

Numerical discretization of port-Hamiltonian plate models ^{*}

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1. INTRODUCTION

2. PLATE MODELS IN PORT-HAMILTONIAN FORM

In this section the models under consideration are recalled. The details can be found in Brugnoli et al. (2019b,a).

2.1 Notations

The space of all, symmetric and skew-symmetric $d \times d$ matrices are denoted by $\mathbb{M}, \mathbb{S}, \mathbb{K}$ respectively. The space of \mathbb{R}^d vectors is denoted by \mathbb{V} . $\Omega \subset \mathbb{R}^d$ is an open connected set. The geometric dimension of interest in this paper is $d = 2$. For a scalar field $u : \Omega \rightarrow \mathbb{R}$ the gradient is defined as

$$\text{grad}(u) = \nabla u := (\partial_{x_1} u \dots \partial_{x_d} u)^\top.$$

For a vector field $\mathbf{u} : \Omega \rightarrow \mathbb{V}$, with components u_j , the gradient is defined as

$$\text{grad}(\mathbf{u})_{ij} := (\nabla \mathbf{u})_{ij} = \partial_{x_i} u_j.$$

The symmetric part of the gradient operator Grad (i. e. the deformation gradient in continuum mechanics) is given by

$$\text{Grad}(\mathbf{u}) := \frac{1}{2} (\nabla \mathbf{u} + \nabla^\top \mathbf{u}).$$

The Hessian operator of u is then computed as follows

$$\text{Hess}(u) = \nabla^2 u = \text{Grad}(\text{grad}(u)),$$

For a tensor field $\mathbf{U} : \Omega \rightarrow \mathbb{M}$, with components u_{ij} , the divergence is a vector, defined column-wise as

$$\text{Div}(\mathbf{U}) = \nabla \cdot \mathbf{U} := \left(\sum_{i=1}^d \partial_{x_i} u_{ij} \right)_{j=1, \dots, d}.$$

The double divergence of a tensor field \mathbf{U} is then a scalar field defined as

$$\text{div}(\text{Div}(\mathbf{U})) := \sum_{i,j=1}^d \partial_{x_i} \partial_{x_j} u_{ij}.$$

The L^2 inner products of scalar, vector and matrix field are defined as

$$(u, v) = \int_{\Omega} u v \, d\Omega, \quad u, v : \Omega \rightarrow \mathbb{R},$$

$$(\mathbf{u}, \mathbf{v}) = \int_{\Omega} \mathbf{u} \cdot \mathbf{v} \, d\Omega, \quad \mathbf{u}, \mathbf{v} : \Omega \rightarrow \mathbb{V},$$

$$(\mathbf{U}, \mathbf{V}) = \int_{\Omega} \mathbf{U} : \mathbf{V} \, d\Omega, \quad \mathbf{U}, \mathbf{V} : \Omega \rightarrow \mathbb{M}$$

where $\mathbf{u} \cdot \mathbf{v} := \sum_i u_i v_i$ is the scalar product in \mathbb{V} and $\mathbf{U} : \mathbf{V} := \sum_{i,j} u_{ij} v_{ij}$ is the tensor contraction. For the tensor field \mathbf{U} , the skew-symmetric part of \mathbf{U} is $\text{skw}(\mathbf{U}) = (\mathbf{U} - \mathbf{U}^\top)/2$. The standard notation $H^m(\Omega)$ denotes the Sobolev space of L^2 integrable functions with m^{th} derivative in L^2 and norm $\|\cdot\|_m$. In particular $H_0^1(\Omega)$ is the space of weakly derivable functions with vanishing trace. For $\mathbb{X} \subseteq \mathbb{M}$, let

$$H(\text{div}, \Omega) = \{\mathbf{u} \in L^2(\Omega, \mathbb{V}) \mid \text{div}(\mathbf{u}) \in L^2(\Omega)\},$$

$$H(\text{Div}, \Omega; \mathbb{X}) = \{\mathbf{U} \in L^2(\Omega, \mathbb{X}) \mid \text{Div}(\mathbf{U}) \in L^2(\Omega; \mathbb{V})\},$$

