

Drawing Bode's Diagrams:

procedure: Given a TF $G(s) = \frac{B(s)}{A(s)}$

1. Find its factors : Gain, s , first-order, second-order
2. Rearrange to make sure each factor has DC gain of 1.
3. Find Bode information for each factor (dB , ϕ) and plot
4. Add them up :

order ↓

→ Draw $s=0$ zero/pole factor

→ Add gain

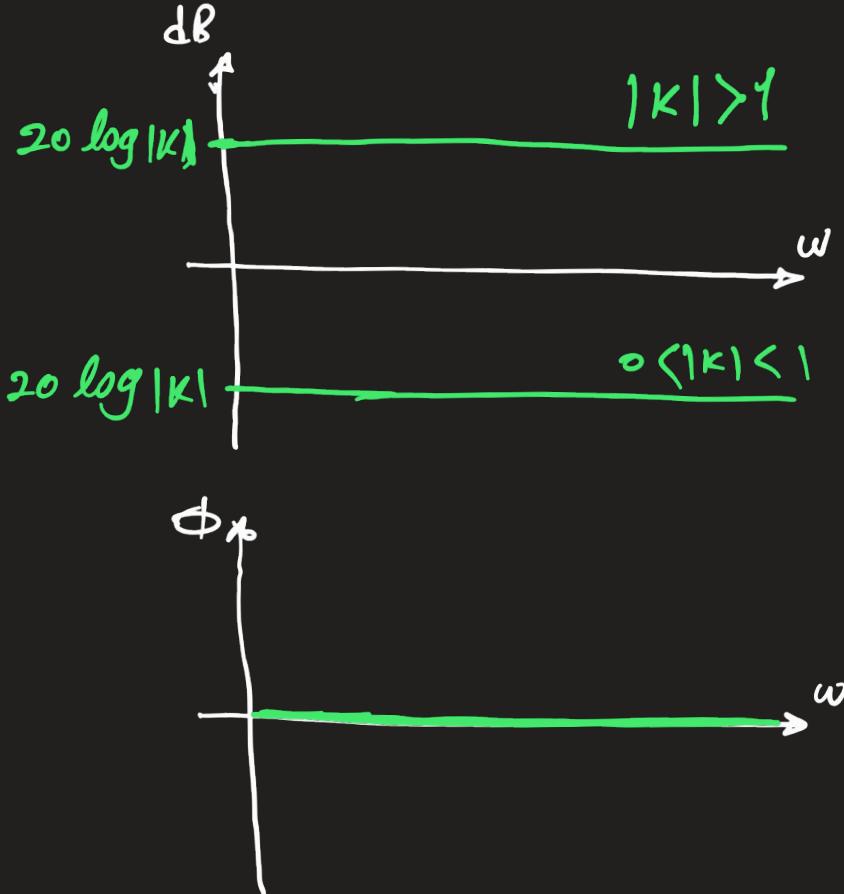
Gain ↓
Phase ↓

→ Add first- and second-order terms from

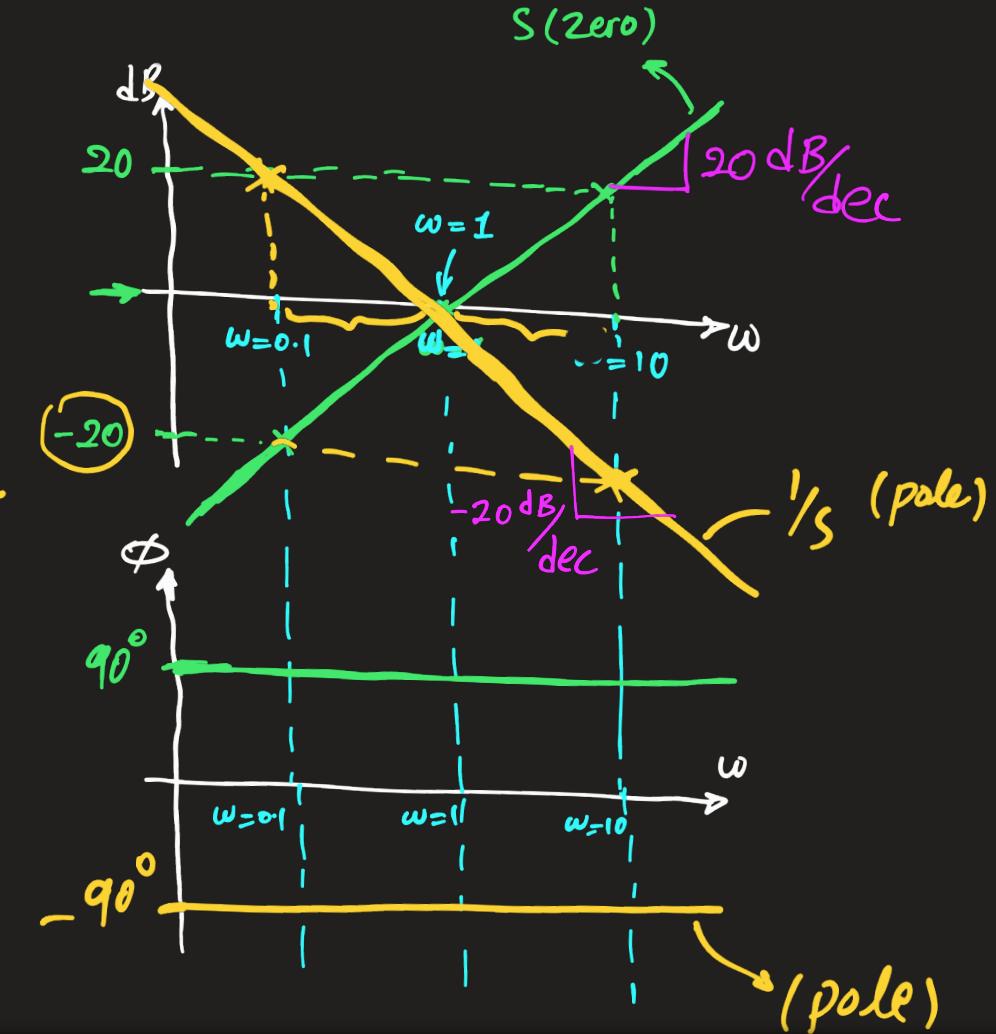
smallest corner frequency (ω_h) to the largest

↳ Add slopes.

