Tuesday, the 24th, 2020

Port-Hamiltonian flexible multibody dynamics

Andrea Brugnoli

[1]ISAE-SUPAERO, Toulouse

Outline

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Using Lie Algebra and differential forms a pH model of a flexible link has already been proposed[1]. This model can be embedded in a complex multibody system[2].

Advantages:

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Drawbacks:

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Floating frame based approach

The floating frame approach relies on the hypothesis of small deformations: elastic motion is described w.r.t a reference that follows the large rigid motion[3].

Advantages

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Drawbacks:

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Advantages

- The most used paradigm in multibody dynamics;
- For control applications other approaches are too complex;
- Model reduction techniques are applicable.

Drawbacks:

- Effect due to geometric non-linearities are not considered: not suitable for large deformations (substructuring can be employed to alleviate this).

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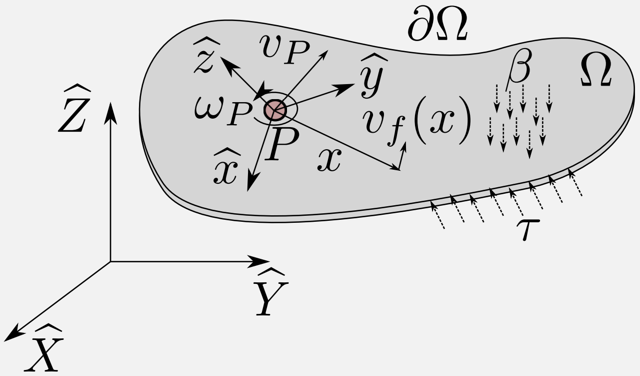

Figure: Thin floating body undergoing a surface traction $\boldsymbol{\tau}$ and body force density $\boldsymbol{\beta}$

Floating body kinematics

The velocity of a generic point is expressed by considering a small flexible displacement superimposed to the rigid motion

$$\boldsymbol{v} = \boldsymbol{v}_P + [\boldsymbol{\omega}_P]_\times (\boldsymbol{x} + \boldsymbol{u}_f) + \boldsymbol{v}_f.$$

This equation is expressed in the body reference frame $\widehat{\boldsymbol{x}}, \widehat{\boldsymbol{y}}, \widehat{\boldsymbol{z}}$.

- $\boldsymbol{x}$ is the position vector of the current point;
- $\boldsymbol{v}_P$, $\boldsymbol{\omega}_P$ are the linear and angular velocities of point P;
- $\boldsymbol{v}_f := \dot{\boldsymbol{u}}_f$ is the time derivative of the deformation displacement $\boldsymbol{u}_f$ (computed in the body frame);
- The cross map $[\boldsymbol{a}]_\times$ denotes the skew-symmetric matrix associated to vector $\boldsymbol{a}$.

Equations of motion

The equations are obtained by application of the virtual work principle[4].

Linear momentum balance

$$m(\dot{\boldsymbol{v}}_P + [\boldsymbol{\omega}_P]_\times \boldsymbol{v}_P) + [\boldsymbol{s}_u]_\times^\top \dot{\boldsymbol{\omega}}_P + \int_\Omega \rho \ddot{\boldsymbol{u}}_f \, \mathrm{d}\Omega =$$
$$- [\boldsymbol{\omega}_P]_\times [\boldsymbol{\omega}_P]_\times \boldsymbol{s}_u - \int_\Omega 2\rho [\boldsymbol{\omega}_P]_\times \dot{\boldsymbol{u}}_f \, \mathrm{d}\Omega + \int_\Omega \boldsymbol{\beta} \, \mathrm{d}\Omega + \int_{\partial\Omega} \boldsymbol{\tau} \, \mathrm{d}\Gamma,$$

- ρ is the mass density;
- $m = \int_\Omega \rho \, \mathrm{d}\Omega$ the total mass;
- $\boldsymbol{s}_u = \int_\Omega \rho(\boldsymbol{x} + \boldsymbol{u}_f) \, \mathrm{d}\Omega$ the static moment.

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$$m\dot{\boldsymbol{v}}_P + [\boldsymbol{s}_u]_\times^\top \dot{\boldsymbol{\omega}}_P + \int_\Omega \rho \dot{\boldsymbol{v}}_f \, \mathrm{d}\Omega =$$

$$\left[m\boldsymbol{v}_P + [\boldsymbol{s}_u]_\times^\top \boldsymbol{\omega}_P + 2\int_\Omega \rho \boldsymbol{v}_f \, \mathrm{d}\Omega\right]_\times \boldsymbol{\omega}_P + \int_\Omega \boldsymbol{\beta} \, \mathrm{d}\Omega + \int_{\partial\Omega} \boldsymbol{\tau} \, \mathrm{d}\Gamma.$$

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Angular momentum balance

$$
[\boldsymbol{s}_u]_\times (\dot{\boldsymbol{v}}_P + [\boldsymbol{\omega}_P]_\times \boldsymbol{v}_P) + \boldsymbol{J}_u \dot{\boldsymbol{\omega}}_P + \int_\Omega \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times \ddot{\boldsymbol{u}}_f \, \mathrm{d}\Omega + [\boldsymbol{\omega}_P]_\times \boldsymbol{J}_u \boldsymbol{\omega}_P = \\
- \int_\Omega 2\rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times [\boldsymbol{\omega}_P]_\times \dot{\boldsymbol{u}}_f \, \mathrm{d}\Omega + \int_\Omega [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{\beta} \, \mathrm{d}\Omega + \int_{\partial\Omega} [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{\tau} \, \mathrm{d}\Gamma,
$$

$\boldsymbol{J}_u := \int_\Omega \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times^\top [\boldsymbol{x} + \boldsymbol{u}_f]_\times \, \mathrm{d}\Omega$ is the inertia matrix.

