

Foundation Calculation Report: «1750 OX Residences - 1750 N Oxford Ave. - Eau Claire, WI»

XC structural engineering

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1 Introduction and scope

This report describes the calculation procedure and data considered in order to design the foundation of a new apartment building in Eau Claire, Wisconsin.

The construction consists in a three-story apartment building with a first-floor footprint of about 19,500 square feet, a below-grade parking garage with a footprint of about 27,200 square feet, perimeter retaining walls, a slab-on-grade, and a conventional foundation system.

The first floor system is precast hollow core concrete plank on precast beams and columns. For the upper floors and roof, the system is wood-framed. Retaining walls and slab on grade are comprised of cast in place concrete, except for three reinforced CMU walls next to the garage aisles, that will be demolished during the second phase of construction.

The foundation uses conventional cast in place concrete footings to transfer axial compression and lateral loads to the ground.

2 Building codes

The following building and material codes were used for the design:

- Building code
 - International Building Code, 2018 Edition (IBC 2018) with reference to Minimum Design Loads for Buildings and Other Structures by the American Society of Civil Engineers, 2016 Edition (ASCE 7).
- Material codes
 - Reinforced Concrete: Building Code Requirements for Structural Concrete and Commentary by the American Concrete Institute, 2019 Edition (ACI 318).
 - Masonry: Building Code Requirements and Specification for Masonry Structures and Companion Commentaries, 2013 Edition (ACI 530/530).

3 Loading criteria

A summary of the project-specific loading criteria follows (see appendix A for a detailed list of load values).

3.1 Gravity loading

The gravity loads listed in Table 1 are in addition to the self weight of the structure. The minimum loading requirements were taken from ASCE 7 as well as the loading criteria supplied by the engineer of record. Loads are given in pounds per square foot (psf).

In addition to these uniform slab loads, a perimeter dead load of 12 psf was applied to the structure to account for the weight of the cladding system.

3.2 Wind design criteria

Wind loading is in accordance with the IBC and ASCE 7 requirements as shown in Table 2.

3.3 Snow loading

Wind loading is in accordance with the ASCE 7 requirements as shown in Table 3.

Table 1: Gravity Loads

Use	Live Loading	Superimposed Dead Loading
Parking Garage	40	3
Storage/HVAC	125	28
Stairways, exits	100	28
Level 1 residential	40	28
Level 1 corridors	100	28
Level 1 office, recreational	100	28
Level 1 courtyard (footprint)	150	150
Elevated levels residential	40	28
Elevated levels corridors	40	28
Cornices	60	-
Balconies	40	28
Roof	20	28

Table 2: Wind Design Criteria

Parameter	Value
Basic Wind Speed, 3-second gust (ultimate)	115 mph
Basic Wind Speed, 3-second gust (nominal)	90 mph
Exposure	B
Occupancy Category	II
Importance Factor (I_w)	1.0
Topographic Factor (K_{zt})	1.0
Enclosure Classification	Enclosed
Mean Roof Height (h)	33'

Table 3: Snow Design Criteria

Parameter	Value
Ground snow load p_g	60 psf
Terrain category	B
Exposure factor C_e	1.0
Thermal factor C_t	1.0
Occupancy Category	II
Snow load importance factor I_s	1.0
Snow load flat roof	42 psf

4 Seismic design criteria

Seismic loads are in accordance with the IBC requirements as shown in Table 4.

Table 4: **Seismic Design Criteria**

Parameter	Value
Building Latitude/Longitude	44°49'01.8"N 91°30'34.8"W
Occupancy Category	II
Importance Factor I_e	1.0
Mapped Spectral Acceleration	$S_s = 0.045; S_1 = 0.038$
Site Class	B
Site Class Coefficients	$F_a = 1.0; F_v = 1.0$
Spectral Response Coefficients	$S_{DS} = 0.03; S_{D1} = 0.025$
Seismic Design Category	A

5 Materials

The material properties used for the design are summarized in Tables 5 and 6.

Table 5: **Concrete properties**

Member	Nominal f'_c
Footings	3.0 ksi
Basement Walls	4.0 ksi
Foundation frost walls	4.0 ksi
Stair landings and treads	4.0 ksi
Slab on grade	4.0 ksi

Table 6: **Reinforcement properties**

Standard	Nominal f_y
All ASTM A615 Grade 60	60 ksi

6 Design and analysis software

The computer software employed for the analysis of the structure is the Finite Element Program called **XC** (see program description at http://xcengineering.xyz/html_files/software.html).

7 Load combinations

The load combinations shown in tables 7 and 8 follow the strength design load combinations listed in IBC, section 1605.

Table 7: Combinations Ultimate Limit States

Identifier	Load Combination
ULS01:	1.4*D
ULS02_a:	1.2*D + 1.6*Lru + Lpu + 0.5*S
ULS02_b:	1.2*D + 1.6*Lrs + Lps + 0.5*S
ULS03_a:	1.2*D + 1.6*S + 0.5*Lru + Lpu
ULS03_b:	1.2*D + 1.6*S + 0.5*Lrs + Lps
ULS04_b:	1.2*D + 1.6*S + 0.5*W_NS
ULS04_a:	1.2*D + 1.6*S + 0.5*W_WE
ULS05_a:	1.2*D + W_WE + 0.5*Lru + Lpu
ULS05_b:	1.2*D + W_NS + 0.5*Lru + Lpu
ULS05_c:	1.2*D + W_WE + 0.5*Lrs + Lps
ULS05_d:	1.2*D + W_NS + 0.5*Lrs + Lps
ULS06_a:	1.2*D + 0.5*Lru + Lpu + 0.2*S
ULS06_b:	1.2*D + 0.5*Lrs + Lps + 0.2*S
ULS07_a:	0.9*D + W_WE
ULS07_b:	0.9*D + W_NS

Where:

D = dead load

Lru = live load (uniform on rooms)

Lrs = live load (staggered pattern on rooms)

Lpu = live load (uniform on patios)

Lps = live load (staggered pattern on patios)

S = snow load

W_WE = Wind West-East

W_NS = Wind North-South

Table 8: Combinations Serviceability Limit States

Identifier	Load Combination
SLS01:	1.0*D
SLS02_a:	1.0*D + 1.0*Lru + Lpu + 0.3*S
SLS02_b:	1.0*D + 1.0*Lrs + Lps + 0.3*S
SLS03_a:	1.0*D + 1.0*S + 0.3*Lru + 0.3*Lpu
SLS03_b:	1.0*D + 1.0*S + 0.3*Lrs + 0.3*Lps
SLS04_a:	1.0*D + W_WE + 1.0*Lru + Lpu
SLS04_b:	1.0*D + W_NS + 1.0*Lru + Lpu
SLS04_c:	1.0*D + W_WE + 1.0*Lrs + Lps
SLS04_d:	1.0*D + W_NS + 1.0*Lrs + Lps
SLS05_a:	1.0*D + W_WE
SLS05_b:	1.0*D + W_NS

Where:

D = dead load

Lru = live load (uniform on rooms)

Lrs = live load (staggered pattern on rooms)

Lpu = live load (uniform on patios)

Lps = live load (staggered pattern on patios)

S = snow load

W_WE = Wind West-East

W_NS = Wind North-South

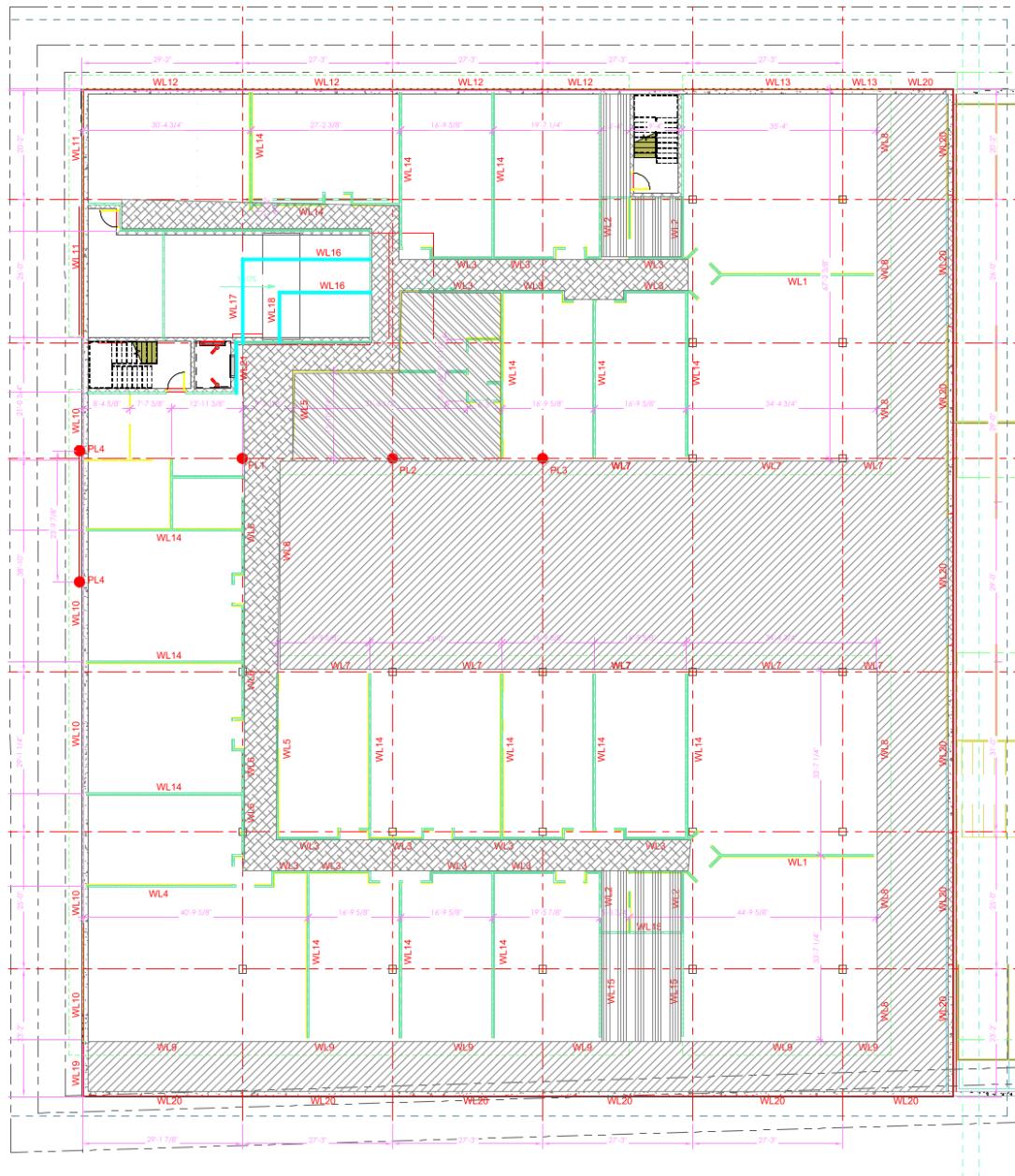
8 Structural model

A three-dimensional elastic computer model of the substructure is analyzed using XC. The model includes first floor frame and columns (see figure 2). The hollow core planks are modelled using shell elements, while beams and columns are modelled using frame elements. Loads transmitted by 2nd, 3rd floors and roof are applied to the 1st. Load layout is shown in figure 1. See figures 3 to 10 load distribution for each load case.

Linear loads are expressed in kN/m and surface loads in kN/m², where:

$$\begin{aligned}1 \text{ kN/m} &= 68.52178 \text{ lb/ft} \\1 \text{ kN/m}^2 &= 20.885434 \text{ psf}\end{aligned}$$

FOUNDATION CALCULATION REPORT



WALL LOAD SCHEDULE									
MARK	ELEV:	DEAD LOAD Ksi/ft	LIVE LOAD Ksi/ft	SNOW LOAD Ksi/ft	W-E WIND LOAD Ksi/ft	SOUTH/EAST W-E Ksi/ft	N-S WIND LOAD Ksi/ft	SOUTH/NORTH N-S Ksi/ft	EARTH PRES Ksi/ft
WL1	0'-0"	1.51	3.32	0.27	0.40	N/A	0.40	N/A	N/A
WL2	0'-0"	0.53	0.24	0.44	0.40	N/A	0.40	N/A	N/A
WL3	0'-0"	1.12	1.84	1.10	0.40	N/A	0.40	0.15	N/A
WL4	0'-0"	1.05	1.57	0.94	0.40	N/A	0.40	0.15	N/A
WL5	0'-0"	0.72	0.33	0.20	0.40	N/A	0.39	0.40	N/A
WL6	0'-0"	1.58	1.67	1.00	0.40	N/A	0.40	0.15	N/A
WL7	0'-0"	0.50	N/A	N/A	0.40	N/A	0.39	1.20	N/A
WL8	0'-0"	1.73	2.26	1.36	1.88	N/A	1.88	0.15	N/A
WL9	0'-0"	1.52	1.44	0.88	0.40	N/A	0.39	1.26	N/A
WL10	0'-0"	0.59	N/A	N/A	0.40	N/A	0.40	2.30	N/A
WL11	0'-0"	1.55	1.57	0.74	1.08	N/A	1.08	0.15	2.30
WL12	0'-0"	1.58	1.67	1.00	1.08	N/A	1.08	0.15	2.30
WL13	0'-0"	0.27	N/A	N/A	0.40	N/A	0.40	1.20	N/A
WL14	0'-0"	1.72	1.33	0.44	0.40	N/A	0.40	0.15	N/A
WL15	0'-0"	0.85	1.00	0.50	0.40	N/A	0.40	0.15	N/A
WL16	11'-2"	0.94	1.07	1.07	0.40	N/A	0.39	0.40	N/A
WL17	11'-2"	0.69	0.20	0.20	0.40	N/A	0.39	0.40	N/A
WL18	11'-2"	N/A	N/A	N/A	0.40	N/A	0.40	N/A	2.30
WL19	11'-2"	N/A	N/A	N/A	0.40	N/A	0.40	N/A	2.30
WL20	11'-2"	N/A	N/A	N/A	0.40	N/A	0.40	N/A	N/A

POINT LOAD SCHEDULE			
MARK	DEAD LOAD kN	LIVE LOAD kN	SNOW LOAD kN
PL1	15.24	25.01	15.01
PL2	30.47	50.02	30.02
PL3	15.24	25.01	15.01
PL4	17.64	17.40	10.30

SUPERIMPOSED UNIFORM LOAD SCHEDULE			
MARK	DEAD LOAD PSF	LIVE LOAD PSF	SNOW LOAD PSF
WALLS	150.00	150.00	42.00
CORRIDORS	20.00	100.00	N/A
STAIRS AND EXITS	20.00	100.00	N/A
STORE	20.00	100.00	N/A
PRIVATE ROOMS	20.00	40.00	N/A
MULTIFAMILY DWELLING			

Figure 1: Load layout on first floor.

8. STRUCTURAL MODEL

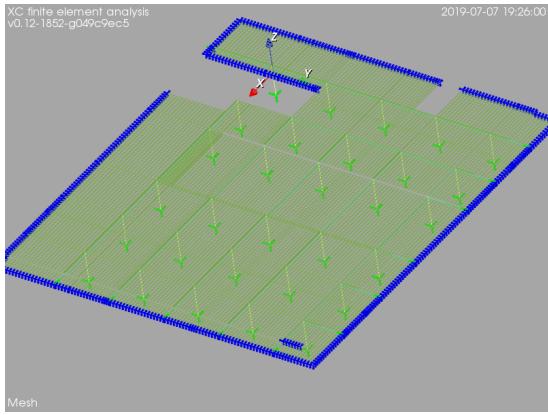


Figure 2: Elastic model, mesh.

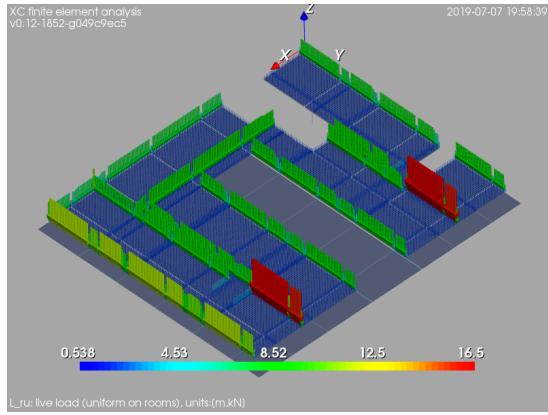


Figure 5: Load case Lrs: live load (staggered pattern on rooms) [units: kN,m].

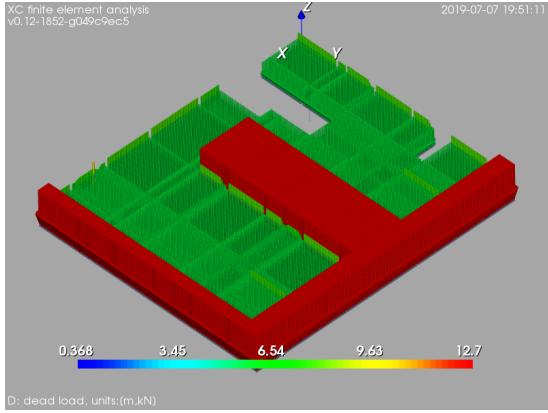


Figure 3: Load case D: dead load (include slab self-weight) [units: kN,m].

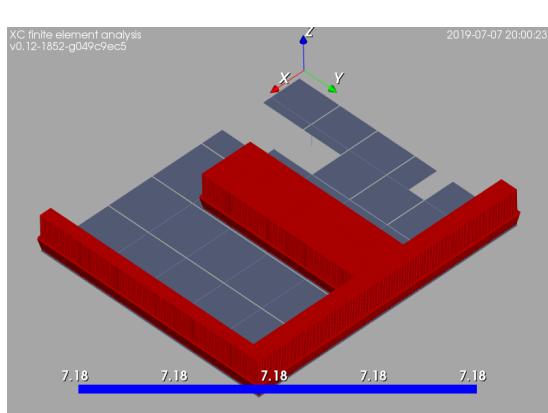


Figure 6: Load case Lpu: live load (uniform on patios) [units: kN,m].

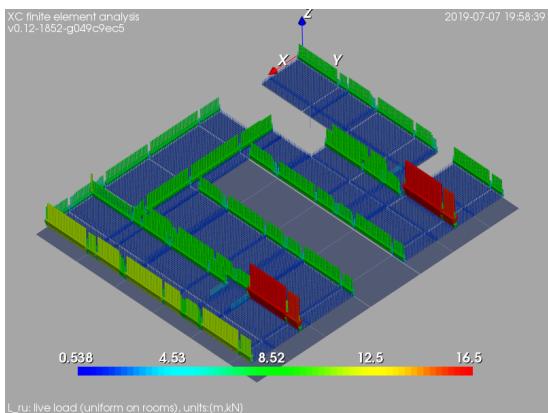


Figure 4: Load case Lru: live load (uniform on rooms) [units: kN,m].

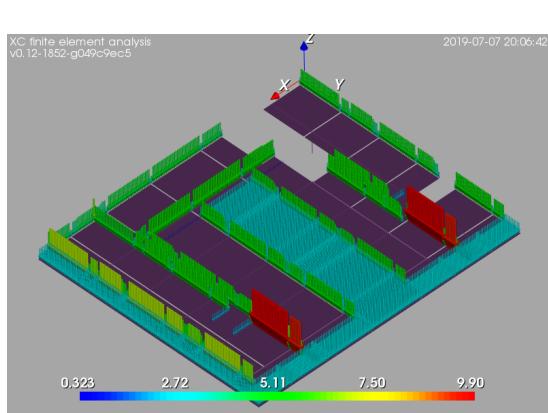


Figure 7: Load case S: snow [units: kN,m].

FOUNDATION CALCULATION REPORT

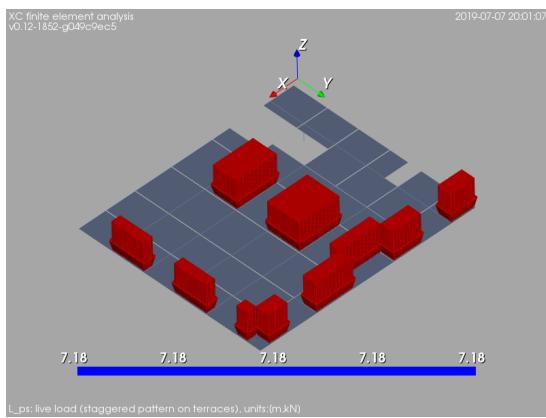


Figure 8: Load case L_{ps} : live load (staggered pattern on patios) [units: kN,m].