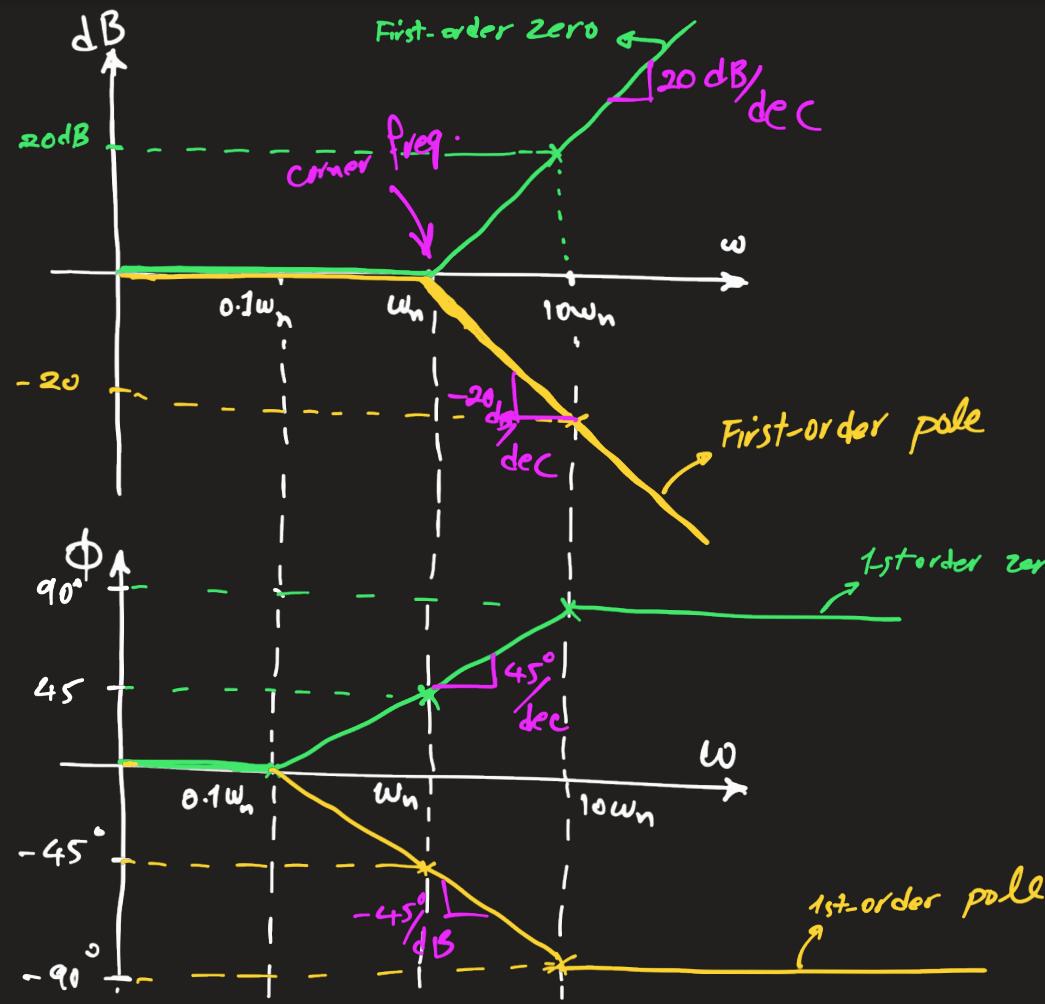
Constant gain



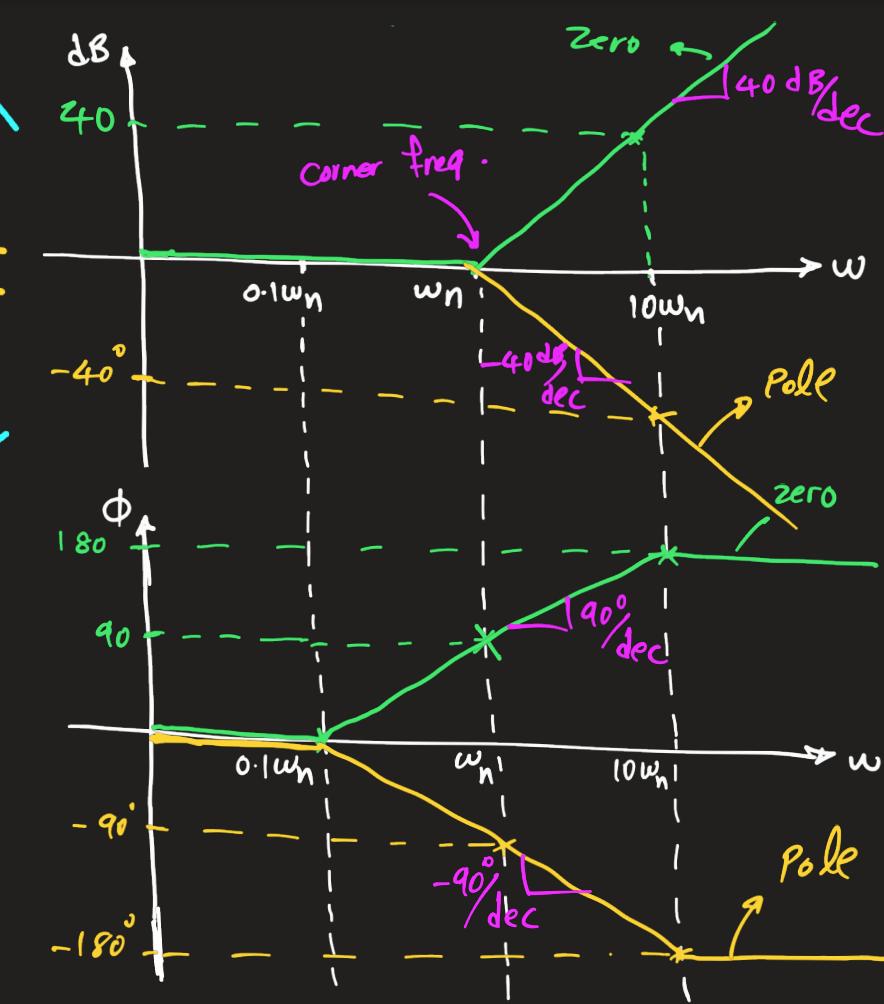
$$\zeta = 0 \text{ (zero/pole)}$$



First-order (zero/pole)