which are Hilbert space with the norm $\|\mathbf{u}\|_{\text{div}}^2 = \|\mathbf{u}\|^2 + \|\text{div}(\mathbf{u})\|^2$, $\|\mathbf{U}\|_{\text{Div}}^2 = \|\mathbf{U}\|^2 + \|\text{Div}(\mathbf{U})\|^2$. The following abbreviations will be used

$$\begin{aligned} M &= H(\text{Div}, \Omega; \mathbb{M}), & D &= H(\text{div}, \Omega), & V &= L^2(\Omega; \mathbb{V}), \\ S &= H(\text{Div}, \Omega; \mathbb{S}), & L &= L^2(\Omega), & K &= L^2(\Omega; \mathbb{K}). \end{aligned}$$

2.2 Mindlin-Reissner plate

The Mindlin model is a generalization to the 2D case of the Timoshenko beam model and is expressed by a system of three coupled PDEs (Timoshenko and Woinowsky-Krieger (1959))

$$\begin{cases} \rho h \frac{\partial^2 w}{\partial t^2} &= \text{div}(\mathbf{q}) + f, & (\mathbf{x}, t) \in \Omega \times [0, t_f] \\ \frac{\rho h^3}{12} \frac{\partial^2 \boldsymbol{\theta}}{\partial t^2} &= \mathbf{q} + \text{Div}(\mathbf{M}) + \boldsymbol{\tau}, \end{cases} \quad (1)$$

where ρ is the mass density, h the plate thickness, w the vertical displacement, $\boldsymbol{\theta} = (\theta_1, \theta_2)^\top$ collects the deflection of the cross section along axes x and y respectively. The fields $f, \boldsymbol{\tau}$ represent distributed forces and momenta. Variables \mathbf{M}, \mathbf{q} represent the momenta tensor and the

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shear stress. The Hooke law relates those to the curvature tensor and shear deformation vector

$$\begin{aligned} \mathbf{M} &:= \mathcal{D}\mathbf{K} \in \mathbb{S}, & \mathbf{K} &:= \text{Grad}(\boldsymbol{\theta}) \in \mathbb{S}, \\ \mathbf{q} &:= \mathcal{C}\boldsymbol{\gamma}, & \boldsymbol{\gamma} &:= \text{grad}(w) - \boldsymbol{\theta}, \end{aligned}$$

where \mathcal{D}, \mathcal{C} are symmetric positive tensors. The kinetic and potential energy E_c, E_p read

$$\begin{aligned} E_c &= \frac{1}{2} \int_{\Omega} \left\{ \rho h \left(\frac{\partial w}{\partial t} \right)^2 + \frac{\rho h^3}{12} \frac{\partial \boldsymbol{\theta}}{\partial t} \cdot \frac{\partial \boldsymbol{\theta}}{\partial t} \right\} d\Omega, \\ E_p &= \frac{1}{2} \int_{\Omega} \{ \mathbf{M} : \mathbf{K} + \mathbf{q} \cdot \boldsymbol{\gamma} \} d\Omega. \end{aligned} \quad (2)$$

The Hamiltonian is easily written as $H = E_c + E_p$. To get a port-Hamiltonian formulation suitable energy variables must be selected. The appropriate set is the following

$$\begin{aligned} \alpha_w &= \rho h \frac{\partial w}{\partial t}, & \alpha_{\theta} &= \frac{\rho h^3}{12} \frac{\partial \boldsymbol{\theta}}{\partial t}, \\ \mathbf{A}_{\kappa} &= \mathbf{K}, & \alpha_{\gamma} &= \boldsymbol{\gamma}. \end{aligned} \quad (3)$$

