The Euler-Bernoulli beam in differential form

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1 Classical formulation

The Euler-Bernoulli beam model consists of one PDE, describing the vertical displacement along the beam length:

$$\rho A(x) \frac{\partial^2 w}{\partial t^2}(x, t) + \frac{\partial^2}{\partial x^2} \left(EI(x) \frac{\partial^2 w}{\partial x^2} \right) = 0, \quad x \in \Omega = \{0, L\},$$
 (1)

where w(x,t) is the transverse displacement of the beam. The coefficients $\rho(x)$, A(x)E(x) and I(x) are the mass density, cross section, Young's modulus of elasticity and the moment of inertia of a cross section. The energy variables are then chosen as follows:

$$\alpha_w = \rho A(x) \frac{\partial w}{\partial t}(x, t)$$
, Linear Momentum, $\alpha_\kappa = \frac{\partial^2 w}{\partial x^2}(x, t)$, Curvature. (2)

Those variables are collected in the vector $\boldsymbol{\alpha} = (\alpha_w, \alpha_\kappa)^T$, so that the Hamiltonian can be written as a quadratic functional in the energy variables:

$$H = \frac{1}{2} \int_{\Omega} \left\{ \frac{1}{\rho A} \alpha_w^2 + E I \alpha_\kappa^2 \right\} d\Omega \tag{3}$$

The co-energy variables are found by computing the variational derivative of the Hamiltonian:

$$e_w := \frac{\delta H}{\delta \alpha_w} = \frac{\partial w}{\partial t}(x, t),$$
 Vertical velocity,
 $e_\kappa := \frac{\delta H}{\delta \alpha_\kappa} = EI(x) \frac{\partial^2 w}{\partial x^2}(x, t),$ Flexural momentum. (4)

The underlying interconnection structure is then found to be:

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_w \\ \alpha_\kappa \end{pmatrix} = \begin{bmatrix} 0 & -\partial_{xx} \\ \partial_{xx} & 0 \end{bmatrix} \begin{pmatrix} e_w \\ e_\kappa \end{pmatrix}. \tag{5}$$

The power flow gives access to the boundary variables:

$$\dot{H} = \int_{\Omega} \{e_w \partial_t \alpha_w + e_\kappa \partial_t \alpha_\kappa\} d\Omega,$$

$$= \int_{\Omega} \{-e_w \partial_{xx} e_\kappa + e_\kappa \partial_{xx} e_w\} d\Omega, \quad \text{Integration by parts,}$$

$$= \int_{\partial\Omega} \{-e_w \partial_x e_\kappa + e_\kappa \partial_x e_w\} ds = \langle -e_w, \partial_x e_\kappa \rangle_{\partial\Omega} + \langle e_\kappa, \partial_x e_w \rangle_{\partial\Omega}$$
(6)

Since the system is of differential order two, two pairing appears, giving rise to four combination of uniform boundary causality

- First case $u_{\partial,1} = e_w$, $u_{\partial,2} = \partial_x e_w$, $y_{\partial,1} = -\partial_x e_\kappa$, $y_{\partial,2} = e_\kappa$. This imposes the vertical $e_w := \partial_t w$ and angular velocity $\partial_x e_w := \partial_{xt} w$ as boundary inputs. If the inputs are null a clamped boundary condition is obtained.
- Second case $u_{\partial,1} = e_w$, $u_{\partial,2} = e_\kappa$, $y_{\partial,1} = -\partial_x e_\kappa$, $y_{\partial,2} = \partial_x e_w$. This imposes the vertical velocity and flexural momentum $e_\kappa := EI\partial_{xx}w$ as boundary inputs. Zero inputs lead to a simply supported condition is found.
- Third case $u_{\partial,1} = -\partial_x e_{\kappa}$, $u_{\partial,2} = e_{\kappa}$, $y_{\partial,1} = e_w$, $y_{\partial,2} = \partial_x e_w$. This imposes the shear force $\partial_x e_{\kappa} := \partial_x (EI\partial_{xx}w)$ and flexural momentum as boundary inputs. Null inputs correspond to a free condition.
- Forth case $u_{\partial,1} = -\partial_x e_{\kappa}$, $u_{\partial,2} = \partial_x e_w$, $y_{\partial,1} = e_w$, $y_{\partial,2} = e_{\kappa}$. This imposes the shear force and angular velocity as boundary inputs.

2 Differential forms formulation

The co-energy now are 0-forms $e_w, e_\kappa \in \Lambda^0(\Omega)$ whereas the flows are 1-forms $f_w = \partial_t \alpha_w, f_\kappa = \partial_t \alpha_\kappa \in \Lambda^1(\Omega)$. To recast (5) using the exterior derivative, the Hodge star operator is needed.

$$*: \Lambda^k(\Omega) \to \Lambda^{n-k}(\Omega), \qquad \Omega \subset \mathbb{R}^n.$$
 (7)

For one dimensional domains $\Omega \subset \mathbb{R}$ and using Euclidian coordinates, this operator can be either used on 1-forms or 0-forms

$$*: \Lambda^{1}(\Omega) \longrightarrow \Lambda^{0}(\Omega),$$

$$f(x) dx \longrightarrow f(x)$$
(8)

or

$$*: \Lambda^0(\Omega) \longrightarrow \Lambda^1(\Omega),$$

$$f(x) \longrightarrow f(x) \, \mathrm{d}x$$
(9)

