

# Dynamic foot morphology explained through 4D scanning and shape modeling

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## Abstract

A detailed understanding of foot morphology can enable the design of more comfortable and better fitting footwear. However, foot morphology varies widely within the population, and changes dynamically during the loading of stance phase. This study presents a parametric statistical shape model from 4D foot scans to capture both the inter- and intra-individual variability in foot morphology. Thirty subjects walked on a treadmill while 4D scans of their right foot were taken at 90 frames-per-second during stance phase. Each subject's height, weight, foot length, foot width, arch length, and sex were also recorded. The 4D scans were all registered to a common high-quality foot scan, and a principal component analysis was done on all processed 4D scans. Elastic-net linear regression models were built to predict the principal component scores, which were then inverse transformed into 4D scans. The best performing model was selected with leave-one-out cross-validation. The chosen model predicts foot morphology across stance phase with a root-mean squared error of  $5.8 \pm 2.5$  mm. This study shows that statistical shape modeling can be used to predict dynamic changes in foot morphology across the population. The model can be used to investigate and improve foot-footwear interaction, allowing for better fitting and more comfortable footwear.

**Keywords:** foot morphology, dynamic scanning, gait biomechanics, shape modeling

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## 1. Introduction

Foot shape is known to be highly variable throughout the population, including by sex (Wunderlich and Cavanagh 2001; Krauss et al. 2008, 2010), age (Tomassoni, Traini, and Amenta 2014), and weight (Price and Nester 2016). This variability is often not captured in footwear sizing, as current footwear fitting standards only use foot length, foot width, and arch length to fit to standardized shoe sizes ("Standard Practice for Fitting Athletic Footwear" 2017).

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Furthermore, footwear is commonly designed around lasts, shoe molds that are sized and shaped by each manufacturer with no common standard, leading to variability in footwear shapes and sizes (Jurca and Dzeroski 2013; Wannop et al. 2019). Such variability can make it hard for consumers to find a proper fit, resulting in users having to wear ill-fitting footwear with suboptimal comfort (Dobson et al. 2018). Footwear comfort has shown benefits in increasing running performance (Luo et al. 2009) and reducing the risk of movement-related injury (Mündermann, Stefanyshyn, and Nigg 2001), and is often the number one (Martínez-Martínez et al. 2017) factor for consumers to select footwear. Footwear should therefore be properly fit to a wide population range in order to be successful.

However, because the current methodology of designing footwear relies on using static lasts, this assumes that the foot consists of rigid segments. This fails to account for dynamic changes in foot morphology, especially when the foot is being loaded during gait. Assumptions of rigid foot segments during foot loading have shown inaccuracies in estimation of ankle joint mechanics (Zelik and Honert 2018; Kessler et al. 2020), suggesting intra-foot motion as the foot is loaded (Lundgren et al. 2008; Wolf et al. 2008). Evidence suggests that foot loading affects linear foot measurements, such as when transitioning from sitting to standing (Xiong et al. 2009; Oladipo, Bob-Manuel, and Ezenatein 2008) or during the stance phase of gait (Kouchi, Kimura, and Mochimaru 2009; Barisch-Fritz et al. 2014a; Grau and Barisch-Fritz 2018). The dynamically changing measurements suggest morphological changes occurring, all of which may not be captured in static linear and circumferential measurements. Thus, it becomes difficult to characterize the wide variety of foot shapes across not only a large population, but within individuals as their foot goes through loading scenarios such as gait.

Statistical shape models (SSMs) can explain morphological differences across populations by identifying shape modes which account for variance from the mean foot,. These have been developed for whole-body digital human modeling applications to study population and individual variance in body shape (Allen, Curless, and Popović 2003; Angelov et al. 2005; Reed et al. 2014; Park and Reed 2015; Park, Ebert, and Reed 2017). Parametric SSMs are extensions which use correlations between subject anthropometric data and SSM deformations to help predict body shape for new individuals in the population (Park and Reed 2015; Park, Ebert, and Reed 2017).

SSMs have recently been applied to characterize static foot shape across a population (Conrad et al. 2019) and recognize foot-shape deviations (Stanković et al. 2020). The aforementioned efforts to capture foot measurement changes over the gait cycle did capture 4D foot images (Barisch-Fritz et al. 2014a; Grau and Barisch-Fritz 2018), but these efforts were not translated into a SSM. All the previously developed systems were also based on a catwalk, requiring subjects to correctly hit the scanning area for a successful data capture, which may not be representative of natural cadence.

The development of the DynaMo software (Boppana and Anderson 2019) for the Intel RealSense D415 Depth Cameras (Intel, Santa Clara CA) allowed a

4D scanning system to be set around a treadmill, where subjects can maintain a  
65 natural cadence. This system captures the majority of the foot’s dorsal surface,  
but does not allow for the capture of the foot’s plantar surface. 4D scans are  
captured at 90 fps, enabling a detailed evaluation of foot morphology changes  
during loading and unloading. This study outlines the development of a para-  
metric SSM, derived from scans captured with this system. The parametric  
70 SSM can characterize and predict dynamic foot morphology at specific points  
during stance phase across the subject population. We hypothesize that there  
will be significant changes in foot morphology across the dorsal surface of the  
foot throughout the gait cycle. We also hypothesize that these changes will be  
predictable from the subject demographics of our population.