The co-energy variables are found by computing the variational derivative of the Hamiltonian

$$\begin{aligned} e_w &:= \frac{\delta H}{\delta \alpha_w} = \frac{\partial w}{\partial t}, & e_{\theta} &:= \frac{\delta H}{\delta \alpha_{\theta}} = \frac{\partial \boldsymbol{\theta}}{\partial t}, \\ \mathbf{E}_{\kappa} &:= \frac{\delta H}{\delta \mathbf{A}_{\kappa}} = \mathbf{M}, & e_{\gamma} &:= \frac{\delta H}{\delta \alpha_{\gamma}} = \mathbf{q}. \end{aligned} \quad (4)$$

Energy and co-energy are relative by a positive symmetric operator $\boldsymbol{\alpha} = \mathcal{H}e$

$$\mathcal{H} = \text{diag}\left(\frac{1}{\rho h}, \frac{12}{\rho h^3}, \mathcal{D}, \mathcal{C}\right) \quad (5)$$

The port-Hamiltonian system is expressed as follows

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_w \\ \alpha_{\theta} \\ \mathbf{A}_{\kappa} \\ \alpha_{\gamma} \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & 0 & 0 & \text{div} \\ 0 & 0 & \text{Div} & \mathbf{I}_{2 \times 2} \\ 0 & \text{Grad} & 0 & 0 \\ \text{grad} & -\mathbf{I}_{2 \times 2} & 0 & 0 \end{bmatrix}}_{\mathcal{J}} \begin{pmatrix} e_w \\ e_{\theta} \\ \mathbf{E}_{\kappa} \\ e_{\gamma} \end{pmatrix} + \begin{pmatrix} f \\ \boldsymbol{\tau} \\ 0 \\ 0 \end{pmatrix}. \quad (6)$$

This system defines a Stokes-Dirac structure, therefore, the boundary values can be found by evaluating the time derivative of the Hamiltonian. In this paper we focus on clamped boundary condition, i.e.

$$e_w|_{\partial\Omega} = 0, \quad e_{\theta}|_{\partial\Omega} = 0.$$

More general boundary conditions may be treated as well.

2.3 Kirchhoff plate

The Kirchhoff plate model is a generalization to the 2D case of the Euler-Bernoulli beam model. The classical equations for this model are (Timoshenko and Woinowsky-Krieger (1959))

$$\rho h \frac{\partial^2 w}{\partial t^2} = -\text{div}(\text{Div}(\mathbf{M})) + f, \quad (\mathbf{x}, t) \in \Omega \times [0, t_f]. \quad (7)$$

The bending moment tensor and the curvature are related as in the Mindlin model $\mathbf{M} = \mathcal{D}\mathbf{K} \in \mathbb{S}$. Following the Kirchhoff assumption the curvature tensor is the Hessian of the vertical displacement

$$\mathbf{K} := \text{Grad}(\text{grad}(w)) \in \mathbb{S}.$$

The kinetic and potential energy E_c, E_p read

$$E_c = \frac{1}{2} \rho h \left(\frac{\partial w}{\partial t} \right)^2, \quad E_p = \frac{1}{2} \mathbf{M} : \mathbf{K}, \quad (8)$$

The Hamiltonian is then given by $H = E_c + E_p$. Selecting as energy variables

$$\alpha_w = \rho h \frac{\partial w}{\partial t}, \quad \mathbf{A}_{\kappa} = \mathbf{K}, \quad (9)$$

the co-energy variables are found by computing the variational derivative of the Hamiltonian

$$e_w := \frac{\delta H}{\delta \alpha_w} = \frac{\partial w}{\partial t}, \quad \mathbf{E}_{\kappa} := \frac{\delta H}{\delta \mathbf{A}_{\kappa}} = \mathbf{M}, \quad (10)$$

The coercive operator linking energy and co-energies reads

$$\mathcal{H} = \text{diag}\left(\frac{1}{\rho h}, \mathcal{D}\right) \quad (11)$$

The port-Hamiltonian system is expressed as follows

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_w \\ \mathbf{A}_{\kappa} \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & -\text{div} \circ \text{Div} \\ \text{Grad} \circ \text{grad} & 0 \end{bmatrix}}_{\mathcal{J}} \begin{pmatrix} e_w \\ \mathbf{E}_{\kappa} \end{pmatrix} + \begin{pmatrix} f \\ 0 \end{pmatrix}. \quad (12)$$

