# 1 Constants and Dimensions

Symbol	Value	Unit	Description
$\overline{g}$	9.81	$\frac{m}{s^2}$	acceleration of gravity
ho	1025	$\frac{\frac{m}{s^2}}{\frac{kg}{m^3}}$	density of water
L	2.0	$\overset{m}{m}$	length of hull
B	1.08	m	beam of hull
m	55.0	kg	mass of hull
$r_g^{hull}$	$\begin{bmatrix} 0.2 & 0 & -0.2 \end{bmatrix}^T$	m	CG of hull
${R}_{44}$	$0.4 \cdot B$	m	radius of gyration
$R_{55}$	$0.25 \cdot L$	m	radius of gyration
$R_{66}$	$0.25 \cdot L$	m	radius of gyration
$T_{yaw}$	1	s	time constant in yaw
$U_{max}$	6	knot	max forward speed
$B_{pont}$	0.25	m	beam of one pontoon
$y_{pont}$	0.395	m	distance from centerline to waterline area center
$Cw_{pont}$	0.75	_	waterline area coefficient
$Cb_{pont}$	0.4	_	block coefficient

Waterline area of one pontoon

$$Aw_{pont} = Cw_{pont}LB_{pont} \tag{1}$$

## 2 Skew symetric matrix

$$S\left(\begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}\right) = \begin{bmatrix} 0 & -a_3 & a_2 \\ a_3 & 0 & -a_1 \\ -a_2 & a_1 & 0 \end{bmatrix}$$
 (2)

## 3 Kinetics

$$\nu_1 = \begin{bmatrix} u & v & w \end{bmatrix}^T \qquad \qquad \nu_2 = \begin{bmatrix} p & q & r \end{bmatrix}^T \tag{3}$$

Inertia matrix of hull in CG

$$I_g^{CG} = m \cdot \text{diag}\left[R_{44}^2, R_{55}^2, R_{66}^2\right] \tag{4}$$

CG location corrected for payload

$$r_g = \frac{m \cdot r_g^{hull} + m_p \cdot r_p}{m + mp} \tag{5}$$

Inertia matrix of hull and payload in CO

$$I_q = I_q^{CG} - m \cdot S(r_q)^2 - m_p \cdot S(r_p)^2$$
(6)

$$M_{RB}^{CG} = \begin{bmatrix} (m+m_p)I & 0\\ 0 & I_g \end{bmatrix} \qquad C_{RB}^{CG}(\nu_2) = \begin{bmatrix} (m+m_p)S(\nu_2) & 0\\ 0 & -S(I_g\nu_2) \end{bmatrix}$$
 (7)

Transform  $M_{RB}$  and  $C_{RB}$  from the  $C_G$  to the  $C_O$ 

$$H = \begin{bmatrix} I & S(r_g)^T \\ 0 & I \end{bmatrix} \tag{8}$$

$$M_{RB} = H^T M_{RB}^{CG} H (9)$$

$$C_{RB}(\nu_2) = H^T C_{RB}^{CG}(\nu_2) H \tag{10}$$

(11)

## 4 Relative velocity

Water current surge and sway velocity

$$u_c = v_{cur}\cos(\beta_{cur} - \psi) \tag{12}$$

$$v_c = v_{cur}\sin(\beta_{cur} - \psi) \tag{13}$$

Where  $v_{cur}$  is the current velocity,  $\beta_{cur}$  is the current direction in rad and  $\psi$  is the yaw of the vessel. Relative velocity vector

$$\nu_r = \nu - \begin{bmatrix} u_c & v_c & 0 & 0 & 0 & 0 \end{bmatrix}^T \tag{14}$$

In the case of no current we have

$$\nu_r = \nu \tag{15}$$

### 5 Hydrodynamics

Hydrodynamic added mass

$$M_A = \begin{bmatrix} mI & 0\\ 0 & I_q \end{bmatrix} M_{A,coef} \tag{16}$$

$$M_{A,coef} = \text{diag} ([0.1 \ 1.5 \ 1.0 \ 0.2 \ 0.8 \ 1.7])$$
 (17)

$$C_A(\nu_{r,1},\nu_{r,2}) = \begin{bmatrix} 0 & -S(M_{A,11}\nu_{r,1} + M_{A,12}\nu_{r,2}) \\ -S(M_{A,11}\nu_{r,1} + M_{A,12}\nu_{r,2}) & -S(M_{A,21}\nu_{r,1} + M_{A,22}\nu_{r,2}) \end{bmatrix}$$
(18)

$$= \begin{bmatrix} 0 & -S(0.1 \cdot m\nu_{r,1}) \\ -S(0.1 \cdot m\nu_{r,1}) & -S(1.5 \cdot m\nu_{r,2}) \end{bmatrix}$$
 (19)

