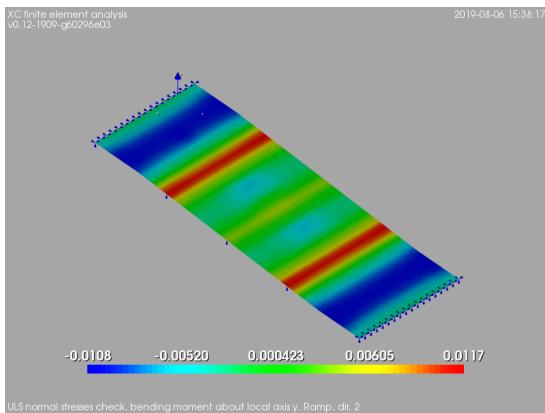


Figure 22: ULS normal stresses check. Bending moment in longitudinal direction [units: kN.m].

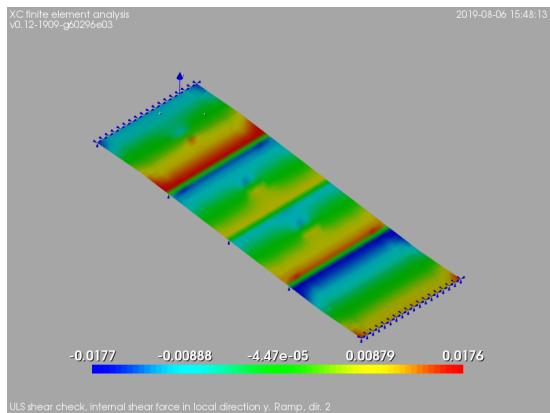


Figure 25: ULS shear check. Internal shear force in longitudinal direction [units: kN].

CALCULATION REPORT

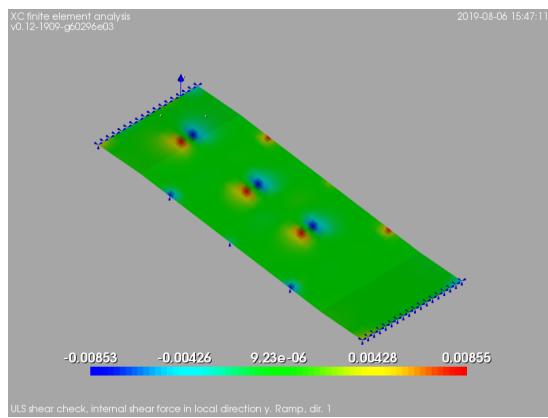


Figure 26: ULS shear check. Internal shear force in transversal direction [units: kN].

Appendices

A Loading criteria

A.1 Dead loads

Materials

Wood structural panel	$36.0 \text{ pcf} = 5655 \frac{\text{newton}}{\text{meter}^3}$
Concrete reinforced stone (including gravel)	$150.0 \text{ pcf} = 23563 \frac{\text{newton}}{\text{meter}^3}$
Steel	$489.0 \text{ pcf} = 76816 \frac{\text{newton}}{\text{meter}^3}$
Gypsum crete	$115.0 \text{ pcf} = 18065 \frac{\text{newton}}{\text{meter}^3}$
Gypsum, loose	$70.0 \text{ pcf} = 10996 \frac{\text{newton}}{\text{meter}^3}$
Earth (not submerged) sand and gravel (wet)	$120.0 \text{ pcf} = 18850 \frac{\text{newton}}{\text{meter}^3}$
Water	$62.4 \text{ pcf} = 9802 \frac{\text{newton}}{\text{meter}^3}$
Frame partitions	
Wood or steel studs, $\frac{1}{2}$ in gypsum board inside	8 psf = 383 pascal
Wood studs, 2x4 unplastered	4 psf = 192 pascal
Wood studs, 2x4 plastered one side	12 psf = 575 pascal
Wood studs, 2x4 plastered two sides	20 psf = 958 pascal
Movable steel partitions	4 psf = 192 pascal
Frame walls	
Exterior stud wall 2x4 @ 16in, $\frac{5}{8}$ gypsum insulated, $\frac{3}{8}$ in siding	11 psf = 526 pascal
Exterior stud wall 2x6 @ 16in, $\frac{5}{8}$ gypsum insulated, $\frac{3}{8}$ in siding	12 psf = 575 pascal
Exterior stud wall with brick veneer	48 psf = 2298 pascal
CMU wall 8in	60 psf = 9425 pascal
Window, glass, frame and sash	8 psf = 383 pascal
Cladding	
Fiber cement panels, large format $38.4\text{in} \times 102\text{in}$	3.2 psf = 153 pascal
Fiber cement panels, small scale $9.6\text{in} \times 102\text{in}$	3.2 psf = 153 pascal
Perforated metal panel at exterior HVAC location	
Floor truss	
Single chord @ 24in o.c. spacing	3.2 psf = 153 pascal
Double chord @ 24in o.c. spacing	4.25 psf = 203 pascal
Sheathing	
Roof sheathing	3.5 psf = 167 pascal
Floor sheathing	2.5 psf = 120 pascal
Ceilings	2.5 psf = 120 pascal
Deck composite sleepers (3in)	9.00 psf = 431 pascal

A.2 Live loads

Occupancy or use	Uniform	Concentrated	Notes
Private rooms and corridors serving them in multifamily dwelling	40.0 psf = 1915 pascal	-	IBC-2018 Table 1607.1
Stairs and exits	100.0 psf = 4788 pascal	300 pound = 1334 newton	IBC-2018 Table 1607.1. Concentrated load on stair treads applied on an area of 2 inches by 2 inches
Balconies and decks	same as occupancy served	-	IBC-2018 Table 1607.1
Garages (passenger vehicles only)	40.0 psf = 1915 pascal	-	IBC-2018 Table 1607.1
Cornices	60.0 psf = 2873 pascal	-	IBC-2018 Table 1607.1
Elevator machine room and control room grating	-	300 pound = 1334 newton	IBC-2018 Table 1607.1. Concentrated load applied on an area of 2 inches by 2 inches
Flat roof (not occupiable) + maintenance	20.0 psf = 958 pascal	300 pound = 1334 newton	IBC-2018 Table 1607.1
Yards and terraces, pedestrians	100.0 psf = 4788 pascal	-	IBC-2018 Table 1607.1
Sidewalks, vehicular driveways and yards, subject to trucking	250.0 psf = 11970 pascal	8000 pound = 35586 newton	IBC-2018 Table 1607.1
Corridors first floor	100.0 psf = 4788 pascal	-	IBC-2018 Table 1607.1
Store first floor	100.0 psf = 4788 pascal	-	IBC-2018 Table 1607.1

A.3 Snow loads

Ground snow load	$p_g = 60.0 \text{ psf} = 2873 \text{ pascal}$	ASCE 7. Figure 7.1
Exposure factor	$C_e = 1.0$	ASCE 7. Table 7-2. Terrain category B, roof partially exposed
Thermal factor	$C_t = 1.0$	ASCE 7. Table 7-3.
Snow load importance factor	$I_s = 1.0$	ASCE 7. Table 7-4. Structure risk category II
Snow load flat roof	$p_f = 0.7 \times C_e \times C_t \times I_s \times p_g = 0.7 \times 1.0 \times 1.0 \times 1.0 \times 60.0 = 42.0 \text{ psf} = 2873 \text{ pascal}$	ASCE 7. Sect. 7.3

A.4 Wind loads

Alternate all-heights method.

$$\text{Ultimate design wind speed } V_{ult} = 115 \frac{\text{miles}}{\text{hour}} = 51 \frac{\text{meters}}{\text{second}}$$

$$\text{Velocity pressure exposure coefficient } K_z = 0.72$$

$$\text{Topographic factor } K_{zt} = 1.0$$

IBC-2018, sect. 1609.6. Regularly shaped building, less than 75 feet in height, not sensitive to dynamic effects, not channeling effects or buffeting, simple diaphragm building

IBC-2018, figure 1609.3(1). Risk category II building

ASCE 7, table 27.3.1. Exposure B, height above ground level $z \approx 33$ feet

ASCE 7, sect. 26.8

Net pressure coefficients C_{net} . Main windforce-resisting frames and systems

Description	$C_{net} + \text{Internal pressure}$	$C_{net} - \text{Internal pressure}$
Windward wall	0.43	0.73
Leeward wall	-0.51	-0.21
Sidewall	-0.66	-0.35
Parapet windward wall		1.28
Parapet leeward wall		-0.85
Flat roof	-1.09	-0.79

IBC-2018, Table 1609.6.2, enclosed

Design wind pressures P_{net} . Main windforce-resisting frames and systems

$$P_{net} = 0.00256 \times V^2 \times K_z \times C_{net} \times K_{zt}$$

Description	$P_{net} + \text{Internal pressure}$	$P_{net} - \text{Internal pressure}$
Windward wall	10.5 psf = 501 pascal	17.8 psf = 852 pascal
Leeward wall	-12.4 psf = -595 pascal	-5.1 psf = -245 pascal
Sidewall	-16.1 psf = -770 pascal	-8.5 psf = -409 pascal
Parapet windward wall		31.2 psf = 1494 pascal
Parapet leeward wall		-20.7 psf = -992 pascal
Flat roof	-26.6 psf = -1272 pascal	-19.3 psf = -992 pascal

IBC-2018, sect. 1609.6.3

A.5 Earthquake loads

Parameter	0.2-second spectral response acceleration	$S_s = 0.045$	IBC-2018, figure 1613.3.1(1). Site class B
Parameter	1-second spectral response acceleration	$S_1 = 0.038$	IBC-2018, figure 1613.3.1(2). Site class B
Seismic design category		$S_1 \leq 0.04 \text{ and } S_s \leq 0.15 \rightarrow \text{SDS A}$	IBC-2018, sect. 1613.3.1
Site coefficients		$F_a = 1.0, F_v = 1.0$	IBC-2018, tables 1613.3.3(1) and 1613.3.3(2). Site class B
Maximum considered earthquake spectral response acceleration for short periods		$S_{MS} = F_a \cdot S_s = 0.045$	IBC-2018, sect. 163.3.3
Design spectral response acceleration parameters		$S_{M1} = F_a \cdot S_1 = 0.038$ $S_{DS} = \frac{2}{3}S_{MS} = 0.03$ $S_{D1} = \frac{2}{3}S_{M1} = 0.025$	IBC-2018, sect. 163.3.4 IBC-2018, sect. 163.3.4

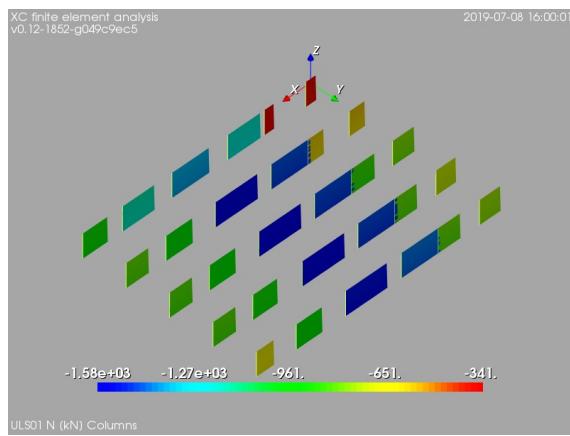


Figure 27: ULS01: 1.4*D. Columns, internal axial force [kN]