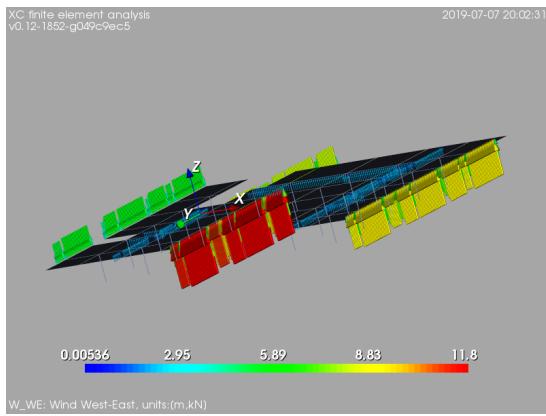


Figure 9: Load case W_{WE} : wind West-East [units: kN,m].

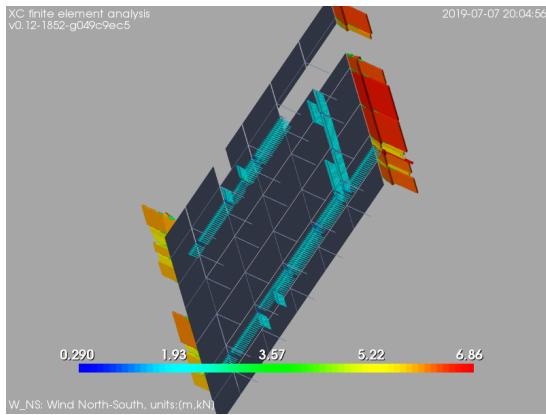


Figure 10: Load case W_{NS} : wind North-South [units: kN,m].

9 Footings

9.1 Introduction

9.2 Loads

The loads acting on the footings are shown in §B.

9.3 Load combinations

The load combinations are shown in tables 7 and 8.

9.4 Footing dimensions and reinforcement

The dimensions and the reinforcement of the footings are indicated in the table 9. The position of the footing in the building grid is indicated at the last column.

9.5 Allowable soil-bearing pressures

The results obtained for the verification of the soil-bearing capacity are the following:

Foundation	Worst combination	Vertical load (kN)	Capacity factor
A1	SLS04_a	-356.20	0.33
A2	SLS02_a	-644.78	0.60
A3	SLS02_a	-950.92	0.88
A4	SLS02_a	-881.82	0.82
A5	SLS04_b	-933.03	0.86
B2	SLS02_a	-670.79	0.56
B3	SLS02_a	-1,030.65	0.86
B4	SLS02_a	-968.24	0.80
B5	SLS04_b	-972.32	0.81
C1	SLS02_a	-1,460.67	0.99
C2	SLS02_a	-1,742.45	0.99
C3	SLS02_a	-1,750.31	0.99
C4	SLS02_a	-1,751.62	0.99
C5	SLS02_a	-1,660.02	0.94
D1	SLS02_a	-1,648.12	1.02
D2	SLS04_a	-1,950.01	1.01
D3	SLS04_a	-1,959.12	1.02
D4	SLS04_a	-1,960.14	1.02
D5	SLS04_a	-1,838.69	0.96
F1	SLS02_a	-1,090.88	0.82
F2	SLS02_a	-997.32	0.75
F3	SLS02_a	-1,011.87	0.76
F4	SLS02_a	-1,005.30	0.75
F5	SLS04_b	-741.90	0.56
G1	SLS02_a	-1,496.86	0.93
G2	SLS02_a	-1,256.06	0.78
G3	SLS02_a	-1,227.94	0.76
G4	SLS02_a	-1,137.75	0.70
G5	SLS04_b	-1,167.26	0.72

COLUMN FOOTING SCHEDULE						
MARK	DIMENSIONS			BOTTOM REINFORCING		COLUMNS
	W	L	D	LONG	SHORT	
FT90a	9'-0"	9'-0"	1'-8"	(10)-#7	(10)-#7	A1 A2
FT90b	9'-0"	9'-0"	1'-8"	(10)-#8	(10)-#8	A3 A4 A5
FT96a	9'-6"	9'-6"	1'-8"	(10)-#7	(10)-#7	B2
FT96b	9'-6"	9'-6"	1'-8"	(10)-#8	(10)-#8	B3 B4 B5
FT100	10'-0"	10'-0"	2'-1"	(11)-#8	(11)-#8	F1 F2 F3 F4 F5
FT106	10'-6"	10'-6"	2'-3"	(11)-#8	(11)-#8	C1
FT110a	11'-0"	11'-0"	2'-1"	(12)-#8	(12)-#8	G2 G3 G4 G5
FT110b	11'-0"	11'-0"	2'-3"	(12)-#8	(12)-#8	D1 G1
FT116	11'-6"	11'-6"	2'-1"	(12)-#8	(12)-#8	C2 C3 C4 C5
FT120	12'-0"	12'-0"	2'-3"	(13)-#8	(13)-#8	D2 D3 D4 D5

COLUMN FOOTING SCHEDULE:

1. REFER TO STRUCTURAL NOTES SHEET FOR LAPS IN STEEL REINFORCEMENT.
2. REFER TO FUNDATION PLAN FOR TOP OF FOOTING ELEVATIONS.
3. ALL FOOTING EXCAVATIONS SHALL BE INSPECTED AND APPROVED BY THE GEOTECHNICAL ENGINEER PRIOR TO PLACING CONCRETE

Table 9: Column footing schedule.

9.6 Flexure design

9.7 Shear design

The results of the shear strength verification are shown in the following table:

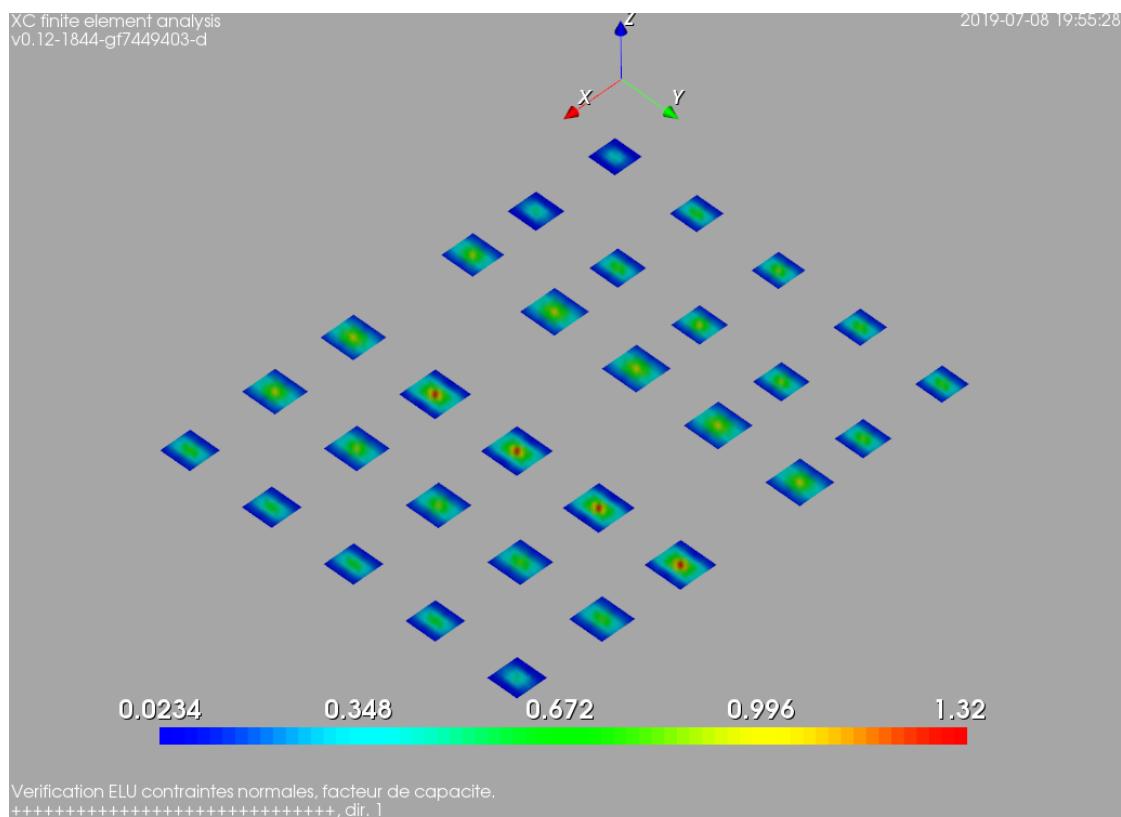


Table 10: Flexure in the longitudinal direction. Capacity factor.

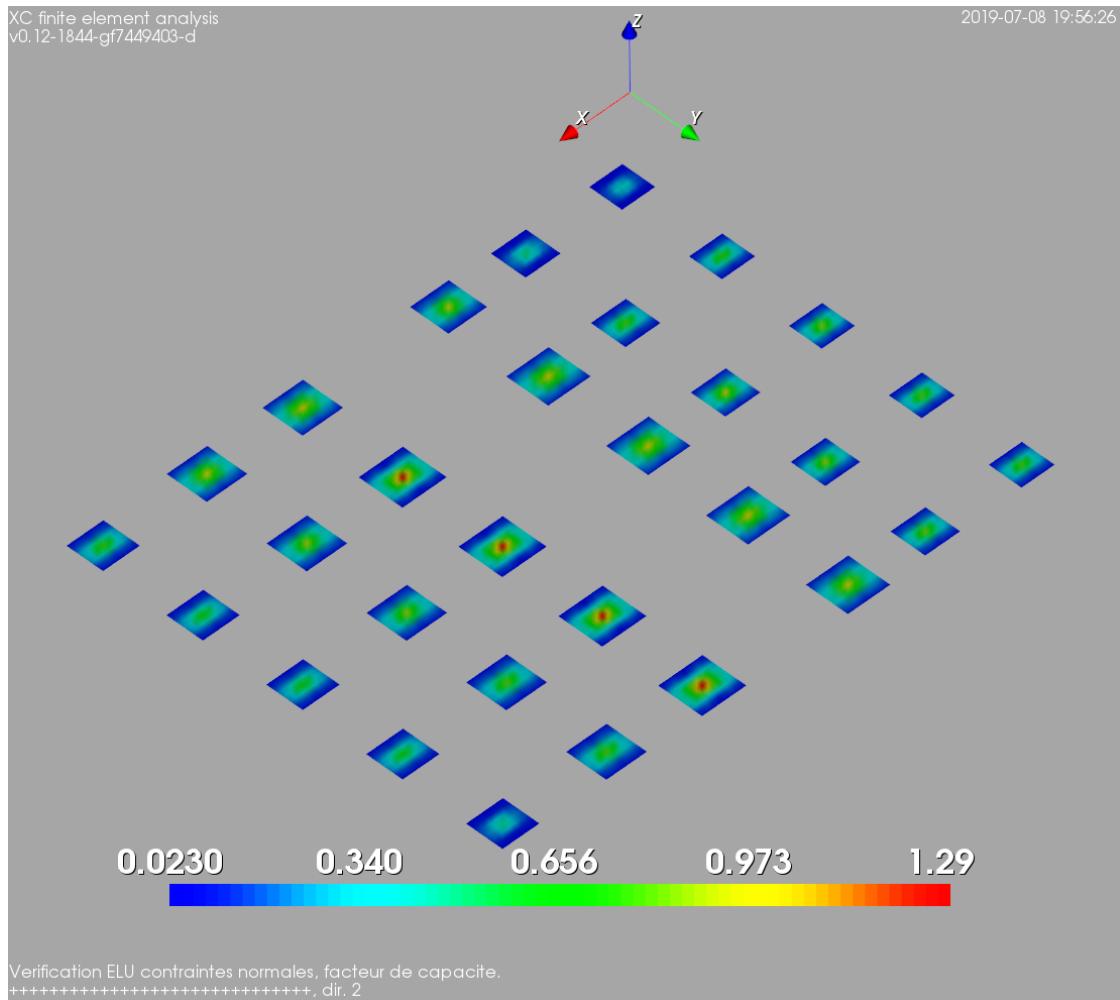


Table 11: Flexure in the transverse direction. Capacity factor.

Footing	Worst combination	Vertical load (kN)	thickness (m)	l (m)	d (m)	c (m)	Vd/l kN/m	Vu kN/m	CF
A1	SLS04_a	-356.20	0.51	2.74	0.46	0.41	33.66	280.00	0.12
A2	SLS02_a	-644.78	0.51	2.74	0.46	0.41	60.94	280.00	0.22
A3	SLS02_a	-950.92	0.51	2.74	0.46	0.41	89.87	280.00	0.32
A4	SLS02_a	-881.82	0.51	2.74	0.46	0.41	83.34	280.00	0.30
A5	SLS04_b	-933.03	0.51	2.74	0.46	0.41	88.18	280.00	0.31
B2	SLS02_a	-670.79	0.51	2.90	0.46	0.41	63.00	280.00	0.22
B3	SLS02_a	-1,030.65	0.51	2.90	0.46	0.41	96.79	280.00	0.35
B4	SLS02_a	-968.24	0.51	2.90	0.46	0.41	90.93	280.00	0.32
B5	SLS04_b	-972.32	0.51	2.90	0.46	0.41	91.31	280.00	0.33
C1	SLS02_a	-1,460.67	0.69	3.20	0.62	0.41	111.20	378.00	0.29
C2	SLS02_a	-1,742.45	0.64	3.51	0.57	0.41	138.68	350.00	0.40
C3	SLS02_a	-1,750.31	0.64	3.51	0.57	0.41	139.31	350.00	0.40
C4	SLS02_a	-1,751.62	0.64	3.51	0.57	0.41	139.42	350.00	0.40
C5	SLS02_a	-1,660.02	0.64	3.51	0.57	0.41	132.12	350.00	0.38
D1	SLS02_a	-1,648.12	0.69	3.35	0.62	0.41	125.50	378.00	0.33
D2	SLS04_a	-1,950.01	0.64	3.66	0.57	0.41	153.65	350.00	0.44
D3	SLS04_a	-1,959.12	0.64	3.66	0.57	0.41	154.37	350.00	0.44
D4	SLS04_a	-1,960.14	0.64	3.66	0.57	0.41	154.45	350.00	0.44
D5	SLS04_a	-1,838.69	0.64	3.66	0.57	0.41	144.88	350.00	0.41
F1	SLS02_a	-1,090.88	0.64	3.05	0.57	0.41	87.98	350.00	0.25
F2	SLS02_a	-997.32	0.64	3.05	0.57	0.41	80.44	350.00	0.23
F3	SLS02_a	-1,011.87	0.64	3.05	0.57	0.41	81.61	350.00	0.23
F4	SLS02_a	-1,005.30	0.64	3.05	0.57	0.41	81.08	350.00	0.23
F5	SLS04_b	-741.90	0.64	3.05	0.57	0.41	59.84	350.00	0.17
G1	SLS02_a	-1,496.86	0.69	3.35	0.62	0.41	113.98	378.00	0.30
G2	SLS02_a	-1,256.06	0.64	3.35	0.57	0.41	100.75	350.00	0.29
G3	SLS02_a	-1,227.94	0.64	3.35	0.57	0.41	98.50	350.00	0.28
G4	SLS02_a	-1,137.75	0.64	3.35	0.57	0.41	91.26	350.00	0.26
G5	SLS04_b	-1,167.26	0.64	3.35	0.57	0.41	93.63	350.00	0.27

9.8 Two-way shear design

The results of the punching shear strength verification are shown in the following table:

Footing	Worst combination	Vertical load (kN)	thickness (m)	L (m)	d (m)	c (m)	Vd/l kN/m	Vu kN/m	CF
A1	SLS04_a	-356.20	0.51	2.74	0.46	0.41	92.90	517.97	0.18
A2	SLS02_a	-644.78	0.51	2.74	0.46	0.41	168.16	517.97	0.32
A3	SLS02_a	-950.92	0.51	2.74	0.46	0.41	248.00	517.97	0.48
A4	SLS02_a	-881.82	0.51	2.74	0.46	0.41	229.98	517.97	0.44
A5	SLS04_b	-933.03	0.51	2.74	0.46	0.41	243.33	517.97	0.47
B1	SLS02_a	-429.53	0.51	2.90	0.46	0.41	113.28	517.97	0.22
B2	SLS02_a	-670.79	0.51	2.90	0.46	0.41	176.91	517.97	0.34
B3	SLS02_a	-1,030.65	0.51	2.90	0.46	0.41	271.82	517.97	0.52
B4	SLS02_a	-968.24	0.51	2.90	0.46	0.41	255.36	517.97	0.49
B5	SLS04_b	-972.32	0.51	2.90	0.46	0.41	256.43	517.97	0.50
C1	SLS02_a	-1,460.67	0.69	3.20	0.62	0.41	320.25	699.26	0.46
C2	SLS02_a	-1,742.45	0.64	3.51	0.57	0.41	410.79	647.47	0.63
C3	SLS02_a	-1,750.31	0.64	3.51	0.57	0.41	412.64	647.47	0.64
C4	SLS02_a	-1,751.62	0.64	3.51	0.57	0.41	412.95	647.47	0.64
C5	SLS02_a	-1,660.02	0.64	3.51	0.57	0.41	391.35	647.47	0.60
D1	SLS02_a	-1,648.12	0.69	3.35	0.62	0.41	365.00	699.26	0.52
D2	SLS04_a	-1,950.01	0.64	3.66	0.57	0.41	462.88	647.47	0.71
D3	SLS04_a	-1,959.12	0.64	3.66	0.57	0.41	465.05	647.47	0.72
D4	SLS04_a	-1,960.14	0.64	3.66	0.57	0.41	465.29	647.47	0.72
D5	SLS04_a	-1,838.69	0.64	3.66	0.57	0.41	436.46	647.47	0.67
F1	SLS02_a	-1,090.88	0.64	3.05	0.57	0.41	250.18	647.47	0.39
F2	SLS02_a	-997.32	0.64	3.05	0.57	0.41	228.72	647.47	0.35
F3	SLS02_a	-1,011.87	0.64	3.05	0.57	0.41	232.06	647.47	0.36
F4	SLS02_a	-1,005.30	0.64	3.05	0.57	0.41	230.55	647.47	0.36
F5	SLS04_b	-741.90	0.64	3.05	0.57	0.41	170.14	647.47	0.26
G1	SLS02_a	-1,496.86	0.69	3.35	0.62	0.41	331.50	699.26	0.47
G2	SLS02_a	-1,256.06	0.64	3.35	0.57	0.41	293.79	647.47	0.45
G3	SLS02_a	-1,227.94	0.64	3.35	0.57	0.41	287.22	647.47	0.44
G4	SLS02_a	-1,137.75	0.64	3.35	0.57	0.41	266.12	647.47	0.41
G5	SLS04_b	-1,167.26	0.64	3.35	0.57	0.41	273.02	647.47	0.42

10 Basement walls

10.1 Introduction

The design is based in the following assumptions:

- Design wall with pinned base and pinned top.
- Neglect corner regions (wall spans one-way only).
- Top slab is in place and has achieved full strength prior to backfilling.
- Vehicular traffic around the building is represented by a uniform load of 250 psf (11.97 kN/m^2).
- The vertical response of the soil calculated using a Winkler model with a subgrade reaction module of set of 200 pounds per cubic inch ($54.29 \times 10^6 \text{ N/m}^3$).
- Water table deep below structure.

10.2 Load determination

10.2.1 Self weight

The self weight of the reinforced concrete is calculated from its density: 2500 kg/m^3 .