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\begin{aligned}
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&\left[[\boldsymbol{s}_u]_\times^\top \boldsymbol{\omega}_P + 2 \int_\Omega \rho \boldsymbol{v}_f \, \mathrm{d}\Omega \right]_\times \boldsymbol{v}_P + \left[[\boldsymbol{s}_u]_\times \boldsymbol{v}_P + \boldsymbol{J}_u \boldsymbol{\omega}_P + 2 \int_\Omega \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{v}_f \, \mathrm{d}\Omega \right]_\times \boldsymbol{\omega}_P + \\
&\int_\Omega 2 \left[\rho \boldsymbol{v}_P + \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times^\top \boldsymbol{\omega}_P \right]_\times \boldsymbol{v}_f \, \mathrm{d}\Omega + \int_\Omega [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{\beta} \, \mathrm{d}\Omega + \int_{\partial\Omega} [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{\tau} \, \mathrm{d}\Gamma.
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Flexibility PDE

$$\rho(\dot{\boldsymbol{v}}_P + [\boldsymbol{\omega}_P]_\times \boldsymbol{v}_P) + \rho([\dot{\boldsymbol{\omega}}_P]_\times + [\boldsymbol{\omega}_P]_\times[\boldsymbol{\omega}_P]_\times)(\boldsymbol{x} + \boldsymbol{u}_f) + \rho(2[\boldsymbol{\omega}_P]_\times \dot{\boldsymbol{u}}_f + \ddot{\boldsymbol{u}}_f) = \mathrm{Div}\, \boldsymbol{\Sigma} + \boldsymbol{\beta},$$

together with boundary conditions

Neumann condition $\boldsymbol{\Sigma} \cdot \boldsymbol{n}|_{\Gamma_N} = \boldsymbol{\tau}|_{\Gamma_N}$, $\boldsymbol{n}$ is the outward normal,

Dirichlet condition $\boldsymbol{u}_f|_{\Gamma_D} = \bar{\boldsymbol{u}}_f|_{\Gamma_D}$,

- $\boldsymbol{\Sigma}$ is the Cauchy stress tensor;
- The infinitesimal strain is given by $\boldsymbol{\varepsilon} = \mathrm{Grad}(\boldsymbol{u}_f) \quad \mathrm{Grad} = \frac{1}{2}[\nabla + \nabla^\top]$;
- To close the system, Hooke's law $\boldsymbol{\Sigma} = \boldsymbol{\mathcal{D}}\boldsymbol{\varepsilon}$, where $\boldsymbol{\mathcal{D}}$ is the stiffness tensor.

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Flexibility PDE

$$\rho \dot{\boldsymbol{v}}_P + \rho[\boldsymbol{x} + \boldsymbol{u}_f]_\times^\top \dot{\boldsymbol{\omega}}_P + \rho \dot{\boldsymbol{v}}_f = \left[\rho \boldsymbol{v}_P + \rho[\boldsymbol{x} + \boldsymbol{u}_f]_\times^\top \boldsymbol{\omega}_P + 2\rho \boldsymbol{v}_f\right]_\times \boldsymbol{\omega}_P + \mathrm{Div}\, \boldsymbol{\Sigma} + \boldsymbol{\beta}.$$

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Outline

Energies and canonical momenta

Consider the total energy (Hamiltonian), given by the sum of kinetic and deformation energy:

$$H = H_{\text{kin}} + H_{\text{def}} = \frac{1}{2}\int_\Omega \left\{ \rho ||\boldsymbol{v}_P + [\boldsymbol{\omega}_P]_\times (\boldsymbol{x} + \boldsymbol{u}_f) + \boldsymbol{v}_f||^2 + \boldsymbol{\Sigma} : \boldsymbol{\varepsilon} \right\} \, \mathrm{d}\Omega.$$

Canonical momenta

$$\begin{aligned}
\boldsymbol{p}_t &:= \frac{\partial H}{\partial \boldsymbol{v}_P} = m\boldsymbol{v}_P + [\boldsymbol{s}_u]_\times^\top \boldsymbol{\omega}_P + \int_\Omega \rho \boldsymbol{v}_f \, \mathrm{d}\Omega, \\
\boldsymbol{p}_r &:= \frac{\partial H}{\partial \boldsymbol{\omega}_P} = [\boldsymbol{s}_u]_\times \boldsymbol{v}_P + \boldsymbol{J}_u \boldsymbol{\omega}_P + \int_\Omega \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{v}_f \, \mathrm{d}\Omega, \\
\boldsymbol{p}_f &:= \frac{\delta H}{\delta \boldsymbol{v}_f} = \rho \boldsymbol{v}_P + \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times^\top \boldsymbol{\omega}_P + \rho \boldsymbol{v}_f, \\
\boldsymbol{\varepsilon} &:= \frac{\delta H}{\delta \boldsymbol{\Sigma}} = \boldsymbol{\mathcal{D}}^{-1} \boldsymbol{\Sigma},
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Canonical momenta

$$\begin{bmatrix} \boldsymbol{p}_t \\ \boldsymbol{p}_r \\ \boldsymbol{p}_f \\ \boldsymbol{\varepsilon} \end{bmatrix} = \underbrace{\begin{bmatrix} m\boldsymbol{I}_{3\times 3} & [\boldsymbol{s}_u]_\times^\top & \mathcal{I}_\rho^\Omega & 0 \\ [\boldsymbol{s}_u]_\times & \boldsymbol{J}_u & \boldsymbol{\mathcal{I}}_{\rho x}^\Omega & 0 \\ (\mathcal{I}_\rho^\Omega)^* & (\boldsymbol{\mathcal{I}}_{\rho x}^\Omega)^* & \rho & 0 \\ 0 & 0 & 0 & \boldsymbol{\mathcal{D}}^{-1} \end{bmatrix}}_{\boldsymbol{\mathcal{M}}\text{: Mass operator}} \begin{bmatrix} \boldsymbol{v}_P \\ \boldsymbol{\omega}_P \\ \boldsymbol{v}_f \\ \boldsymbol{\Sigma} \end{bmatrix}, \qquad \begin{aligned} \mathcal{I}_\rho^\Omega &:= \int_\Omega \rho(\cdot)\,\mathrm{d}\Omega, \\ \boldsymbol{\mathcal{I}}_{\rho x}^\Omega &:= \int_\Omega \rho[\boldsymbol{x}+\boldsymbol{u}_f]_\times(\cdot). \end{aligned}$$