System mass and Coriolis-centripetal matrices

$$M = M_{RB} + M_A \tag{20}$$

$$C = C_{RB}(\nu_2) + C_A(\nu_{r,1}, \nu_{r,2}) \tag{21}$$

### 6 Hydro statics

Water volume displacement

$$\nabla = \frac{m + m_p}{\rho} \tag{22}$$

Draft

$$T = \frac{\nabla}{2Cb_{pont}B_{pont}L} \tag{23}$$

$$KB = \frac{1}{3} (5\frac{T}{2} - \frac{\nabla}{2LB_{nont}});$$
 (24)

$$I_T = \frac{2}{12} L B_{pont}^3 \frac{6 \cdot C w_{pont}^3}{(1 + C w_{pont})(1 + 2C w_{nont})} + 2 \cdot A w_{pont} y_{pont}^2$$
 (25)

$$I_L = \frac{0.8 \cdot 2}{12} B_{pont} L^3 \tag{26}$$

$$GM_T = KB + \frac{I_T}{\nabla} - T + r_{g,z} \tag{27}$$

$$GM_L = KB + \frac{I_L}{\nabla} - T + r_{g,z} \tag{28}$$

(29)

$$G = H^T G_{CF} H (31)$$

$$\omega_3 = \sqrt{G_{33}/M_{33}} \tag{32}$$

$$\omega_4 = \sqrt{G_{44}/M_{44}} \tag{33}$$

$$\omega_5 = \sqrt{G_{55}/M_{55}} \tag{34}$$

## 7 Linear Damping

$$h(r) = \begin{bmatrix} -24.4 \frac{g}{U_{max}} \\ 0 \\ -2 \cdot 0.3 \cdot \omega_3 M_{33} \\ -2 \cdot 0.2 \cdot \omega_4 M_{44} \\ -2 \cdot 0.4 \cdot \omega_5 M_{55} \\ \frac{-M_{66}}{T_{yaw}} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -\frac{M_{66}}{T_{yaw}} 10 \cdot abs(r) \end{bmatrix}$$
(35)

The matrix to the right includes non-linear damping for yaw

$$\tau_{damp}(r) = h(r) \bullet \nu_r \tag{36}$$

### 8 Crossflow Drag

The crossflow is computed using strip theory and is a function of  $\nu_r$ 

$$\tau_{cf} = \begin{bmatrix} 0 \\ Yh \\ 0 \\ 0 \\ 0 \\ Nh \end{bmatrix}$$
(37)

 $\tau_{cf}$  Has components only in v and r

#### 9 Ballast

$$g_0 = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ trim\_moment \\ 0 \end{bmatrix}$$

$$(38)$$

 $g_0$  represents a dynamic torque in q (pitch)

#### 10 Transformation

$$R = R_z R_y R_x = \begin{bmatrix} \cos(\phi) & -\sin(\phi) & 0 \\ \sin(\phi) & \cos(\phi) & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos(\theta) & 0 & \sin(\theta) \\ 0 & 1 & 0 \\ -\sin(\theta) & \cos(\theta) \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\phi) & -\sin(\phi) \\ 0 & \sin(\phi) & \cos(\phi) \end{bmatrix}$$
(39)

$$T = \begin{bmatrix} 1 & \sin(\phi)\tan(\theta) & \cos(\phi)\tan(\theta) \\ 0 & \cos(\phi) & -\sin(\phi) \\ 0 & \frac{\sin(\phi)}{\cos(\theta)} & \frac{\cos(\phi)}{\cos(\theta)} \end{bmatrix}$$
(40)

$$J = \begin{bmatrix} R & 0 \\ 0 & T \end{bmatrix} \tag{41}$$

#### 11 State derivative

$$M\dot{\nu} + C\nu_r + G\eta + g_0 = \tau + \tau_{damp} + \tau_{cf} \tag{42}$$

$$\dot{x} = \begin{bmatrix} \dot{\nu} \\ \dot{\eta} \end{bmatrix} = \begin{bmatrix} M^{-1}(\tau + \tau_{damp} + \tau_{cf} - C\nu_r - G\eta - g_0) \\ J\nu \end{bmatrix}$$
(43)

$$M = H^T M_{RB}^{CG} H + M_A (44)$$

$$= \begin{bmatrix} I & 0 \\ S(r_g) & I \end{bmatrix} \begin{bmatrix} (m+m_p)I & 0 \\ 0 & I_g \end{bmatrix} \begin{bmatrix} I & S(r_g)^T \\ 0 & I \end{bmatrix} + \begin{bmatrix} mI & 0 \\ 0 & I_g \end{bmatrix} M_{A,coef}$$
(45)

$$= (m+m_p) \begin{bmatrix} I & S(r_g)^T \\ S(r_g) & S(r_g)I_gS(r_g)^T \end{bmatrix} + \begin{bmatrix} mI & 0 \\ 0 & I_g \end{bmatrix} M_{A,coef}$$

$$(46)$$

$$C = H^{T}C_{RB}^{CG}(\nu_{2})H + C_{A}(\nu_{r,1}, \nu_{r,2})$$

$$= \begin{bmatrix} I & 0 \\ S(r_{g}) & I \end{bmatrix} \begin{bmatrix} (m+m_{p})S(\nu_{2}) & 0 \\ 0 & -S(I_{g}\nu_{2}) \end{bmatrix} \begin{bmatrix} I & S(r_{g})^{T} \\ 0 & I \end{bmatrix} + \begin{bmatrix} 0 & -S(0.1 \cdot m\nu_{r,1}) \\ -S(0.1 \cdot m\nu_{r,1}) & -S(1.5 \cdot m\nu_{r,2}) \end{bmatrix}$$

$$(47)$$

$$= (m + m_p) \begin{bmatrix} S(\nu_2) & S(\nu_2)S(r_g)^T \\ S(r_g)S(\nu_2) & -S(r_g)S(I_g\nu_2)S(r_g)^T \end{bmatrix} + \begin{bmatrix} 0 & -S(0.1 \cdot m\nu_{r,1}) \\ -S(0.1 \cdot m\nu_{r,1}) & -S(1.5 \cdot m\nu_{r,2}) \end{bmatrix}$$
(48)

(49)