10.2.2 Axial loads from building

The loads transferred by the top slab to the wall are as follows:

Building side	Load	Phase 1 (kN/m)	Phase 2 (kN/m)
North	SnowL	10.06	10.06
	LiveL	21.67	21.67
	Wind_NS	-15.12	-15.12
	Wind_WE	-1.33	-1.33
	DeadL	31.54	31.54
South	SnowL	8.04	16.08
	LiveL	14.22	28.44
	Wind_NS	4.97	9.95
	Wind_WE	-0.23	-0.46
	DeadL	20.58	41.15
East	SnowL	11.96	11.96
	LiveL	23.75	23.75
	Wind_NS	-0.07	-0.07
	Wind_WE	12.97	12.97
	DeadL	30.87	30.87
West	SnowL	15.02	15.02
	LiveL	27.15	27.15
	Wind_NS	-0.20	-0.20
	Wind_WE	-13.20	-13.20
	DeadL	29.81	29.81

10.3 Load combinations

Serviceability limit states		
Equation 16-8	EQ1608	$1.0*\text{selfWeight}+1.0*\text{deadLoad}$
Equation 16-9	EQ1609A	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+1.0*\text{trafficLoad}$
Equation 16-9	EQ1609B	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+1.0*\text{liveLoad}$
Equation 16-10	EQ1610	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+1.0*\text{snowLoad}$
Equation 16-11	EQ1611A	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+0.75*\text{trafficLoad}+0.75*\text{snowLoad}$
Equation 16-11	EQ1611B	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+0.75*\text{liveLoad}+0.75*\text{snowLoad}$
Equation 16-12	EQ1612	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+0.6*\text{windLoad}$
Equation 16-13	EQ1613A	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+0.45*\text{windLoad}+0.75*\text{trafficLoad}+0.75*\text{snowLoad}$
Equation 16-13	EQ1613B	$1.0*\text{selfWeight}+1.0*\text{deadLoad}+0.45*\text{windLoad}+0.75*\text{liveLoad}+0.75*\text{snowLoad}$
Equation 16-14	doesn't apply	
Equation 16-15	EQ1615	$0.6*\text{selfWeight}+0.6*\text{deadLoad}+0.6*\text{windLoad}$
Equation 16-16	doesn't apply	

CONCRETE WALL REINFORCING SCHEDULE					
MARK	TYPE	THICKNESS	REINFORCEMENT		REMARKS
			VERTICAL	HORIZONTAL	
W1	CONCRETE	10"	5#'s AT 18"o.c.	5#'s AT 12"o.c.	inside face
W2	CONCRETE	10"	5#'s AT 12"o.c.	5#'s AT 12"o.c.	inside face
W3	CONCRETE	10"	6#'s AT 12"o.c.	5#'s AT 12"o.c.	inside face
W4	CONCRETE	8"	4#'s AT 12"o.c.	3#'s AT 12"o.c.	centered in wall thickness

CONCRETE WALL REINFORCING SCHEDULE NOTES:
1. REFER TO STRUCTURAL NOTES SHEET FOR LAPS IN STEEL REINFORCEMENT.
2. COORDINATE AND VERIFY ALL DIMENSIONS WITH ARCHITECTURAL DRAWINGS AND EXIST. CONDITIONS

Table 12: Concrete walls reinforcing schedule

Ultimate limit states.		
Equation 16-1	EQ1601	1.4*selfWeight+1.4*deadLoad
Equation 16-2	EQ1602A	1.2*selfWeight+1.2*deadLoad+1.6*trafficLoad+0.5*snowLoad
Equation 16-2	EQ1602B	1.2*selfWeight+1.2*deadLoad+1.6*liveLoad+0.5*snowLoad
Equation 16-3	EQ1603A	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*trafficLoad
Equation 16-3	EQ1603B	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*liveLoad
Equation 16-3	EQ1603C	1.2*selfWeight+1.2*deadLoad+1.6*snowLoad+0.5*windLoad
Equation 16-4	EQ1604A	1.2*selfWeight+1.2*deadLoad+1.0*windLoad+0.5*trafficLoad+0.5*snowLoad
Equation 16-4	EQ1604B	1.2*selfWeight+1.2*deadLoad+1.0*windLoad+0.5*liveLoad+0.5*snowLoad
Equation 16-5	EQ1605A	1.2*selfWeight+1.2*deadLoad+0.5*trafficLoad+0.7*snowLoad
Equation 16-5	EQ1605B	1.2*selfWeight+1.2*deadLoad+0.5*liveLoad+0.7*snowLoad
Equation 16-6	doesn't apply	
Equation 16-7	doesn't apply	

10.3.1 Earth pressure

The soil pressure over the wall has been calculated using the lateral pressure at rest with a coefficient $K_0 = 0.5$.

10.4 Stem dimensions and reinforcement

The thickness and the reinforcement for the walls are indicated in the table 12.

10.4.1 Wall types

For analysis purposes we have considered the following wall types:

Wall	Stem height (m)
T1	3.15
T2	2.74
T3	3.53
T4	3.12
T5	2.51
T6	3.43

10.4.2 Internal forces

The envelope of internal forces envelope for each of the walls are given in tables 13 to 18.

10.4.3 Reinforcement checks

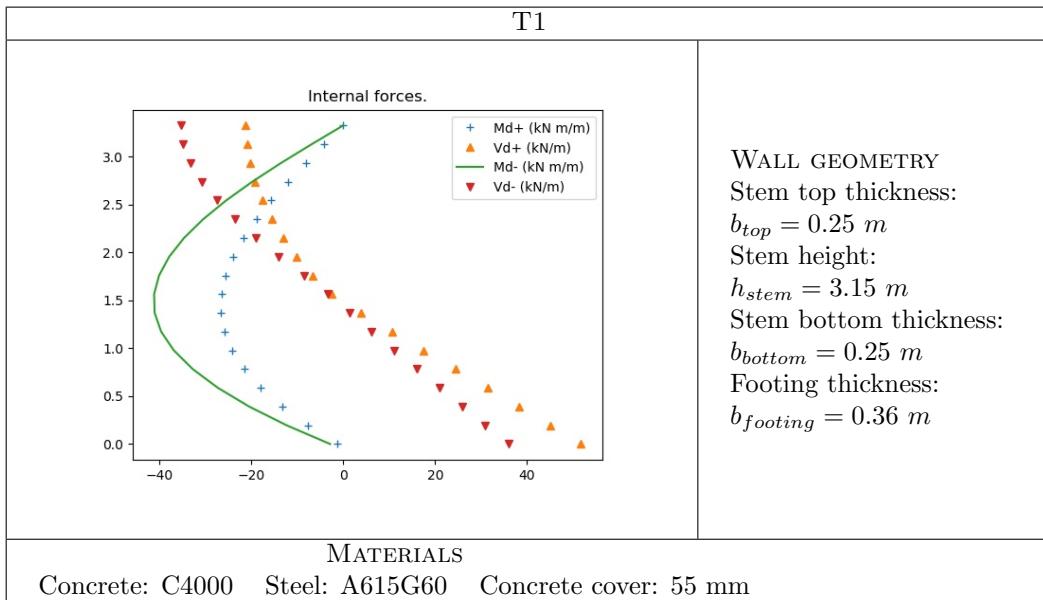


Table 13: Wall materials and dimensions T1

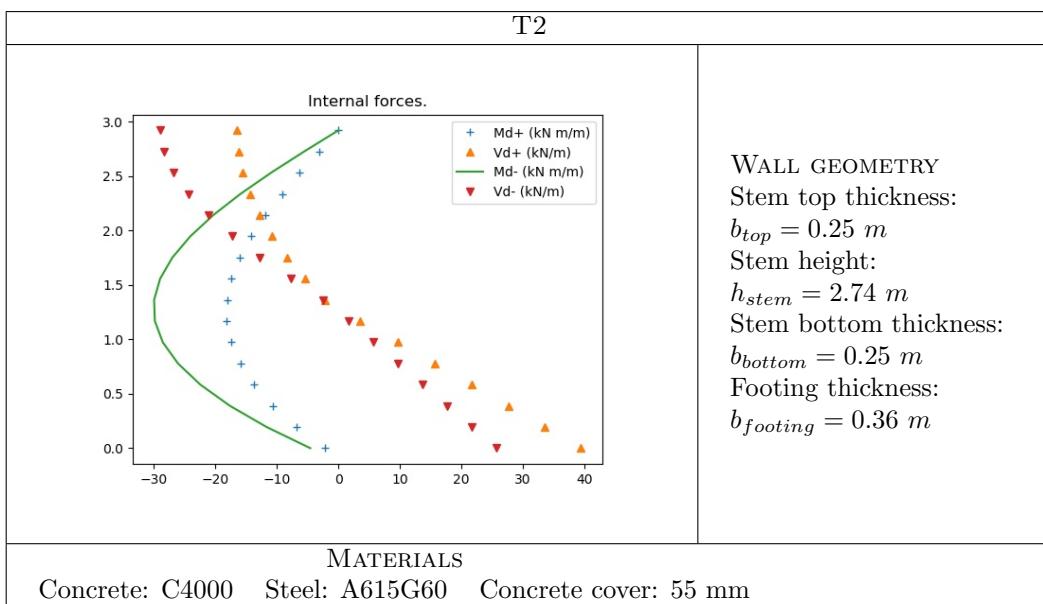


Table 14: Wall materials and dimensions T2

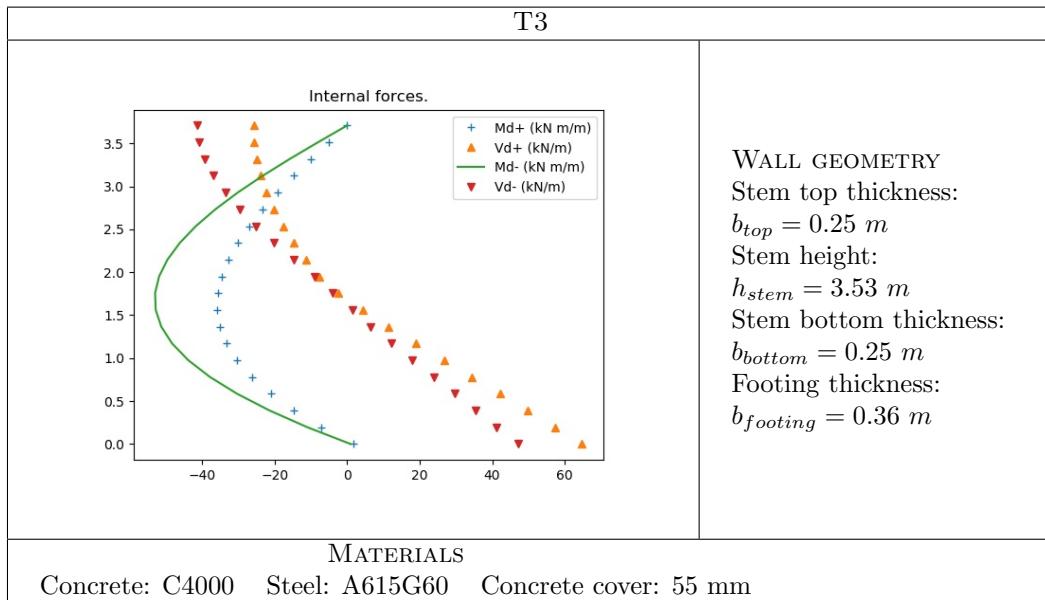


Table 15: Wall materials and dimensions T3

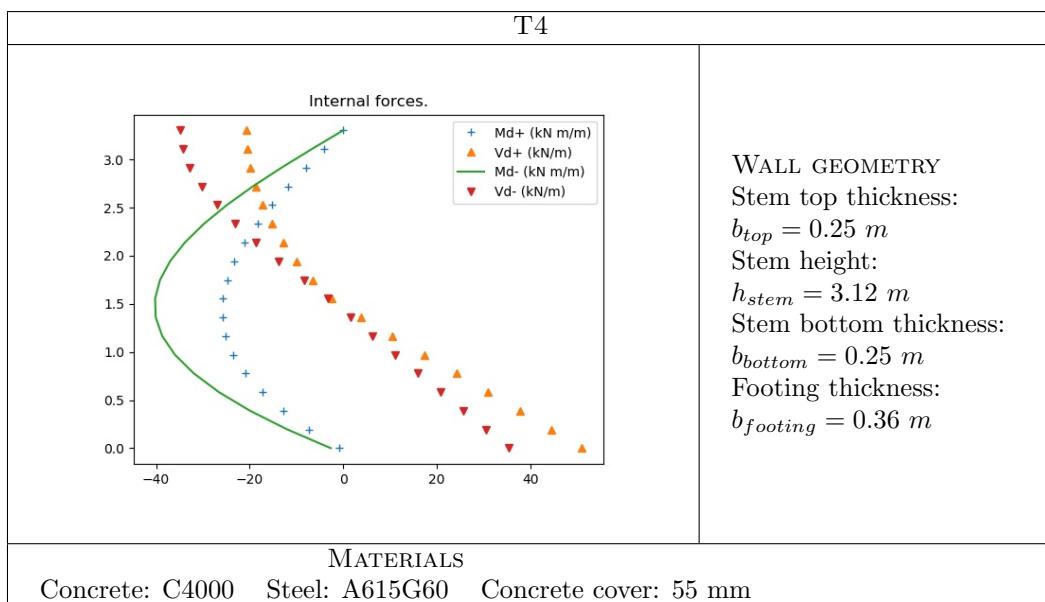


Table 16: Wall materials and dimensions T4

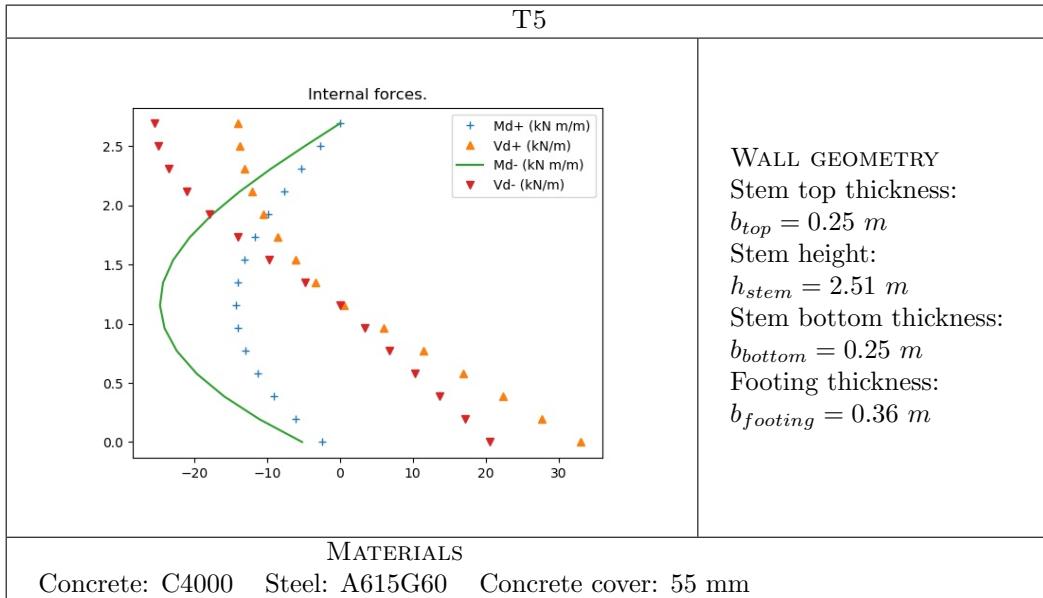


Table 17: Wall materials and dimensions T5

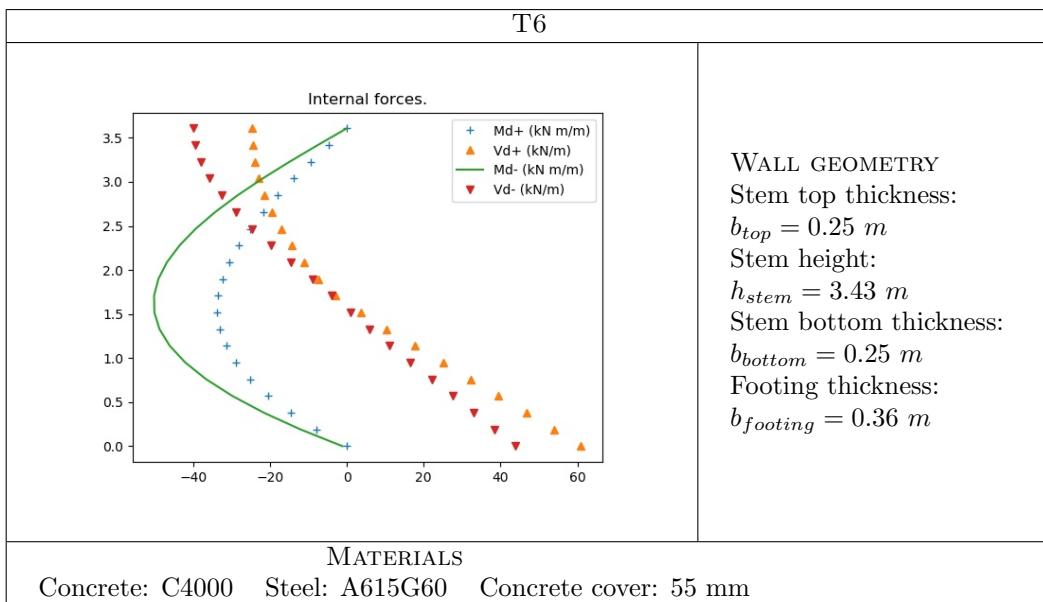


Table 18: Wall materials and dimensions T6

WALL VERTICAL REINFORCEMENTS
T1 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 16 mm, spacing: 300 mm reinf. development L=0.34 m (22 diameters). area: As= 6.67 cm ² /m areaMin: 4.56 cm ² /m F(As)= 1.46 OK! Bending check: Md= 40.09 kN m, MR= 41.36kN m F(M)= 1.03 OK! Shear check: Vd= 7.61 kN, VR= 199.37 kN F(V)= 26.21 OK!
T2 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 16 mm, spacing: 400 mm reinf. development L=0.34 m (22 diameters). area: As= 5.00 cm ² /m areaMin: 4.56 cm ² /m F(As)= 1.10 OK! Bending check: Md= 29.02 kN m, MR= 31.02kN m F(M)= 1.07 OK! Shear check: Vd= 6.84 kN, VR= 199.37 kN F(V)= 29.15 OK!
T3 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 19 mm, spacing: 300 mm reinf. development L=0.61 m (32 diameters). area: As= 9.47 cm ² /m areaMin: 4.56 cm ² /m F(As)= 2.08 OK! Bending check: Md= 51.88 kN m, MR= 58.26kN m F(M)= 1.12 OK! Shear check: Vd= 7.98 kN, VR= 199.37 kN F(V)= 24.98 OK!
T4 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 16 mm, spacing: 300 mm reinf. development L=0.34 m (22 diameters). area: As= 6.67 cm ² /m areaMin: 4.56 cm ² /m F(As)= 1.46 OK! Bending check: Md= 39.19 kN m, MR= 41.36kN m F(M)= 1.06 OK! Shear check: Vd= 7.46 kN, VR= 199.37 kN F(V)= 26.73 OK!
T5 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 16 mm, spacing: 400 mm reinf. development L=0.34 m (22 diameters). area: As= 5.00 cm ² /m areaMin: 4.56 cm ² /m F(As)= 1.10 OK! Bending check: Md= 23.62 kN m, MR= 31.02kN m F(M)= 1.31 OK! Shear check: Vd= 6.42 kN, VR= 199.37 kN F(V)= 31.05 OK!
T6 wall. Inside stem reinforcement: RC section dimensions; b= 1.00 m, h= 0.25 m diam: 19 mm, spacing: 300 mm reinf. development L=0.61 m (32 diameters). area: As= 9.47 cm ² /m areaMin: 4.56 cm ² /m F(As)= 2.08 OK! Bending check: Md= 49.02 kN m, MR= 58.26kN m F(M)= 1.19 OK! Shear check: Vd= 8.13 kN, VR= 199.37 kN F(V)= 24.54 OK!

SHEAR CHECK
T1 wall. Shear check: Shear check: Vd= 42.99 kN, VR= 199.37 kN F(V)= 4.64 OK!
T2 wall. Shear check: Shear check: Vd= 31.78 kN, VR= 199.37 kN F(V)= 6.27 OK!
T3 wall. Shear check: Shear check: Vd= 55.00 kN, VR= 199.37 kN F(V)= 3.63 OK!
T4 wall. Shear check: Shear check: Vd= 42.35 kN, VR= 199.37 kN F(V)= 4.71 OK!
T5 wall. Shear check: Shear check: Vd= 26.03 kN, VR= 199.37 kN F(V)= 7.66 OK!
T6 wall. Shear check:
..../..