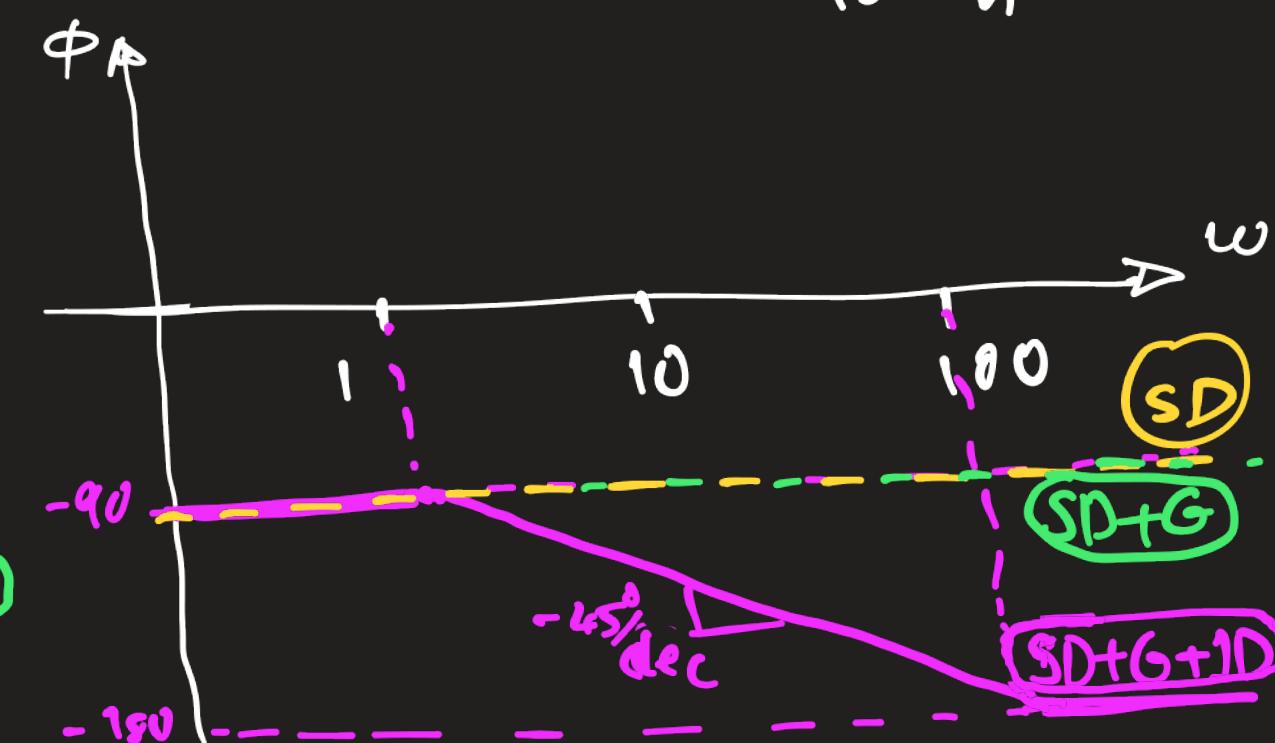
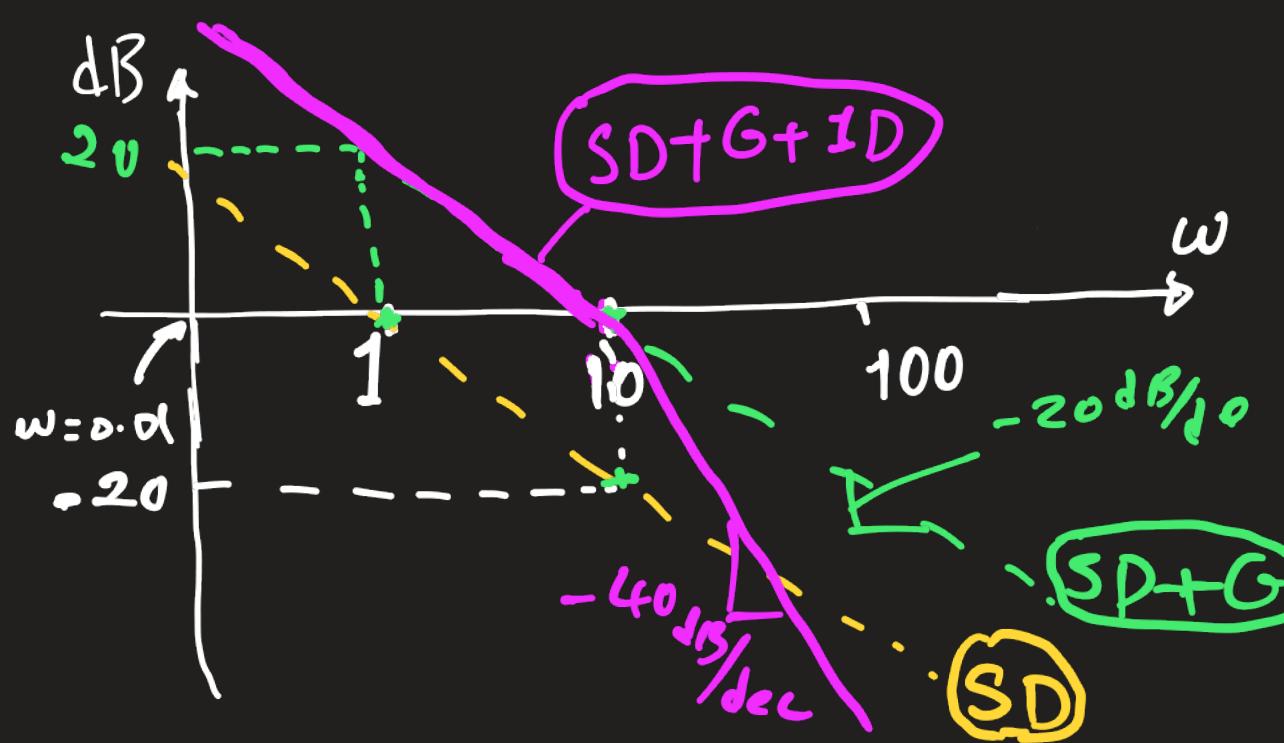