The mass operator $\boldsymbol{\mathcal{M}}$ is a self-adjoint, positive operator. It holds

$$H_{\text{kin}} + H_{\text{def}} = \frac{1}{2}\langle \boldsymbol{e}_{\text{kd}},\ \boldsymbol{\mathcal{M}}\boldsymbol{e}_{\text{kd}}\rangle, \qquad \boldsymbol{e}_{\text{kd}} = [\boldsymbol{v}_P;\ \boldsymbol{\omega}_P;\ \boldsymbol{v}_f; \boldsymbol{\Sigma}]$$

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Notice that the kinetic energy also depends on the flexible displacement

$$\frac{\delta H_{\mathsf{kin}}}{\delta \boldsymbol{u}_f} = [\boldsymbol{p}_f]_\times \boldsymbol{\omega_P}.$$

This term is responsible for a coupling between the kinematic coordinates and the velocities.

Outline

Generalized coordinates

Generalized coordinates are required for a complete formulation:

- ${}^{i}\boldsymbol{r}_P$ the position of point P in the inertial frame of reference;
- $\boldsymbol{R}$ the direction cosine matrix (other attitude parametrizations are possible);
- $\boldsymbol{u}_f$ the flexible displacement;

The direction cosine matrix is converted into a vector by concatenating its rows

$$\boldsymbol{R}_{\mathsf{v}} = \mathsf{vec}(\boldsymbol{R}^\top) = [\boldsymbol{R}_1 \ \boldsymbol{R}_2 \ \boldsymbol{R}_3]^\top,$$

where $\boldsymbol{R}_1, \boldsymbol{R}_2, \boldsymbol{R}_3$ are the rows of matrix $\boldsymbol{R}$. Furthermore the corresponding cross map will be given by

$$[\boldsymbol{R}_{\mathsf{v}}]_\times = \begin{bmatrix} [\boldsymbol{R}_1]_\times \\ [\boldsymbol{R}_2]_\times \\ [\boldsymbol{R}_3]_\times \end{bmatrix}, \qquad [\boldsymbol{R}_{\mathsf{v}}]_\times : \mathbb{R}^9 \to \mathbb{R}^{9\times 3}.$$

PH formulation

The overall port-Hamiltonian formulation

$$\underbrace{\left[\begin{array}{c:c} \boldsymbol{I} & 0 \\ \hdashline 0 & \boldsymbol{\mathcal{M}} \end{array}\right]}_{\boldsymbol{\mathcal{E}}} \frac{d}{dt} \underbrace{\begin{bmatrix} {}^{i}\boldsymbol{r}_P \\ \boldsymbol{R}_{\mathsf{v}} \\ \boldsymbol{u}_f \\ \hdashline \boldsymbol{v}_P \\ \boldsymbol{\omega}_P \\ \boldsymbol{v}_f \\ \boldsymbol{\Sigma} \end{bmatrix}}_{\boldsymbol{e}} = \underbrace{\left[\begin{array}{ccc:cccc} 0 & 0 & 0 & \boldsymbol{R} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & [\boldsymbol{R}_{\mathsf{v}}]_\times & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & \boldsymbol{I}_{3\times 3} & 0 \\ \hdashline -\boldsymbol{R}^\top & 0 & 0 & 0 & [\widetilde{\boldsymbol{p}}_t]_\times & 0 & 0 \\ 0 & -[\boldsymbol{R}_{\mathsf{v}}]_\times^\top & 0 & [\widetilde{\boldsymbol{p}}_t]_\times & [\widetilde{\boldsymbol{p}}_r]_\times & \boldsymbol{\mathcal{I}}_{p_f}^{\Omega} & 0 \\ 0 & 0 & -\boldsymbol{I}_{3\times 3} & 0 & -(\boldsymbol{\mathcal{I}}_{p_f}^{\Omega})^* & 0 & \mathrm{Div} \\ 0 & 0 & 0 & 0 & 0 & \mathrm{Grad} & 0 \end{array}\right]}_{\boldsymbol{\mathcal{J}}} \underbrace{\begin{bmatrix} \partial_{\boldsymbol{r}_P} H \\ \partial_{\boldsymbol{R}_{\mathsf{v}}} H \\ \delta_{\boldsymbol{u}_f} H \\ \hdashline \boldsymbol{v}_P \\ \boldsymbol{\omega}_P \\ \boldsymbol{v}_f \\ \boldsymbol{\Sigma} \end{bmatrix}}_{\boldsymbol{z}}.$$

Variables $\widetilde{\boldsymbol{p}}_t, \widetilde{\boldsymbol{p}}_r$ are defined as:

$$\widetilde{\boldsymbol{p}}_t = \boldsymbol{p}_t + \int_\Omega \rho \boldsymbol{v}_f \, \mathrm{d}\Omega, \qquad \widetilde{\boldsymbol{p}}_r = \boldsymbol{p}_r + \int_\Omega \rho [\boldsymbol{x} + \boldsymbol{u}_f]_\times \boldsymbol{v}_f \, \mathrm{d}\Omega.$$

The operator $\boldsymbol{\mathcal{I}}_{p_f}^{\Omega}$ is defined as: $\boldsymbol{\mathcal{I}}_{p_f}^{\Omega} := \int_\Omega \left\{2[\boldsymbol{p}_f]_\times + \rho[\boldsymbol{v}_f]_\times\right\}(\cdot) \, \mathrm{d}\Omega$.