SHEAR CHECK (CONT.)			
Shear check: Vd= 51.43 kN, VR= 199.37 kN F(V)= 3.88 OK!			

10.4.4 Wall foundations

The results obtained for the verifications of the footing stability and the soil-bearing capacity. According to the geotechnical report the allowable soil bearing pressure is 3000 psf (143.64 kN/m^2).

WALL FOUNDATION: T1			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.23	1.00	EQ1609A
Adm. pressure:	1.09	1.00	EQ1613B
WALL FOUNDATION: T2			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.46	1.00	EQ1609A
Adm. pressure:	1.13	1.00	EQ1613B
WALL FOUNDATION: T3			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.13	1.00	EQ1609A
Adm. pressure:	1.12	1.00	EQ1613B
WALL FOUNDATION: T4			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.45	1.00	EQ1609A
Adm. pressure:	1.08	1.00	EQ1613B
WALL FOUNDATION: T5			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1613B
Sliding:	1.69	1.00	EQ1609A
Adm. pressure:	1.22	1.00	EQ1613B
WALL FOUNDATION: T6			
Vérification:	F_{disp}	F_{req}	Combination
Overturning:	$\gg 1$	1.00	EQ1609A
Sliding:	1.10	1.00	EQ1609A
Adm. pressure:	1.03	1.00	EQ1613B
$F_{avail.}$: available security.			
F_{req} : required security.			

11 Ramp

11.1 Design criteria

Materials	Concrete: $f'_c = 4.0 \text{ ksi}$ Reinforcing steel: $f_y = 60 \text{ ksi}$
Structural loads	Self weight reinforced concrete: 2500 kg/m^3 Live load garages (passenger vehicles): 40 psf Concentrated load vehicle : 3000 pound
Load cases	D: dead load (see fig. 13) Lunif: uniform live load (see fig. 14) LconcSpan1: concentrated live load on mid-span 1 (see fig. 15) LconcSpan2: concentrated live load on mid-span 2 (see fig. 16) LconcSpan3: concentrated live load on mid-span 3 (see fig. 17)
Ultim. Limit States	ULS01: $1.4*D$ ULS02: $1.2*D + 1.6*L\text{unif}$ ULS03: $1.2*D + 1.6*L\text{concSpan1}$ ULS04: $1.2*D + 1.6*L\text{concSpan2}$ ULS05: $1.2*D + 1.6*L\text{concSpan3}$
Structural model	3D elastic computer model (see fig. 12) analyzed using XC

11.2 Acceptance criteria

Figure 11 shows the design thickness of the ramp slab and the reinforcing layout.

The slab is checked for the load combinations summarized in section 11.1. The limit state checking was performed in general compliance with ACI 318, using the program XC. The representative plots for the results obtained are shown in figs. 20 to 20 for the normal stresses check, and figs. 21 to 24 for the shear check. In every case, all the elements have a demand to capacity ratio of 1.0 or less.

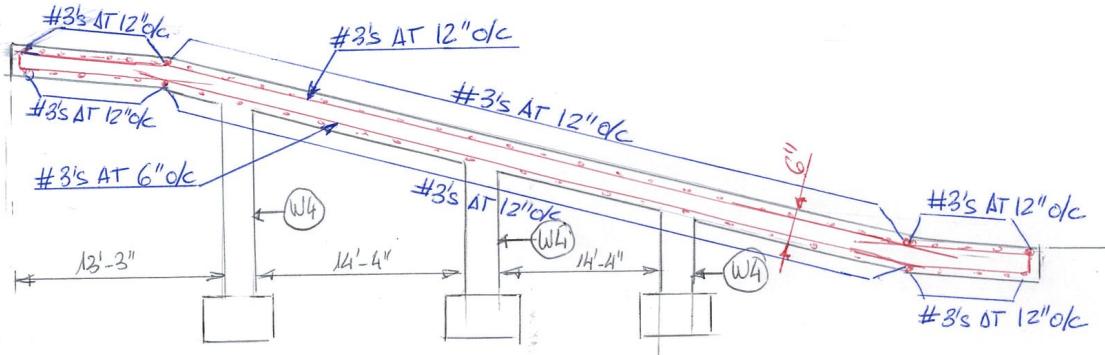


Figure 11: Ramp. Reinforcing layout.

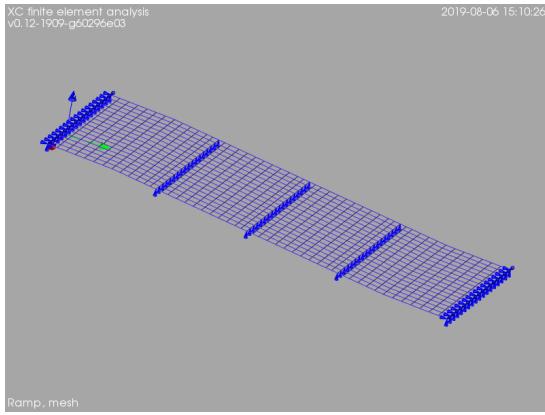


Figure 12: Ramp elastic model, mesh.

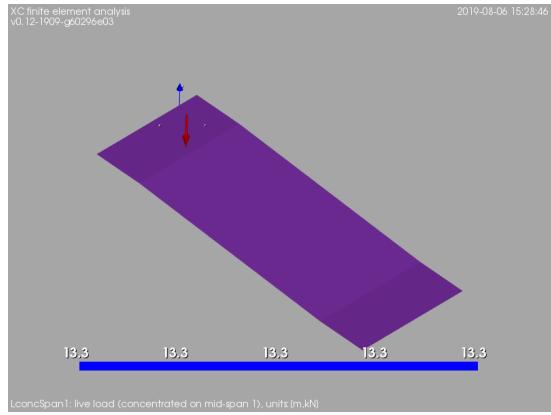


Figure 15: Load case $Lv_{conc,s1}$: concentrated live load (vehicles) on mid-span 1 [units: kN].

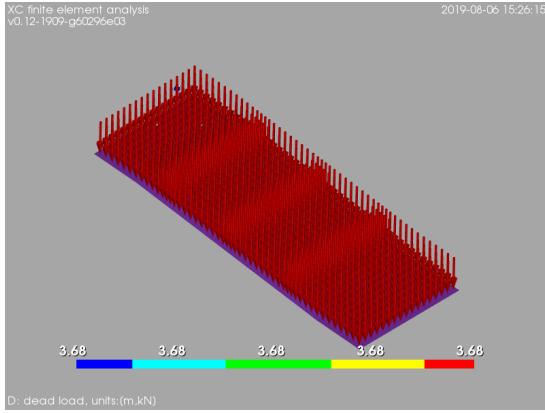


Figure 13: Load case D: dead load (include slab self-weight) [units: kN/m^2].

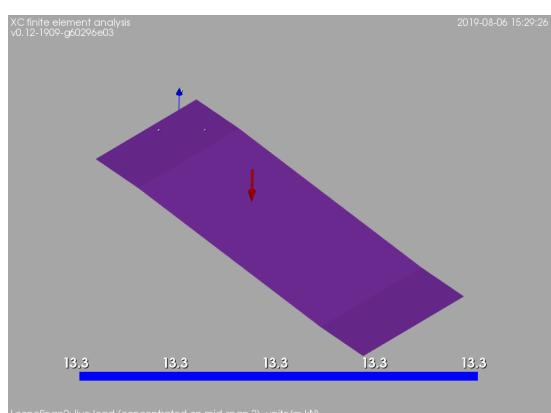


Figure 16: Load case $Lv_{conc,s2}$: concentrated live load (vehicles) on mid-span 2 [units: kN].

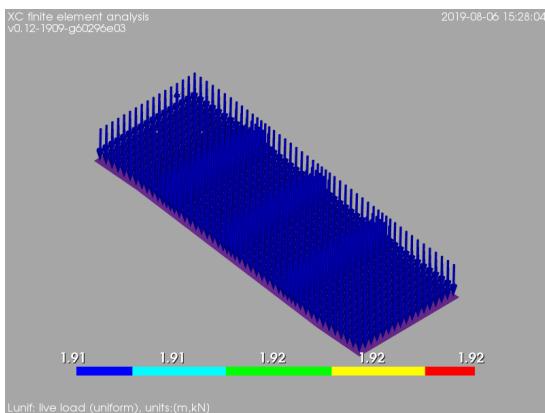


Figure 14: Load case Lv_{unif} : uniform live load (vehicles) [units: kN/m^2].

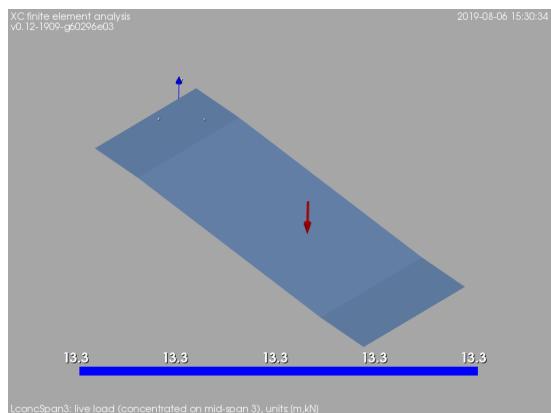


Figure 17: Load case $Lv_{conc,s3}$: concentrated live load (vehicles) on mid-span 3 [units: kN].

FOUNDATION CALCULATION REPORT

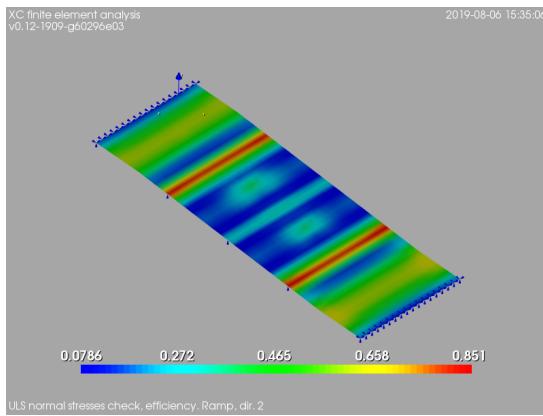


Figure 18: ULS normal stresses check. Efficiency in longitudinal direction

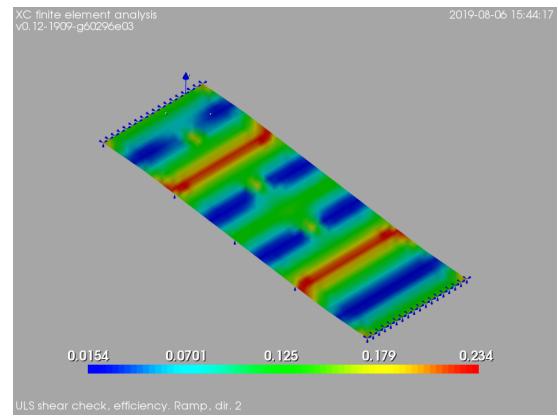


Figure 21: ULS shear check. Efficiency in longitudinal direction

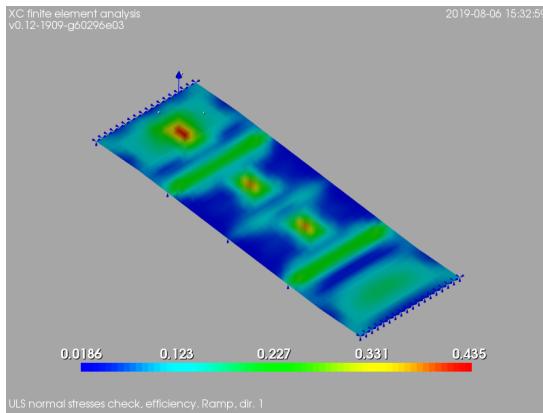


Figure 19: ULS normal stresses check. Efficiency in transversal direction

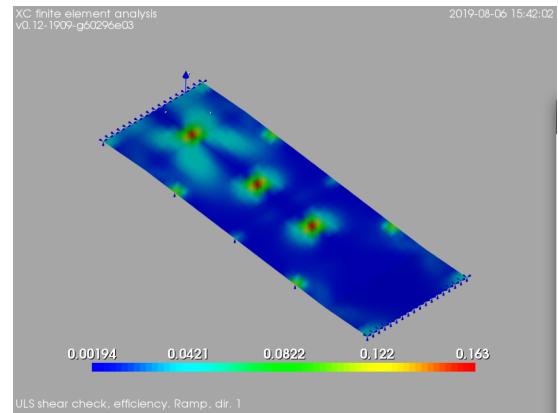


Figure 22: ULS shear check. Efficiency in transversal direction

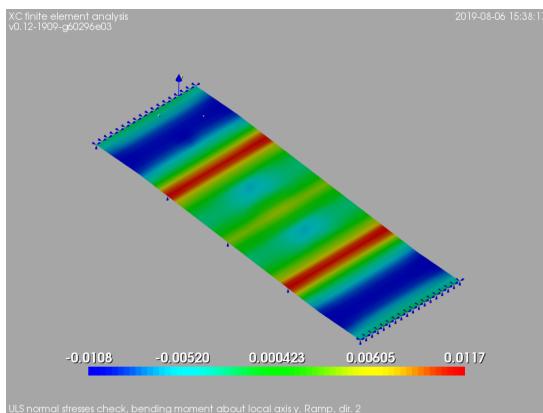


Figure 20: ULS normal stresses check. Bending moment in longitudinal direction [units: kN.m].

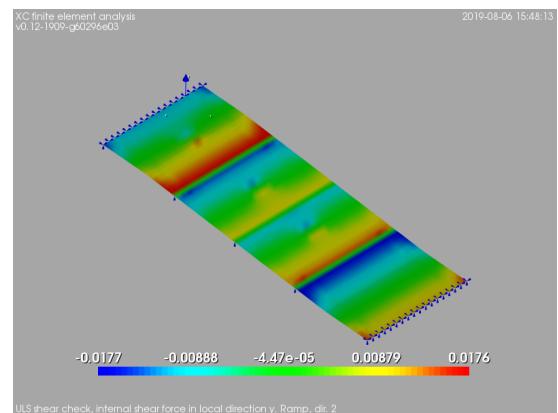


Figure 23: ULS shear check. Internal shear force in longitudinal direction [units: kN].

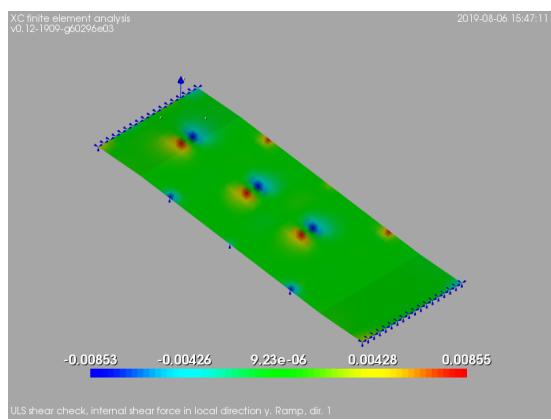


Figure 24: ULS shear check. Internal shear force in transversal direction [units: kN].

Appendices

A Loading criteria

A.1 Dead loads

Materials

Wood structural panel	$36.0 \text{ pcf} = 5655 \frac{\text{newton}}{\text{meter}^3}$
Concrete reinforced stone (including gravel)	$150.0 \text{ pcf} = 23563 \frac{\text{newton}}{\text{meter}^3}$
Steel	$489.0 \text{ pcf} = 76816 \frac{\text{newton}}{\text{meter}^3}$
Gypsum crete	$115.0 \text{ pcf} = 18065 \frac{\text{newton}}{\text{meter}^3}$
Gypsum, loose	$70.0 \text{ pcf} = 10996 \frac{\text{newton}}{\text{meter}^3}$
Earth (not submerged) sand and gravel (wet)	$120.0 \text{ pcf} = 18850 \frac{\text{newton}}{\text{meter}^3}$
Water	$62.4 \text{ pcf} = 9802 \frac{\text{newton}}{\text{meter}^3}$

Frame partitions

Wood or steel studs, $\frac{1}{2}$ in gypsum board inside	8 psf = 383 pascal
Wood studs, 2x4 unplastered	4 psf = 192 pascal
Wood studs, 2x4 plastered one side	12 psf = 575 pascal
Wood studs, 2x4 plastered two sides	20 psf = 958 pascal
Movable steel partitions	4 psf = 192 pascal

Frame walls

Exterior stud wall 2x4 @ 16in, $\frac{5}{8}$ gypsum insulated, $\frac{3}{8}$ in siding	11 psf = 526 pascal
Exterior stud wall 2x6 @ 16in, $\frac{5}{8}$ gypsum insulated, $\frac{3}{8}$ in siding	12 psf = 575 pascal
Exterior stud wall with brick veneer	48 psf = 2298 pascal
CMU wall 8in	60 psf = 9425 pascal
Window, glass, frame and sash	8 psf = 383 pascal

Cladding

Fiber cement panels, large format 38.4in \times 102in	3.2 psf = 153 pascal
Fiber cement panels, small scale 9.6in \times 102in	3.2 psf = 153 pascal
Perforated metal panel at exterior HVAC location	

Floor truss

Single chord @ 24in o.c. spacing	3.2 psf = 153 pascal
Double chord @ 24in o.c. spacing	4.25 psf = 203 pascal

Sheathing

Roof sheathing	3.5 psf = 167 pascal
Floor sheathing	2.5 psf = 120 pascal
Ceilings	2.5 psf = 120 pascal
Deck composite sleepers (3in)	9.00 psf = 431 pascal

A.2 Live loads

Occupancy or use	Uniform		Concentrated	Notes
Private rooms and corridors serving them in multifamily dwelling	40.0 psf 1915 pascal	=	-	<i>IBC-2018 Table 1607.1</i>
Stairs and exits	100.0 psf 4788 pascal	=	300 pound 1334 newton	<i>IBC-2018 Table 1607.1.</i> <i>Concentrated load on stair treads applied on an area of 2 inches by 2 inches</i> <i>IBC-2018 Table 1607.1</i>
Balconies and decks	same as occupancy served		-	
Garages (passenger vehicles only)	40.0 psf 1915 pascal	=	-	<i>IBC-2018 Table 1607.1</i>
Cornices	60.0 psf 2873 pascal	=	-	<i>IBC-2018 Table 1607.1</i>
Elevator machine room and control room grating	-		300 pound 1334 newton	<i>IBC-2018 Table 1607.1.</i> <i>Concentrated load applied on an area of 2 inches by 2 inches</i> <i>IBC-2018 Table 1607.1</i>
Flat roof (not occupiable) + maintenace	20.0 psf 958 pascal	=	300 pound 1334 newton	<i>IBC-2018 Table 1607.1</i>
Yards and terraces, pedestrians	100.0 psf 4788 pascal	=	-	<i>IBC-2018 Table 1607.1</i>
Sidewalks, vehicular driveways and yards, subject to trucking	250.0 psf 11970 pascal	=	8000 pound 35586 newton	<i>IBC-2018 Table 1607.1</i>
Corridors first floor	100.0 psf 4788 pascal	=	-	<i>IBC-2018 Table 1607.1</i>
Store first floor	100.0 psf 4788 pascal	=	-	<i>IBC-2018 Table 1607.1</i>

A.3 Snow loads

Ground snow load	$p_g = 60.0 \text{ psf} = 2873 \text{ pascal}$	<i>ASCE 7. Figure 7.1</i>
Exposure factor	$C_e = 1.0$	<i>ASCE 7. Table 7-2. Terrain category B, roof partially exposed</i>
Thermal factor	$C_t = 1.0$	<i>ASCE 7. Table 7-3.</i>
Snow load importance factor	$I_s = 1.0$	<i>ASCE 7. Table 7-4. Structure risk category II</i>
Snow load flat roof	$p_f = 0.7 \times C_e \times C_t \times I_s \times p_g = 0.7 \times 1.0 \times 1.0 \times 1.0 \times 60.0 = 42.0 \text{ psf} = 2873 \text{ pascal}$	<i>ASCE 7. Sect. 7.3</i>

A.4 Wind loads

Alternate all-heights method.