## 75 2. Methods [#sec:methods]

### 2.1. Subjects

A total of 30 healthy subjects (15 men and 15 women, ages  $23.1 \pm 3.7$ )  
participated in this study. Subjects were recruited in a stratified sample into  
one of six groups (5 subjects per group) to maximize variance in population foot  
80 length. Height was used as the grouping factor since height is well correlated  
to foot length (Giles and Vallandigham 1991). The general population may not  
know offhand their exact foot length, and shoe size varies by manufacturer and  
does not correspond directly to foot length (Jurca and Dzeroski 2013; Wannop  
et al. 2019). Groups consisted of 5th-35th, 35th-65th, and 65th-95th height  
85 percentiles for each sex. Height percentile values were taken from the ANSUR  
II survey (Gordon et al. (2014)) and converted to imperial units as it was  
expected most subjects would report their height in imperial units. Population  
recruitment groups are summarized in tbl. 1.

Prior to recruitment, subjects completed a prescreening survey to ensure  
90 they were adequately healthy by the American College of Sports Medicine guide-  
lines(Riebe et al. 2015), and between the ages of 18-65. Subjects provided their  
sex and height, and were only enrolled in the study if their population group  
was not fully enrolled.

### 2.2. Experimental Procedures

95 The experimental protocol was approved by the University of Colorado Insti-  
tutional Review Board. Procedures were explained to each subject and written  
consent was obtained prior to participation. Subjects’ height and weight were  
recorded with a tape measure and scale, respectively. Subjects’ foot length,  
foot width, and arch length were measured with a Brannock device (The Bran-  
100 nnock Device Company, Liverpool, NY) (“Standard Practice for Fitting Athletic  
Footwear” 2017). Both foot length and arch length were measured in centime-  
ters. Foot width was measured as an ordinal size (e.g. A, B, C, D, E), and  
then converted to a linear measurement in centimeters (The Brannock Device  
Company, Liverpool, NY).

105 Six Intel RealSense D415 Depth Cameras (Intel, Santa Clara, CA) were placed and calibrated around a custom-built level treadmill in the University of Colorado Boulder Locomotion Laboratory, as shown in fig. 1. The DynaMo software package was used to capture depth images of the right foot at 90 frames-per-second while subjects walked on the treadmill, and convert each  
110 frame’s depth images to a single point cloud (Boppana and Anderson 2019).

The treadmill was set to an average walking pace of 1.4 m/s (Browning et al. 2006). Reflective markers were placed on the subject’s right foot and a black sock over their left foot to aid in right foot identification. Subjects first walked for one minute to warm-up and fall into a natural cadence. The operator then  
115 collected 10 seconds of data to capture approximately 10 steps. The data were reviewed to ensure the subject stayed in frame from heel-strike to toe-off during capture. If needed, the subject’s placement was shifted and data was collected again, up to two times.

### 2.3. Data Processing

120 For each subject, a candidate heel-strike to toe-off event was manually identified across all captures by taking into account point cloud quality due to the high computational power required to process all heel-strike to toe-off events. The depth images captured by each depth camera were processed into point clouds using the DynaMo package (Boppana and Anderson 2019). From each  
125 point cloud, the right foot was isolated and transformed into a triangle mesh (Rusu and Cousins 2011; Fischler and Bolles 1981). Since every depth image was captured independently by the cameras, the amount and location of points which represented the foot were not consistent. In addition, the captured data may have holes in the surface representing the foot. Registration of all scans to a common template represents every scan by an equal number  
130 of points, and ensures any missing points are properly interpolated. The right foot meshes were then iteratively registered using a three-step fitting process to an averaged high-quality static template scan from a previous study (Reed, Ebert, and Corner 2013). First scans were roughly aligned using a point-to-place iterative-closest-point algorithm (Chen and Medioni 1992), implemented  
135 in Open3d (Zhou, Park, and Koltun 2018). Next, the radial-basis function fitting algorithm from the GIAS2 software package (Zhang, Hislop-Jambrich, and Besier 2016) was run twice using a thin-plate spline to approximate the foot surface (Park and Reed 2015; Kim et al. 2016). The mid-stance scan from each  
140 subject was registered first to the template, and then the registration process was run both forwards towards toe-off and backwards towards heel-strike, on a scan-by-scan basis, using the previously registered scan as a template for the next scan. Accuracy was checked by comparing registered scans with the processed scans by finding corresponding points between both, and calculating the  
145 root-mean-squared error (RMSE) between the corresponding points.

Anatomical landmarks can be reliably approximated from the registered scans (Van den Herrewegen et al. 2014). The first metatarsal head, fifth metatarsal head, and second toe landmarks were used to align all scans to

be centered at the second metatarsal head, with the forward axis pointing to-  
 150 wards the second toe. Landmarks around the metatarsal-phalangeal (MTP)  
 joint and ankle joint were used to calculate ankle, MTP, and foot kinemat-  
 ics for each subject’s scans with respect to the joint angles at the subject’s  
 mid-stance scan. Relevant joint angles include dorsi/plantarflexion, ankle in-  
 version/eversion, ankle internal/external rotation, MTP dorsi/plantarflexion,  
 155 foot inversion/eversion, and foot internal/external rotation angles

Further details on the mesh processing, registration, and joint angle calcu-  
 lation processes can be found in section 5.