Final pHDAE system

This system fits into the framework detailed in[5] and extends it.

$$
\begin{aligned}
\boldsymbol{\mathcal{E}}(e)\frac{\partial e}{\partial t} &= \boldsymbol{\mathcal{J}}(e)\boldsymbol{z}(e) + \boldsymbol{\mathcal{B}}_d(e)\boldsymbol{u}_d + \boldsymbol{\mathcal{B}}_r(e)\boldsymbol{u}_\partial, \qquad \text{where } \boldsymbol{u}_d := \boldsymbol{\beta} \\
\boldsymbol{y}_d &= \boldsymbol{\mathcal{B}}_d^*(e)\boldsymbol{z}(e), \\
\boldsymbol{y}_r &= \boldsymbol{\mathcal{B}}_r^*(e)\boldsymbol{z}(e), \\
\boldsymbol{u}_\partial &= \boldsymbol{\mathcal{B}}_\partial \boldsymbol{z}(e) = \boldsymbol{\Sigma}\cdot\boldsymbol{n}|_{\partial\Omega} = \boldsymbol{\tau}|_{\partial\Omega}, \\
\boldsymbol{y}_\partial &= \boldsymbol{\mathcal{C}}_\partial \boldsymbol{z}(e) = \boldsymbol{v}_f|_{\partial\Omega},
\end{aligned}
$$

with $\boldsymbol{y}_r = (\boldsymbol{v}_P + [\boldsymbol{x}+\boldsymbol{u}_f]_\times^\top \boldsymbol{\omega}_P)|_{\partial\Omega}$, $\boldsymbol{y}_d = (\boldsymbol{v}_P + [\boldsymbol{x}+\boldsymbol{u}_f]_\times^\top \boldsymbol{\omega}_P + \boldsymbol{v}_f)|_\Omega$.

Operator $\boldsymbol{\mathcal{E}}$ is positive self-adjoint, $\boldsymbol{\mathcal{J}}$ is formally skew-symmetric. The Hamiltonian satisfies

$$\partial_{\boldsymbol{e}} H = \boldsymbol{\mathcal{E}}^* \boldsymbol{z}.$$

[5] Volker Mehrmann and Riccardo Morandin. "Structure-preserving discretization for port-Hamiltonian descriptor systems". In: *Proceedings of the 59th IEEE Conference on Decision and Control*. 2019, pp. 6663–6868.

Energy balance

State space $\mathscr{X} = \mathbb{R}^3 \times \mathbb{R}^9 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathbb{R}^3 \times \mathbb{R}^3 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathscr{L}^2(\Omega, \mathbb{R}^{3\times 3}_{\mathsf{sym}})$.

$$\dot{H}(\boldsymbol{e}) = \langle \partial_{\boldsymbol{e}} H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}},$$

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\begin{aligned}
\dot{H}(\boldsymbol{e}) &= \langle \partial_{\boldsymbol{e}} H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
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\dot{H}(\boldsymbol{e}) &= \langle \partial_{\boldsymbol{e}} H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{\mathcal{E}}^* \boldsymbol{z}, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{E}} \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \quad \text{Adjoint definition},
\end{aligned}
$$

Energy balance

State space $\mathscr{X} = \mathbb{R}^3 \times \mathbb{R}^9 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathbb{R}^3 \times \mathbb{R}^3 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathscr{L}^2(\Omega, \mathbb{R}^{3\times 3}_{\text{sym}})$.

$$
\begin{aligned}
\dot{H}(\boldsymbol{e}) &= \langle \partial_e H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{\mathcal{E}}^* \boldsymbol{z}, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{E}} \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \quad \text{Adjoint definition}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{J}} \boldsymbol{z} + \boldsymbol{\mathcal{B}}_d(\boldsymbol{e}) \boldsymbol{u}_d + \boldsymbol{\mathcal{B}}_r(\boldsymbol{e}) \boldsymbol{u}_\partial \rangle_{\mathscr{X}},
\end{aligned}
$$

Energy balance

State space $\mathscr{X} = \mathbb{R}^3 \times \mathbb{R}^9 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathbb{R}^3 \times \mathbb{R}^3 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathscr{L}^2(\Omega, \mathbb{R}^{3\times 3}_{\text{sym}})$.

$$
\begin{aligned}
\dot{H}(\boldsymbol{e}) &= \langle \partial_e H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{\mathcal{E}}^* \boldsymbol{z}, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{E}} \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \quad \text{Adjoint definition}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{J}} \boldsymbol{z} + \boldsymbol{\mathcal{B}}_d(\boldsymbol{e}) \boldsymbol{u}_d + \boldsymbol{\mathcal{B}}_r(\boldsymbol{e}) \boldsymbol{u}_\partial \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{y}_\partial, \boldsymbol{u}_\partial \rangle_{\mathscr{L}^2(\partial\Omega, \mathbb{R}^3)} + \langle \boldsymbol{\mathcal{B}}_d^* \boldsymbol{z}, \boldsymbol{u}_d \rangle_{\mathscr{X}} + \langle \boldsymbol{\mathcal{B}}_r^* \boldsymbol{z}, \boldsymbol{u}_\partial \rangle_{\mathscr{X}}, \quad \text{I.B.P. on } \boldsymbol{\mathcal{J}},
\end{aligned}
$$

where the integration by parts (Stokes theorem) has been used

$$
\int_\Omega \boldsymbol{\Sigma} : \mathrm{Grad}(\boldsymbol{v}_f) \, \mathrm{d}\Omega + \int_\Omega \mathrm{Div}(\boldsymbol{\Sigma}) \cdot \boldsymbol{v}_f \, \mathrm{d}\Omega = \int_{\partial\Omega} (\boldsymbol{\Sigma} \cdot \boldsymbol{n}) \cdot \boldsymbol{v}_f \, \mathrm{d}\Gamma = \langle \boldsymbol{y}_\partial, \boldsymbol{u}_\partial \rangle_{\mathscr{L}^2(\partial\Omega)}.
$$