$$\text{Ultimate design wind speed} \quad V_{ult} = 115 \frac{\text{miles}}{\text{hour}} = 51 \frac{\text{meters}}{\text{second}}$$

$$\text{Velocity pressure exposure coefficient} \quad K_z = 0.72$$

$$\text{Topographic factor} \quad K_{zt} = 1.0$$

IBC-2018, sect. 1609.6. Regularly shaped building, less than 75 feet in height, not sensitive to dynamic effects, not channeling effects or buffeting, simple diaphragm building

IBC-2018, figure 1609.3(1). Risk category II building

ASCE 7, table 27.3.1. Exposure B, height above ground level $z \approx 33$ feet

ASCE 7, sect. 26.8

Net pressure coefficients C_{net} . Main windforce-resisting frames and systems

Description	$C_{net} + \text{Internal pressure}$	$C_{net} - \text{Internal pressure}$
Windward wall	0.43	0.73
Leeward wall	-0.51	-0.21
Sidewall	-0.66	-0.35
Parapet windward wall		1.28
Parapet leeward wall		-0.85
Flat roof	-1.09	-0.79

IBC-2018, Table 1609.6.2, enclosed

Design wind pressures P_{net} . Main windforce-resisting frames and systems

$$P_{net} = 0.00256 \times V^2 \times K_z \times C_{net} \times K_{zt}$$

Description	$P_{net} + \text{Internal pressure}$	$P_{net} - \text{Internal pressure}$
Windward wall	10.5 psf = 501 pascal	17.8 psf = 852 pascal
Leeward wall	-12.4 psf = -595 pascal	-5.1 psf = -245 pascal
Sidewall	-16.1 psf = -770 pascal	-8.5 psf = -409 pascal
Parapet windward wall		31.2 psf = 1494 pascal
Parapet leeward wall		-20.7 psf = -992 pascal
Flat roof	-26.6 psf = -1272 pascal	-19.3 psf = -992 pascal

IBC-2018, sect. 1609.6.3

A.5 Earthquake loads

Parameter 0.2-second spectral response acceleration	$S_s = 0.045$	<i>IBC-2018, figure 1613.3.1(1). Site class B</i>
Parameter 1-second spectral response acceleration	$S_1 = 0.038$	<i>IBC-2018, figure 1613.3.1(2). Site class B</i>
Seismic design category	$S_1 \leq 0.04$ and $S_s \leq 0.15 \rightarrow \text{SDS A}$	<i>IBC-2018, sect. 1613.3.1</i>
Site coefficients	$F_a = 1.0, F_v = 1.0$	<i>IBC-2018, tables 1613.3.3(1) and 1613.3.3(2). Site class B</i>
Maximum considered earthquake spectral response acceleration for short periods	$S_{MS} = F_a \cdot S_s = 0.045$	<i>IBC-2018, sect. 163.3.3</i>
Design spectral response acceleration parameters	$S_{M1} = F_a \cdot S_1 = 0.038$ $S_{DS} = \frac{2}{3}S_{MS} = 0.03$ $S_{D1} = \frac{2}{3}S_{M1} = 0.025$	<i>IBC-2018, sect. 163.3.4</i>

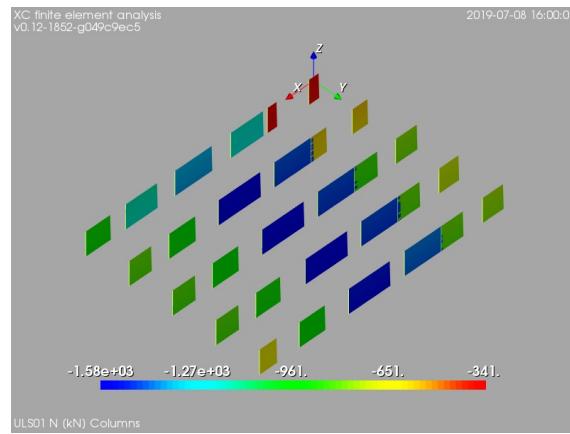


Figure 25: ULS01: 1.4*D. Columns, internal axial force [kN]

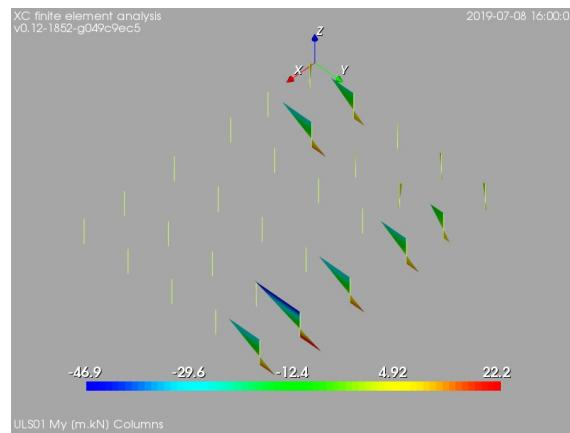


Figure 26: ULS01: 1.4*D. Columns, bending moment about local axis y [m.kN]

B Calculation results. Internal forces on columns

B.1 Ultimate limit states

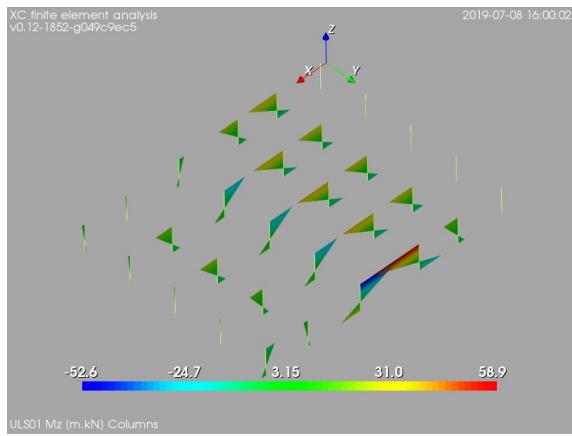


Figure 27: ULS01: 1.4*D. Columns, bending moment about local axis z [m.kN]

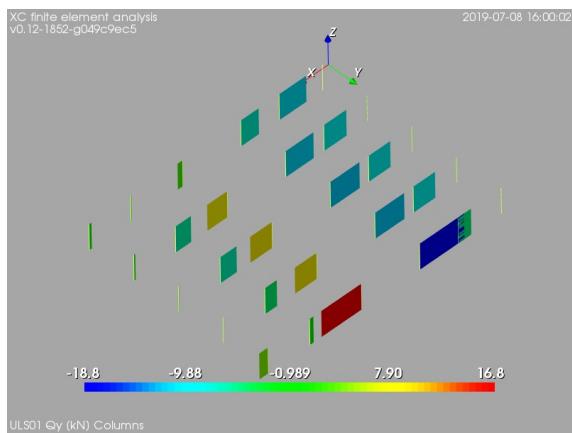


Figure 28: ULS01: 1.4*D. Columns, internal shear force in local direction y [kN]

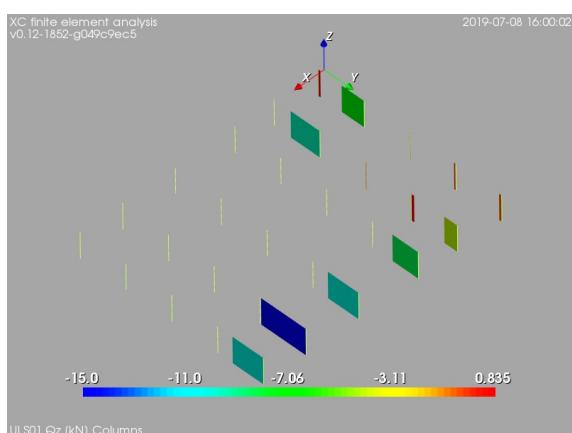


Figure 29: ULS01: 1.4*D. Columns, internal shear force in local direction z [kN]

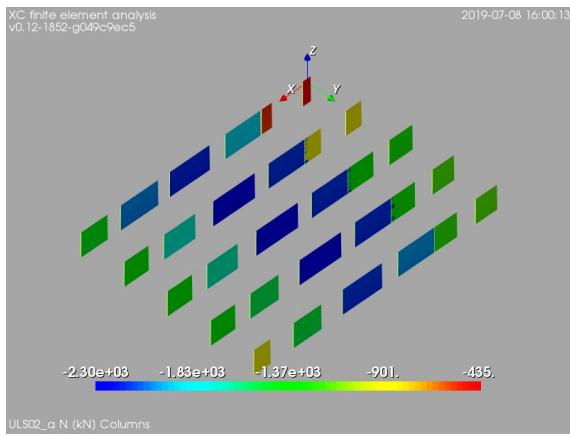


Figure 30: ULS02_a: $1.2*D + 1.6*Lru + Lpu + 0.5*S$. Columns, internal axial force [kN]

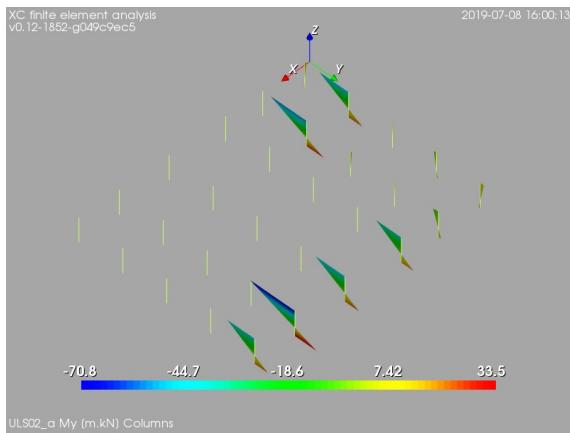


Figure 31: ULS02_a: $1.2*D + 1.6*Lru + Lpu + 0.5*S$. Columns, bending moment about local axis y [m.kN]

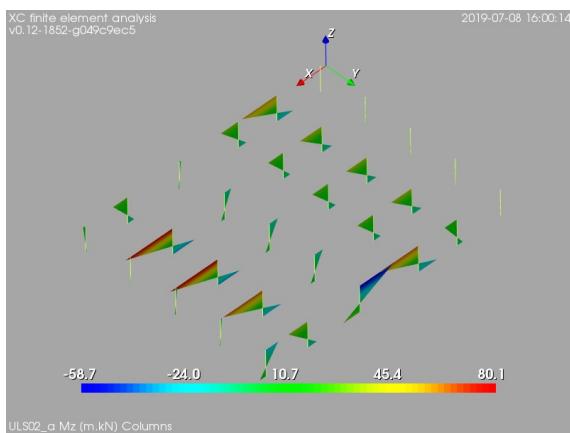


Figure 32: ULS02_a: $1.2*D + 1.6*Lru + Lpu + 0.5*S$. Columns, bending moment about local axis z [m.kN]

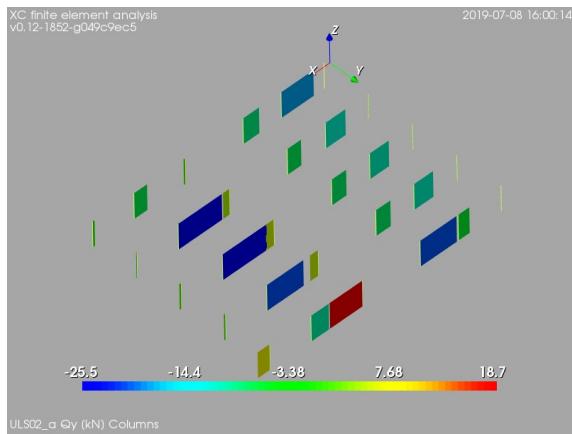


Figure 33: ULS02_a: $1.2*D + 1.6*L_{ru} + L_{pu} + 0.5*S$. Columns, internal shear force in local direction y [kN]

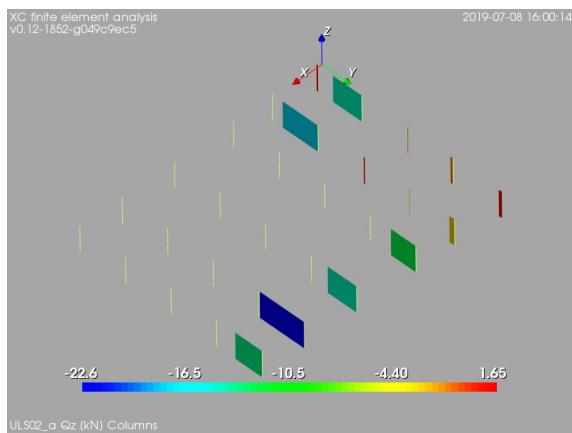


Figure 34: ULS02_a: $1.2*D + 1.6*L_{ru} + L_{pu} + 0.5*S$. Columns, internal shear force in local direction z [kN]

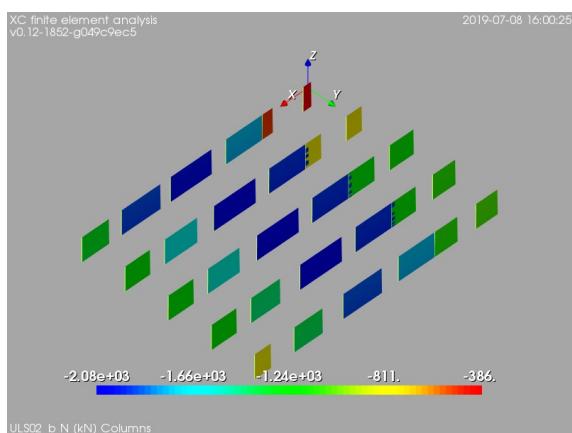


Figure 35: ULS02_b: $1.2*D + 1.6*L_{rs} + L_{ps} + 0.5*S$. Columns, internal axial force [kN]

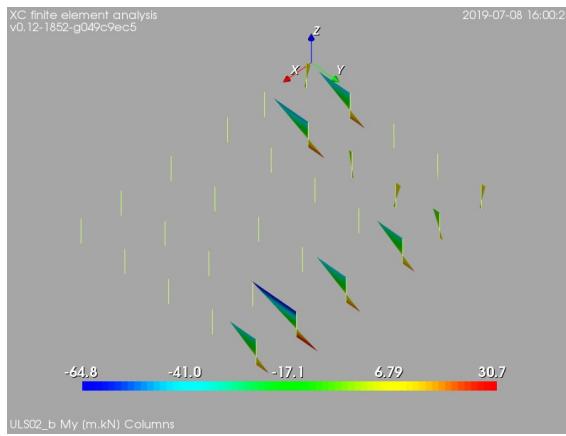


Figure 36: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, bending moment about local axis y [m.kN]

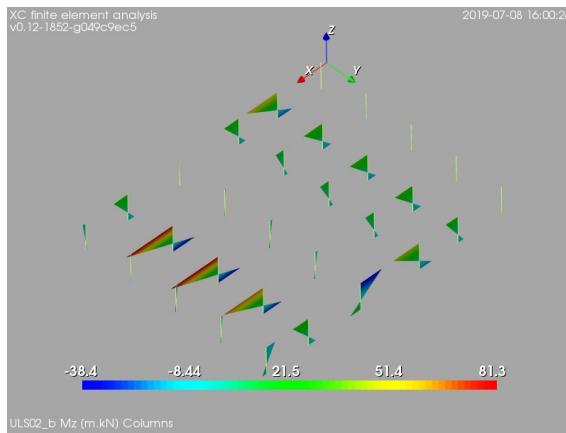


Figure 37: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, bending moment about local axis z [m.kN]

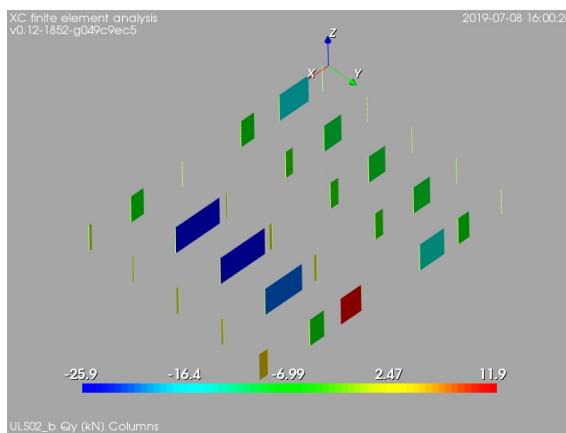


Figure 38: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, internal shear force in local direction y [kN]

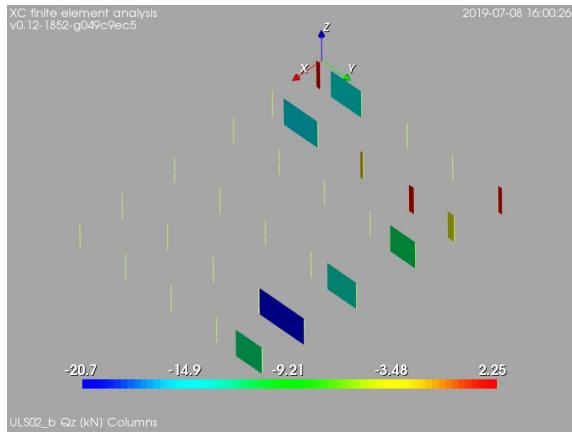


Figure 39: ULS02_b: $1.2*D + 1.6*Lrs + Lps + 0.5*S$. Columns, internal shear force in local direction z [kN]

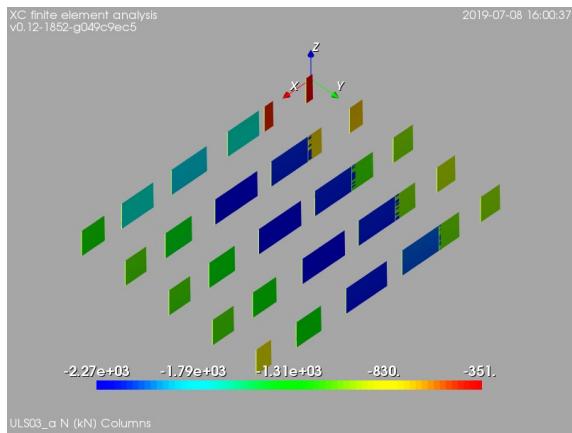


Figure 40: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal axial force [kN]

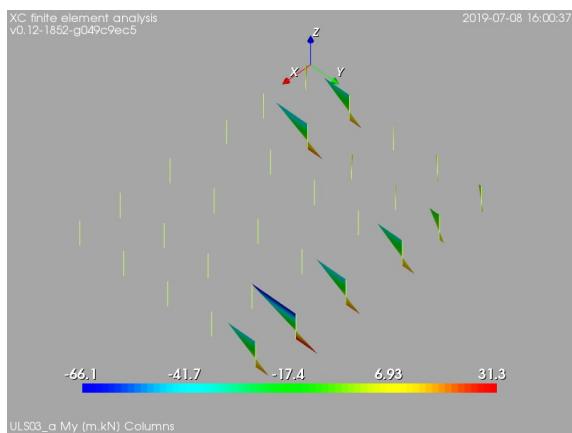


Figure 41: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, bending moment about local axis y [m.kN]

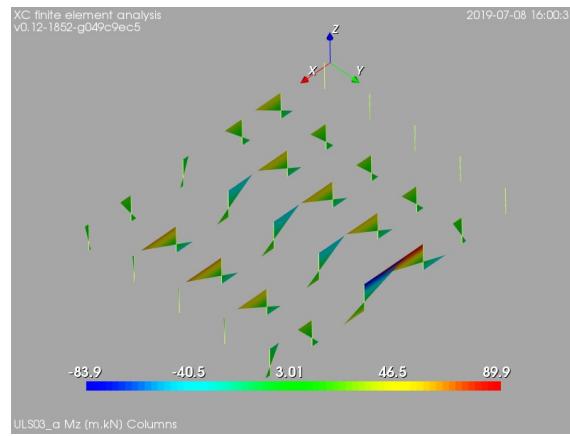


Figure 42: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, bending moment about local axis z [m.kN]

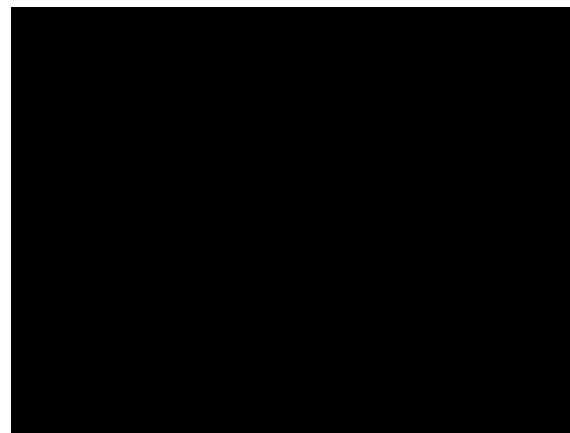


Figure 43: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal shear force in local direction y [kN]