$$\zeta = 0 \text{ (zero/pole)}$$



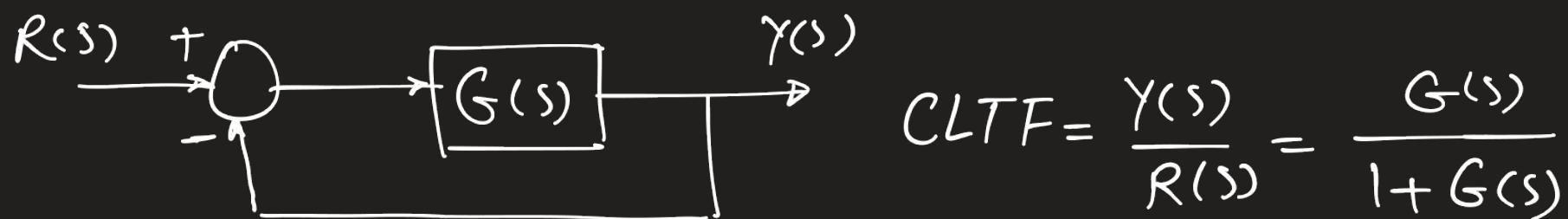
Example: $G(s) = \frac{100}{s(s+10)} = \frac{100}{s \frac{(s+10)}{10} 10} = \frac{10}{s(\frac{s}{10} + 1)}$

Factor	Gain	Phase
(SD) $s=0$ pole	$0 \rightarrow \infty : -20 \text{ dB/dec}$ $0 \text{ dB @ } \omega=1$	$-90^\circ : 0 < \omega < \infty$
(G) 10	$0 \rightarrow \infty : 20 \log 10 = 20 \text{ dB}$ slope: 0 dB/dec	$0^\circ : 0 < \omega < \infty$
(ID) first-order $\omega_n = 10$	$10 \rightarrow \infty : -20 \text{ dB/dec}$	$-45^\circ/\text{dec} : 1 < \omega < 100$ \downarrow $0.1\omega_n$ $10\omega_n$



Stability and performance analysis in Frequency Domain:

unity-feedback control system :