#### 2.4. Model Construction

Principal component (PC) analysis is a dimensionality-reduction method  
 160 commonly used to build statistical body shape models, with applications for  
 whole-body (Reed and Parkinson 2008; Park and Reed 2015) as well as foot  
 shape models (Conrad et al. 2019; Stanković et al. 2020). The first PC repre-  
 sents an axis containing the largest variance in the dataset, and each subsequent  
 PC describes the largest variance orthogonal to the previous component’s axis.  
 165 Therefore, PCs allow for a new, smaller set of orthogonal variables to be defined  
 which represent the variance in the dataset.

Let  $N$  equal the number of total scans in the dataset, and  $n = 29873$  equal  
 the number of vertices in each registered scan. The scikit-learn module (Pe-  
 dredgosa et al. 2011) was used to incrementally calculate the maximum  $N$  PCs  
 170 which represent the dataset. Each scan in the dataset is represented in the PC  
 model with  $N$  PC scores. All PC scores are centered around 0, which represents  
 the mean foot scan of the dataset containing all subjects. Each PC represents a  
 shape mode in the SSM, where each score represents a deviation from the mean  
 foot along the shape mode axis. The resultant PC model can be used to inverse  
 175 transform a vector of length  $N$  PC scores into a  $29873 \times 3$  vector, which repre-  
 sents the location of the vertices in the foot shape. Not all PCs were retained  
 in the model since the first few principal components explain a majority of the  
 variance, while additional PCs may be accounting for noise.

Subject demographic data and calculated joint angles were incorporated into  
 180 the SSM by developing multivariate linear regression models based on these  
 features. This was used to predict each PC score, which can then be inverse-  
 transformed into a foot shape. Subject demographic data and joint angles were  
 normalized and power-transformed to aid in regression development (Yeo and  
 Johnson 2000). An elastic net regularization algorithm (Zou and Hastie 2005)  
 185 was run for each multivariate regression to calculate normalized feature coef-  
 ficients for each PC score’s regression. Two different sets of predictors were  
 created, one with all subject demographic data and calculated joint angles, and  
 one with the highly cross-correlated predictors of arch length, body-mass index,  
 and height were removed fig. 9. Six potential models were built as combinations  
 190 between the number of PCs predicted which explained 95%, 97.5%, and 99.2%  
 of the variance, and the two predictor sets.

### 2.5. Model Validation

All six models were validated for performance using leave-one-out cross-validation, where scans from each subject were set as the validation set, and models were trained on the remaining dataset. Model performance during validation was quantified with the root mean squared error (RMSE) of the predicted foot shape to the corresponding registered scan. A two-way RMANOVA analysis was run on the error distributions to test the effect of constructing a predictor with the different number of principal components, and between using the two variable sets. The chosen model was retrained on the whole dataset before being analyzed. # Results [#sec:results]

A total of 1771 scans were analyzed across all 30 subjects. Each subject's stance phase included an average of 59 scans. Figure 4 shows a set of raw and registered scans from one subject. All processed scans were registered to the template with a median registration accuracy of  $1.044 \pm 0.623$  mm.

The PCA analysis of all registered scans found the first 14 PCs to represent approximately 95% of the variance, the first 29 PCs to represent approximately 97.5% of the variance, and the first 118 PCs to represent approximately 99.72% of the variance. Figure 5 shows the distribution of cross-validation RMSEs for each of the six elastic net regression models tested. RMSE distributions did not meet assumptions for normality, but RMANOVA was still used to compare models due to its resiliency to deviations from normality. A significant difference was found between predicting different numbers of principal components ( $F=1070.8$ ,  $p<0.001$ ), predicting between the two variable sets ( $F=28.06$ ,  $p<0.001$ ), and the interaction between both factors ( $F=106.1$ ,  $p<0.001$ ). Significant differences were found between all three levels of the predicted number of principal components ( $p\text{-adj}=0.001$ ) with a Tukey post-hoc HSD test. No significant difference was found between the two variable sets ( $p\text{-adj}=0.48$ ). Therefore, the model predicting 14 principal components with the selected variable set was chosen as it was the simplest model with the best performance.

Each retained principal component is a shape mode in the model. Figure 6 shows the chosen model's normalized regression coefficient values for each shape mode. The coefficients for the sex predictor are not shown as they were calculated to be zero for every shape mode.

Figure 7 shows each shape mode's axis represented on the mean foot, highlighting which areas of the foot are affected by deformations in each shape mode. Figure 8 shows the  $\pm 2$  standard deviations of deformation along shape modes 1,2,3,4,5, and 9, overlaid on the mean foot. Supplementary information includes correlation between figures, ratio of total variance each retained principal component accounts for, and a video showing the predictive capability of the model.