Again this system defines a Stokes-Dirac structure and so the boundary values define the power balance. In this paper simply supported boundary conditions are considered, i.e.

$$e_w|_{\partial\Omega} = 0, \quad \mathbf{n}^{\top} \mathbf{E}_{\kappa} \mathbf{n}|_{\partial\Omega} := m_{nn}|_{\partial\Omega} = 0.$$

Differently from the Mindlin plate case, generic boundary conditions demands an accurate analysis, see for instance Blum and Rannacher (1990); Rafetseder and Zulehner (2018).

3. DISCRETIZATION AND CONNECTION WITH EXISTING MIXED FINITE ELEMENTS

In this section suitable semi-discretized are derived for the two models. For the Mindlin plate model two different formulations are presented: the first enforces the symmetry of the momenta tensor strongly, the second weakly. For the Kirchhoff plate, the formulation is based on the non-conforming Hellan-Herrmann-Johnson method.

Remark 1. System (6), (12) can be expressed using either the energy or the co-energy variables. The most adapted formulation for existing mixed finite element literature is the co-energy based one, which reads

$$\mathcal{H}^{-1} \partial_t \mathbf{e} = \mathcal{J} \mathbf{e}$$

3.1 Mindlin plate with strongly imposed symmetry

The weak formulation with strongly imposed symmetry seeks $(e_w, \mathbf{e}_{\theta}, \mathbf{E}_{\kappa}, e_{\gamma})$ in $L \times V \times S \times D$ so that

$$\begin{aligned} (v_w, \rho h \dot{e}_w) &= (v_w, \text{div} \mathbf{e}_{\gamma}) + (v_w, f), & v_w &\in L, \\ (\mathbf{v}_{\theta}, \rho h^3 / 12 \dot{\mathbf{e}}_{\theta}) &= (\mathbf{v}_{\theta}, \text{Div} \mathbf{E}_{\kappa} + \mathbf{e}_{\gamma}) + (\mathbf{v}_{\theta}, \boldsymbol{\tau}), & \mathbf{v}_{\theta} &\in V, \\ (\mathbf{V}_{\kappa}, \mathcal{D}^{-1} \dot{\mathbf{E}}_{\kappa}) &= -(\text{Div} \mathbf{V}_{\kappa}, \mathbf{e}_{\theta}), & \mathbf{V}_{\kappa} &\in S, \\ (\mathbf{v}_{\gamma}, \mathcal{C}^{-1} \dot{\mathbf{e}}_{\gamma}) &= -(\text{div} \mathbf{v}_{\gamma}, e_w) + (\mathbf{v}_{\gamma}, \mathbf{e}_{\theta}), & \mathbf{v}_{\gamma} &\in D. \end{aligned} \quad (13)$$

This system is obtained by integrating by parts the last two lines of (6) and considering clamped boundary conditions. Obtaining stable finite element that embeds the symmetry of the stress tensor for the general elastodynamics problem has proven to be a difficult task. The easiest implementation manageable by the Firedrake library (Rathgeber et al. (2017)) is the one presented in Bécache et al. (2000, 2001). The main disadvantage is

that this scheme requires the domain to be given by union of rectangles, as the mesh elements have to be squared. This allows constructing a simple element for the momenta tensor. The polynomial spaces for the discretization are

$$Q_k = \{p(x_1, x_2) \mid p(x_1, x_2) = \sum_{i \leq k, j \leq k} a_{ij} x_1^i x_2^j\},$$

Given a regular mesh \mathcal{Q}_h with squared elements Q the following spaces are introduced as discretization spaces

$$\begin{aligned} L_h^{\text{BEC}} &= \{w_h \in L \mid \forall Q, w_h|_Q \in Q_k\}, \\ V_h^{\text{BEC}} &= \{\theta_h \in V \mid \forall Q, \theta_h|_Q \in (Q_k)^2\}, \\ S_h^{\text{BEC}} &= \{m_{12} \in H^1(\Omega) \mid \forall Q, m_{12}|_Q \in Q_{k+1}\} \\ &\quad \cup \{(m_{11}, m_{22}) \in D \mid \forall Q, (m_{11}, m_{22})|_Q \in Q_{k+1}\}, \\ D_h^{\text{BEC}} &= \{q_h \in D \mid \forall Q, q_h|_Q \in Q_{k+1}\}. \end{aligned}$$

