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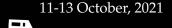
Mixed finite elements for port-Hamiltonian models of von Kármán beams

7th IFAC Conference on Lagrangian and Hamiltonian method for non linear control
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### Overview

- 1 Von-Kármán theory of thin beams in pH form
- 2 Numerical discretization
- Numerical convergence study

### Outline

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# Linear vs Von-Kármán plate theory

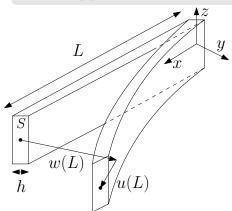


Geoometrical non-linearities allow describing bifurcations (i.e. buckling).

# The von-Kármán assumption

### Basic geometric assumption

Out of plane deflection comparable compared to the thickness:  $w/h = \mathcal{O}(1)$ .



Aspect ratio:  $\delta = h/L$ . The following terms are kept in the expansion:

$$w/L = \mathcal{O}(\delta),$$
  
 $u/L = \mathcal{O}(\delta^2),$ 

# Linear isotropic beams

The axial and bending behavior are uncoupled if  $w/h \ll 1$ :

### Axial displacement (wave equation)

$$\rho A \partial_{tt} u = \partial_x n_{xx}, \qquad n_{xx} = E A \partial_x u.$$

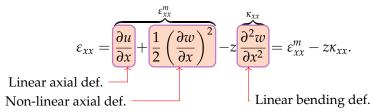
# Vertical displacement (Euler-Bernoulli equation)

$$\rho A \partial_{tt} w = -\partial_{xx} m_{xx}, \qquad m_{xx} = E I \partial_{xx} w.$$

For Von-Kármán beams the two are coupled.

### Stresses and Strains in Von-Kármán beams

#### Decomposition strain field



# Membrane and bending stresses (isotropic material)

$$n_{xx} = \int_{S} E \, dS \varepsilon_{xx}^{m} = EA \varepsilon_{xx}^{m}$$
 Axial stress resultant  $m_{xx} = -\int_{S} Ez^{2} \, dS \kappa_{xx} = EI\kappa_{xx}$ , Bending stress resultant

# Port-Hamiltonian Von-Kármán beams

#### **Dynamics**

$$\rho A \partial_{tt} u = \partial_x \overline{n_{xx}}, 
\rho A \partial_{tt} w = -\partial_{xx}^2 m_{xx} + \partial_x (\overline{n_{xx}} \partial_x w),$$

#### Energy and coenergy variables

Same selection as usual:

$$\alpha_u = \rho A \partial_t u, \qquad \alpha_\varepsilon = \varepsilon_{xx}^m, 
\alpha_w = \rho A \partial_t w, \qquad \alpha_\kappa = \kappa_{xx}.$$

Linear constitutive relation  $e = Q\alpha$  with

$$Q = \text{Diag} [\rho A, C_a, \rho A, C_b]^{-1}, \quad C_a = (EA)^{-1}, \quad C_b = (EI)^{-1},$$

where  $C_a$ ,  $C_b$  are the axial and bending compliances.

# The port-Hamiltonian realization

To close the system, variable w has to be accessible.

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_u \\ \alpha_\varepsilon \\ \alpha_w \\ \alpha_k \\ w \end{pmatrix} = \underbrace{\begin{bmatrix} 0 & \partial_x & 0 & 0 & 0 \\ \partial_x & 0 & \boxed{(\partial_x w) \, \partial_x} & 0 & 0 \\ 0 & \boxed{\partial_x (\cdot \, \partial_x w)} & 0 & -\partial_{xx}^2 & -1 \\ 0 & 0 & \partial_{xx}^2 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}}_{\mathcal{J}} \begin{pmatrix} e_u \\ e_\varepsilon \\ e_w \\ e_k \\ \delta_w H \end{pmatrix}.$$

#### Proposition

*The operator*  $\mathcal{J}$  *is formally skew-adjoint.* 

The construction is analogous for plate problems<sup>1</sup>.

<sup>1</sup>Andrea Brugnoli and Denis Matignon (2022). "A port-Hamiltonian formulation for the full von-Kàrmàn plate model". In: *10th European Nonlinear Dynamics Conference (ENOC)*.

# Energy rate and boundary conditions

### Proposition

The energy rate reads

$$\dot{H} = \langle e_u, e_{\varepsilon} \rangle_{\partial \Omega} + \langle e_w, e_{\varepsilon} \partial_x w - \partial_x e_{\kappa} \rangle_{\partial \Omega} + \langle \partial_x e_w, e_{\kappa} \rangle_{\partial \Omega}.$$

with  $\Omega = [0, L]$  and  $\langle \cdot, \cdot \rangle_{\Omega}$  the  $L^2$  inner product.