State space $\mathscr{X} = \mathbb{R}^3 \times \mathbb{R}^9 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathbb{R}^3 \times \mathbb{R}^3 \times \mathscr{L}^2(\Omega, \mathbb{R}^3) \times \mathscr{L}^2(\Omega, \mathbb{R}^{3\times 3}_{\mathsf{sym}})$.

$$
\begin{aligned}
\dot{H}(\boldsymbol{e}) &= \langle \partial_{\boldsymbol{e}} H, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{\mathcal{E}}^* \boldsymbol{z}, \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{E}} \partial_t \boldsymbol{e} \rangle_{\mathscr{X}}, \quad \text{Adjoint definition}, \\
&= \langle \boldsymbol{z}, \boldsymbol{\mathcal{J}} \boldsymbol{z} + \boldsymbol{\mathcal{B}}_d(\boldsymbol{e}) \boldsymbol{u}_d + \boldsymbol{\mathcal{B}}_r(\boldsymbol{e}) \boldsymbol{u}_\partial \rangle_{\mathscr{X}}, \\
&= \langle \boldsymbol{y}_\partial, \boldsymbol{u}_\partial \rangle_{\mathscr{L}^2(\partial\Omega, \mathbb{R}^3)} + \langle \boldsymbol{\mathcal{B}}_d^* \boldsymbol{z}, \boldsymbol{u}_d \rangle_{\mathscr{X}} + \langle \boldsymbol{\mathcal{B}}_r^* \boldsymbol{z}, \boldsymbol{u}_\partial \rangle_{\mathscr{X}}, \quad \text{I.B.P. on } \boldsymbol{\mathcal{J}}, \\
&= \langle \boldsymbol{y}_\partial + \boldsymbol{y}_r, \boldsymbol{u}_\partial \rangle_{\mathscr{L}^2(\partial\Omega, \mathbb{R}^3)} + \langle \boldsymbol{y}_d, \boldsymbol{u}_d \rangle_{\mathscr{L}^2(\Omega, \mathbb{R}^3)},
\end{aligned}
$$

where the integration by parts (Stokes theorem) has been used

$$
\int_\Omega \boldsymbol{\Sigma} : \mathrm{Grad}(\boldsymbol{v}_f) \, \mathrm{d}\Omega + \int_\Omega \mathrm{Div}(\boldsymbol{\Sigma}) \cdot \boldsymbol{v}_f \, \mathrm{d}\Omega = \int_{\partial\Omega} (\boldsymbol{\Sigma} \cdot \boldsymbol{n}) \cdot \boldsymbol{v}_f \, \mathrm{d}\Gamma = \langle \boldsymbol{y}_\partial, \boldsymbol{u}_\partial \rangle_{\mathscr{L}^2(\partial\Omega)}.
$$

Energy balance

Power balance

The power balance equals the power due to body force and surface traction

$$\begin{aligned}\dot{H}(\boldsymbol{e}) &= \int_{\partial\Omega} \boldsymbol{\tau} \cdot \boldsymbol{v} \, \mathrm{d}\Gamma + \int_{\Omega} \boldsymbol{\beta} \cdot \boldsymbol{v} \, \mathrm{d}\Omega, \\ &= \int_{\partial\Omega} \boldsymbol{u}_d \cdot \boldsymbol{y}_d \, \mathrm{d}\Gamma + \int_{\Omega} \boldsymbol{u}_\partial \cdot (\boldsymbol{y}_\partial + \boldsymbol{y}_r) \, \mathrm{d}\Omega,\end{aligned}$$

where $\boldsymbol{v} := \boldsymbol{v}_P + [\boldsymbol{\omega}_P]_\times (\boldsymbol{x} + \boldsymbol{u}_f) + \boldsymbol{v}_f$ is the velocity field with the body

Some remarks

- Generic linear elastic model can be included.
- Conservative forces are easily accounted for by introducing an appropriate potential energy. The gravitational potential

$$H_{\mathrm{pot}} = \int_\Omega \rho g \, {}^i r_z \, \mathrm{d}\Omega = \int_\Omega \rho g \left[{}^i r_{P,z} + \boldsymbol{R}_z(\boldsymbol{x} + \boldsymbol{u}_f) \right] \, \mathrm{d}\Omega.$$

- Geometric stiffening could be considered by adding a potential energy associated to centrifugal forces or using a substructuring technique.
- If case of vanishing deformations $\boldsymbol{u}_f \equiv 0$, the Newton-Euler equations on the Euclidean group $SE(3)$ are retrieved

$$\begin{bmatrix} {}^i\dot{\boldsymbol{r}}_P \\ \boldsymbol{R}_{\mathsf{v}} \\ \dot{\boldsymbol{p}}_t \\ \dot{\boldsymbol{p}}_r \end{bmatrix} = \begin{bmatrix} 0 & 0 & \boldsymbol{R} & 0 \\ 0 & 0 & 0 & [\boldsymbol{R}_{\mathsf{v}}]_\times \\ -\boldsymbol{R}^\top & 0 & 0 & [\boldsymbol{p}_t]_\times \\ 0 & -[\boldsymbol{R}_{\mathsf{v}}]_\times^\top & [\boldsymbol{p}_t]_\times & [\boldsymbol{p}_r]_\times \end{bmatrix} \begin{bmatrix} \partial_{\boldsymbol{r}_P} H \\ \partial_{\boldsymbol{R}_{\mathsf{v}}} H \\ \boldsymbol{v}_P \\ \boldsymbol{\omega}_P \end{bmatrix}, \qquad \begin{bmatrix} \boldsymbol{p}_t \\ \boldsymbol{p}_r \end{bmatrix} = \begin{bmatrix} m\boldsymbol{I} & [\boldsymbol{s}]_\times^\top \\ [\boldsymbol{s}]_\times & \boldsymbol{J} \end{bmatrix} \begin{bmatrix} \boldsymbol{v}_P \\ \boldsymbol{\omega}_P \end{bmatrix}.$$