Combining the results of Bécache et al. (2000) and Bécache et al. (2001), the following error estimates are conjectured: *Conjecture 1.* Assuming a smooth solution to problem (13), the following error estimates hold

$$\begin{aligned} \|e_w - e_w^h\|_{L^\infty L^2} &\lesssim h^{k+1}, \quad \|\mathbf{E}_\kappa - \mathbf{E}_\kappa^h\|_{L^\infty L^2} \lesssim h^{k+1}, \\ \|e_\theta - e_\theta^h\|_{L^\infty L^2} &\lesssim h^{k+1}, \quad \|e_\gamma - e_\gamma^h\|_{L^\infty L^2} \lesssim h^{k+1}, \end{aligned} \quad (14)$$

where the notation $A \lesssim B$ means $A \leq CB$. The constant depends only on the true solution and on the final time.

3.2 Mindlin plate with weakly imposed symmetry

The formulation (13) has to be modified to impose the symmetry of the momenta tensor weakly. Taking the weak form of the third equation in (6)

$$(\mathbf{V}_\kappa, \mathcal{D}^{-1} \dot{\mathbf{E}}_\kappa) = (\mathbf{V}_\kappa, \text{Grad} \mathbf{e}_\theta).$$

The symmetric gradient can be rewritten as

$$\text{Grad } \theta = \text{grad } \theta - \text{skwgrad } \theta,$$

where $\text{skw}(\mathbf{A})$ is the skew-symmetric part of matrix \mathbf{A} . Introducing the new variable $\mathbf{E}_r = \text{skw}(\text{grad}(\theta))$ then $(e_\theta, \mathbf{E}_\kappa, \mathbf{E}_r) \in V \times M \times K$ satisfy (reminding that $e_\theta = \dot{\theta}$)

$$\begin{aligned} (\mathbf{V}_\kappa, \mathcal{D}^{-1} \dot{\mathbf{E}}_\kappa) &= (\mathbf{V}_\kappa, \text{grad}(e_\theta)) - (\mathbf{V}_\kappa, \dot{\mathbf{E}}_r), \\ &= -(\text{Div} \mathbf{V}_\kappa, e_\theta) - (\mathbf{V}_\kappa, \dot{\mathbf{E}}_r). \end{aligned}$$

The momenta tensor is weakly symmetric if $\mathbf{V}_r, \mathbf{E}_\kappa$. The weak formulation then consists in finding $(e_w, e_\theta, \mathbf{E}_\kappa, e_\gamma)$ in $L \times V \times M \times D \times K$ so that

$$\begin{aligned} (v_w, \rho h \dot{e}_w) &= (v_w, \text{div} e_\gamma) + (v_w, f), & v_w &\in L, \\ (v_\theta, \rho h^3 / 12 \dot{e}_\theta) &= (v_\theta, \text{Div} \mathbf{E}_\kappa + e_\gamma) + (v_\theta, \tau), & v_\theta &\in V, \\ (\mathbf{V}_\kappa, \mathcal{D}^{-1} \dot{\mathbf{E}}_\kappa) &= -(\text{Div} \mathbf{V}_\kappa, e_\theta) - (\mathbf{V}_\kappa, \dot{\mathbf{E}}_r), & \mathbf{V}_\kappa &\in S, \\ (v_\gamma, \mathcal{C}^{-1} \dot{e}_\gamma) &= -(\text{div} v_\gamma, e_w) + (v_\gamma, e_\theta), & v_\gamma &\in D, \\ (\mathbf{V}_r, \dot{\mathbf{E}}_\kappa) &= 0 & \mathbf{V}_r &\in K, \end{aligned} \quad (15)$$