Boundary conditions classification

BCs	Traction	Bending	
Dirichlet BCs.	$e_u _0^L$	$e_w _0^L$	$\partial_x e_w _0^L$
Neumann BCs.	$ e_{\varepsilon} _{0}^{L}$	$ e_{\varepsilon}\partial_{x}w-\partial_{x}e_{\kappa} _{0}^{L}$	$ e_{\kappa} _{0}^{L}$

Same bcs. as in Puel and Tucsnak 1996 for global existence and uniqueness result.

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# Pure coenergy formulation

# Coenergy formulation for linear constitutive equations

If the Q operator is inverted:

$$\begin{pmatrix} \rho A \dot{e}_u \\ C_a \dot{e}_\varepsilon \\ \rho A \dot{e}_w \\ C_b \dot{e}_\kappa \\ \dot{w} \end{pmatrix} = \begin{bmatrix} 0 & \partial_x & 0 & 0 & 0 \\ \partial_x & 0 & \partial_x w \, \partial_x & 0 & 0 \\ 0 & \partial_x (\cdot \, \partial_x w) & 0 & -\partial_{xx}^2 & -1 \\ 0 & 0 & \partial_{xx}^2 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix} \begin{pmatrix} e_u \\ e_\varepsilon \\ e_w \\ e_\kappa \\ \delta_w H \end{pmatrix}.$$

In the sequel, the quantity  $\delta_w H$  is removed as no displacement dependent potential (e.g. gravity) is considered

#### Weak formulation

Introducing test functions and integrating by parts the first, third and fourth, we get the weak formulation.

#### Weak formulation

Find 
$$e = (e_u, e_\varepsilon, e_w, e_\kappa) \in H^1 \times L^2 \times H^1 \times H^1$$
 such that

$$m(\boldsymbol{\psi}, \partial_t \boldsymbol{e}) = j_w(\boldsymbol{\psi}, \boldsymbol{e}) + b(\boldsymbol{\psi}) \mathbf{u},$$
  
 $\partial_t w = \begin{bmatrix} 0 & 0 & 1 & 0 \end{bmatrix} \boldsymbol{e},$   
 $\mathbf{y} = b^\top(\boldsymbol{e}),$ 

$$\forall \boldsymbol{\psi} \in H^1 \times L^2 \times H^1 \times H^1 \times H^1 := X$$

- ► *m* is a symmetric, coercive, bilinear form;
- $ightharpoonup j_w$  is a skew-symmetric bilinear form modulated by w;
- ▶  $b: X \to \mathbb{R}^6$  vector-valued functional.

# Mixed finite element construction<sup>2</sup>

Crucial concept: Hilbert complex  $H^1 \xrightarrow{\partial_x} L^2$ .

# Key requirements for mixed Galerkin approximation

- ► The subspaces  $H_h^1 \subset H^1$ ,  $L_h^2 \subset L^2$  form a subcomplex  $H_h^1 \xrightarrow{\partial_x} L_h^2$  (i.e.  $\partial_x H_h^1 \subset L_h^2$ ).
- ▶ they admit bounded linear projections  $\pi_h^{H^1}: H^1 \to H_h^1$  and  $\pi_h^{L^2}: L^2 \to L_h^2$  which commute with  $\partial_x$ :  $\partial_x \pi_h^{H^1} = \pi_h^{L^2} \partial_x$ .

Satisfied for  $CG_k \xrightarrow{\partial_x} DG_{k-1}$ ,  $k \ge 1$  with

$$CG_k = \{u \in H^1(\Omega) | \forall \text{edge in the mesh}, \ u|_{\text{edge}} \in P_k\},$$

$$DG_{k-1} = \{u \in L^2(\Omega) | \forall \text{edge in the mesh}, \ u|_{\text{edge}} \in P_{k-1}\},$$

where  $P_k$  space of polynomials of degree k.

<sup>&</sup>lt;sup>2</sup>Arnold, Falk, and Winther 2006.

# Finite element choice and final system

For the proposed weak formulation, the FE spaces become

$$e_u^h \in CG_{2k-1}, \qquad e_\varepsilon^h \in DG_{2k-2}, \qquad (e_w^h, \ e_\kappa^h, \ w^h) \in CG_k, \quad k \geq 1.$$

Implications:

- ► Subcomplex property for the linear part:  $\partial_x CG_{k-1} \subset DG_{2k-2}$ .
- ► The non linear part respects

$$\partial_x CG_k \cdot \partial_x CG_k \subset DG_{2k-2}$$
.

# Finite dimensional system (Galerkin projection)

$$\begin{aligned} \mathbf{M}\dot{\mathbf{e}} &= \mathbf{J}(\mathbf{w})\mathbf{e} + \mathbf{B}\mathbf{u},\\ \dot{\mathbf{w}} &= \begin{bmatrix} \mathbf{0} & \mathbf{0} & \mathbf{I} & \mathbf{0} \end{bmatrix}\mathbf{e},\\ \mathbf{y} &= \mathbf{B}^{\top}\mathbf{e}. \end{aligned}$$

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### Manufactured solution

The following manufactured solution is considered

$$u^{\text{ex}} = x^3 [1 - (x/L)^3] \sin(2\pi t), \qquad w^{\text{ex}} = \sin(\pi x/L) \sin(2\pi t),$$

together with the boundary conditions

$$u|_0^L = 0$$
,  $w|_0^L = 0$ ,  $m_{xx}|_0^L = 0$ .