Then the equivalent system reads

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_w \\ \alpha_\kappa \end{pmatrix} = \begin{bmatrix} 0 & -d*d \\ d*d & 0 \end{bmatrix} \begin{pmatrix} e_w \\ e_\kappa \end{pmatrix}. \tag{10}$$

Proof 1 The operator $d*d: \Lambda^0(\Omega) \to \Lambda^1(\Omega)$ is a composition of operators that reads in Euclidean coordinates

$$d*de = d*(\frac{\partial e}{\partial x} dx), \qquad e \in \Lambda^{0}(\Omega)$$

$$= d(\frac{\partial e}{\partial x}),$$

$$= \frac{\partial^{2} e}{\partial x^{2}} dx \in \Lambda^{1}(\Omega)$$
(11)

The Hamiltonian energy is then

$$H = \frac{1}{2} \int_{\Omega} e_w \wedge \alpha_w + e_\kappa \wedge \alpha_\kappa \tag{12}$$

To find the appropriate power balance, consider the integration by parts formula for smooth differential forms $\lambda \in \Lambda^k(\Omega)$ and $\mu \in \Lambda^{n-k-1}(\Omega)$,

$$\langle d\lambda, \mu \rangle = \langle \operatorname{Tr} \lambda, \operatorname{Tr} \mu \rangle - (-1)^k \langle \lambda, d\mu \rangle$$
 (13)

For uni-dimensional domains n=1, and we take $\lambda \in \Lambda^0(\Omega)$ and $\mu \in \Lambda^0(\Omega)$, implying

$$\langle d\lambda, \, \mu \rangle = \langle \operatorname{Tr} \lambda, \, \operatorname{Tr} \mu \rangle - \langle \lambda, \, d\mu \rangle \,, \langle \lambda, \, d\mu \rangle = \langle \operatorname{Tr} \lambda, \, \operatorname{Tr} \mu \rangle - \langle d\lambda, \, \mu \rangle \,.$$
(14)

Then we can state

$$\langle -e_w, d(*de_\kappa) \rangle = \langle -\operatorname{Tr} e_w, \operatorname{Tr}(*de_\kappa) \rangle + \langle de_w, *de_\kappa \rangle.$$
 (15)

and

$$\langle e_{\kappa}, d(*de_{w}) \rangle = \langle \operatorname{Tr} e_{\kappa}, \operatorname{Tr}(*de_{w}) \rangle - \langle de_{\kappa}, *de_{w} \rangle,$$
 (16)

The power rate then reads

$$\dot{H} = \int_{\Omega} e_{w} \wedge \partial_{t} \alpha_{w} + e_{\kappa} \wedge \partial_{t} \alpha_{\kappa},$$

$$= \int_{\Omega} e_{w} \wedge \partial_{t} \alpha_{w} + e_{\kappa} \wedge \partial_{t} \alpha_{\kappa},$$

$$= \int_{\Omega} -e_{w} \wedge (d*de_{\kappa}) + e_{\kappa} \wedge (d*de_{w}), \quad \text{From (15), (16)}$$

$$= \langle -\operatorname{Tr} e_{w}, \operatorname{Tr}(*de_{\kappa}) \rangle + \langle de_{w}, *de_{\kappa} \rangle + \langle \operatorname{Tr} e_{\kappa}, \operatorname{Tr}(*de_{w}) \rangle - \langle de_{\kappa}, *de_{w} \rangle$$

The wedge product is such that for $\lambda \in \Lambda^k(\Omega)$ and $\mu \in \Lambda^l(\Omega)$ it holds

$$\lambda \wedge \mu = (-1)^{kl} \mu \wedge \lambda \tag{18}$$

Furthermore, the Hodge star is such that

$$(\alpha, \beta) := \langle \alpha, *\beta \rangle = \langle *\alpha, \beta \rangle = (\beta, \alpha), \qquad \alpha, \beta \in \Lambda^k(\Omega)$$
(19)

Then for $e_w, e_{\kappa} \in \Lambda^0$ it holds

$$\langle de_w, *de_\kappa \rangle = \langle *de_w, de_\kappa \rangle,$$

$$= \int_{\Omega} (*de_w) \wedge (de_\kappa),$$

$$= \int_{\Omega} (de_\kappa) \wedge (*de_w),$$

$$= \langle de_\kappa, *de_w \rangle$$
(20)

It can be then stated

$$\langle de_w, *de_\kappa \rangle - \langle de_\kappa, *de_w \rangle = 0 \tag{21}$$

The power balance is then

$$\dot{H} = \langle -\operatorname{Tr} e_w, \operatorname{Tr}(*de_\kappa) \rangle + \langle \operatorname{Tr} e_\kappa, \operatorname{Tr}(*de_w) \rangle$$
(22)

That in vector calculus notation reads

$$\dot{H} = \left\langle -\operatorname{Tr} e_w, \operatorname{Tr} \frac{\partial e_\kappa}{\partial x} \right\rangle + \left\langle \operatorname{Tr} e_\kappa, \operatorname{Tr} \frac{\partial e_w}{\partial x} \right\rangle = \left\langle -e_w, \partial_x e_\kappa \right\rangle_{\partial\Omega} + \left\langle e_\kappa, \partial_x e_w \right\rangle_{\partial\Omega}$$
 (23)

Completely equivalent to Eq. (6).

References

[1] P. Kotyczka. Numerical Methods for Distributed Parameter Port-Hamiltonian Systems. TUM University Press, 2019.