Consider a regular triangulation \mathcal{T}_h with elements T . The space of polynomials of order k on a mesh cell is denoted by P_k . The following space are used as discretization spaces

$$\begin{aligned} L_h^{\text{AFW}} &= \{w_h \in L \mid \forall T, w_h|_T \in P_k\}, \\ V_h^{\text{AFW}} &= \{\theta_h \in V \mid \forall T, \theta_h|_T \in (P_k)^2\}, \\ S_h^{\text{AFW}} &= \{(m_{11}, m_{12}) \in D \mid \forall T, (m_{11}, m_{12})|_T \in \text{BDM}_{k+1}\} \\ &\quad \cup \{(m_{21}, m_{22}) \in D \mid \forall T, (m_{21}, m_{22})|_T \in \text{BDM}_{k+1}\}, \\ D_h^{\text{AFW}} &= \{q_h \in D \mid \forall T, q_h|_T \in \text{RT}_{[k]}\}, \\ K_h^{\text{AFW}} &= \{\mathbf{R}_h \in K \mid \forall T, \mathbf{R}_h|_T \in R_k\}, \end{aligned}$$

where BDM is the Brezzi-Douglas-Marini element and RT the Raviart-Thomas element. A convergence analysis for the general elastodynamics problem with weak symmetry is detailed Arnold and Lee (2014). A convergence study for the wave equation with mixed finite elements is presented in Geveci (1988). Combining the result of the two the following error estimate are conjectured:

Conjecture 2. Assuming a smooth solution to problem (13), the following error estimates hold

$$\begin{aligned} \|e_w - e_w^h\|_{L^\infty L^2} &\lesssim h^{k+1}, & \|\mathbf{E}_\kappa - \mathbf{E}_\kappa^h\|_{L^\infty L^2} &\lesssim h^{k+1}, \\ \|e_\theta - e_\theta^h\|_{L^\infty L^2} &\lesssim h^{k+1}, & \|e_\gamma - e_\gamma^h\|_{L^\infty L^2} &\lesssim h^{k+1}, \\ \|\mathbf{E}_r - \mathbf{E}_r^h\|_{L^\infty L^2} &\lesssim h^{k+1}. \end{aligned} \quad (16)$$

3.3 The HHJ scheme for the Kirchhoff plate

For the Kirchhoff plate, the HHJ scheme can be used to obtain a structure preserving discretization. Given the non conforming nature of this scheme, it is necessary to first introduce the discrete functional spaces and state the problem directly in discrete form. The vertical displacement is approximated using continuous Lagrange polynomials.

$$W_h = \{w_h \in H_0^1(\Omega) \mid \forall T, w_h|_T \in P_{k+1}\}$$

The bending moment tensor is to be sought in the HHJ space

$$U_h = \{\mathbf{M}_h \in L^2(\Omega, \mathbb{S}) \mid \forall T, \mathbf{M}_h|_T \in P_k(\mathbb{S}),$$

\mathbf{M}_h is normal-normal continuous across elements\}.

The normal to normal continuous means that if two triangles T_1, T_2 share a common edge then $\mathbf{n}^\top(\mathbf{M}_h|_{T_1})\mathbf{n} = \mathbf{n}^\top(\mathbf{M}_h|_{T_2})\mathbf{n}$. Taking system (12) and multiplying the first equation by $v_w \in W_h$ and integrating over a triangle

$$\begin{aligned} -(v_w, \text{div Div} \mathbf{E}_\kappa)_T &= (\nabla v_w, \text{Div} = \mathbf{E}_\kappa)_T, \\ -(\nabla^2 v_w, \mathbf{E}_\kappa)_T &+ (\partial_n v_w, \mathbf{n}^\top \mathbf{E}_\kappa \mathbf{n})_{\partial T} + (\partial_s v_w, \mathbf{s}^\top \mathbf{E}_\kappa \mathbf{n})_{\partial T}, \end{aligned}$$

4. CONCLUSION

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