Oblig 1

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i)

We are asked to verify the analytical solution for flow in ducts of different shapes.

$$\mu \frac{d^2 u}{dy^2} = \frac{d\hat{p}}{dx} = \text{constant} \tag{1}$$

Transforming it into its variational form we get

$$(u'', v) = (\frac{d\hat{p}}{dx}, v)$$

$$u'v|_{d\Omega} - \int_{\Omega} u'v'dy = \int_{\Omega} \frac{d\hat{p}}{dx}vdy$$

$$- \int_{\Omega} u'v'dy = \int_{\Omega} \frac{d\hat{p}}{dx}vdy$$
(2)

Implemented in fenics as

-mu*inner(grad(u),grad(v))*dx == dpdx * v * dx

Ellipse

meshsize: 0.0591501982186 P 1: error: 0.198612991237

Qdif: 0.297069394929 P 2 : error: 0.210289258749

Qdif: 0.262444333081 P 3 : error: 0.209726175255

Qdif: 0.261816464212

meshsize: 0.0286080707886

P 1 : error: 0.0490186164831

Qdif: 0.0742216200784

P 2 : error: 0.0523161573248

Qdif: 0.0653951481331

P 3 : error: 0.0522316313421 Qdif: 0.0653017153615

meshsize: 0.0139846868179

P 1 : error: 0.012118367695

Qdif: 0.0183633262084

P 2 : error: 0.0129971279264

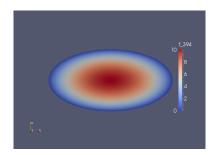
Qdif: 0.016265804744

P 3 : error: 0.0129865902472

Qdif: 0.0162541180776

The mesh refinement does make the errornorm and flowrate-difference better, for all chosen 'CG' elements. Comparing P1, P2 and P3 at the same meshsize shows that there isn't much of a difference.

Figure 1: numerical velocity field. Fine mesh



Triangle

Qdif: 1.82520665248e-13

7.22977233636e-13

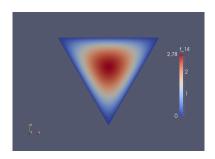
meshsize: 0.00840202867406

Qdif:

P 1 : error: 0.000121216065957 Qdif: 0.000325354790669 P 2 : error: 2.73151840825e-07 Qdif: 6.13381312409e-09 P 3 : error: 3.54823796132e-07 Qdif: 2.97228908153e-12

Comparing the numerical solution with the analytical solution for the triangle gives us great results. Not much difference when we refine for P3. P1 gives us a convergence rate of 2 and P2 gives us a convergence rate of 3.

Figure 2: numerical velocity field. Fine mesh



Annulus

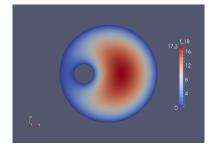
meshsize: 0.0588455214472 P 1 Qdif: 0.856400783432 P 2 Qdif: 0.696032328298 P 3 Qdif: 0.692098040142

meshsize: 0.0283145494553 P 1 Qdif: 0.214641713003 P 2 Qdif: 0.171826383154 P 3 Qdif: 0.17126495232

meshsize: 0.0136809542295 P 1 Qdif: 0.0535579359806 P 2 Qdif: 0.0425287440364 P 3 Qdif: 0.042454583381

For the annulus we can only compare the flow rate. We can see that we get better results when refining our mesh, even though the results aren't that good.

Figure 3: numerical velocity field. Fine mesh



ii)

148

$$F''' + FF'' + 1 - (F')^2 = 0 (3)$$

By using the hint, F' = H, we get

$$H'' + FH' + 1 - H^2 = 0 (4)$$

Then the boundary conditions become

$$F(0) = F'(0) = 0 \to F(0) = H(0) = 0$$

$$F'(\infty) = 1 \to H(\infty) = 1$$
 (5)

Using two test functions, vh and vf, we may display our problem as follows

$$(H, vf) = (F', vf) \tag{6}$$

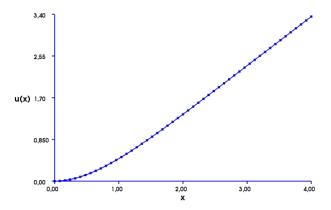
$$-(H', vh') + (FH', vh) + (1, vh) - (H^2, vh) = 0$$
(7)

We then use Newton- and Picard iteration because of the non linearity.