Outline

Partitioned finite element method

The procedure boils down to three simple steps

1. The system is written in weak form;
2. An integration by parts is applied to highlight the appropriate boundary control;
3. A Galerkin method is employed to obtain a finite-dimensional system.

Galerkin projection

Test functions w, state e and effort functions z are discretized using the same bases

$$\boldsymbol{w}(\boldsymbol{x},t) = \boldsymbol{\phi}(\boldsymbol{x})^\top \mathbf{w}(t), \quad \boldsymbol{e}(\boldsymbol{x},t) = \boldsymbol{\phi}(\boldsymbol{x})^\top \mathbf{e}(t), \quad \boldsymbol{z}(\boldsymbol{x},t) = \boldsymbol{\phi}(\boldsymbol{x})^\top \mathbf{z}(t),$$

Finite-dimensional pHDAE system

After integration by parts of the Div operator

$$\begin{aligned}
\mathbf{E}(\mathbf{e})\dot{\mathbf{e}} &= \mathbf{J}(\mathbf{e})\mathbf{z}(\mathbf{e}) + \mathbf{B}_d(\mathbf{e})\mathbf{u}_d + \mathbf{B}_\partial(\mathbf{e})\mathbf{u}_\partial, \\
\mathbf{y}_d &:= \mathbf{M}_d\widetilde{\mathbf{y}}_d = \mathbf{B}_d^\top \mathbf{z}(\mathbf{e}), \\
\mathbf{y}_\partial &:= \mathbf{M}_\partial\widetilde{\mathbf{y}}_\partial = \mathbf{B}_\partial^\top \mathbf{z}(\mathbf{e}).
\end{aligned}$$

Dirichlet conditions

The set Γ_D for the Dirichlet condition has to be non empty, otherwise the deformation field is allowed for rigid movement, leading to a singular mass matrix. Test and state shape functions must verify an homogeneous Dirichlet condition.

Computation of the effort functions

The computation of vector $\mathbf{z}$ is based on the discrete Hamiltonian gradient:

$$\frac{\partial H_d}{\partial \mathbf{e}} = \mathbf{E}^\top \mathbf{z}, \qquad H_d = H_{d,\text{kin}} + H_{d,\text{def}} + H_{d,\text{pot}}.$$

The only term that requires additional care is $\boldsymbol{z}_u = \delta_{\boldsymbol{u}_f} H$.
Flexible displacement contribution to the power balance

$$\dot{H}_u = \int_\Omega \frac{\partial \boldsymbol{u}_f}{\partial t} \cdot \boldsymbol{z}_u \, \mathrm{d}\Omega = \int_\Omega \frac{\partial \boldsymbol{u}_f}{\partial t} \cdot \frac{\delta H}{\delta \boldsymbol{u}_f} \, \mathrm{d}\Omega$$

Given that $\boldsymbol{u}_f = \boldsymbol{\phi}_u^\top \mathbf{u}_f$, $\boldsymbol{z}_u = \boldsymbol{\phi}_u^\top \mathbf{z}_u$, the discrete Hamiltonian rate assumes the expressions

$$\dot{H}_{u,d}(\mathbf{u}_f) = \begin{cases} \dot{\mathbf{u}}_f^\top \mathbf{M}_u \, \mathbf{z}_u, \\ \dot{\mathbf{u}}_f^\top \dfrac{\partial H_d}{\partial \mathbf{u}_f}, \end{cases} \implies \mathbf{z}_u = \mathbf{M}_u^{-1} \frac{\partial H_d}{\partial \mathbf{u}_f}, \quad \text{where } \mathbf{M}_u = \int_\Omega \boldsymbol{\phi}_u \, \boldsymbol{\phi}_u^\top \, \mathrm{d}\Omega$$

Outline

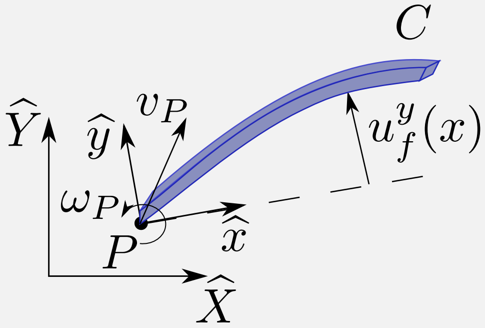


Figure: Floating beam.