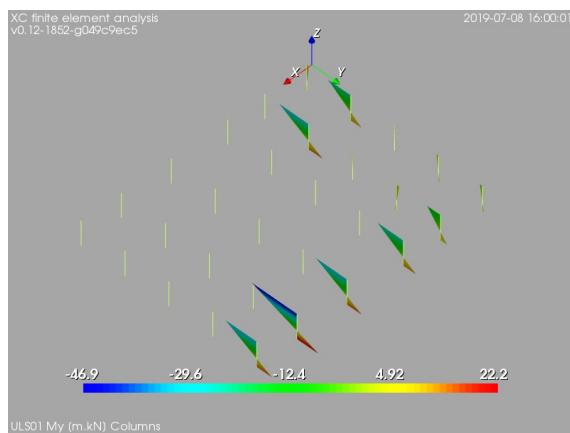


Figure 28: ULS01: 1.4*D. Columns, bending moment about local axis y [m.kN]

B Calculation results. Internal forces on columns

B.1 Ultimate limit states

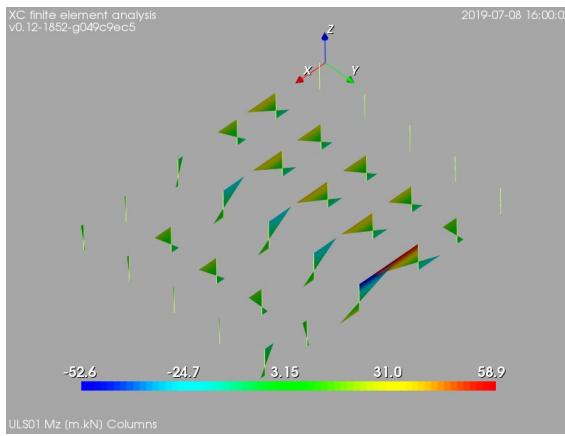


Figure 29: ULS01: 1.4*D. Columns, bending moment about local axis z [m.kN]

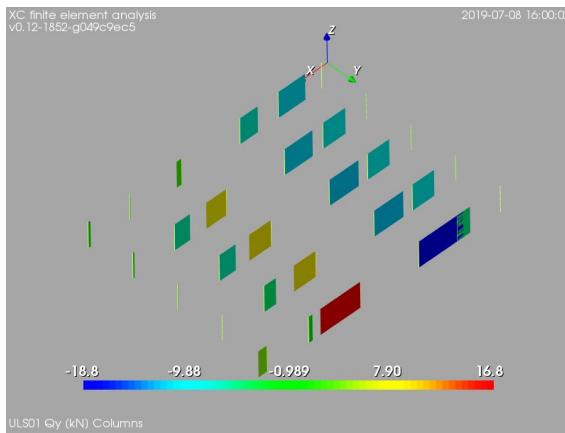


Figure 30: ULS01: 1.4*D. Columns, internal shear force in local direction y [kN]

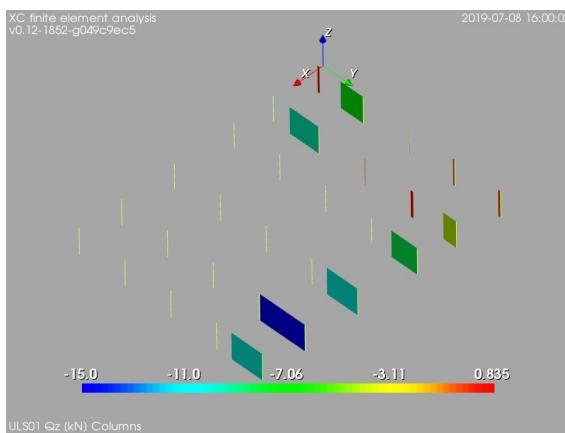


Figure 31: ULS01: 1.4*D. Columns, internal shear force in local direction z [kN]

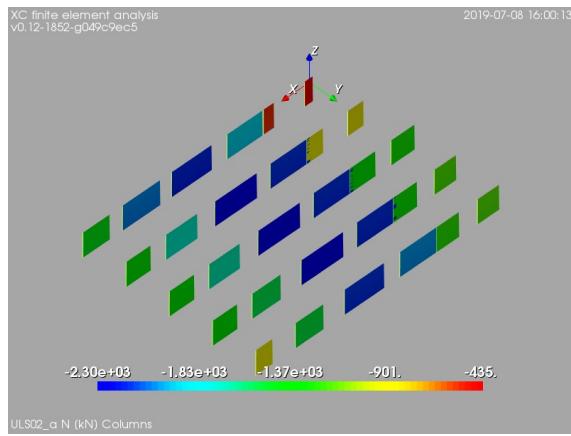


Figure 32: ULS02_a: $1.2*D + 1.6*L_{ru} + L_{pu} + 0.5*S$. Columns, internal axial force [kN]

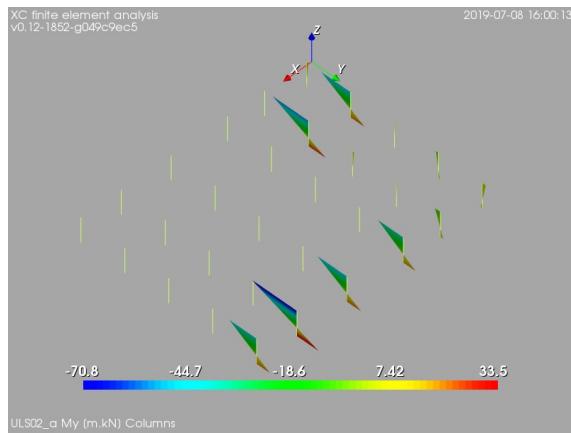


Figure 33: ULS02_a: $1.2*D + 1.6*L_{ru} + L_{pu} + 0.5*S$. Columns, bending moment about local axis y [m.kN]

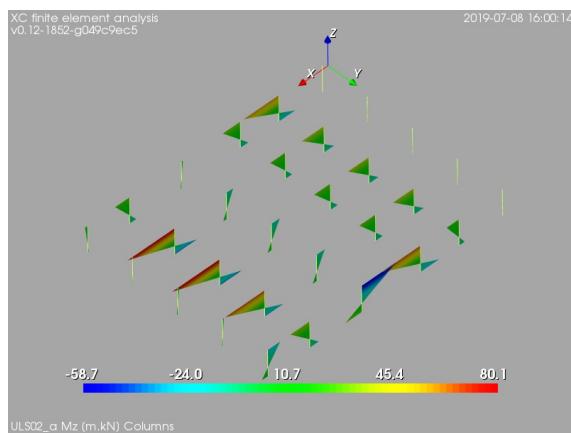


Figure 34: ULS02_a: $1.2*D + 1.6*L_{ru} + L_{pu} + 0.5*S$. Columns, bending moment about local axis z [m.kN]

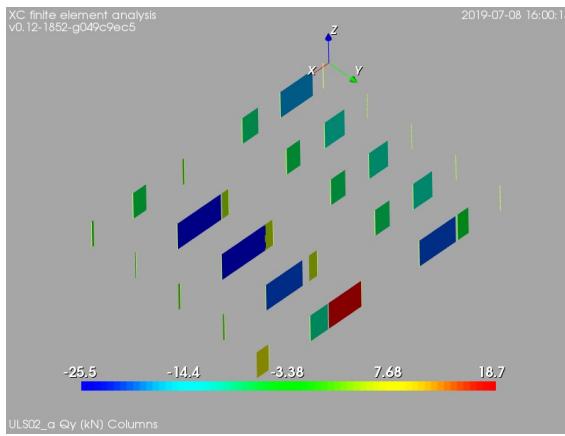


Figure 35: ULS02_a: $1.2*D + 1.6*Lru + Lpu + 0.5*S$. Columns, internal shear force in local direction y [kN]

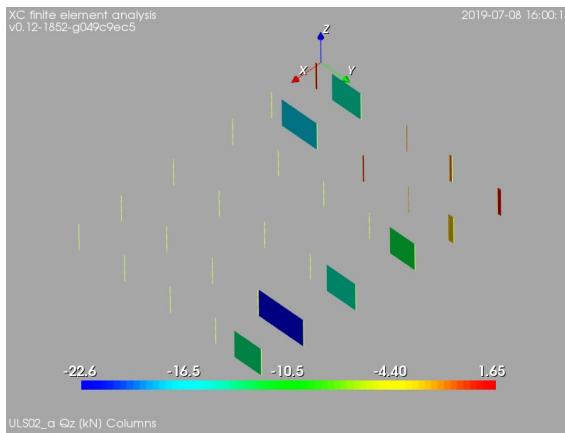


Figure 36: ULS02_a: $1.2*D + 1.6*Lru + Lpu + 0.5*S$. Columns, internal shear force in local direction z [kN]

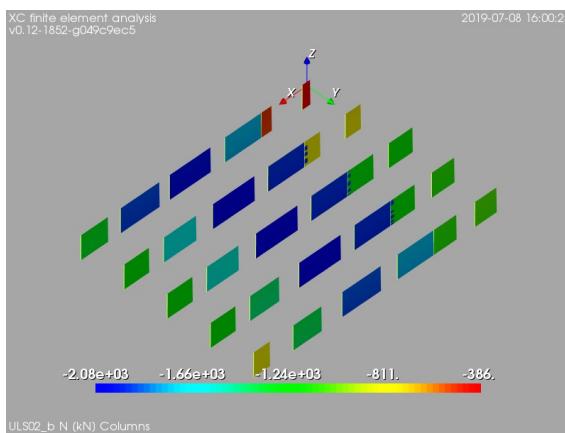


Figure 37: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, internal axial force [kN]

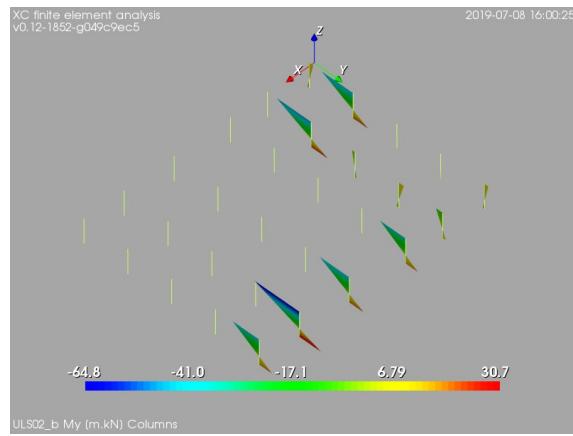


Figure 38: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, bending moment about local axis y [m.kN]