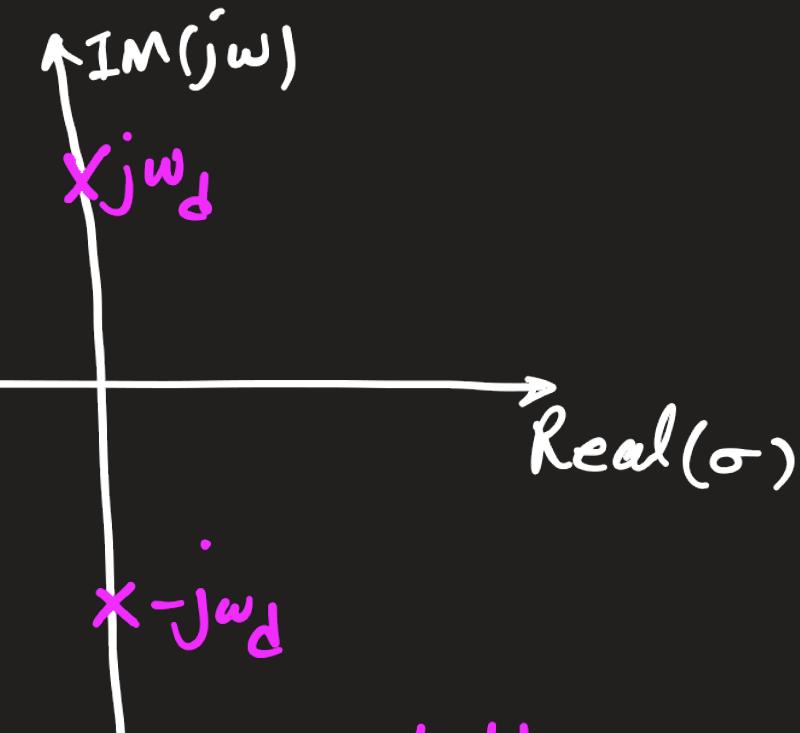
* For the closed-loop system

to be on the verge of instability :

Char. eq. must have a root at $\underline{s=j\omega_d}$

$$\Rightarrow 1+G(s)=0 \Rightarrow 1+G(j\omega_d)=0$$

$$\Rightarrow \boxed{G(j\omega_d)=-1}$$



marginally stable
critically stable

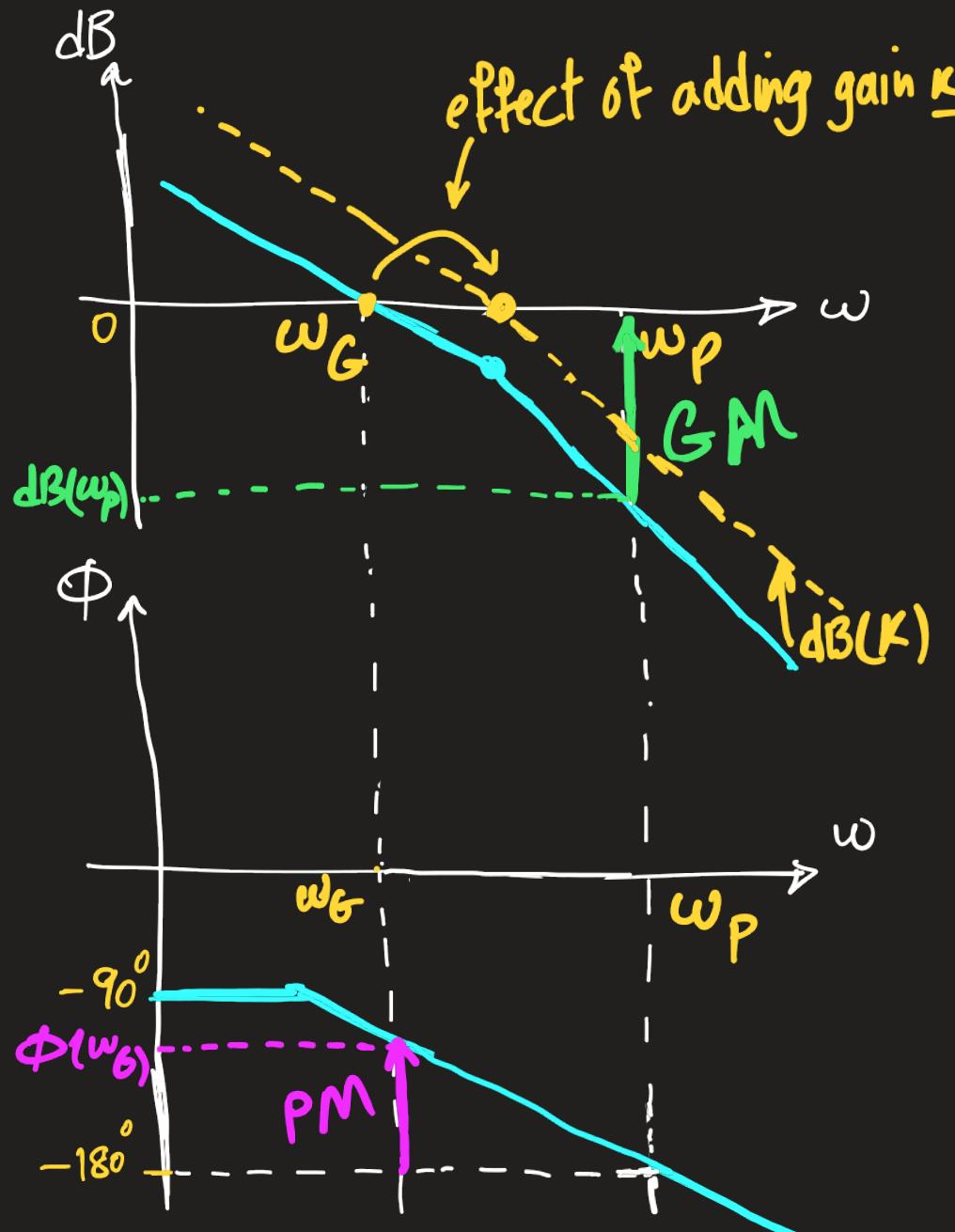
$$\Rightarrow |G(j\omega_d)|=1 \Rightarrow 20 \log(1) = \boxed{0 \text{ dB}} \rightarrow \text{can be used to}$$