Beam discretized system

Neglecting the dependence on the deformation field in the mass matrix ($\mathbf{M} = \text{const}$)

$$\begin{aligned} \mathbf{E}\dot{\mathbf{e}} &= \mathbf{J}(\mathbf{e})\mathbf{z}(\mathbf{e}) + \mathbf{B}\mathbf{u}, \\ \mathbf{y} &= \mathbf{B}^\top \mathbf{z}, \end{aligned}$$

with boundary variables

$$\begin{aligned} \mathbf{u} &= [F_P^x,\ F_P^y,\ T_P^z,\ F_C^x,\ F_C^y,\ T_C^z]^\top, \\ \mathbf{y} &= [v_P^x,\ v_P^y,\ \omega_P^z,\ v_C^x,\ v_C^y,\ \omega_C^z]^\top. \end{aligned}$$

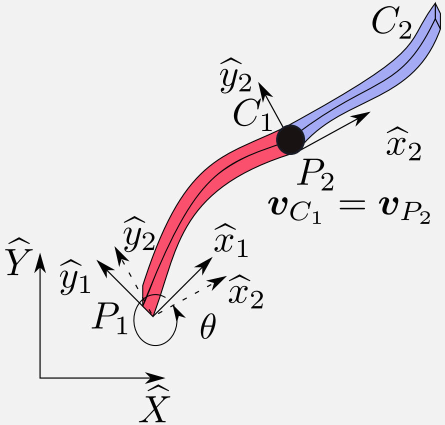


Figure: Two hinged beams.

The interconnection variables are

$$
\begin{aligned}
\mathbf{u}_1^{\text{int}} &= [F_{C_1}^x,\ F_{C_1}^y]^\top := \mathbf{F}_{C_1}, \\
\mathbf{u}_2^{\text{int}} &= [F_{P_2}^x,\ F_{P_2}^y]^\top := \mathbf{F}_{P_2}, \\
\mathbf{y}_1^{\text{int}} &= [v_{C_1}^x,\ v_{C_1}^y]^\top := \mathbf{v}_{C_1}, \\
\mathbf{y}_2^{\text{int}} &= [v_{P_2}^x,\ v_{P_2}^y]^\top := \mathbf{v}_{P_2}.
\end{aligned}
$$

Final system

Hinged interconnected beams

The transformer interconnection

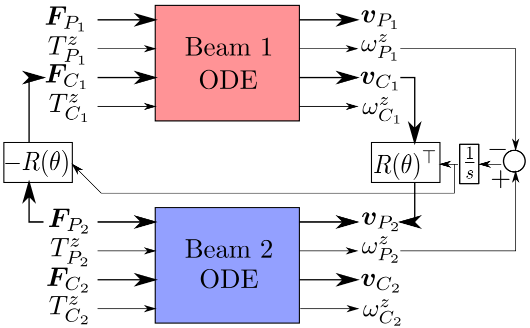
$$\mathbf{u}_1^{\text{int}} = -\mathbf{R}(\theta)\mathbf{u}_2^{\text{int}}, \qquad \mathbf{y}_2^{\text{int}} = \mathbf{R}(\theta)^\top \mathbf{y}_1^{\text{int}},$$

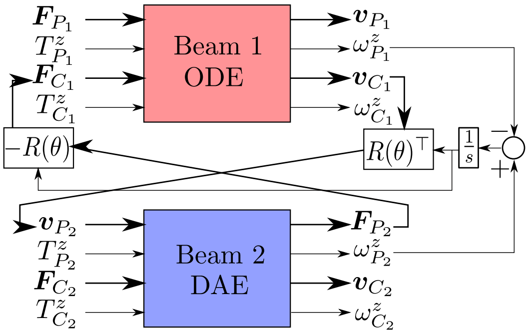
where $\mathbf{R}(\theta)$ is the relative rotation matrix, imposes the constraints on the velocity level and gives rise to a quasi-linear index 2 pHDAE.

$$\begin{bmatrix} \mathbf{E}_1 & 0 & 0 \\ 0 & \mathbf{E}_2 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\mathbf{e}}_1 \\ \dot{\mathbf{e}}_2 \\ \dot{\boldsymbol{\lambda}} \end{bmatrix} = \begin{bmatrix} \mathbf{J}_1(\mathbf{e}_1) & 0 & -\mathbf{B}_1^{\text{int}}\mathbf{R} \\ 0 & \mathbf{J}_2(\mathbf{e}_2) & \mathbf{B}_2^{\text{int}} \\ \mathbf{R}^\top \mathbf{B}_1^{\text{int}\top} & -\mathbf{B}_2^{\text{int}\top} & 0 \end{bmatrix} \begin{bmatrix} \mathbf{z}_1 \\ \mathbf{z}_2 \\ \boldsymbol{\lambda} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_{\partial 1}^{\text{ext}} & 0 \\ 0 & \mathbf{B}_{\partial 2}^{\text{ext}} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{u}_1^{\text{ext}} \\ \mathbf{u}_2^{\text{ext}} \end{bmatrix},$$

$$\begin{bmatrix} \mathbf{y}_1^{\text{ext}} \\ \mathbf{y}_2^{\text{ext}} \end{bmatrix} = \begin{bmatrix} \mathbf{B}_{\partial 1}^{\text{ext}\top} & 0 & 0 \\ 0 & \mathbf{B}_{\partial 2}^{\text{ext}\top} & 0 \end{bmatrix} \begin{bmatrix} \mathbf{z}_1 \\ \mathbf{z}_2 \\ \boldsymbol{\lambda} \end{bmatrix}.$$

The same result can be obtained by using a pHDAE system and a gyrator interconnection. It is sufficient to interchange the role of output and input of the second system $\mathbf{u}_2^{\text{int}} \leftrightarrow \mathbf{y}_2^{\text{int}}$.





Outline

Hypothesis:

1. small angular velocities;
2. small relative configuration.

$$\begin{bmatrix} \mathbf{M}_{rr} & \mathbf{M}_{rf} & 0 \\ \mathbf{M}_{fr} & \mathbf{M}_{ff} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\mathbf{p}}_r \\ \dot{\mathbf{p}}_f \\ \dot{\boldsymbol{\lambda}} \end{bmatrix} = \begin{bmatrix} 0 & 0 & \mathbf{G}_r^\top \\ 0 & \mathbf{J}_{ff} & \mathbf{G}_f^\top \\ -\mathbf{G}_r & -\mathbf{G}_f & 0 \end{bmatrix} \begin{bmatrix} \mathbf{p}_r \\ \mathbf{p}_f \\ \boldsymbol{\lambda} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_r \\ \mathbf{B}_f \\ 0 \end{bmatrix} \mathbf{u}.$$

with Hamiltonian $H = \frac{1}{2}\mathbf{p}^\top \mathbf{M}\mathbf{p}$. The modular construction of complex multi-body systems is then analogous to a sub-structuring technique[6].