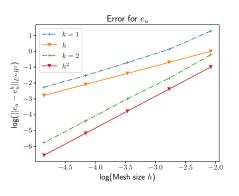
A Crank-Nicholson scheme is used for time integration.

#### Convergence measure

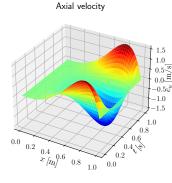
The discrete time-space norm  $L^{\infty}_{\Delta t}(\mathcal{X})(\mathcal{X} = H^1 \text{ or } L^2)$  is used to measure convergence

$$||\cdot||_{L^{\infty}(\mathcal{X})} \approx ||\cdot||_{L^{\infty}_{\Delta t}(\mathcal{X})} = \max_{t \in t_i} ||\cdot||_{\mathcal{X}},$$

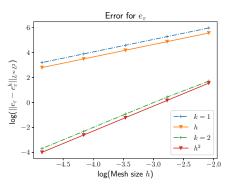
where  $t_i$  are the discrete simulation instants.



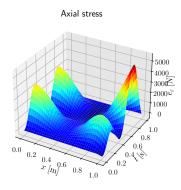
 $L^{\infty}_{\Delta t}(H^1)$  error for  $e_u$ .



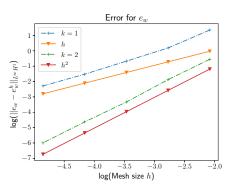
$$e_u^h (h = 2^{-5}, k = 2).$$



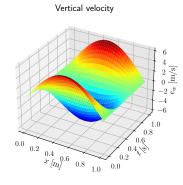
 $L^{\infty}_{\Delta t}(L^2)$  error for  $e_{\varepsilon}$ .



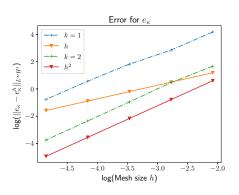
 $e_{\varepsilon}^{h}$  for  $h = 2^{-5}, k = 2$ .



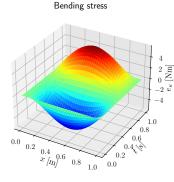
 $L^{\infty}_{\Delta t}(H^1)$  error for  $e_w$ .



 $e_w^h$  for  $h = 2^{-5}$ , k = 2.



 $L^{\infty}_{\Delta t}(H^1)$  error for  $e_{\kappa}$ .



 $e_{\kappa}^{h}$  for  $h = 2^{-5}$ , k = 2.

#### Conclusion and Outlook

- ► First step into pH non linear mechanics. The geometrical non linearities belong to the interconnection operator.
- ▶ Natural extension for the 2D case (fancier FE).
- ► Can be used to study more complex phenomena. The discretization method guarantees energy conservation.

#### References I



Arnold, Douglas N., Richard S. Falk, and Ragnar Winther (2006). "Finite element exterior calculus, homological techniques, and applications". In: *Acta Numerica* 15, 1–155.



Brugnoli, Andrea and Denis Matignon (2022). "A port-Hamiltonian formulation for the full von-Kàrmàn plate model". In: 10th European Nonlinear Dynamics Conference (ENOC).



Puel, J.P. and M. Tucsnak (1996). "Global existence for the full von Kármán system". In: Applied Mathematics and Optimization 34.2, pp. 139–160.

# Port-Hamiltonian von-Kármán plates

$$\frac{\partial}{\partial t} \begin{pmatrix} \alpha_u \\ A_{\varepsilon} \\ w \\ \alpha_w \\ A_{\kappa} \end{pmatrix} = \underbrace{\begin{bmatrix} \mathbf{0} & \mathrm{Div} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathrm{Grad} & \mathbf{0} & \mathbf{0} & -\mathcal{C}(w)^* & \mathbf{0} \\ 0 & 0 & 0 & 1 & 0 \\ 0 & \mathcal{C}(w) & -1 & 0 & -\mathrm{div}\,\mathrm{Div} \\ \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathrm{Grad}\,\mathrm{grad} & \mathbf{0} \end{bmatrix}}_{\mathcal{J}} \begin{pmatrix} \delta_{\alpha_u} H \\ \delta_{A_{\varepsilon}} H \\ \delta_{\alpha_w} H \\ \delta_{A_{\kappa}} H \end{pmatrix},$$

where

$$C(w)(T) = \operatorname{div}(T\operatorname{grad} w),$$

$$C(w)^*(\cdot) = -\frac{1}{2} \left[ \operatorname{grad}(\cdot) \otimes \operatorname{grad}(w) + \operatorname{grad}(w) \otimes \operatorname{grad}(\cdot) \right].$$