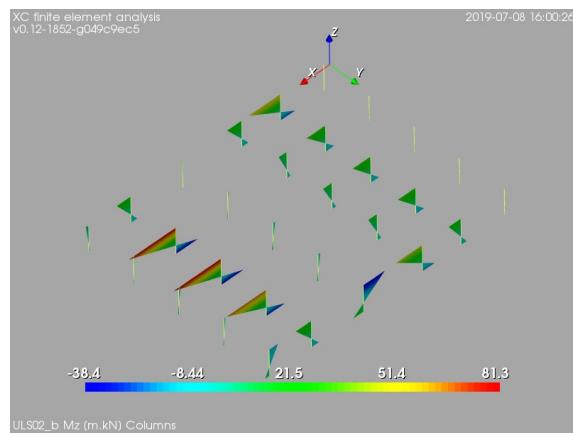


Figure 39: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, bending moment about local axis z [m.kN]

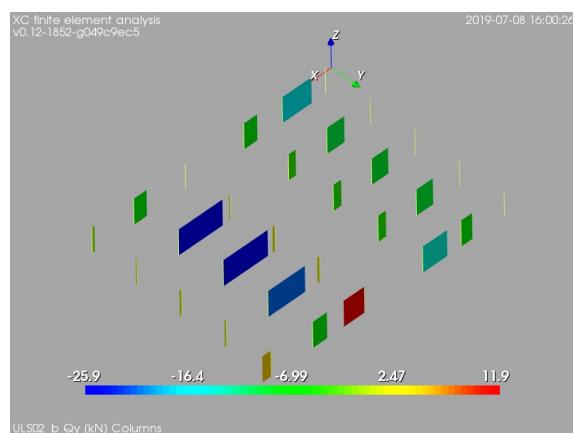


Figure 40: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, internal shear force in local direction y [kN]

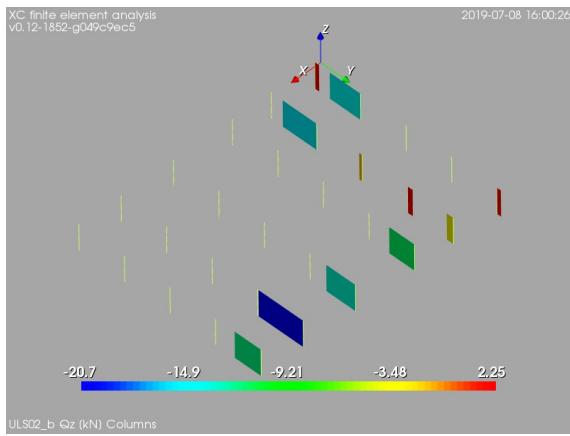


Figure 41: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, internal shear force in local direction z [kN]

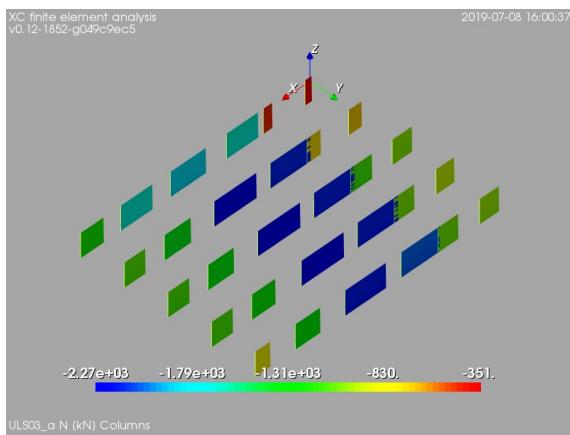


Figure 42: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal axial force [kN]

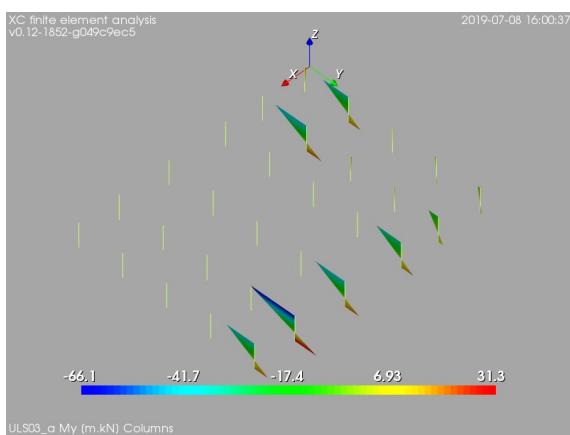


Figure 43: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, bending moment about local axis y [m.kN]

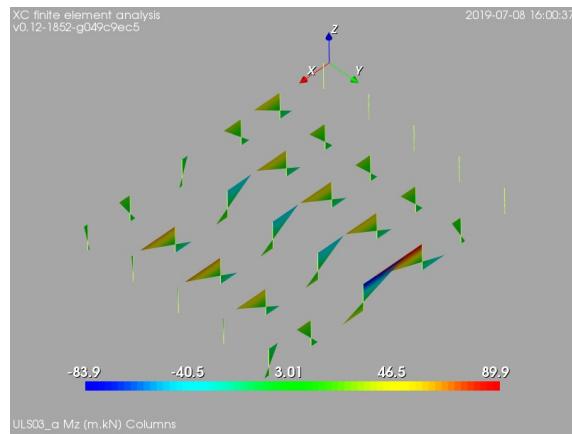


Figure 44: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, bending moment about local axis z [m.kN]

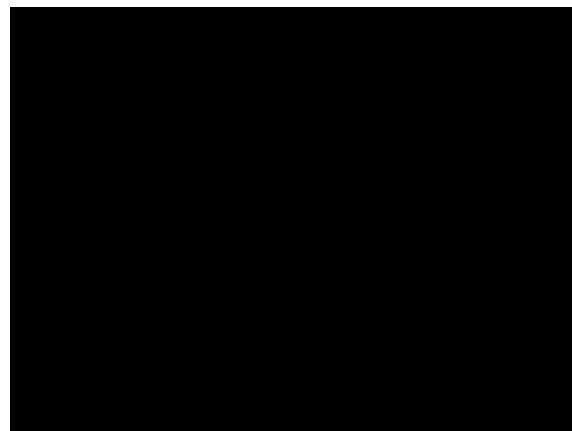


Figure 45: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal shear force in local direction y [kN]

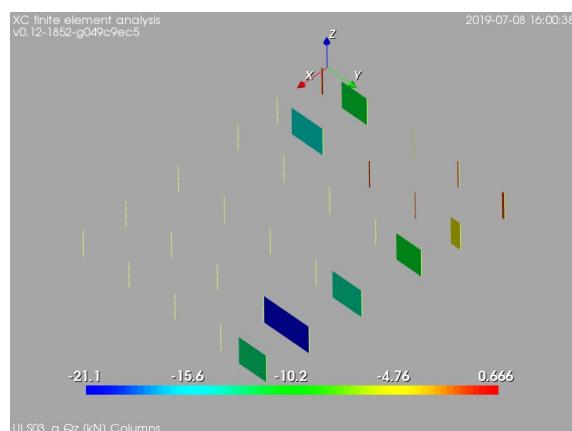


Figure 46: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal shear force in local direction z [kN]

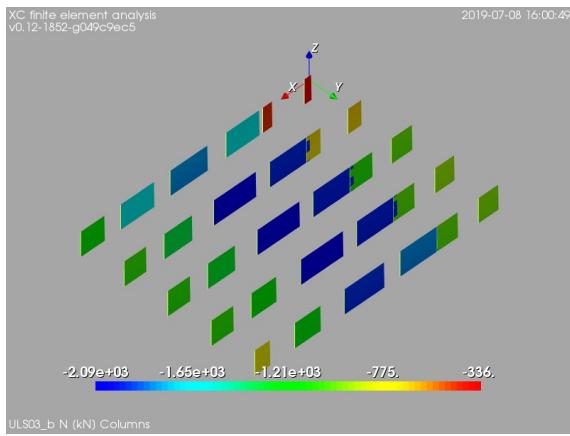


Figure 47: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal axial force [kN]

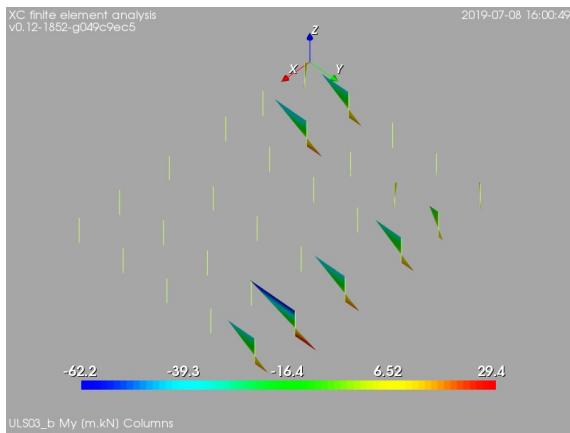


Figure 48: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, bending moment about local axis y [m.kN]

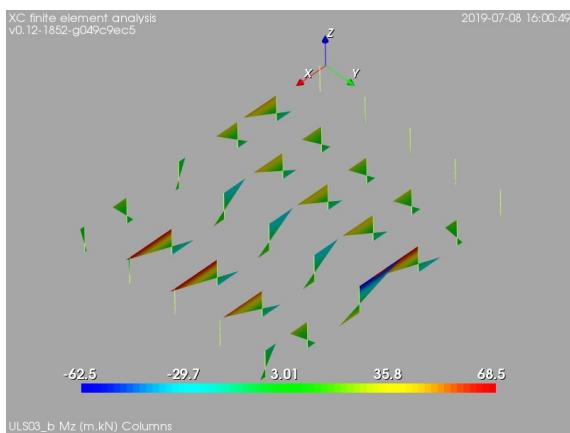


Figure 49: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, bending moment about local axis z [m.kN]

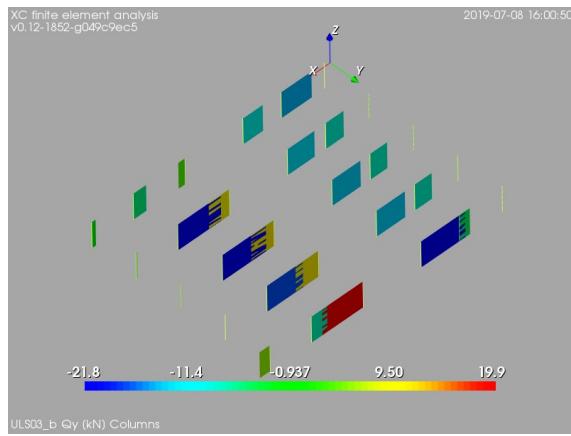


Figure 50: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal shear force in local direction y [kN]

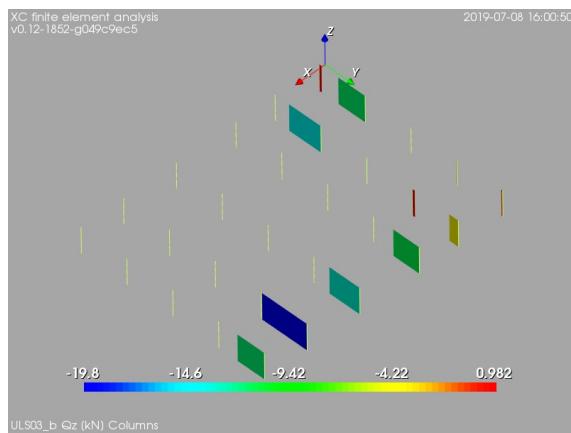


Figure 51: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal shear force in local direction z [kN]