### 3. Discussion [#sec:discussion]

This study was designed to construct and evaluate a parametric statistical shape model in explaining and predicting dynamic foot morphology changes across the subject population. The model was able to predict dynamic foot

shape across the subject population with an average RMSE of  $5.8 \pm 2.5$  mm. For context, if all possible prediction error was accumulated to only affect length and width, it would be higher than the half-size step of the American shoe sizing system (Luximon and Luximon 2013), but less than inter-brand variability of shoe length and shoe width (Wannop et al. 2019). Further, this error is lower than the RMSEs of other parametric statistical shape models that predicted static standing child body shape (mean=10.4mm) (Park and Reed 2015), dynamic shoulder deformation (mean=11.98mm) (Kim et al. 2016) and child torso shape (mean=9.5mm) (Park, Ebert, and Reed 2017). Note though, that the presented model may have lower prediction errors due to the foot being a relatively smaller section of the body to model. Grant et al’s model reconstructed internal foot bones with much lower RMSEs from sparse anatomical landmarks (1.21-1.66 mm for various foot segments) (Grant et al. 2020) but was trained with higher resolution MRI images. Other efforts to create statistical foot shape models did not incorporate parametric prediction of foot shape (Conrad et al. 2019; Stanković et al. 2020).

The first, second, and fourth shape modes, accounting for a total of 81.6% of total variance, capture gross movement of the foot and ankle joint. Foot motion during stance is dominated by MTP and ankle dorsi/plantarflexion (Leardini et al. 2007), which is captured in the first shape mode fig. 8. The second and fourth shape modes capture gross changes in foot rotation from movements in the frontal and transverse planes at the MTP and ankle joints, respectively fig. 8. The second shape mode is most affected by the three MTP joint angles. The second shape mode also captures girth scaling at the ankle joint, as seen in figure 8 by how the ankle girth increases along the axis; this is affected by foot width, weight, and foot length fig. 6. The fourth shape mode is affected by ankle inversion/eversion and internal/external rotation. Foot inversion/eversion, foot internal/external rotation, ankle inversion/eversion, and ankle internal/external rotation are expected to vary across the stance phase (Leardini et al. 2007), which leads to the observed changes in gross movement. However, the fourth shape mode is also affected by foot length, which may suggest inter-individual effects in ankle inversion/eversion and internal/external rotation angles during gait. Figure 9 shows a slight correlation between these angles and foot length, which may be due to differences in cadence when walking at the treadmill’s set speed. Individuals were given time to acclimate to the treadmill’s set speed, but the speed may not have been their preferred walking speed.

The third shape mode, accounting for 6.6% of total variance, captures foot shape scaling and morphological changes at the rearfoot, as highlighted in fig. 7. Foot length shrinks when moving positively along the third shape mode fig. 8, and thus has a negative effect from foot length. Rearfoot morphology along this shape mode has a more rounded shape in the negative direction, and a sharper shape in the positive direction fig. 8. There is a positive effect for this shape mode from MTP joint dorsi/plantarflexion and foot inversion/eversion, indicating that with MTP joint flexion and foot eversion, a sharper rearfoot shape is expected. This may be due to the flattening of the rearfoot when it makes contact with the ground; as the rearfoot is lifted off the ground during

MTP joint flexion, it returns to a sharper non-weight-bearing shape.

Midfoot girth increases along the fifth shape mode's axis fig. 8, accounting for 1.6% of total variance. This shape mode is primarily affected by foot length, with slight positive effects from weight, foot width, and ankle inversion/eversion, and a slight negative effect from MTP dorsi/plantarflexion. This suggests that static midfoot girth may increase with larger foot lengths, foot widths, and weights, and decrease as the foot is unloaded at heel-off. It was previously suggested that midfoot girth decreases during stance phase compared to statically standing (Grau and Barisch-Fritz 2018), most likely due to intrinsic and extrinsic foot muscle contraction (Scott and Winter 1993; Gefen et al. 2000). However, it was not noted where during stance phase midfoot girth decreases, but it can now be assumed it occurs during heel-off.

Subsequent principal components, accounting for 5.5% of total variance, capture more minor morphology variance. The seventh shape mode is affected by foot length, ankle inversion/eversion, ankle dorsi/plantarflexion and ankle internal/external rotation at the calcaneus and first phalange regions highlighted in fig. 7. This shape mode may have a similar mechanism to the third shape mode, where morphology is affected by flattening of the foot. The ninth principal component focuses on the MTP joint region, where the positive direction increases MTP joint girth as shown in figure 8. Figure 6 shows that this shape mode is affected positively by foot inversion/eversion and MTP joint dorsi/plantarflexion, and negatively by ankle internal/external rotation, ankle inversion/eversion, foot length, and foot width. This suggests that MTP joint girth may decrease with increasing foot length and foot width, but increase during heel-off. Similar mechanisms may also be occurring in the 11th, 13th, and 14th shape modes, as shown by the similar areas of correlation in figure 7, where morphology of the metatarsals and MTP joint may be expanding during heel-off. The foot is stiffened through tension in the MTP joints in order to prepare for push-off (Hicks 1954), and the MTP joints are known to move relatively within the foot during gait (Wolf et al. 2008; Lundgren et al. 2008) which may be resulting in the increased girth at the MTP joint.