$$\Rightarrow \angle G(j\omega_d) = \pm 180^\circ \Rightarrow \phi = \boxed{-180^\circ} \rightarrow \text{analyze stability of}$$

the closed-loop system

Note: $G(s)$ is the open-loop TF.

Stability Margins : (Distance to instability)



ω_G : Gain crossover frequency

ω_P : Phase crossover frequency

GM: Gain Margin:

the additional gain required to bring the system to instability

$$\boxed{\text{GM} = 0 - \text{dB}(\omega_P)} \quad \text{GM} > 0 \text{ for stability}$$

PM: Phase Margin:

the additional phase required to bring the system to instability

$$\text{PM} = \phi(\omega_G) - (-180)$$

$$\Rightarrow \boxed{\text{PM} = \phi(\omega_G) + 180}$$

$\text{PM} > 0$ for stability

* open-loop Bode Diagram :

✓ Four parameters : ω_G , ω_p , G_m , PM

* Increasing the constant gain \Rightarrow decreases both G_m & PM

✓ Easy to evaluate the effect of gain

Closed-loop system performance : (Calculating Maximum Overshoot(M_p))

For a second-order system, ξ is related to PM through the following eq.

$$PM = \tan^{-1} \left(\frac{2\xi}{\sqrt{1+4\xi^4} - 2\xi^2} \right) \xrightarrow{\text{Plot}}$$



$$\text{For } PM < 60 \Rightarrow \xi \approx \frac{PM \text{ (degrees)}}{100}$$

Procedure of calculating M_p from PM:

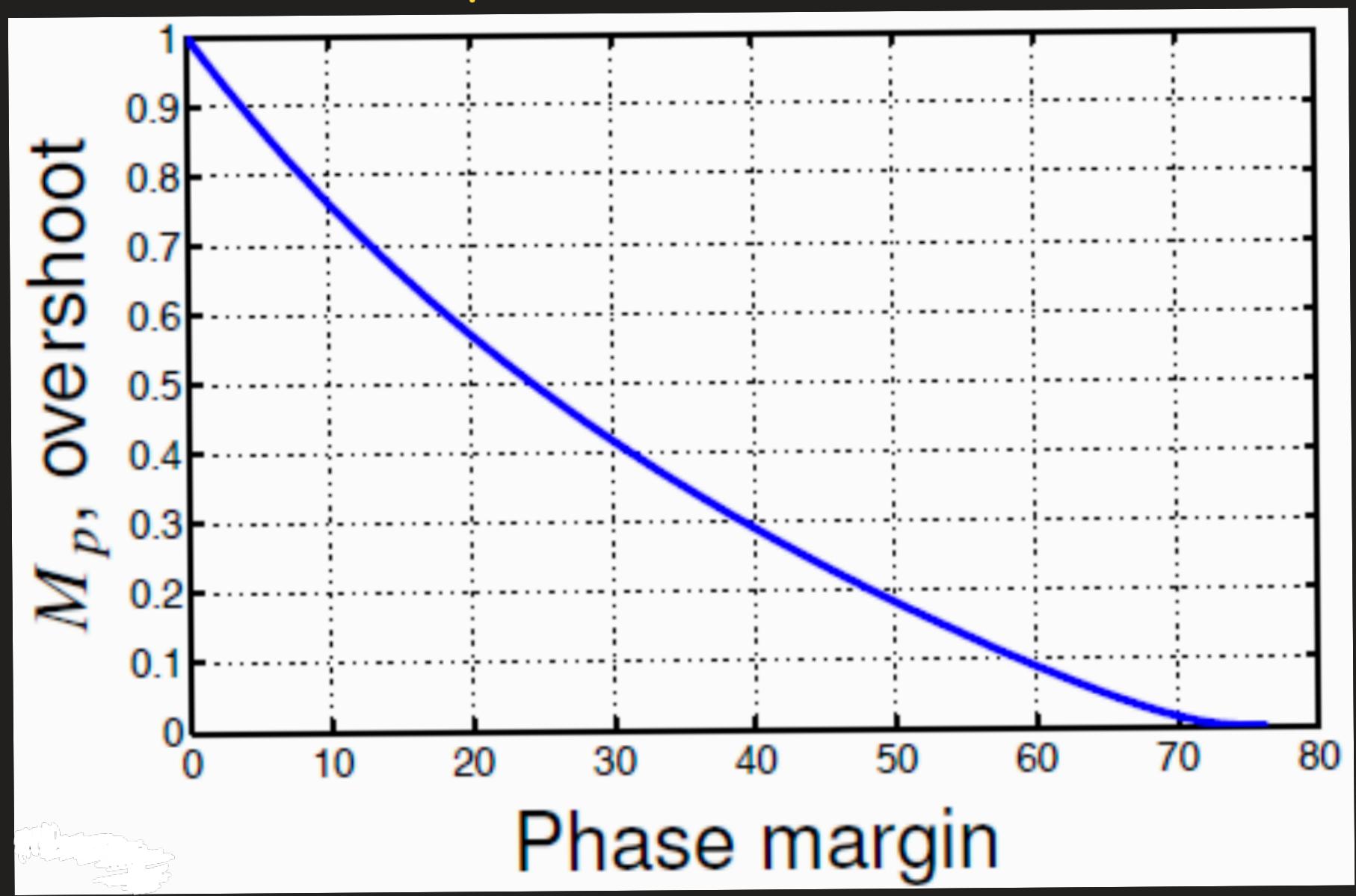
If $PM \leq 60^\circ \Rightarrow$ calculate $\zeta \approx \frac{PM \text{ (degrees)}}{100}$