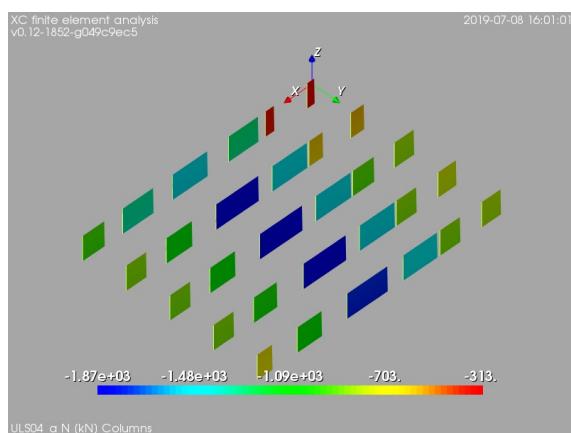


Figure 52: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal axial force [kN]

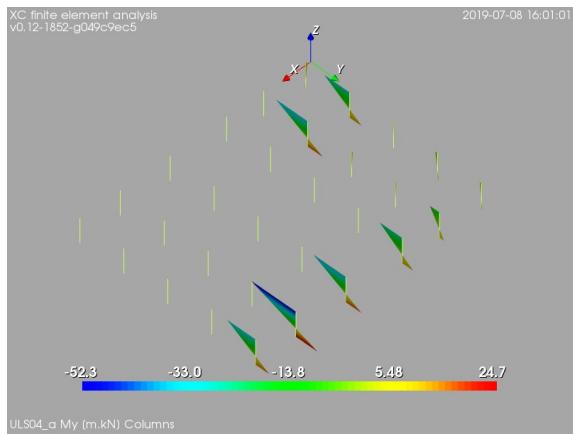


Figure 53: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, bending moment about local axis y [m.kN]

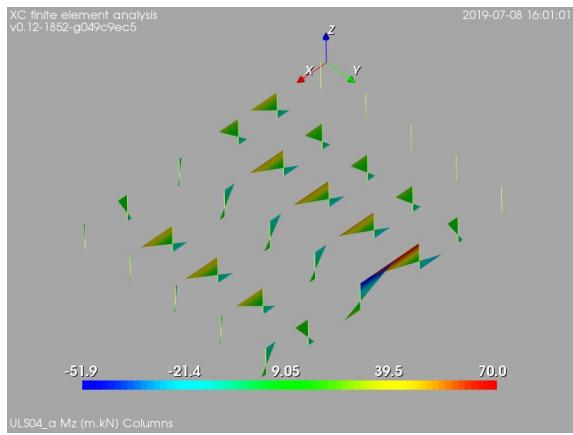


Figure 54: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, bending moment about local axis z [m.kN]

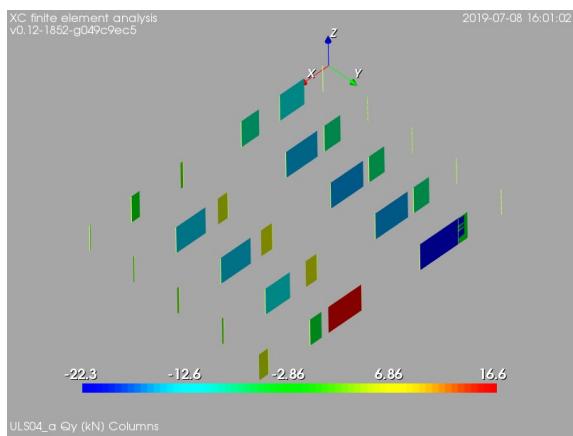


Figure 55: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal shear force in local direction y [kN]

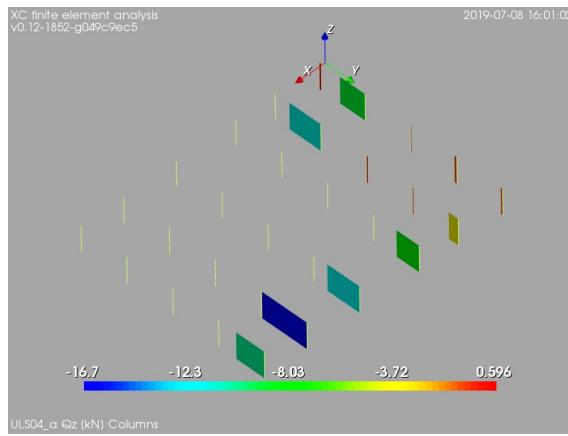


Figure 56: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal shear force in local direction z [kN]

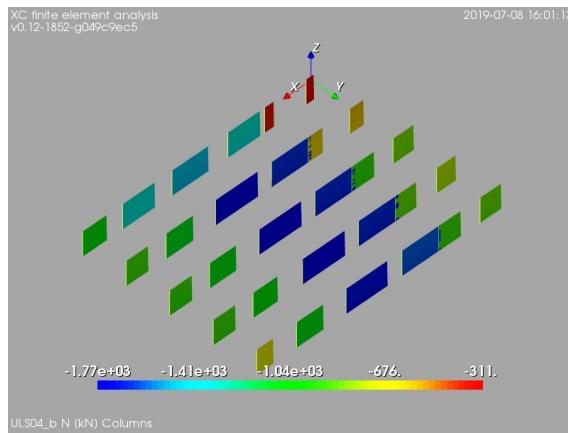


Figure 57: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, internal axial force [kN]

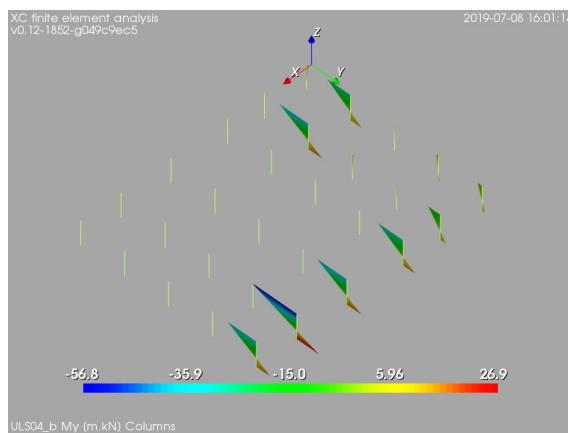


Figure 58: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, bending moment about local axis y [m.kN]

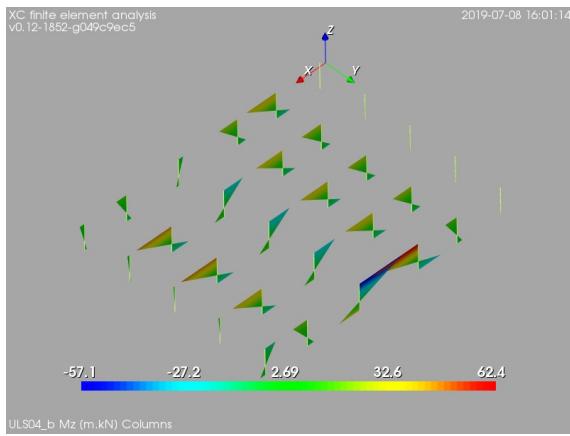


Figure 59: ULS04_b: $1.2*D + 1.6*S + 0.5*W_{NS}$. Columns, bending moment about local axis z [m.kN]

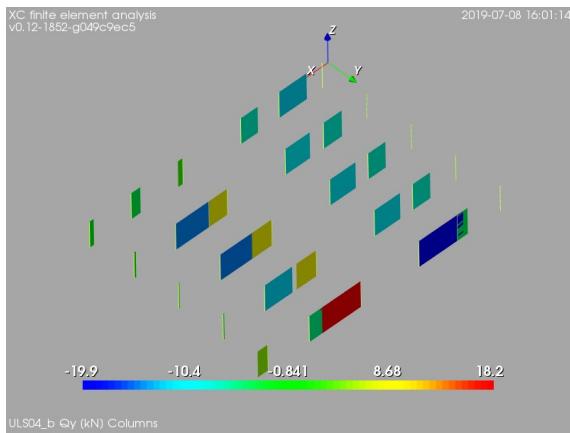


Figure 60: ULS04_b: $1.2*D + 1.6*S + 0.5*W_{NS}$. Columns, internal shear force in local direction y [kN]

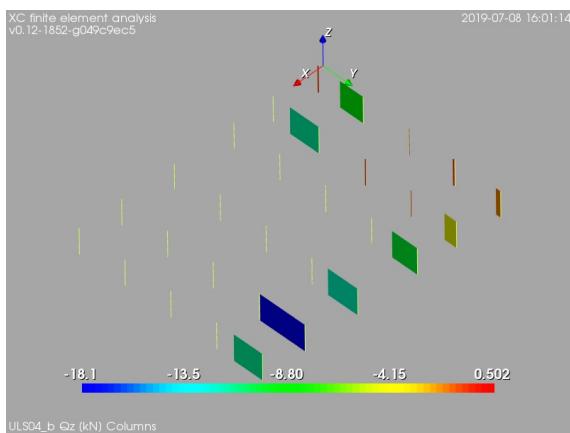


Figure 61: ULS04_b: $1.2*D + 1.6*S + 0.5*W_{NS}$. Columns, internal shear force in local direction z [kN]

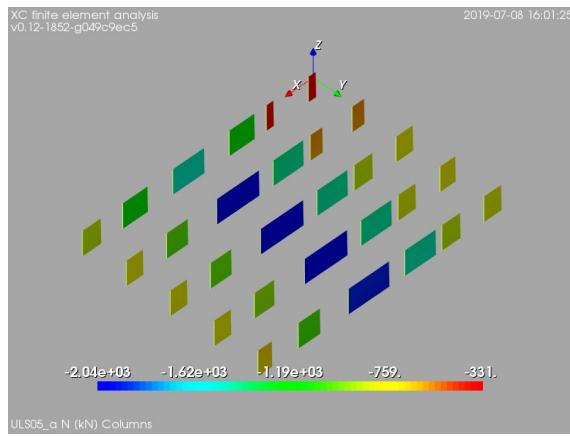


Figure 62: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal axial force [kN]

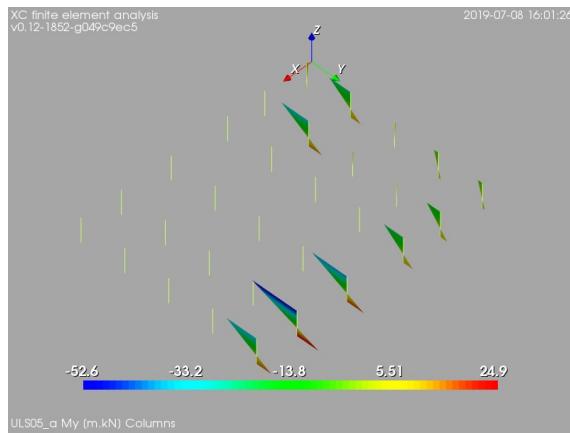


Figure 63: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, bending moment about local axis y [m.kN]