Girth changes at the midfoot and MTP joint may be directly mapped to footwear recommendations for increased fit and comfort. The midfoot should remain supported through heel-off, as this part of the foot drives footwear plantarflexion through contact while the MTP joint is dorsiflexing. Since there was an observed decrease in midfoot girth, footwear may need to contract to ensure proper contact. Decrease in midfoot girth through heel-off may suggest further support at this area, as the midfoot is still driving shoe plantarflexion through dorsiflexion of the MTP joint. An allowance of space at the MTP joint will accommodate the increases in MTP joint girth at heel-off.

There are a number of limitations in this study that must be noted. The elastic-net method is able to retain cross-correlated predictors, but still requires some bias in the dataset to be able to predict scenarios where cross-correlated predictors are independent (Zou and Hastie 2005). Therefore, the presented model may not be valid for predicting changes in morphology due to independent changes in joint angles outside of stance phase, or for variance in foot width or



weight compared to foot length not captured in the subject population.

The model did not find any differences between male and female feet. Studies found that sex differences in foot shape after scaling for foot length were not significant (Kouchi, Kimura, and Mochimaru 2009; Barisch-Fritz et al. 2014b; Conrad et al. 2019), or were small in magnitude (Wunderlich and Cavanagh 2001; Krauss et al. 2008). No subject demographic data was collected to account for differences in foot shape due to ethnicity (Jurca, Žabkar, and Džeroski 2019). No data was captured on the foot’s plantar surface due to limitations with the scanning system; therefore foot arch changes were not captured. Data captured around the toes had high noise, which necessitated the smoothing of the toes in the template to ease fitting. Future advances in 4D scanning may be able to alleviate some of these concerns, and also allow for expansion of this model to foot motions with higher movement frequencies, such as running.

#### 4. Conclusions

To the authors’ knowledge, this is the first parametric statistical foot shape model that captures and reconstructs dynamic motion. The model was able to identify specific changes in foot morphology as they related to subject and kinematic parameters, and suggest increased support at the midfoot and increased volume allowance at the MTP joint. The model is able to reconstruct a full 3D model when parameter values are provided, which offers shoe and last designers a design starting point, and the ability to test their designs on a range of subjects throughout stance phase.

#### 5. Supplemental Information

Following is more details on the mesh construction, template registration, and joint angle calculation methods.

##### 5.1. Mesh Construction

The C++ implementation of the PointCloud Library (Rusu and Cousins 2011) was used to identify and isolate the right foot from the point set. First, the point clouds were downsampled with a voxel size of 3 mm to reduce required computing power. A RANSAC algorithm (Fischler and Bolles 1981) was used to identify the flat treadmill floor with a plane model, and remove it from the point cloud. Euclidean cluster extraction was then used to detect the point clusters that make up each foot. The total color value of each point cluster was used to identify the right foot from the left foot, as the left foot had a lower total color value due to the black sock. The left foot was then removed from the point cloud, leaving only the right foot for processing.

Surface reconstruction was done through Meshlab (Cignoni et al. 2008). A surface mesh adds a topological layer interpreted from the pointcloud. Point normals were calculated for the point cloud using the 10 nearest neighbors. An APSS Marching Cubes algorithm (Guennebaud and Gross 2007; Guennebaud,

Germann, and Gross 2008) is then used with the point normals to estimate the surface from the point cloud and construct the foot scan mesh.

## 5.2. Foot Template Registration

From the provided template, the toes were smoothed into a single structure and parts of the upper shank removed to be better fit to the captured data, with a finalized structure of 29873 points. The overall registration process follows a three-step process: a rough alignment followed by two radial-basis function (RBF) fine alignment steps

The registration process was first completed for each subject’s data with a foot scan mesh manually identified near mid-stance. A point-to-plane iterative-closest-point (ICP) algorithm (Chen and Medioni 1992) was used to roughly align the template foot to the scan mesh with the Open3D library (Zhou, Park, and Koltun 2018).

Corresponding points between both the scan mesh and the ICP-aligned template were found using a radial-search KD-Tree implemented in the Open3D library (Zhou, Park, and Koltun 2018). Any points on the scan mesh which were not within 1 cm of a corresponding point on the aligned template were deleted; these points represented parts of the treadmill floor which were missed in the RANSAC identification and parts of the upper shank. Similarly, any points on the template not within 1cm of a corresponding point on the scan mesh were temporarily set aside from the template; these points correspond to those near holes in the scan mesh which would be refilled in later processing

Thin-plate spline RBFs have been used to surface fit templates to scanned body shapes (Park and Reed 2015; Kim et al. 2016), and so were used in two stages in this research. A first-pass RBF registration, using a thin-plate spline for interpolation, was done between the template and the scan using the GIAS2 package (Zhang, Hislop-Jambrich, and Besier 2016) To prevent overfitting of the RBF to the noise on the edges of the captured pointcloud, a maximum of five iterations were done on the first-pass RBF registration process. The first-pass registered RBF template was then appended with the points previously removed from the template. This intermediate template represents the template fitted to the known scan data, with any unknown sections (e.g. holes in the scan data), taking the value of the template. However, the disparity between the known and unknown sections created major discrepancies in the morphed template not representative of the scan data.