Newton

Newton solver finished in 6 iterations and 6 linear solver iterations.

Figure 4: plot of F, using Newtons method



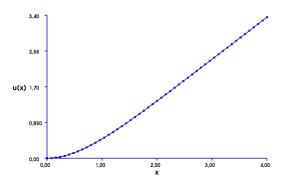
Picard

iter=1: norm=9.1337
iter=2: norm=7.14
iter=3: norm=3.97771

.

iter=64: norm=2.85202e-12
iter=65: norm=1.92189e-12
iter=66: norm=4.34496e-13

Figure 5: plot of F, using Picard iteration



Both methods give similar result. Newtons method was however much faster

150

$$F''' + 2FF'' + 1 - (F')^2 = 0 (8)$$

As above we substitute, get two equations, and use two test functions. We end up with

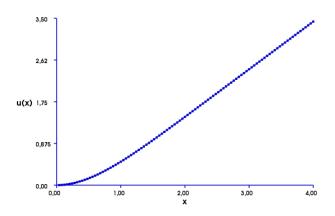
$$(H, vf) = (F', vf) \tag{9}$$

$$-(H', vh') + 2(FH', vh) + (1, vh) - (H^2, vh) = 0$$
(10)

Newton

Newton solver finished in 6 iterations and 6 linear solver iterations

Figure 6: plot of F, using Newtons method



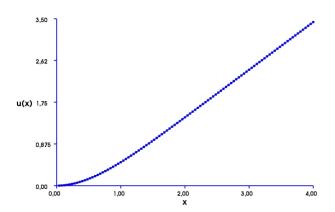
Picard

iter=1: norm=2.59437
iter=2: norm=2.20915
iter=3: norm=0.272425

.

iter=16: norm=1.75043e-11
iter=17: norm=2.37214e-12
iter=18: norm=3.51235e-13

Figure 7: plot of F, using Picard iteration

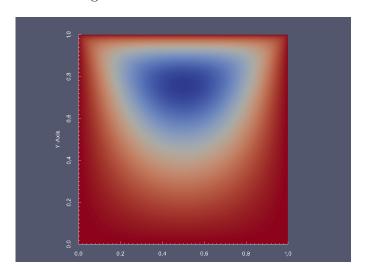


iii)

Meshsize: 0.0141421356236

Vortex center at x: 0.5 and y: 0.76

Figure 8: Plot of stream function



iv)

I've chosen L=2. With Re=0.01 I get $\mu=200$

a)

meshsize: 0.111027, minvalue: -0.0579006617083

Vortex center at x: 0.0 and y: 0.2

meshsize: 0.055514, minvalue: -0.0547620168121

Vortex center at x: 0.0 and y: 0.2

meshsize: 0.027757, minvalue: -0.0537767674796

Vortex center at x: 1.06551379861 and y: 0.0778896071092

meshsize: 0.013878, minvalue: -0.0533669982984

Vortex center at x: 1.07097328183 and y: 0.077088741035

meshsize: 0.006939, minvalue: -0.0531659519101

Vortex center at x: 1.06824354022 and y: 0.0806141740721

b)

Figure 9: Figure 3-37b in White shows the recirculation bubble in flow past a step

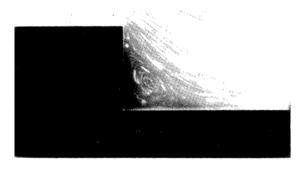
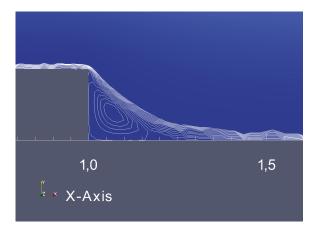


Figure 10: Numerical recirculation bubble in flow past step



c)

Flux inn: 0.425219807767 Flux out: 0.425219807767 Flux diff: 6.66133814775e-16

Since the difference is approximately zero, we have conservation of mass.

d)

The vortex center is at exactly the same point when direction of the flow is reversed. Vortex location is not dependent on flow direction, it's determined by the geometry.

e)

Normal stress on the bottom wall for flow i positive x-direction:

normal stress: 243.204770541

Normal stress on bottom wall for flow i negative x-direction:

normal stress: -243.204770541