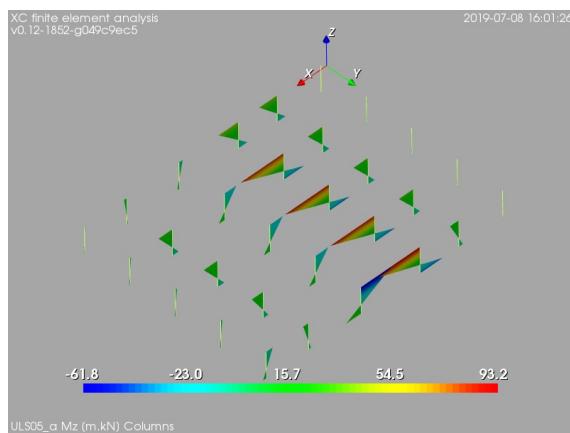


Figure 64: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, bending moment about local axis z [m.kN]

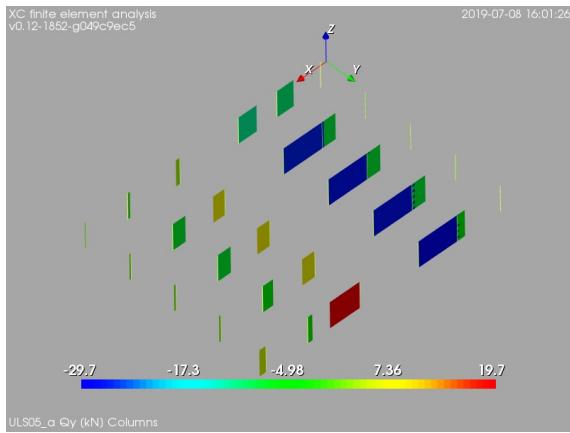


Figure 65: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal shear force in local direction y [kN]

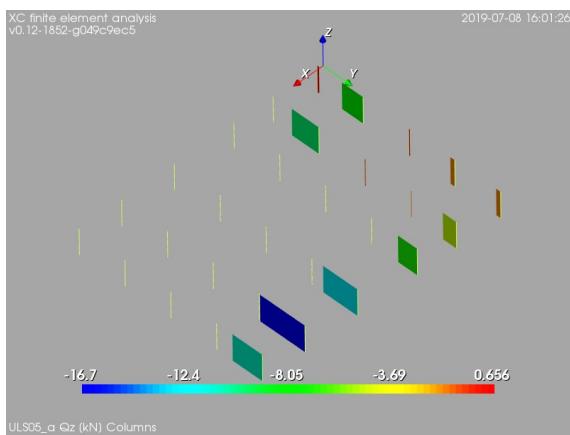


Figure 66: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal shear force in local direction z [kN]

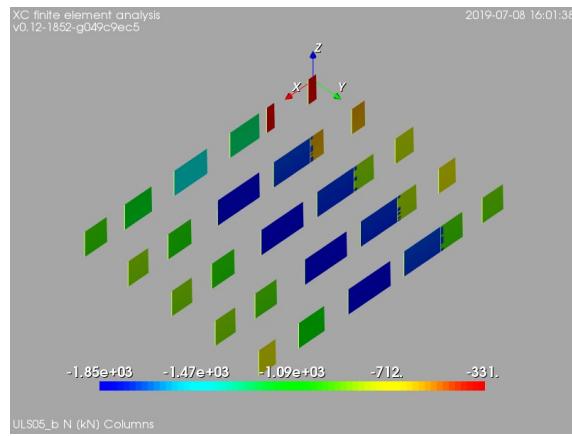


Figure 67: ULS05_b: $1.2*D + W_{NS} + 0.5*L_{ru} + L_{pu}$. Columns, internal axial force [kN]

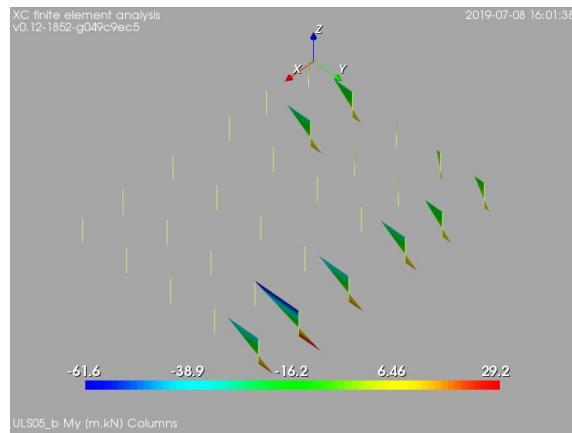


Figure 68: ULS05_b: $1.2*D + W_{NS} + 0.5*L_{ru} + L_{pu}$. Columns, bending moment about local axis y [m.kN]

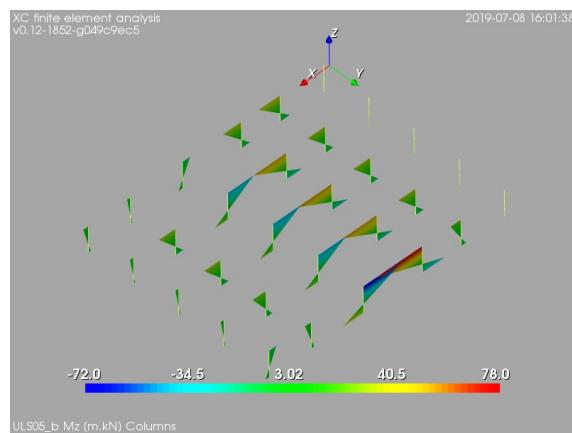


Figure 69: ULS05_b: $1.2*D + W_{NS} + 0.5*L_{ru} + L_{pu}$. Columns, bending moment about local axis z [m.kN]

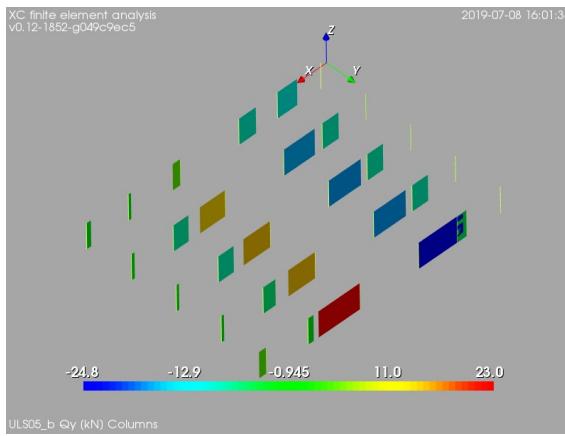


Figure 70: ULS05_b: 1.2*D + W_NS + 0.5*Lru + Lpu. Columns, internal shear force in local direction y [kN]

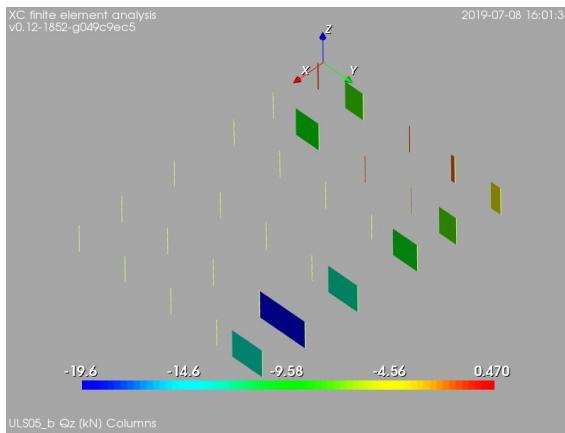


Figure 71: ULS05_b: 1.2*D + W_NS + 0.5*Lru + Lpu. Columns, internal shear force in local direction z [kN]

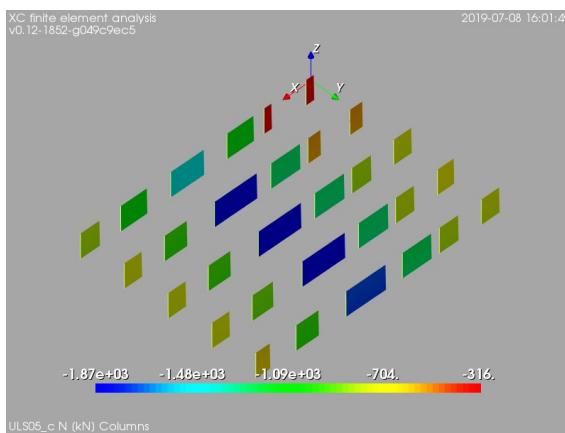


Figure 72: ULS05_c: 1.2*D + W_WE + 0.5*Lrs + Lps. Columns, internal axial force [kN]

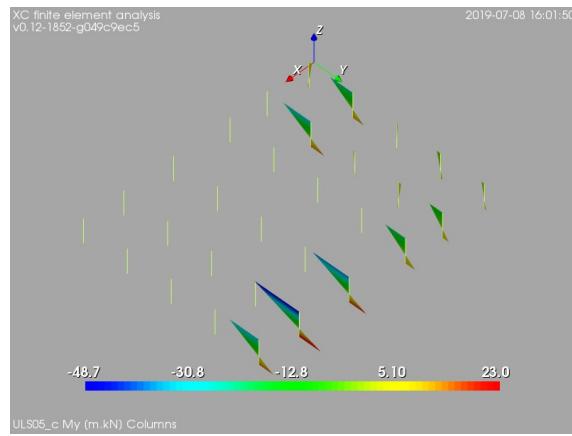


Figure 73: ULS05_c: 1.2*D + W_WE + 0.5*Lrs + Lps. Columns, bending moment about local axis y [m.kN]

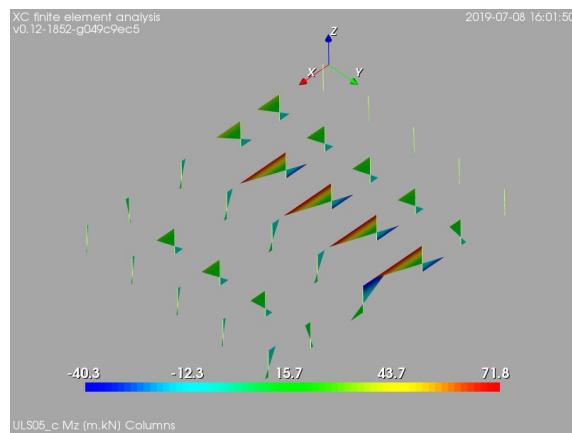


Figure 74: ULS05_c: 1.2*D + W_WE + 0.5*Lrs + Lps. Columns, bending moment about local axis z [m.kN]

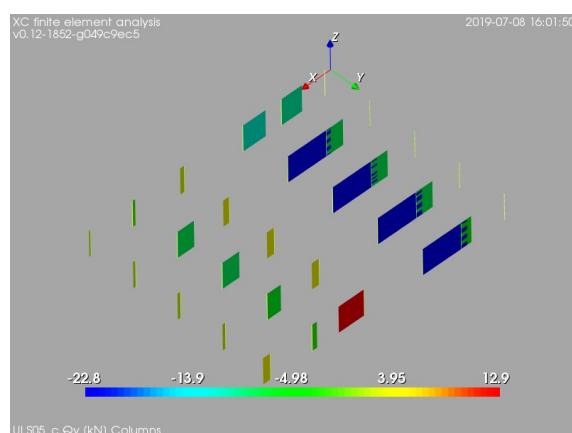


Figure 75: ULS05_c: 1.2*D + W_WE + 0.5*Lrs + Lps. Columns, internal shear force in local direction y [kN]