[6] D. De Klerk, D. J. Rixen, and S. N. Voormeeren. "General Framework for Dynamic Substructuring: History, Review and Classification of Techniques". In: *AIAA Journal* 46.5 (2008), pp. 1169–1181. DOI: 10.2514/1.33274. URL: https://doi.org/10.2514/1.33274.

Model and index reduction

Model reduction

Such system can be reduced using Linear model reduction methods directly in the DAE[7].
Vector $\mathbf{p}_f$ is projected on a meaningful subspace $\mathbf{p}_f \approx \mathbf{V}_f^{\text{red}} \mathbf{p}_f^{\text{red}}$

$$\begin{bmatrix} \mathbf{M}_{rr} & \mathbf{M}_{rf}^{\text{red}} & 0 \\ \mathbf{M}_{fr}^{\text{red}} & \mathbf{M}_{ff}^{\text{red}} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \dot{\mathbf{p}}_r \\ \dot{\mathbf{p}}_f^{\text{red}} \\ \dot{\lambda} \end{bmatrix} = \begin{bmatrix} 0 & 0 & \mathbf{G}_r^\top \\ 0 & \mathbf{J}_{ff}^{\text{red}} & \mathbf{G}_f^{\text{red}\top} \\ -\mathbf{G}_r & -\mathbf{G}_f^{\text{red}} & 0 \end{bmatrix} \begin{bmatrix} \mathbf{p}_r \\ \mathbf{p}_f^{\text{red}} \\ \lambda \end{bmatrix} + \begin{bmatrix} \mathbf{B}_r \\ \mathbf{B}_f^{\text{red}} \\ 0 \end{bmatrix} \mathbf{u},$$

[7] H. Egger et al. "On Structure-Preserving Model Reduction for Damped Wave Propagation in Transport Networks". In: *SIAM Journal on Scientific Computing* 40.1 (2018), A331–A365. DOI: 10.1137/17M1125303.

Index reduction

$$\mathbf{M}\dot{\mathbf{p}} = \mathbf{J}\mathbf{p} + \mathbf{G}^\top \boldsymbol{\lambda} + \mathbf{B}\mathbf{u},$$
$$\mathbf{0} = \mathbf{G}\mathbf{p},$$

A null space matrix can employed to eliminate the Lagrange multiplier and preserve the port-Hamiltonian structure.

$$\mathrm{range}\{\mathbf{P}\} = \mathrm{null}\{\mathbf{G}\}.$$

Then, the range of $\mathbf{P}$ automatically satisfies the constraints. Considering the transformation $\widehat{\mathbf{p}} = \mathbf{P}\mathbf{p}$ and pre-multiplying the system by $\mathbf{P}^\top$ an equivalent ODE is obtained

$$\widehat{\mathbf{M}}\ \dot{\widehat{\mathbf{p}}} = \widehat{\mathbf{J}}\ \widehat{\mathbf{p}} + \widehat{\mathbf{B}}\ \mathbf{u},$$

with $\widehat{\mathbf{M}} = \mathbf{P}^\top \mathbf{M}\mathbf{P}$, $\widehat{\mathbf{J}} = \mathbf{P}^\top \mathbf{J}\mathbf{P}$, $\widehat{\mathbf{B}} = \mathbf{P}^\top \mathbf{B}$.

Conclusion

Summarizing:

- Port-Hamiltonian formulation of floating bodies;
- Finite element discretization;
- Interconnection of subcomponents;
- Linearized case.

Some open questions:

- Stability and convergence of finite element;
- Time discretization;
- Non-linear model reduction of pHDAE;
- Control strategies.

Additional information `https://arxiv.org/abs/2002.12816`

Thanks for your attention
Questions?

References

H. Egger et al. "On Structure-Preserving Model Reduction for Damped Wave Propagation in Transport Networks". In: *SIAM Journal on Scientific Computing* 40.1 (2018), A331–A365. DOI: 10.1137/17M1125303.

D. De Klerk, D. J. Rixen, and S. N. Voormeeren. "General Framework for Dynamic Substructuring: History, Review and Classification of Techniques". In: *AIAA Journal* 46.5 (2008), pp. 1169–1181. DOI: 10.2514/1.33274. URL: https://doi.org/10.2514/1.33274.

A. Macchelli, C. Melchiorri, and S. Stramigioli. "Port-Based Modeling and Simulation of Mechanical Systems With Rigid and Flexible Links". In: *IEEE Transactions on Robotics* 25.5 (2009), pp. 1016–1029. DOI: 10.1109/TRO.2009.2026504.

A. Macchelli, C. Melchiorri, and S. Stramigioli. "Port-Based Modeling of a Flexible Link". In: *IEEE Transactions on Robotics* 23 (2007), pp. 650 –660. DOI: 10.1109/TRO.2007.898990.

Volker Mehrmann and Riccardo Morandin. "Structure-preserving discretization for port-Hamiltonian descriptor systems". In: *Proceedings of the 59th IEEE Conference on Decision and Control*. 2019, pp. 6663 –6868.

Bernd Simeon. *Computational flexible multibody dynamics*. Springer, 2013.

Tamer M. Wasfy and Ahmed K. Noor. "Computational strategies for flexible multibody systems". In: *Applied Mechanics Reviews* 56.6 (Nov. 2003), pp. 553–613. ISSN: 0003-6900. DOI: 10.1115/1.1590354.

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