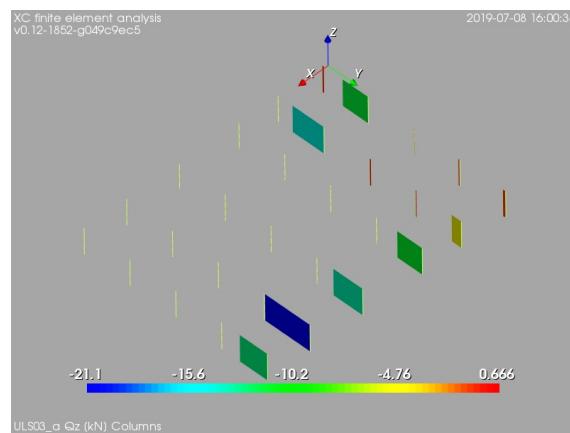


Figure 44: ULS03_a: $1.2*D + 1.6*S + 0.5*Lru + Lpu$. Columns, internal shear force in local direction z [kN]

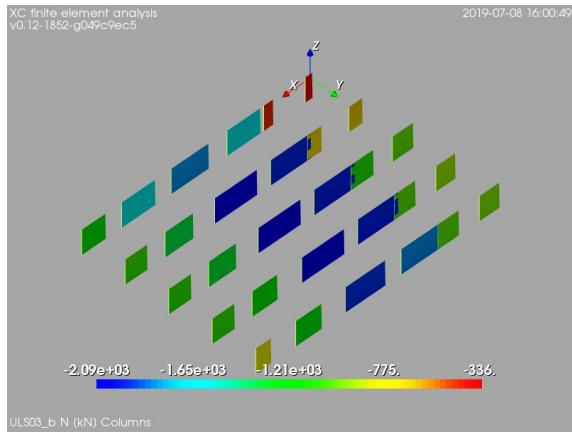


Figure 45: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal axial force [kN]

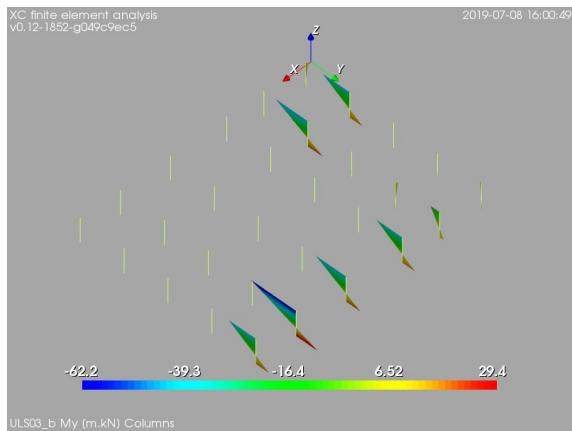


Figure 46: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, bending moment about local axis y [m.kN]

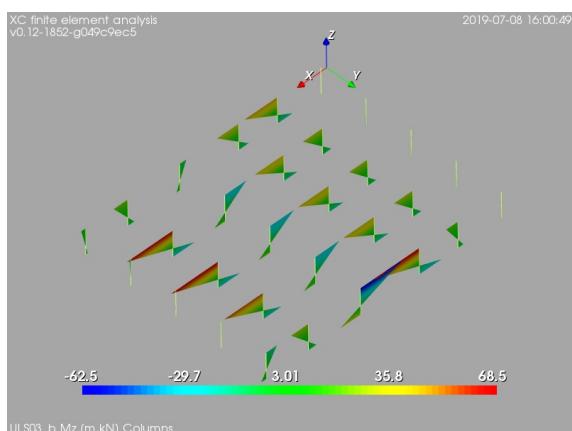


Figure 47: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, bending moment about local axis z [m.kN]

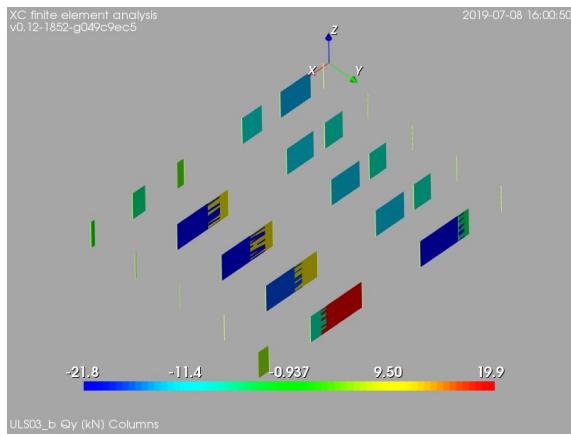


Figure 48: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal shear force in local direction y [kN]

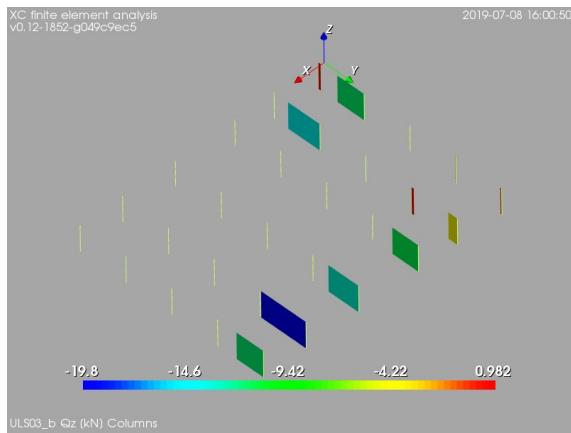


Figure 49: ULS03_b: $1.2*D + 1.6*S + 0.5*Lrs + Lps$. Columns, internal shear force in local direction z [kN]

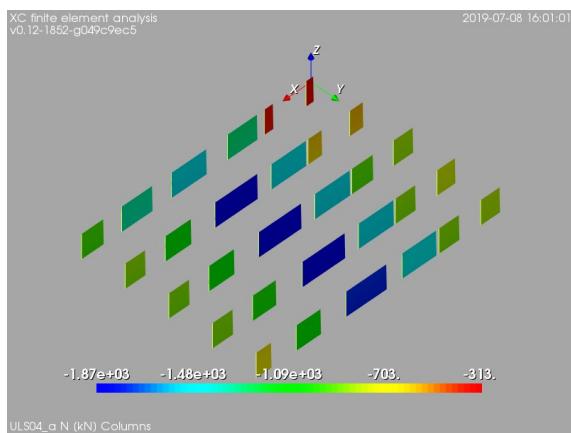


Figure 50: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal axial force [kN]

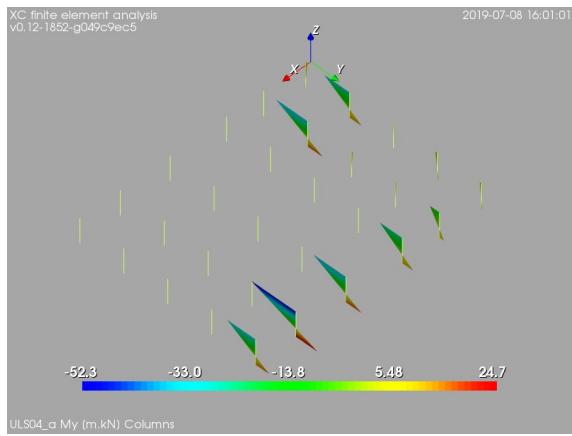


Figure 51: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, bending moment about local axis y [m.kN]

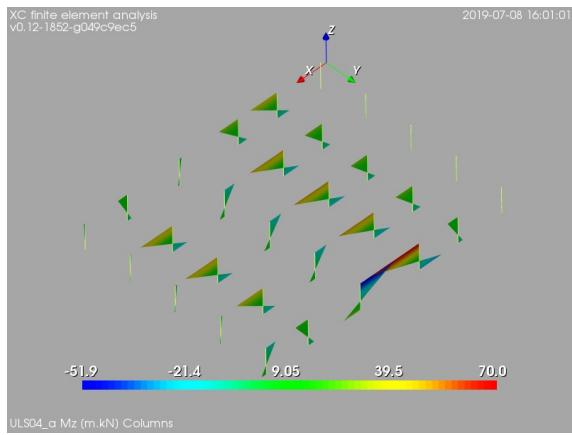


Figure 52: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, bending moment about local axis z [m.kN]

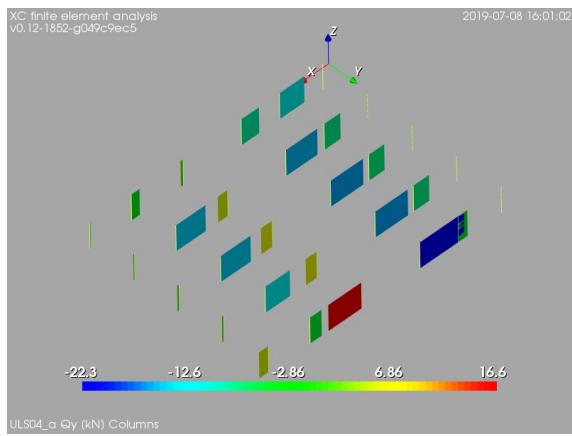


Figure 53: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal shear force in local direction y [kN]

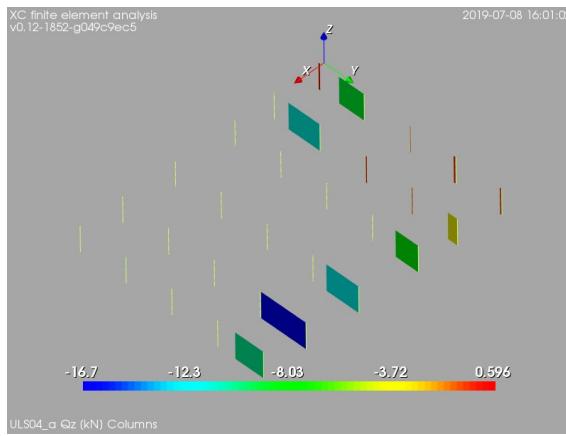


Figure 54: ULS04_a: $1.2*D + 1.6*S + 0.5*W_WE$. Columns, internal shear force in local direction z [kN]

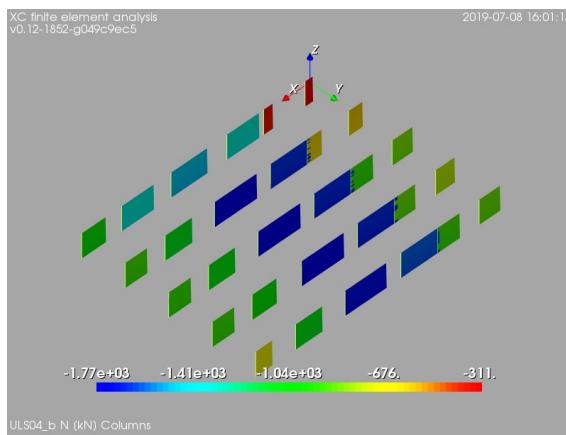


Figure 55: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, internal axial force [kN]

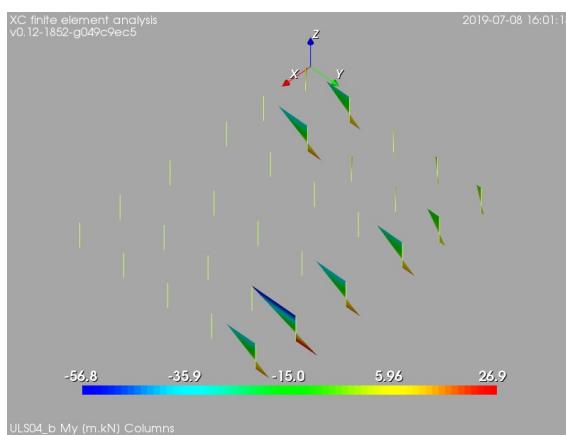


Figure 56: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, bending moment about local axis y [m.kN]

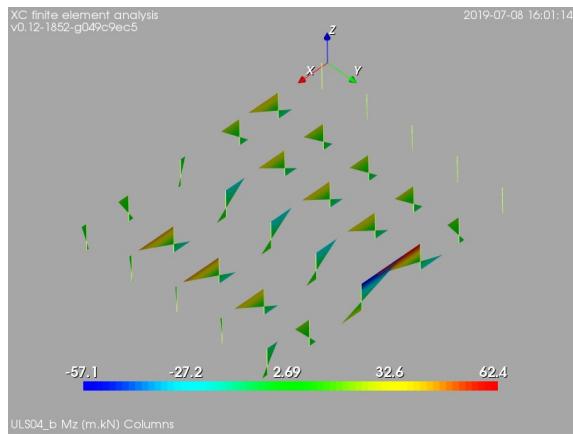


Figure 57: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, bending moment about local axis z [m.kN]

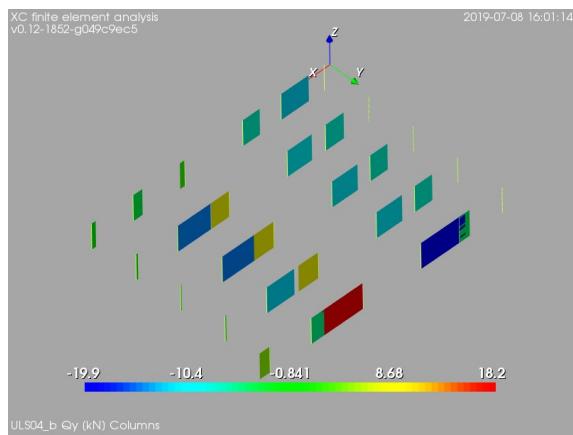


Figure 58: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, internal shear force in local direction y [kN]

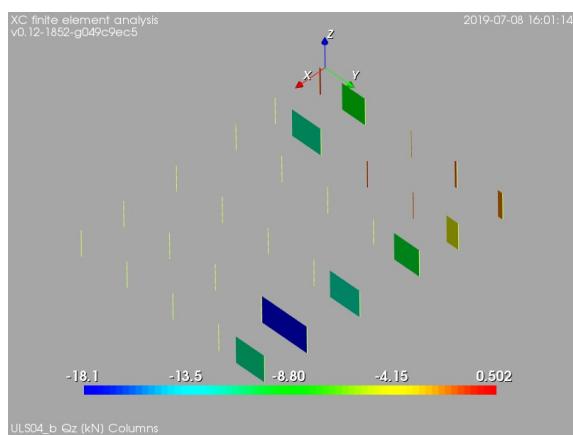


Figure 59: ULS04_b: $1.2*D + 1.6*S + 0.5*W_NS$. Columns, internal shear force in local direction z [kN]

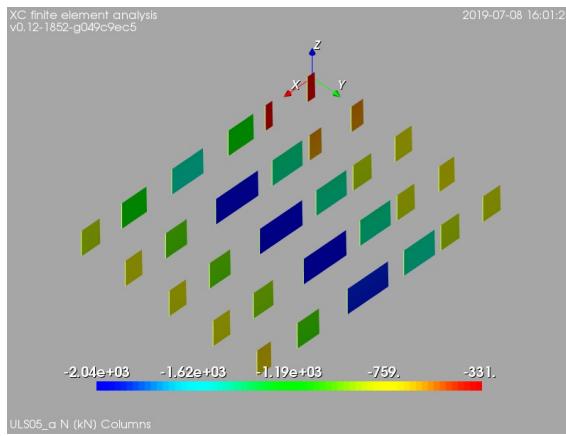


Figure 60: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal axial force [kN]

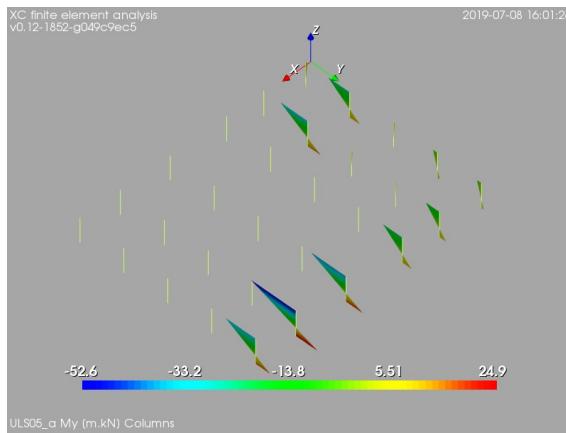


Figure 61: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, bending moment about local axis y [m.kN]

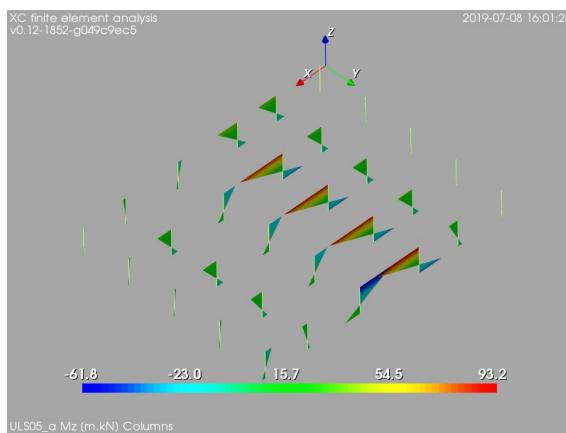


Figure 62: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, bending moment about local axis z [m.kN]

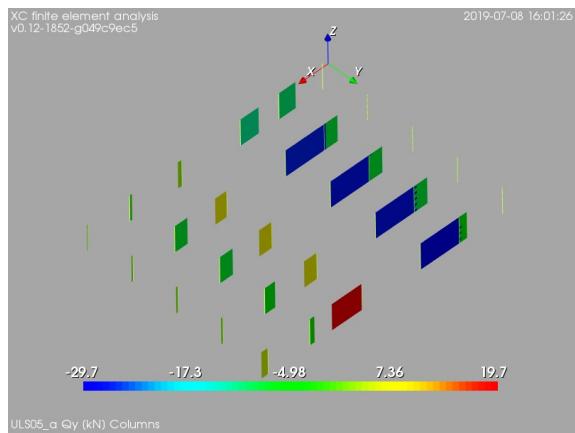


Figure 63: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal shear force in local direction y [kN]

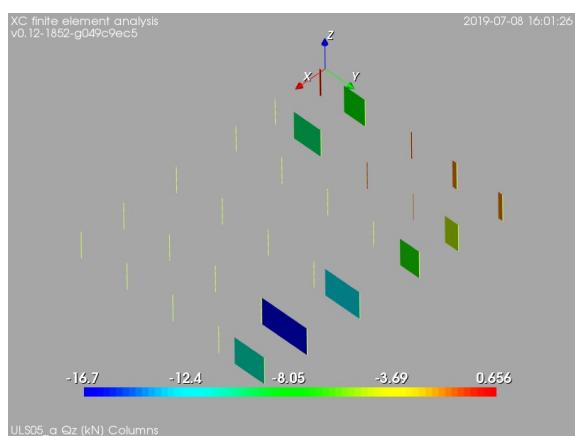


Figure 64: ULS05_a: $1.2*D + W_WE + 0.5*Lru + Lpu$. Columns, internal shear force in local direction z [kN]

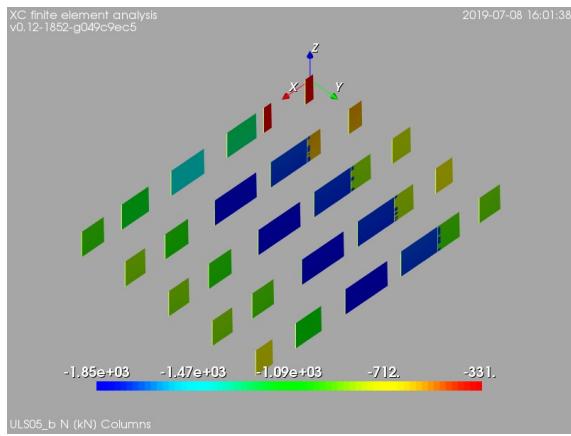


Figure 65: ULS05_b: $1.2*D + W_{NS} + 0.5*Lru + Lpu$. Columns, internal axial force [kN]