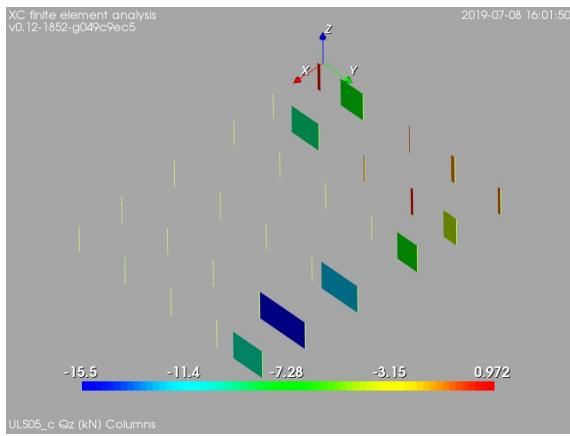


Figure 76: ULS05_c: 1.2*D + W_WE + 0.5*Lrs + Lps. Columns, internal shear force in local direction z [kN]

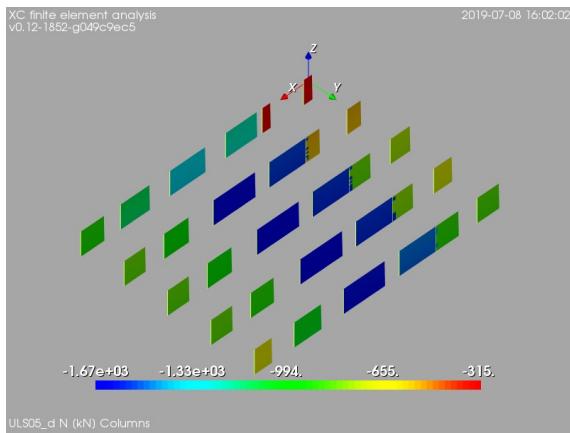


Figure 77: ULS05_d: 1.2*D + W_NS + 0.5*Lrs + Lps. Columns, internal axial force [kN]

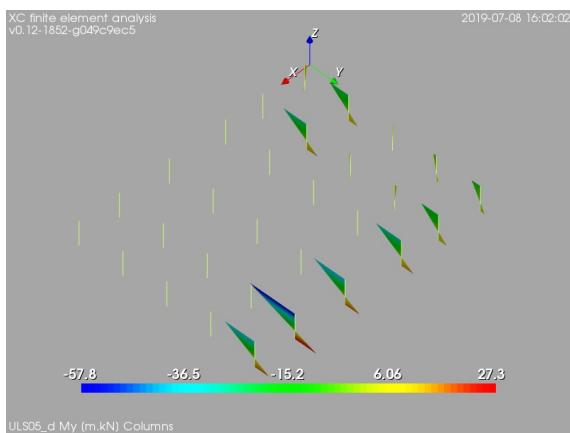


Figure 78: ULS05_d: 1.2*D + W_NS + 0.5*Lrs + Lps. Columns, bending moment about local axis y [m.kN]

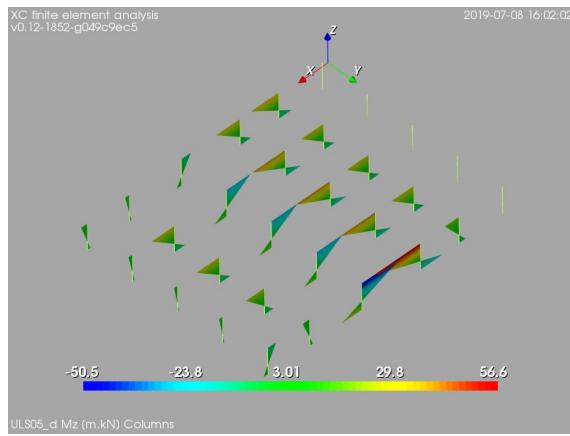


Figure 79: ULS05_d: 1.2*D + W_Ns + 0.5*Lrs + Lps. Columns, bending moment about local axis z [m.kN]

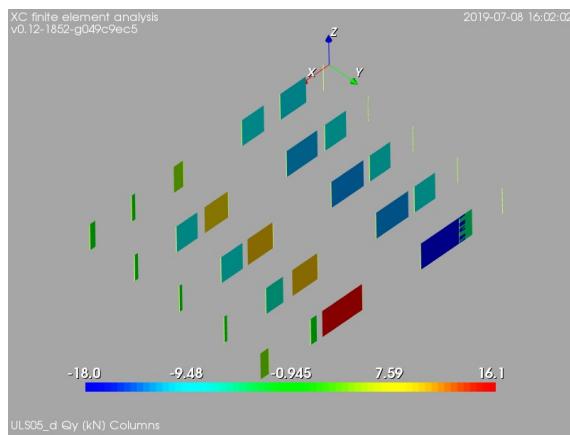


Figure 80: ULS05_d: 1.2*D + W_Ns + 0.5*Lrs + Lps. Columns, internal shear force in local direction y [kN]

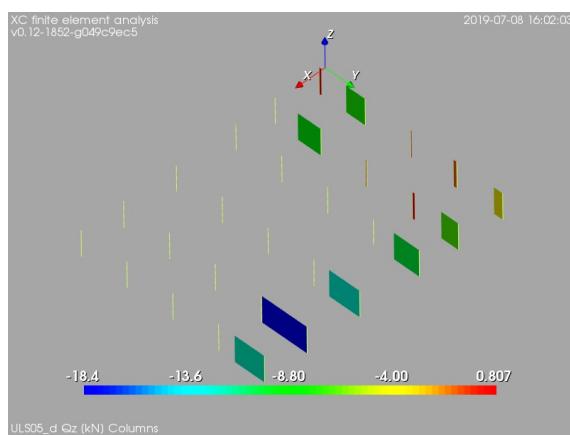


Figure 81: ULS05_d: 1.2*D + W_Ns + 0.5*Lrs + Lps. Columns, internal shear force in local direction z [kN]

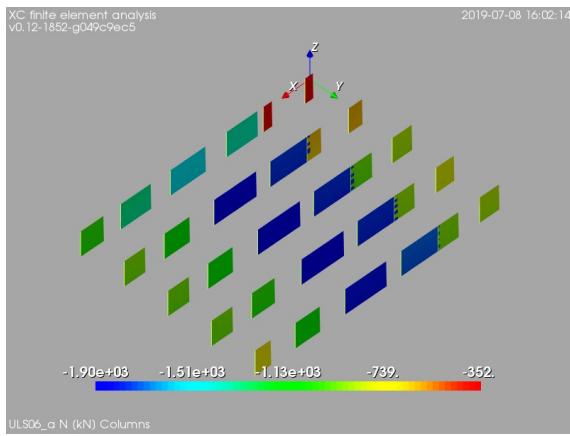


Figure 82: ULS06_a: 1.2*D + 0.5*Lru + Lpu + 0.2*S. Columns, internal axial force [kN]

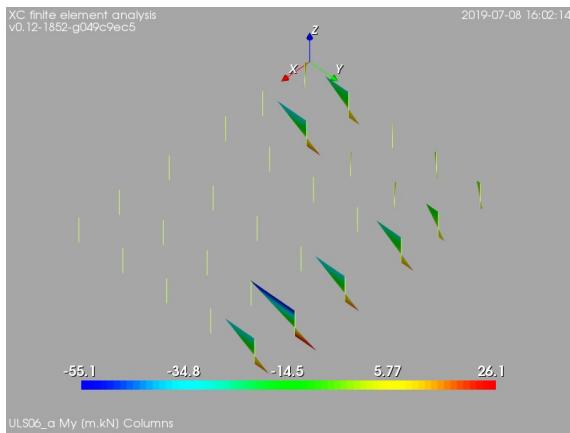


Figure 83: ULS06_a: 1.2*D + 0.5*Lru + Lpu + 0.2*S. Columns, bending moment about local axis y [m.kN]

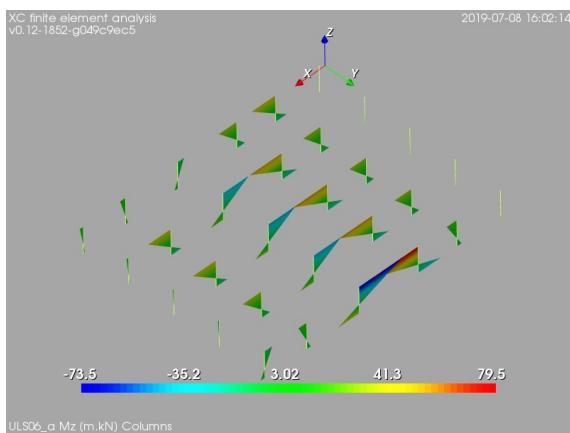


Figure 84: ULS06_a: 1.2*D + 0.5*Lru + Lpu + 0.2*S. Columns, bending moment about local axis z [m.kN]

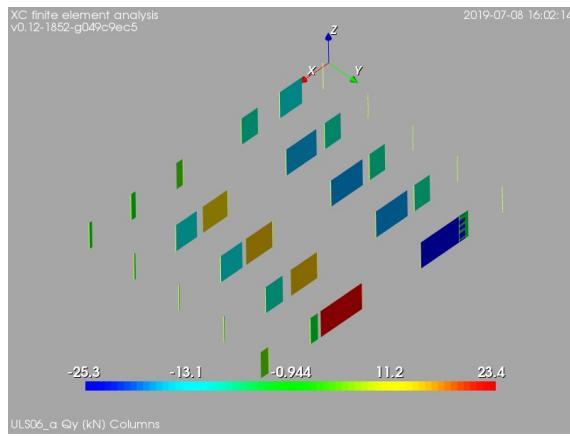


Figure 85: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, internal shear force in local direction y [kN]

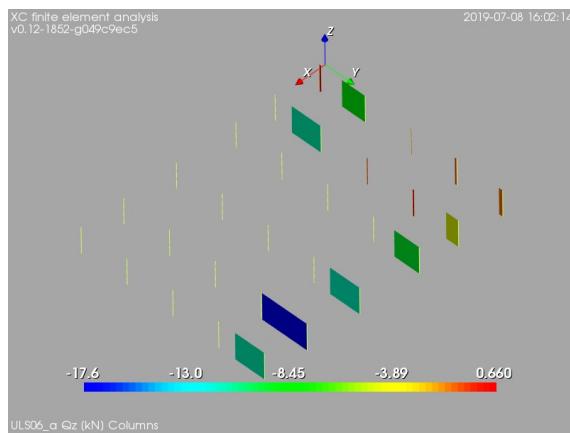


Figure 86: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, internal shear force in local direction z [kN]