A second-pass RBF registration was done from the ICP-aligned template to the intermediate template with the same parameters as the first-pass registration. This smooths out the unknown sections representing holes in the scan data with the surrounding known sections. The second-pass registered template was saved as the final registered template.

Following the registration of the mid-stance scan, the process was repeated both forwards towards toe-off and backwards toward heel-strike on a scan-by-scan basis. In this iterative fashion, the previous scan’s registered template was used as the template for the following scan. During the iterative registration

process, the RBF alignment was only conducted for one iteration for both the first-pass and second-pass to prevent over-fitting.

### 5.3. Joint Angle Calculation

The original template identified the lateral malleolus, medial malleolus, 1st metatarsal head, 5th metatarsal head, and 2nd toe landmarks as certain vertices. New landmark vertices for the lateral shank and medial shank were manually picked on the template.

Post-registration scans were aligned to a common coordinate frame based around the toes. The origin was defined as the point along the vector from the 1st metatarsal head landmark to the 5th metatarsal head landmark which is orthogonal to the second phalange. From the origin, the x-axis, was defined as pointing towards the 2nd toe. The y-axis, was pointing towards the 5th metatarsal. The z-axis was the cross-product of both x- and y-axes, pointing upward. This coordinate system also served as the static coordinate system for the MTP joint.

The ankle joint center was defined as the midpoint between the medial and lateral malleolus. The ankle's local z-axis is aligned vertically with the shank center, defined as the center between the lateral shank and medial shank landmarks. The ankle's local y-axis is aligned from the shank center to the lateral malleolus. The ankle's x-axis is the cross-product of the y- and z- axis, pointing in the forward direction towards the toes.

Static reference angles were taken from these coordinate systems at mid-stance. For the ankle joint, the z-axis served as the internal/external rotation axis, the y-axis as the dorsi/plantarflexion axis, and the x-axis as the inversion/eversion axis. Since the model's origin was at the toes, the calculation for MTP dorsi/plantarflexion was modified. The new local MTP joint coordinate system had the x-axis defined as pointing from the ankle joint center to the MTP joint center, as such the y-axis represented MTP dorsi/plantarflexion. Since there is little flexibility in the transverse and frontal planes of the MTP joint, the x-axis therefore represented whole foot inversion/eversion, and the z-axis represented whole foot internal/external rotation around the origin. MTP and ankle joint angles were calculated for every other scan as the Euler angle difference from the static joint coordinate system around each axis. Each subject's joint angles are low-pass filtered with a 2nd order low-pass Butterworth filter with a cutoff frequency of 15 Hz. The global and local coordinate systems are summarized in fig. 3

## Figures

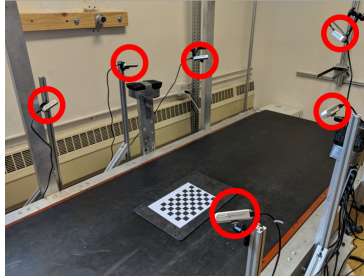


Figure 1: Capture setup of 6 Intel RealSense D415 Depth Cameras (circled in red) placed around a treadmill. The checkerboard shown was used to calibrate the cameras using the DynaMo package.

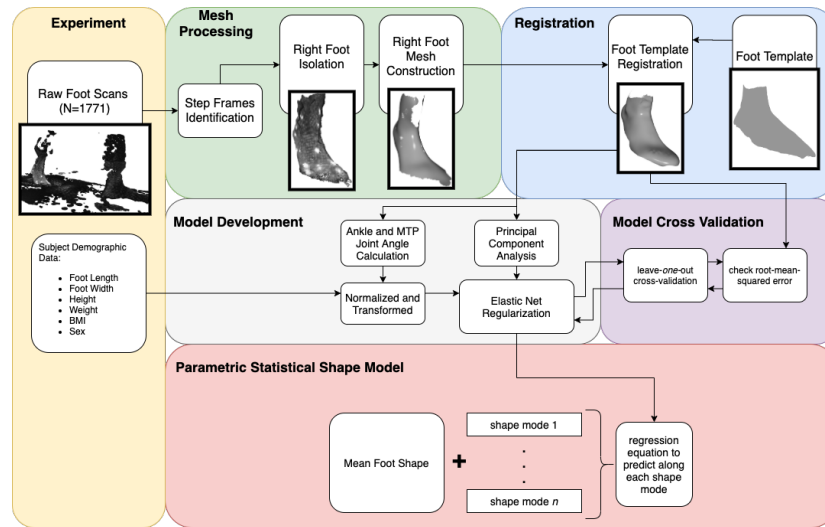


Figure 2: Flowchart of processing steps for statistical shape model creation

Table 1: Enrollment groups based on reported height. 5 subjects were enrolled in each group

Sex	5th-35th percentile Height	35th-65th percentile Height	65th-95th percentile Height
Female	4'11 "-5'3"	5'3 "-5'5"	5'5 "-5'8"
Male	5'4 "-5'8"	5'8 "-5'11"	5'11 "-6'2"

## 6. Supplemental Figures

450 Allen, Brett, Brian Curless, and Zoran Popović. 2003. "The space of human body shapes: Reconstruction and parameterization from range scans." *ACM Transactions on Graphics* 22 (3): 587–94. <https://doi.org/10.1145/882262.882311>.