$$M_p = e^{-\pi \zeta / \sqrt{1-\zeta^2}}$$

Maximum Overshoot

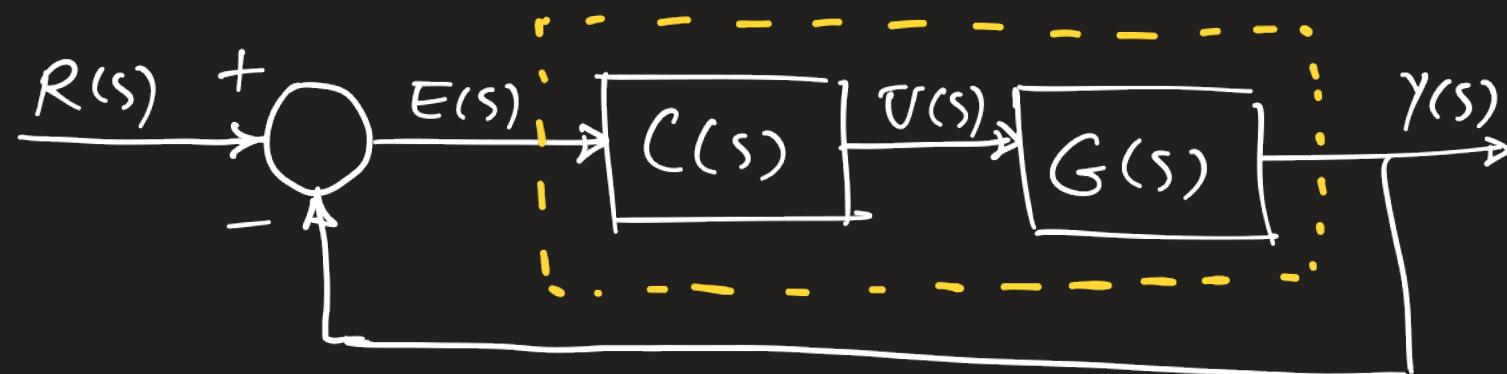
Phase Margin

M_p Vs. PM



Controller Analysis: (PD and Lead compensator)

* PD Controller: $C(s) = K_P + K_D \cdot s$ $\Rightarrow C(s) = K_P(1 + \frac{K_D}{K_P} \cdot s)$



$$T_D = \frac{1}{\omega_D}$$

$$\Rightarrow C(s) = K_P \left(\frac{s}{\omega_D} + 1 \right)$$

$$DLTF: C(s)G(s) = K_P \left(\frac{s}{\omega_D} + 1 \right) G(s)$$

\Rightarrow PD controller adds a gain & 1-st order term

to the numerator of DLTF