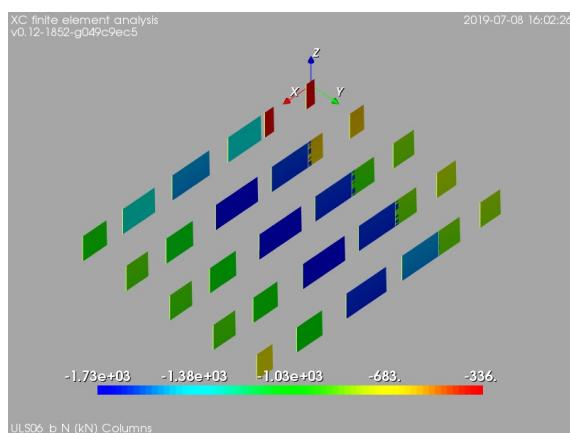


Figure 87: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal axial force [kN]

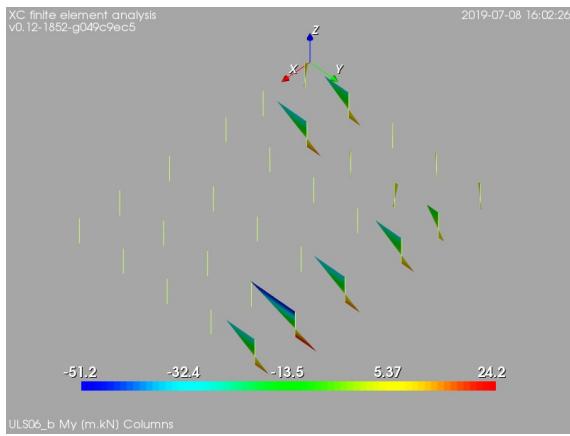


Figure 88: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, bending moment about local axis y [m.kN]

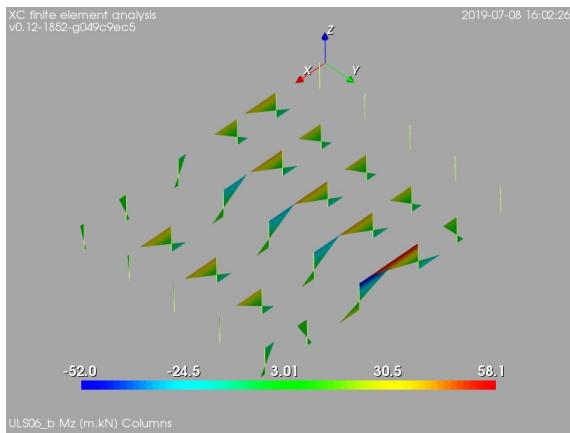


Figure 89: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, bending moment about local axis z [m.kN]

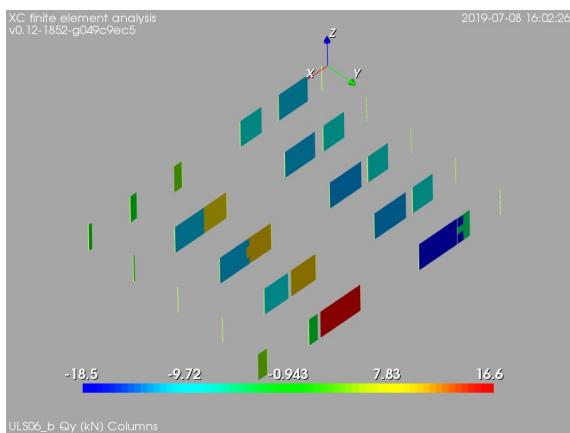


Figure 90: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal shear force in local direction y [kN]

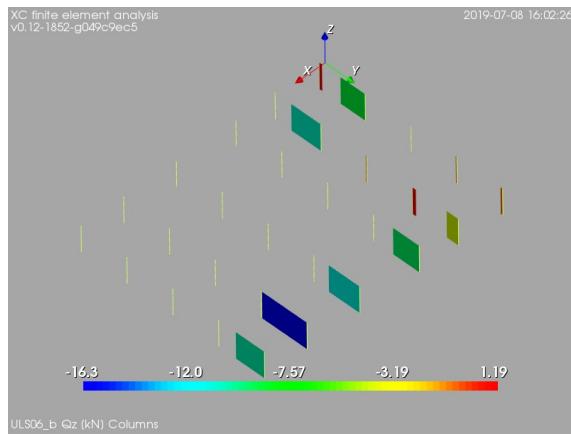


Figure 91: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal shear force in local direction z [kN]

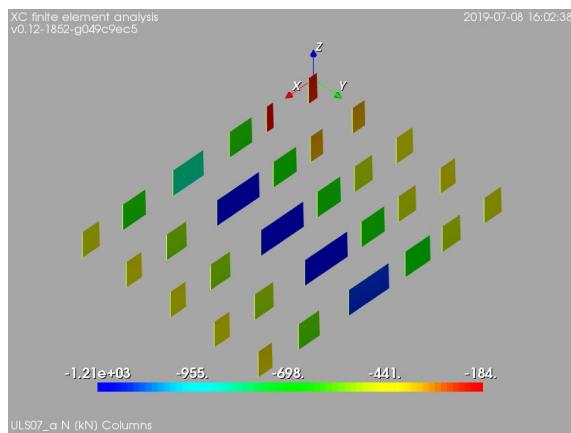


Figure 92: ULS07_a: $0.9*D + W_WE$. Columns, internal axial force [kN]

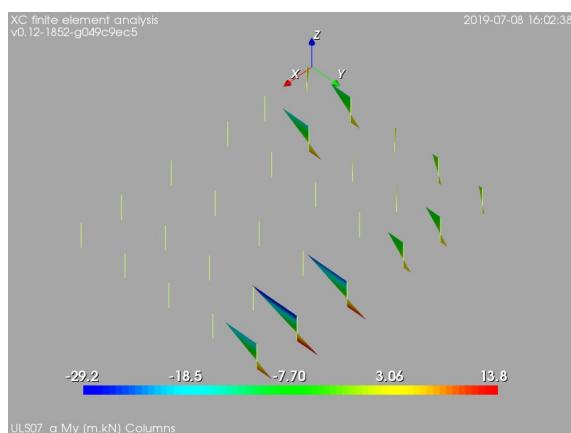


Figure 93: ULS07_a: $0.9*D + W_WE$. Columns, bending moment about local axis y [m.kN]

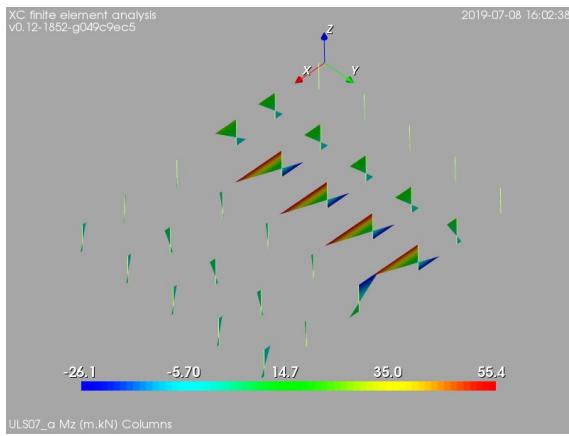


Figure 94: ULS07_a: 0.9*D + W_WE. Columns, bending moment about local axis z [m.kN]

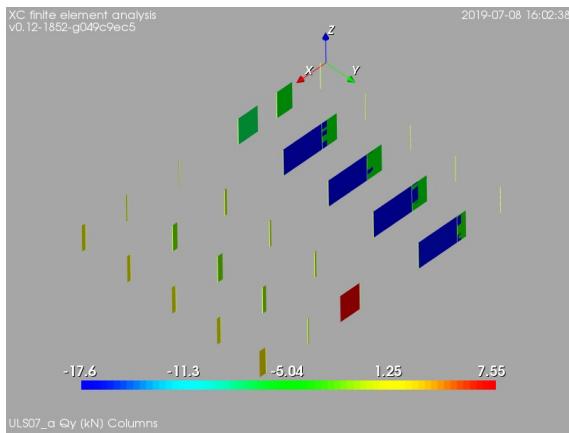


Figure 95: ULS07_a: 0.9*D + W_WE. Columns, internal shear force in local direction y [kN]

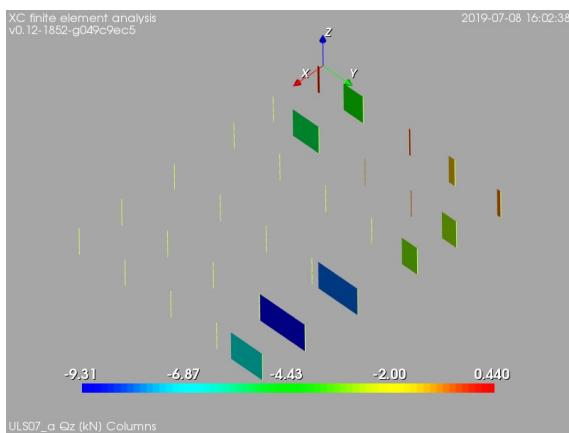


Figure 96: ULS07_a: 0.9*D + W_WE. Columns, internal shear force in local direction z [kN]

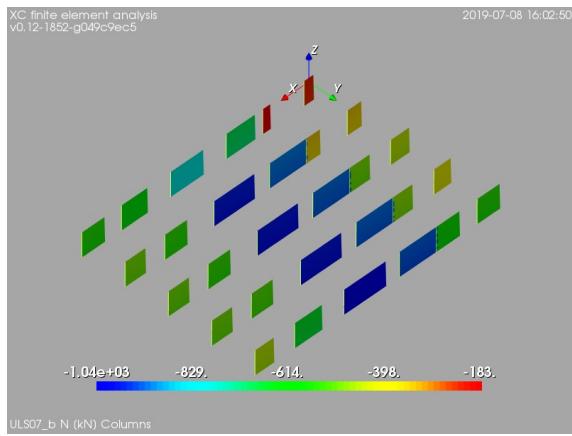


Figure 97: ULS07_b: 0.9*D + W_NS. Columns, internal axial force [kN]

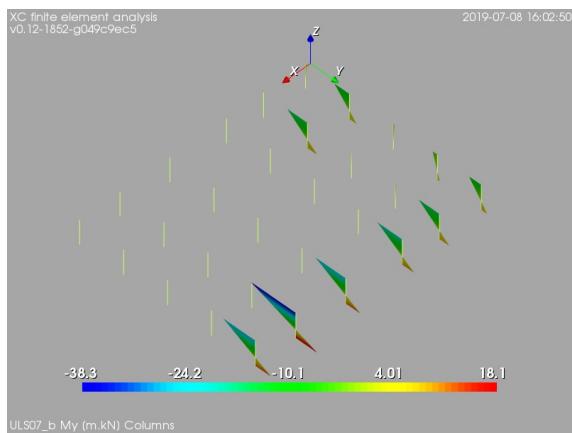


Figure 98: ULS07_b: 0.9*D + W_NS. Columns, bending moment about local axis y [m.kN]

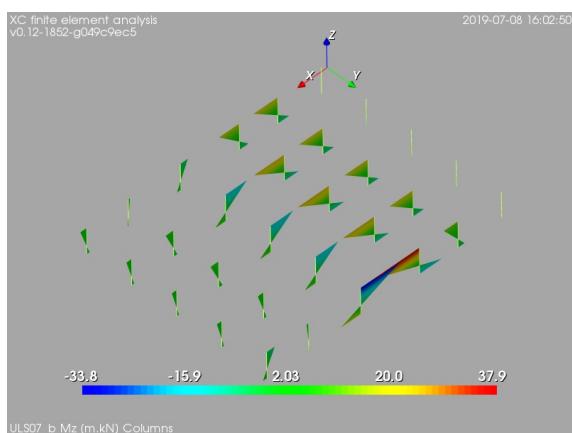


Figure 99: ULS07_b: 0.9*D + W_NS. Columns, bending moment about local axis z [m.kN]