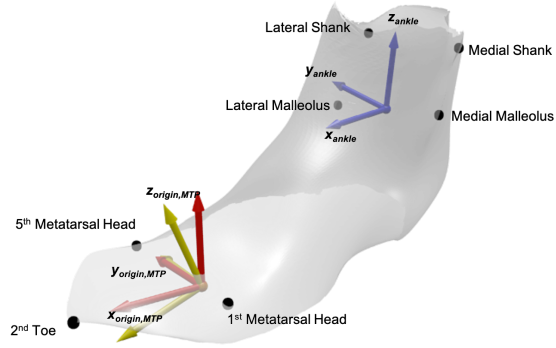


Figure 3: Coordinate system defined from registered scans. Anatomical landmarks are shown as black dots. The ankle joint's local coordinate system is shown in blue, the MTP joint's local coordinate system is shown in yellow, and the model's origin coordinate system is shown in red. Directions for each coordinate system are shown in bold text

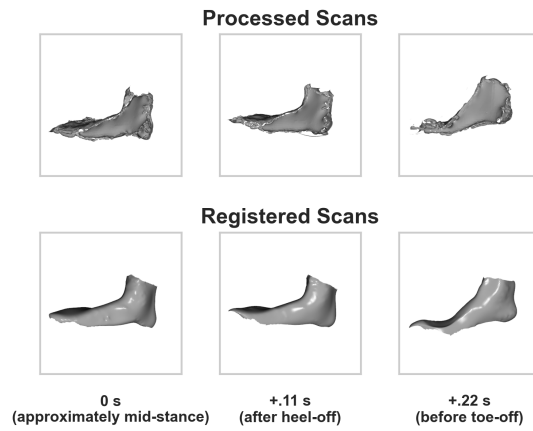


Figure 4: Processed and registered scans of one subject during heel-off, shown 10 frames (.11 seconds) apart

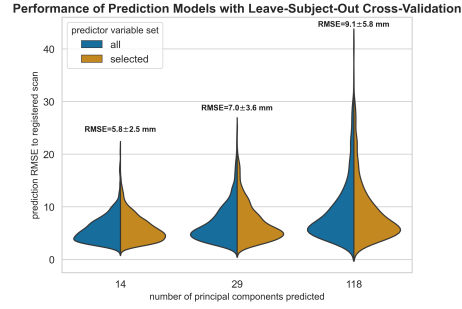


Figure 5: Distribution of errors across the various prediction models leave-subject-out cross-validation results. Model RMSE mean and standard deviation are shown above each distribution

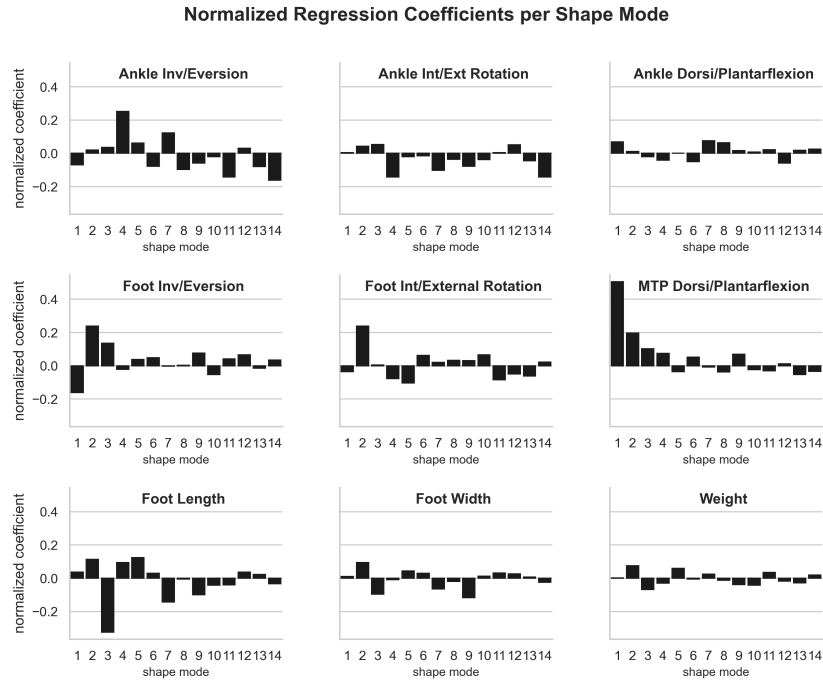


Figure 6: Each graph represents the predictor's effects on the shape mode by visualizing the model's normalized coefficients. Larger absolute values indicate a larger effect from the predictor on the shape mode.