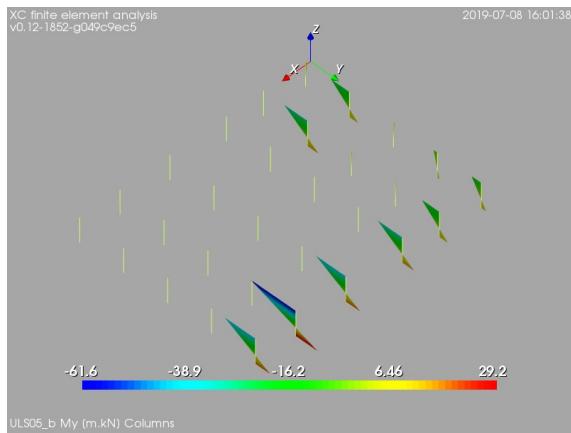


Figure 66: ULS05_b: $1.2*D + W_{NS} + 0.5*Lru + Lpu$. Columns, bending moment about local axis y [m.kN]

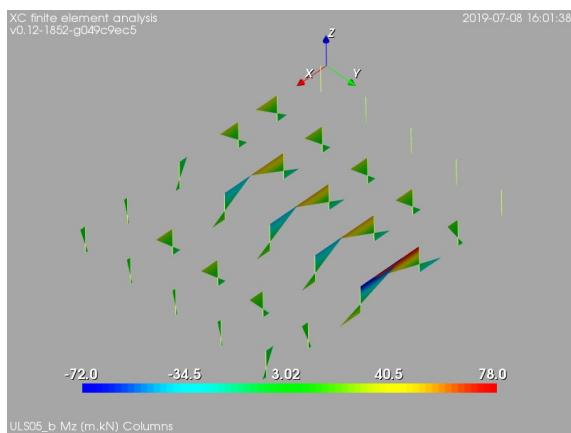


Figure 67: ULS05_b: $1.2*D + W_{NS} + 0.5*Lru + Lpu$. Columns, bending moment about local axis z [m.kN]

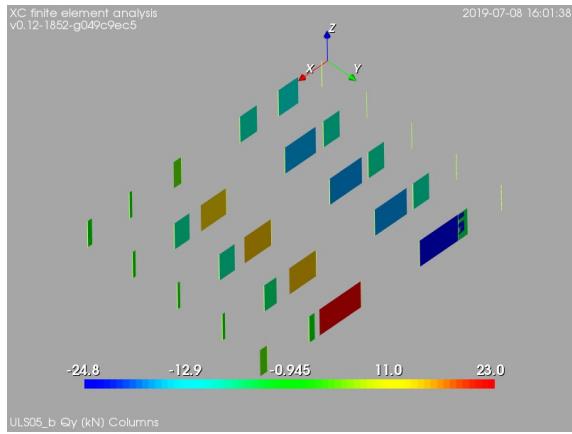


Figure 68: ULS05_b: $1.2*D + W_NS + 0.5*Lru + Lpu$. Columns, internal shear force in local direction y [kN]

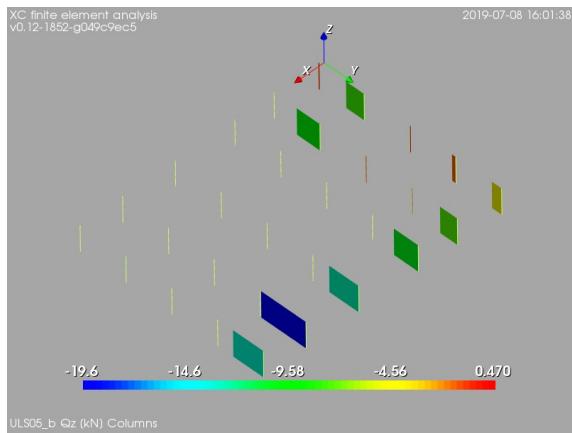


Figure 69: ULS05_b: $1.2*D + W_NS + 0.5*Lru + Lpu$. Columns, internal shear force in local direction z [kN]

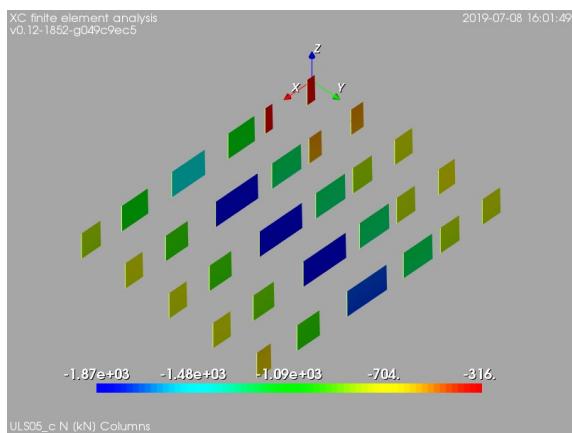


Figure 70: ULS05_c: $1.2*D + W_WE + 0.5*Lrs + Lps$. Columns, internal axial force [kN]

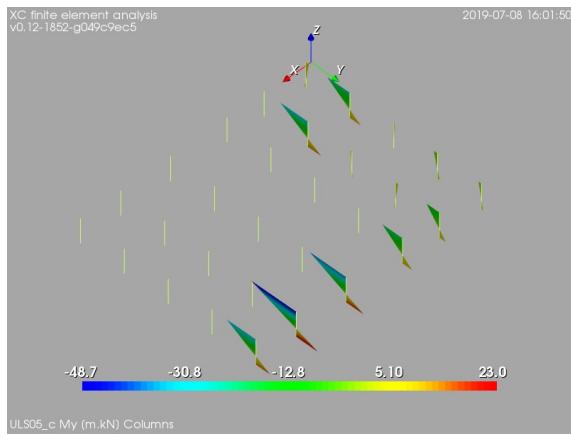


Figure 71: ULS05_c: $1.2*D + W_WE + 0.5*Lrs + Lps$. Columns, bending moment about local axis y [m.kN]

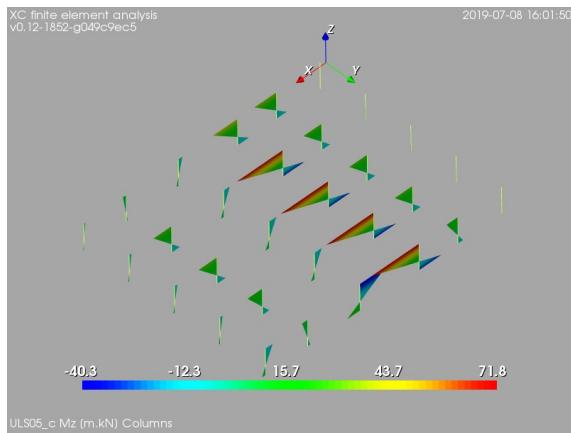


Figure 72: ULS05_c: $1.2*D + W_WE + 0.5*Lrs + Lps$. Columns, bending moment about local axis z [m.kN]

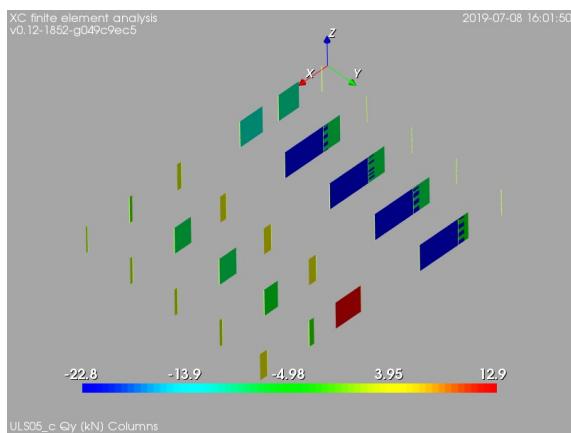


Figure 73: ULS05_c: $1.2*D + W_WE + 0.5*Lrs + Lps$. Columns, internal shear force in local direction y [kN]

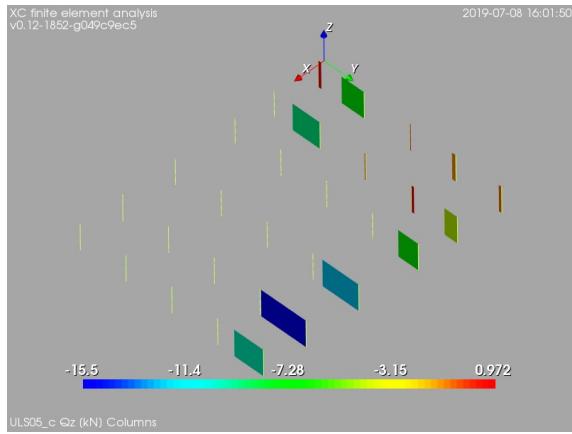


Figure 74: ULS05_c: $1.2*D + W_WE + 0.5*Lrs + Lps$. Columns, internal shear force in local direction z [kN]

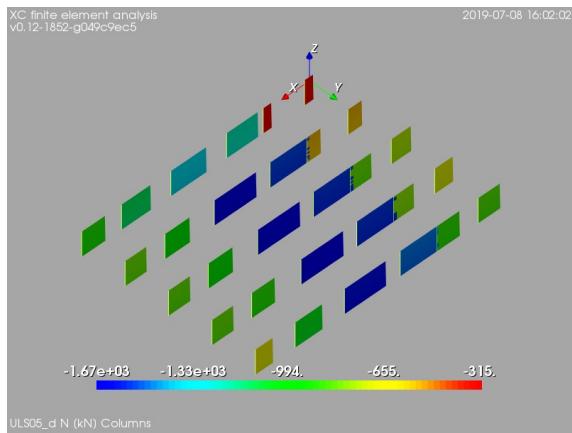


Figure 75: ULS05_d: $1.2*D + W_NS + 0.5*Lrs + Lps$. Columns, internal axial force [kN]

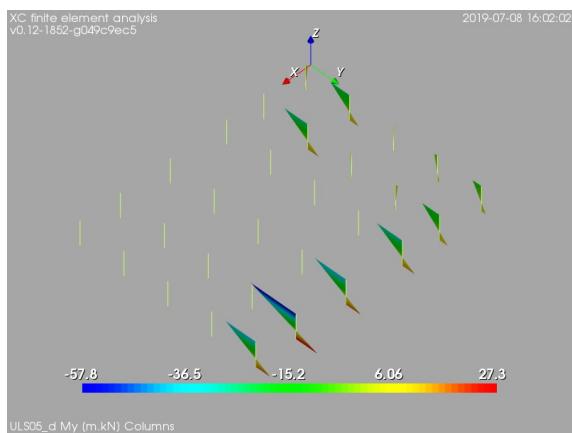


Figure 76: ULS05_d: $1.2*D + W_NS + 0.5*Lrs + Lps$. Columns, bending moment about local axis y [m.kN]

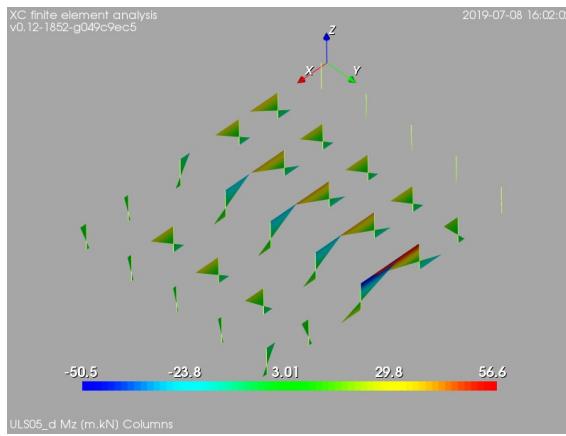


Figure 77: ULS05_d: 1.2*D + W_NS + 0.5*Lrs + Lps. Columns, bending moment about local axis z [m.kN]

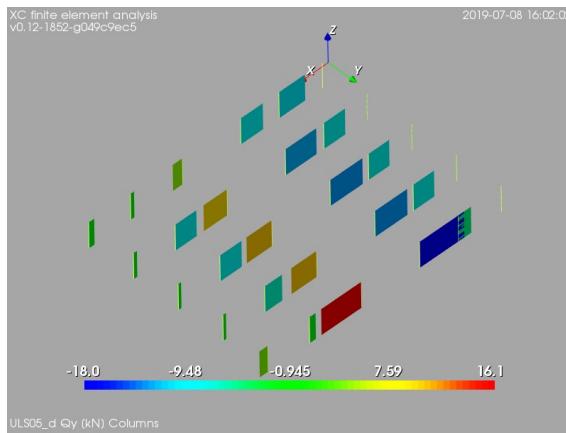


Figure 78: ULS05_d: 1.2*D + W_NS + 0.5*Lrs + Lps. Columns, internal shear force in local direction y [kN]

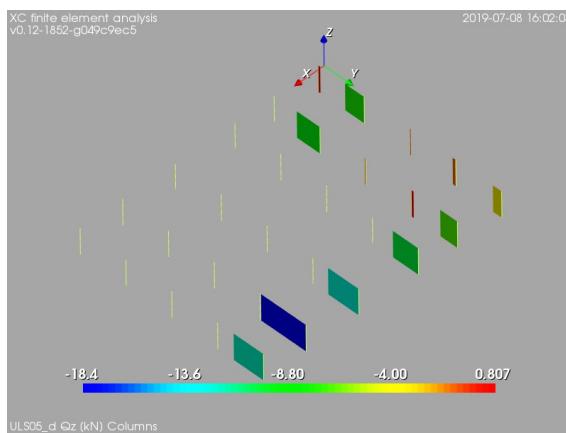


Figure 79: ULS05_d: 1.2*D + W_NS + 0.5*Lrs + Lps. Columns, internal shear force in local direction z [kN]

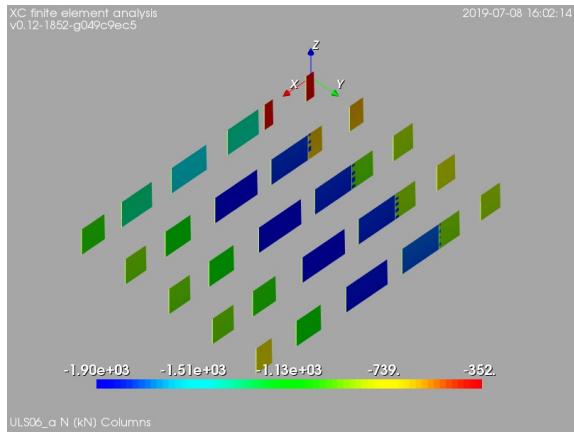


Figure 80: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, internal axial force [kN]

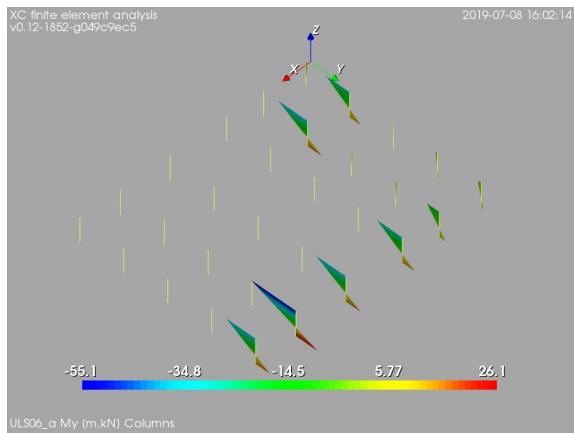


Figure 81: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, bending moment about local axis y [m.kN]

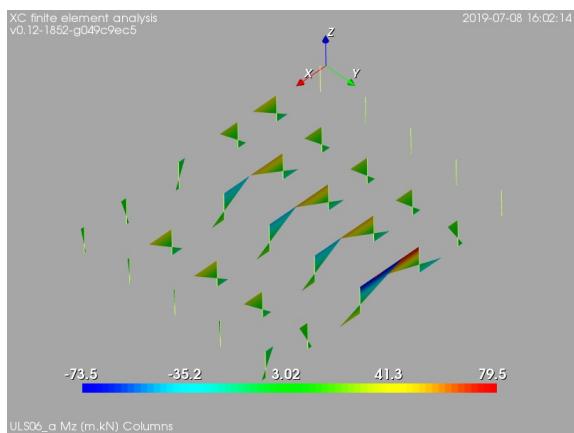


Figure 82: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, bending moment about local axis z [m.kN]

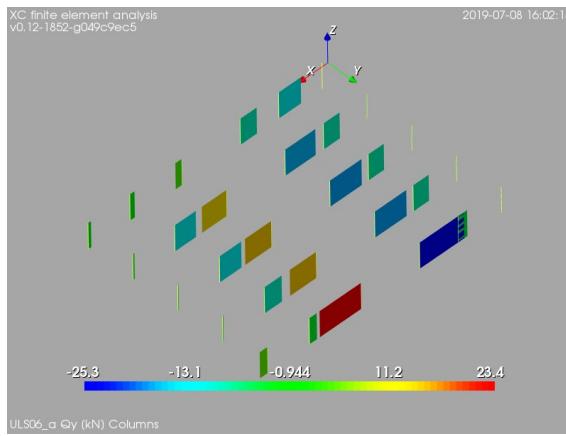


Figure 83: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, internal shear force in local direction y [kN]

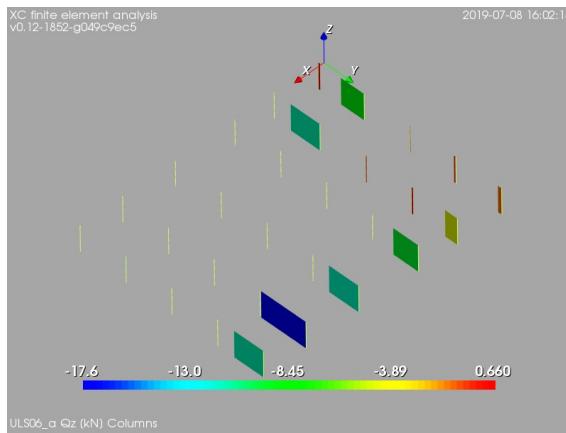


Figure 84: ULS06_a: $1.2*D + 0.5*Lru + Lpu + 0.2*S$. Columns, internal shear force in local direction z [kN]

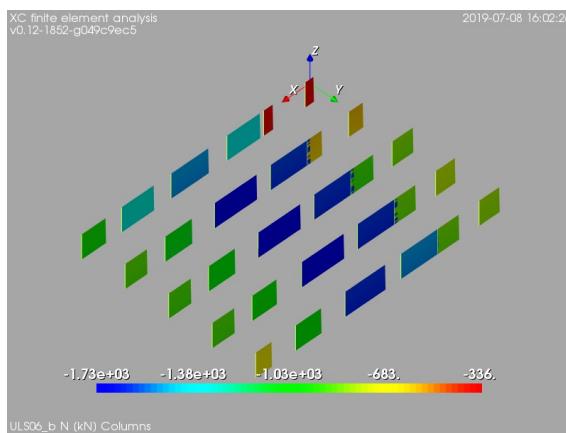


Figure 85: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal axial force [kN]

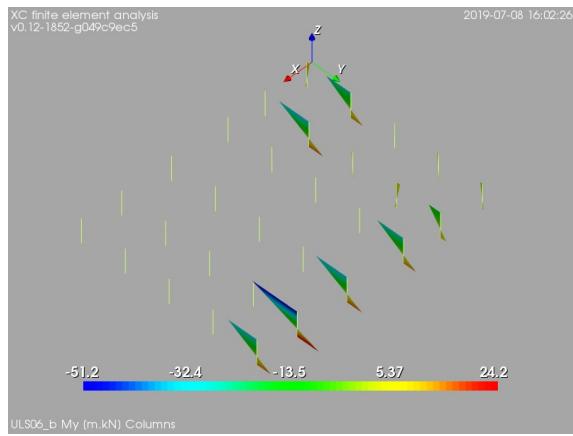


Figure 86: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, bending moment about local axis y [m.kN]

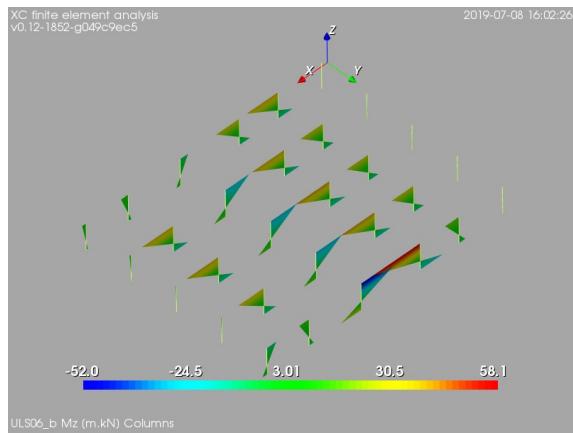


Figure 87: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, bending moment about local axis z [m.kN]