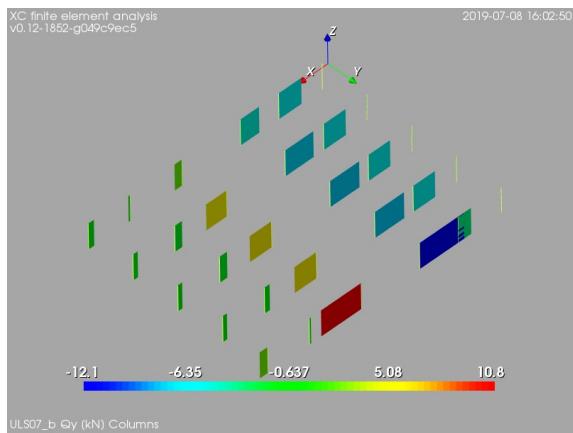


Figure 100: ULS07_b: 0.9*D + W_NS. Columns, internal shear force in local direction y [kN]

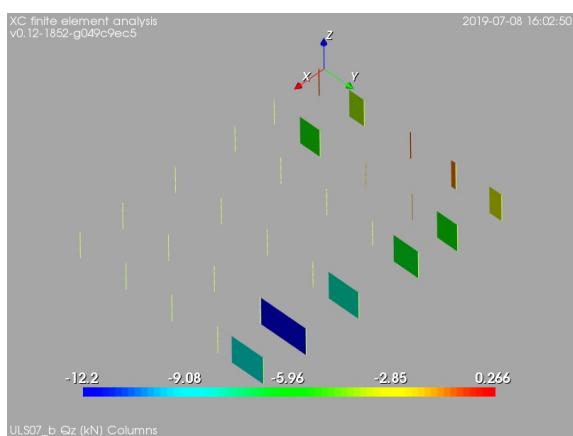


Figure 101: ULS07_b: 0.9*D + W_NS. Columns, internal shear force in local direction z [kN]

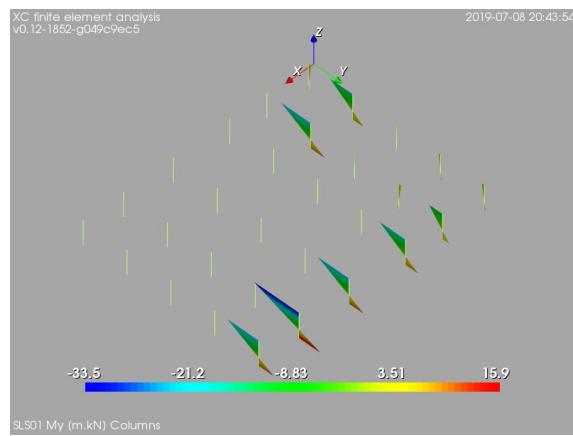


Figure 102: SLS01: 1.0*D. Columns, bending moment about local axis y [m.kN]

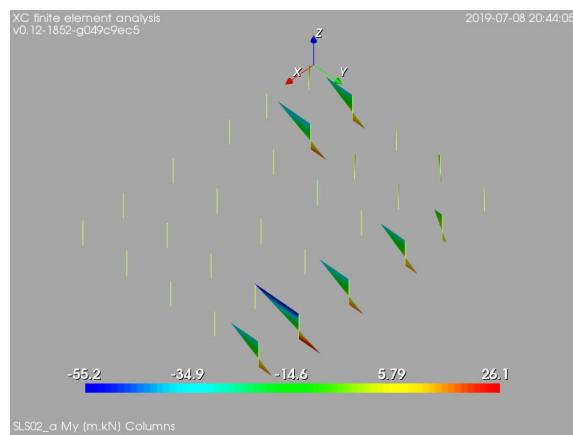


Figure 103: SLS02_a: 1.0*D + 1.0*Lru + Lpu + 0.3*S. Columns, bending moment about local axis y [m.kN]

B.2 Serviceability limit states

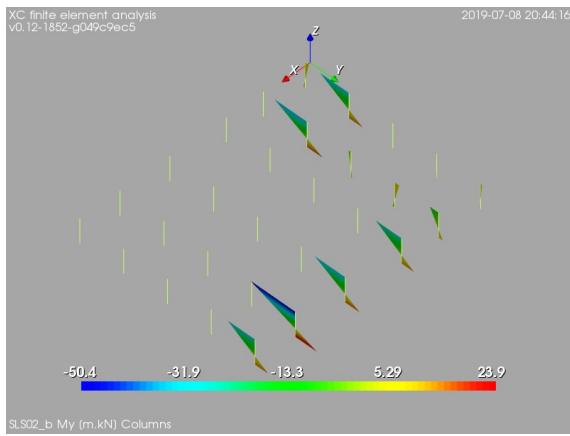


Figure 104: SLS02_b: $1.0*D + 1.0*Lrs + Lps + 0.3*S$. Columns, bending moment about local axis y [m.kN]

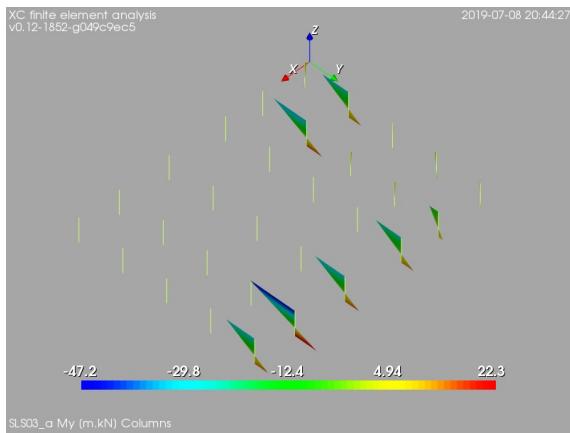


Figure 105: SLS03_a: $1.0*D + 1.0*S + 0.3*Lru + 0.3*Lpu$. Columns, bending moment about local axis y [m.kN]

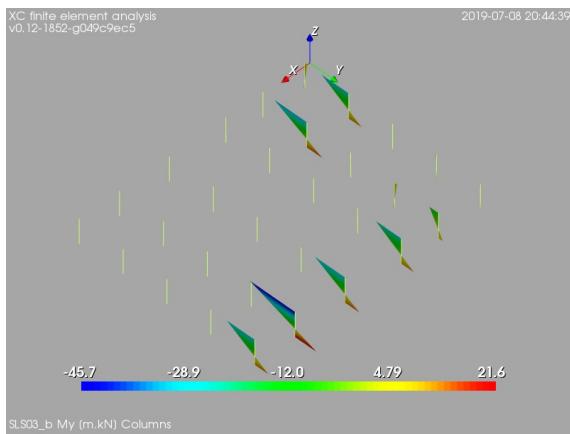


Figure 106: SLS03_b: $1.0*D + 1.0*S + 0.3*Lrs + 0.3*Lps$. Columns, bending moment about local axis y [m.kN]

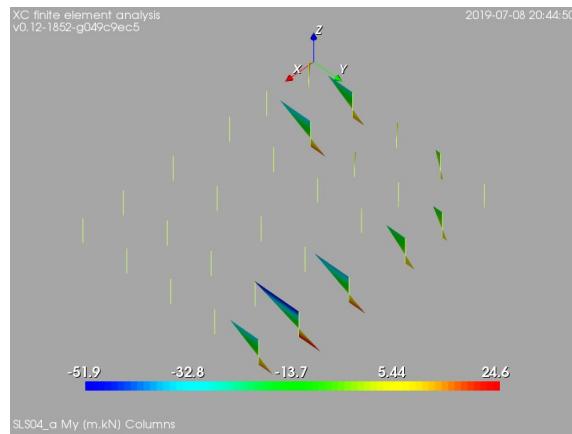


Figure 107: SLS04_a: 1.0*D + W_WE + 1.0*Lru + Lpu. Columns, bending moment about local axis y [m.kN]

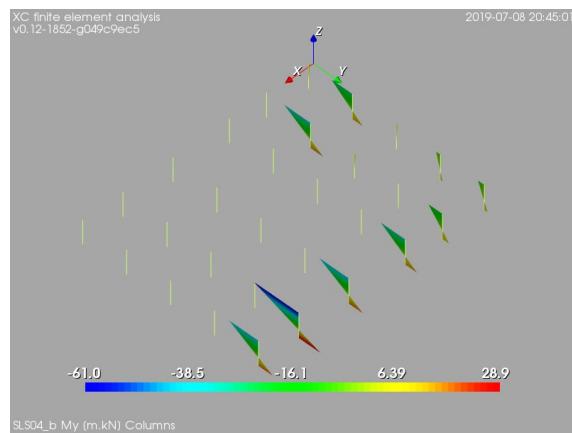


Figure 108: SLS04_b: 1.0*D + W_NS + 1.0*Lru + Lpu. Columns, bending moment about local axis y [m.kN]

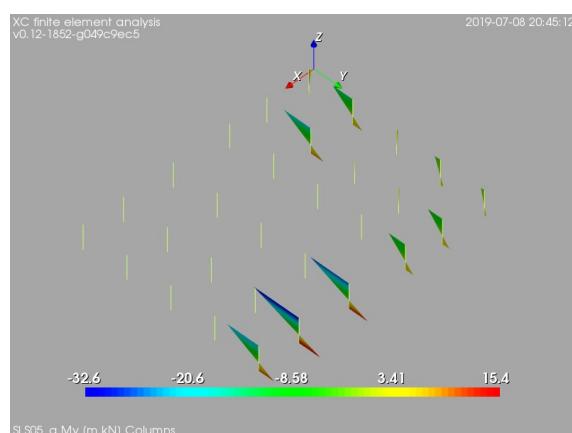


Figure 109: SLS05_a: 1.0*D + W_WE. Columns, bending moment about local axis y [m.kN]

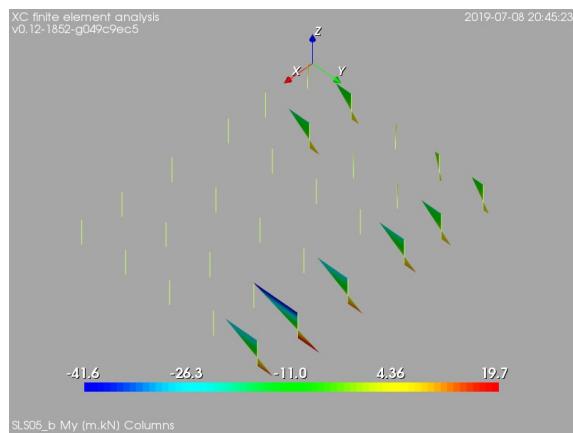


Figure 110: SLS05_b: 1.0*D + W_NS. Columns, bending moment about local axis y [m.kN]