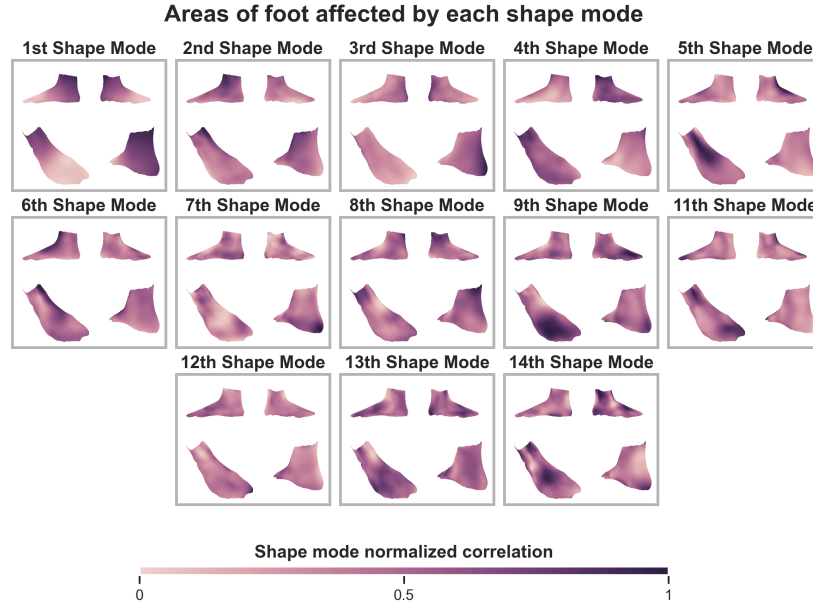


Figure 7: Each shape mode's principal axis represented as a heatmap overlaid on the mean foot and shown from 4 different point-of-views. The darker regions represent vertices which are most correlated with the shape mode's principal axis, and therefore see deformations in the shape mode.

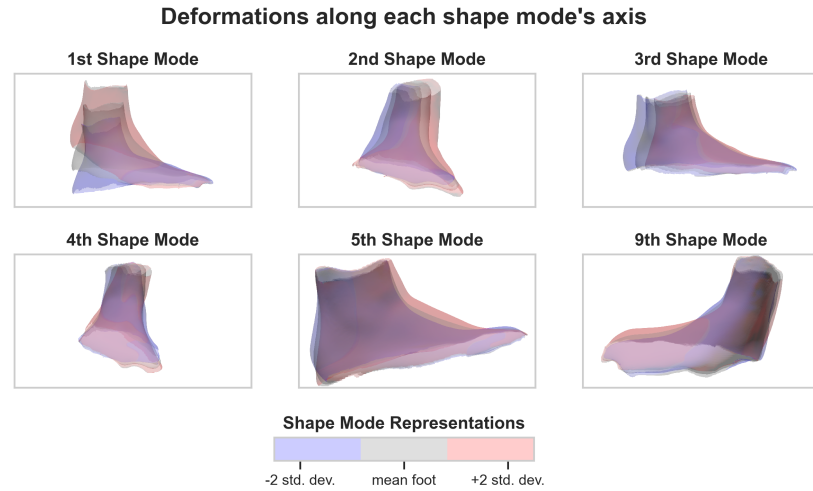


Figure 8: Foot shape deformation at +2 and -2 standard deviations along each shape mode's principal axis, overlaid on the mean foot. The point-of-view is set to highlight the major variance along each shape mode's axis.

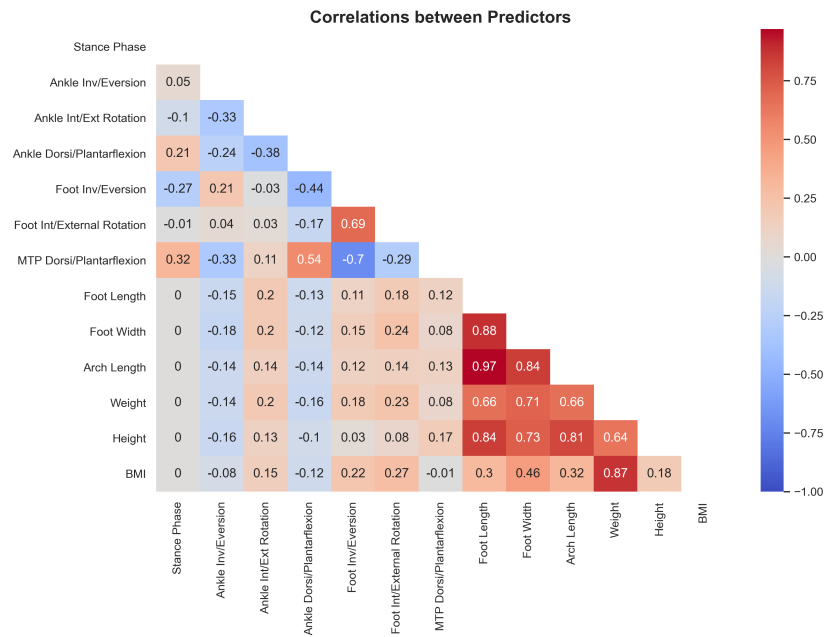


Figure 9: Correlation coefficients across all predictors

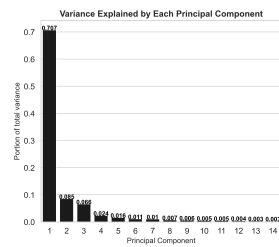


Figure 10: Ratio of variance explained by each of the first 14 principal components.



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