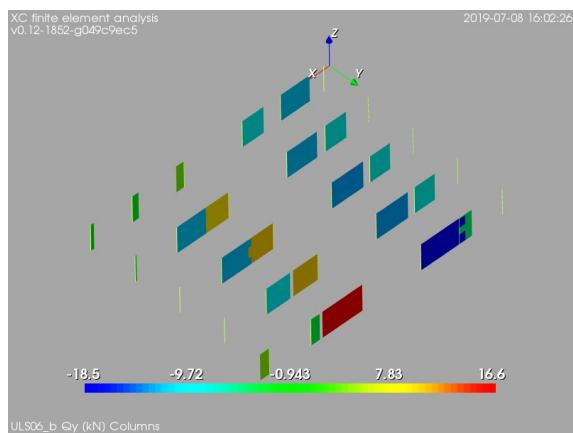


Figure 88: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal shear force in local direction y [kN]

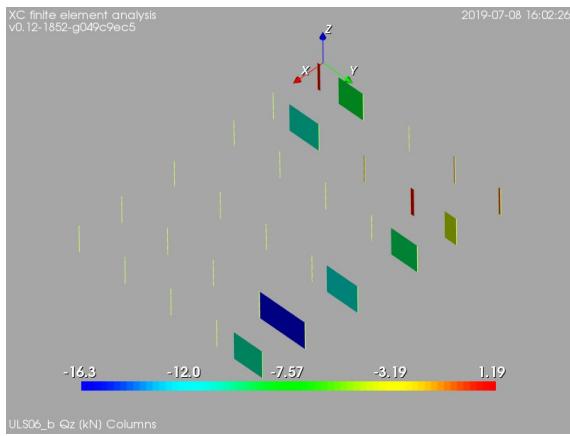


Figure 89: ULS06_b: $1.2*D + 0.5*Lrs + Lps + 0.2*S$. Columns, internal shear force in local direction z [kN]

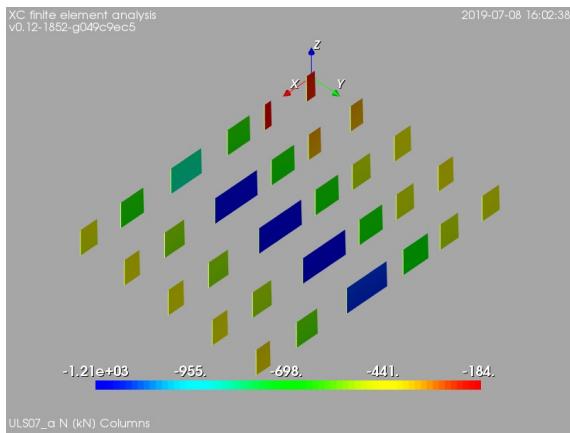


Figure 90: ULS07_a: $0.9*D + W_WE$. Columns, internal axial force [kN]

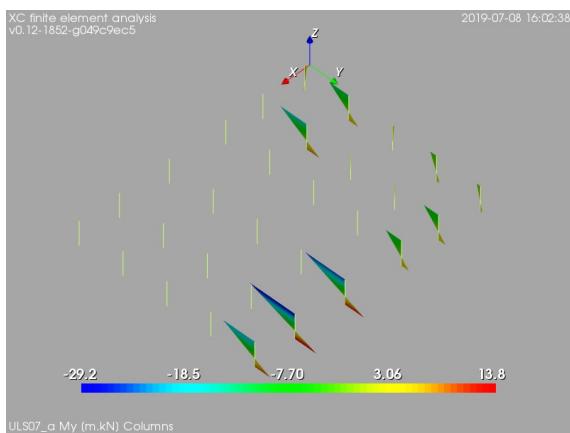


Figure 91: ULS07_a: $0.9*D + W_WE$. Columns, bending moment about local axis y [m.kN]

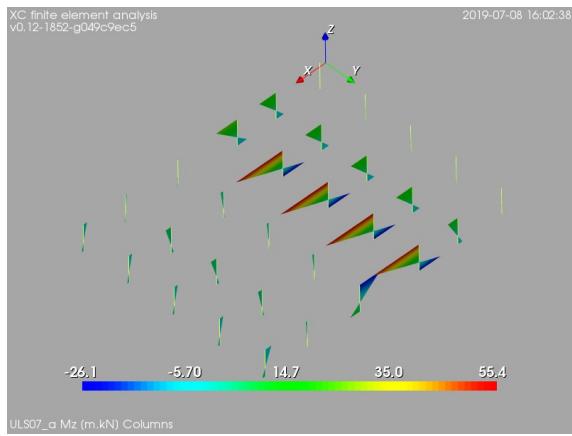


Figure 92: ULS07_a: 0.9*D + W_WE. Columns, bending moment about local axis z [m.kN]

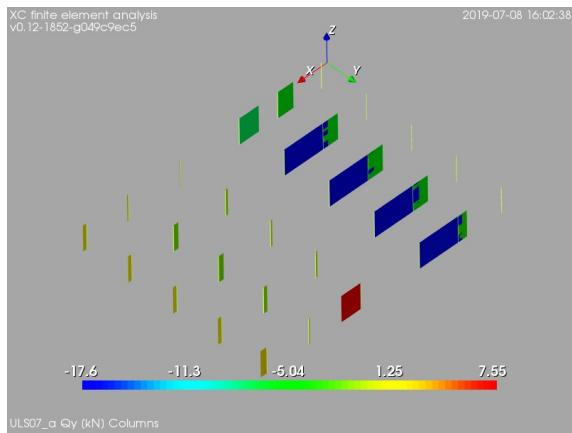


Figure 93: ULS07_a: 0.9*D + W_WE. Columns, internal shear force in local direction y [kN]

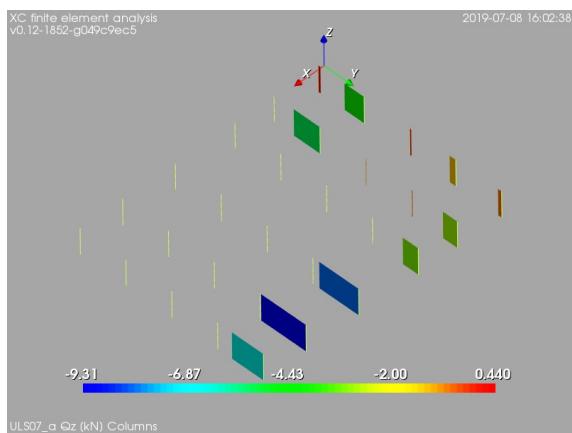


Figure 94: ULS07_a: 0.9*D + W_WE. Columns, internal shear force in local direction z [kN]

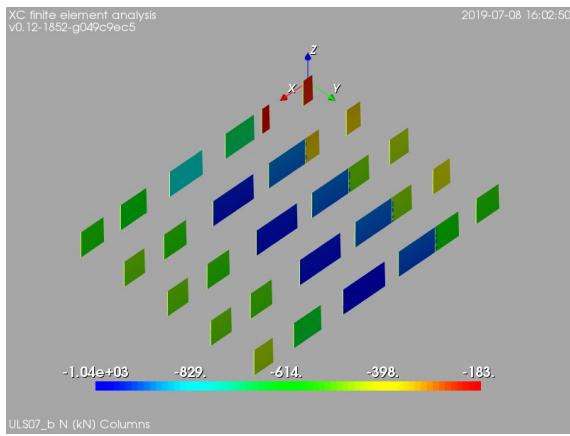


Figure 95: ULS07_b: 0.9*D + W_NS. Columns, internal axial force [kN]

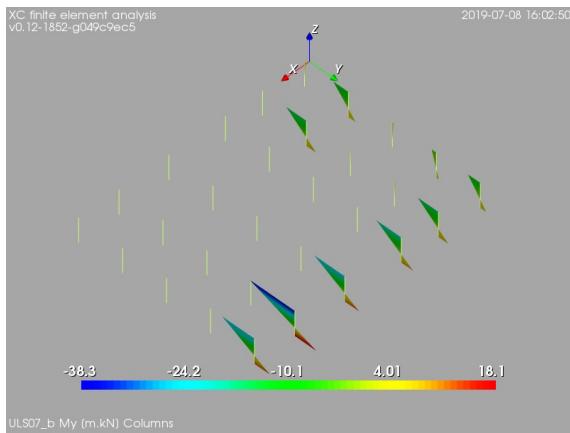


Figure 96: ULS07_b: 0.9*D + W_NS. Columns, bending moment about local axis y [m.kN]

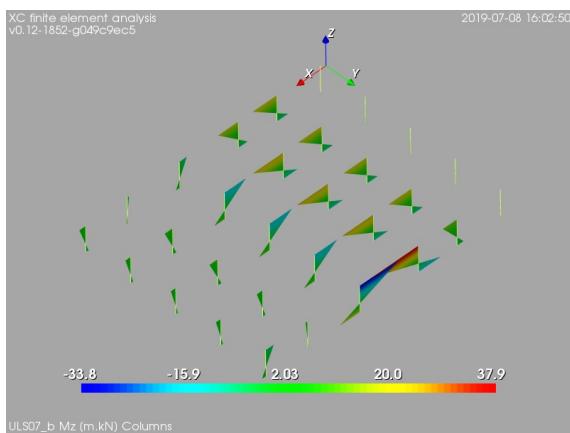


Figure 97: ULS07_b: 0.9*D + W_NS. Columns, bending moment about local axis z [m.kN]

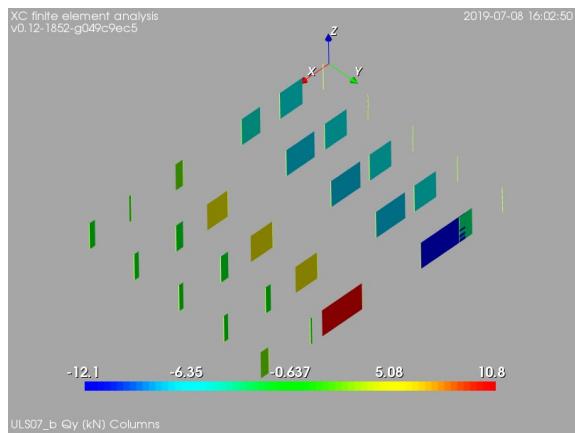


Figure 98: ULS07_b: 0.9*D + W_NS. Columns, internal shear force in local direction y [kN]

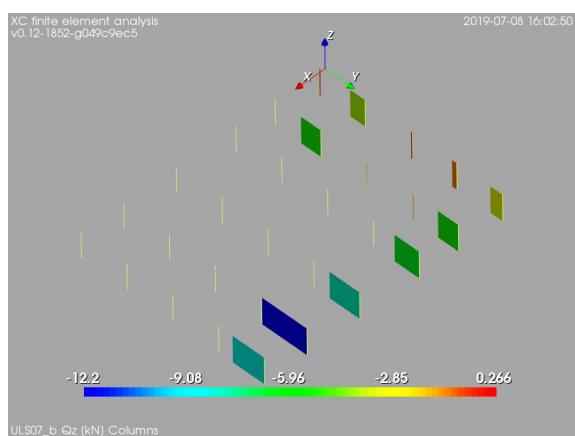


Figure 99: ULS07_b: 0.9*D + W_NS. Columns, internal shear force in local direction z [kN]

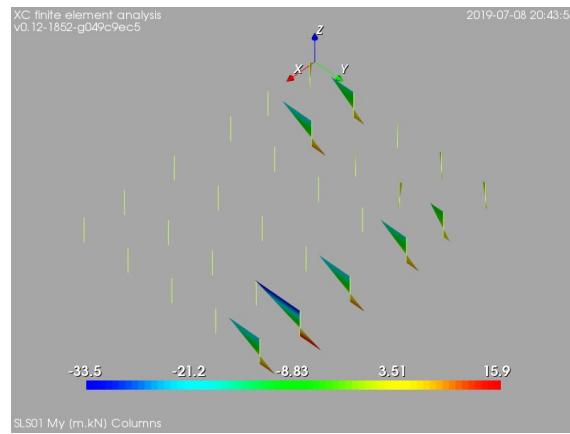


Figure 100: SLS01: 1.0*D. Columns, bending moment about local axis y [m.kN]

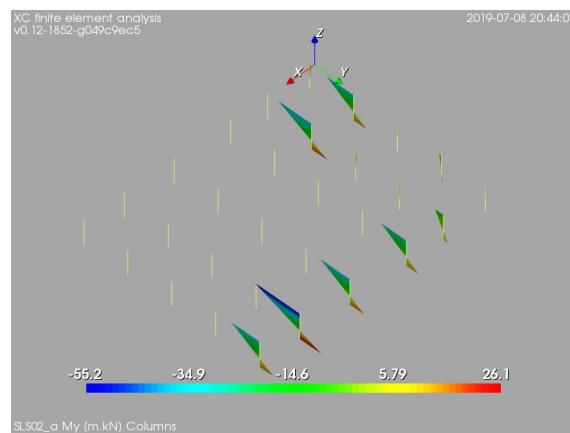


Figure 101: SLS02_a: 1.0*D + 1.0*Lru + Lpu + 0.3*S. Columns, bending moment about local axis y [m.kN]

B.2 Serviceability limit states

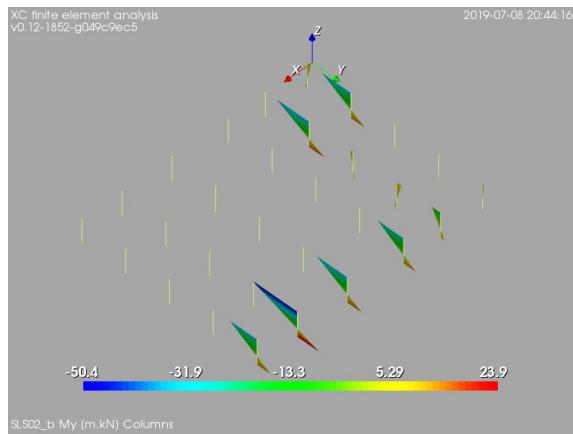


Figure 102: SLS02_b: $1.0*D + 1.0*Lrs + Lps + 0.3*S$. Columns, bending moment about local axis y [m.kN]

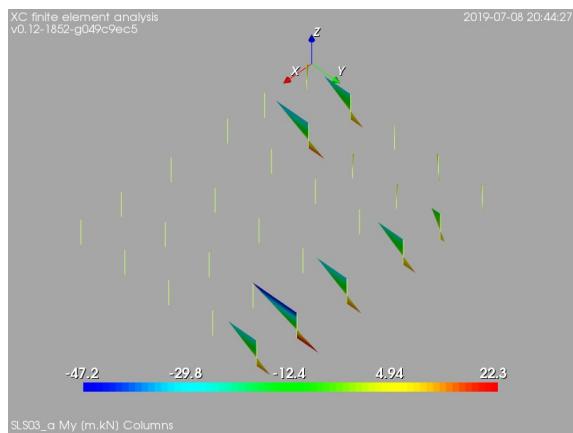


Figure 103: SLS03_a: $1.0*D + 1.0*S + 0.3*Lru + 0.3*Lpu$. Columns, bending moment about local axis y [m.kN]

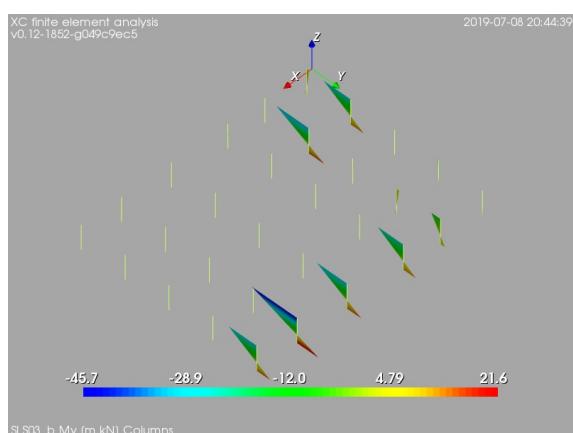


Figure 104: SLS03_b: $1.0*D + 1.0*S + 0.3*Lrs + 0.3*Lps$. Columns, bending moment about local axis y [m.kN]

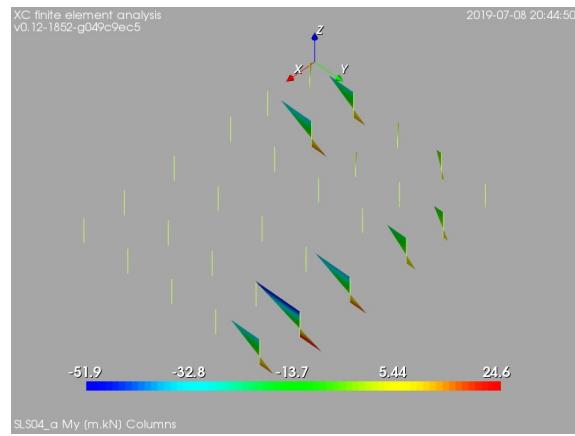


Figure 105: SLS04_a: 1.0*D + W_WE + 1.0*Lru + Lpu. Columns, bending moment about local axis y [m.kN]

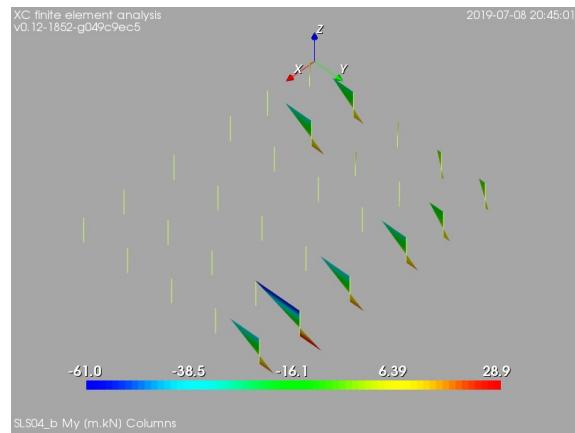


Figure 106: SLS04_b: 1.0*D + W_NS + 1.0*Lru + Lpu. Columns, bending moment about local axis y [m.kN]

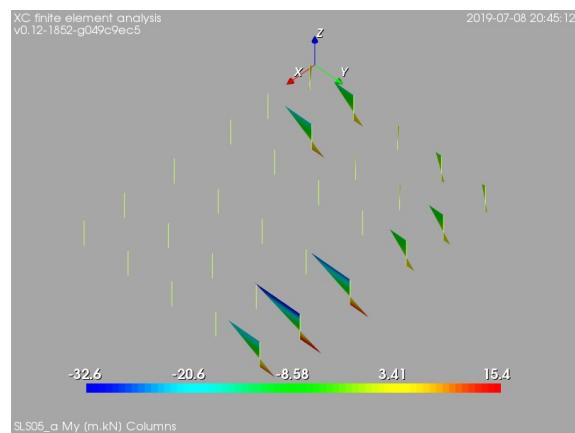


Figure 107: SLS05_a: 1.0*D + W_WE. Columns, bending moment about local axis y [m.kN]

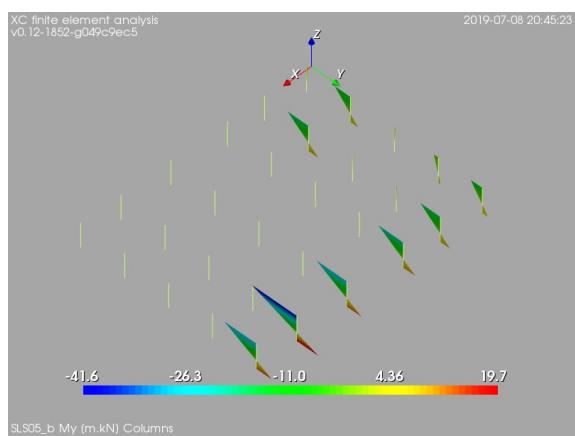


Figure 108: SLS05_b: 1.0*D + W_NS. Columns, bending moment about local axis y [m.kN]