run	$\boldsymbol{M}_{\text{tar}}$	$\boldsymbol{M}_{\text{imp}}$	θ	V _{imp}	impactor	$\delta f_{_{\!$	$f_{_{\!$	M _{moon}	$L_{_{\rm D}}$	$M_{_{\mathrm{D}}}[M_{_{\mathrm{L}}}]$			$\mathcal{L}_{ ext{bound}}$	L L imp	
	$[M_{E}]$	$[M_{E}]$	[°]	[v _{esc}]	[wt% Fe/SiO ₂ /H ₂ O]			$[M_{_{ m L}}]$	$[L_{_{E\text{-}M}}]$	SiO ₂	Fe	$H_{2}O$	$[L_{_{E\text{-}M}}]$	$[L_{E-M}]$	
cA01	0.90	0.10	30.0	1.35		-18%	77%	0.03	0.02	0.12	0.00	0.00	0.67	1.04	
cA02	0.90	0.10	32.5	1.30		-26%	69%	0.05	0.02	0.13	0.01	0.00	0.70	1.07	
cA03	0.90	0.10	32.5	1.50		-35%	61%	0.10	0.03	0.18	0.02	0.00	0.57	1.24	
cA04	0.90	0.10	35.0	1.30		-36%	60%	0.16	0.05	0.23	0.06	0.00	0.68	1.14	
cA05	0.90	0.10	35.0	1.35	30 / 70 / 0	-36%	61%	0.20	0.06	0.26	0.07	0.00	0.64	1.19	
cA06	0.90	0.10	35.0	2.00	30 / 70 / 0	-31%	68%	0.02	0.01	0.09	0.01	0.00	0.33	1.76	
cA07	0.90	0.10	45.0	1.00		-49%	46%	0.53	0.14	0.81	0.00	0.00	0.95	1.08	
cA08	0.90	0.10	48.0	1.00		-66%	31%	1.50	0.28	1.27	0.00	0.00	0.97	1.14	
cA09	0.90	0.10	50.0	1.00		-66%	32%	0.68	0.15	0.80	0.02	0.00	0.94	1.18	
cA10	0.90	0.10	53.0	1.00		-75%	23%	0.89	0.21	0.96	0.15	0.00	0.96	1.23	
cB01	0.90	0.15	32.5	1.15		-41%	53%	0.10	0.03	0.23	0.00	0.00	1.06	1.49	
cB02	0.90	0.15	35.0	1.15	20 / 70 / 0	-35%	58%	0.23	0.06	0.37	0.01	0.00	1.10	1.59	
cB03	0.90	0.15	35.0	1.20	30 / 70 / 0	-33%	60%	0.53	0.15	0.86	0.05	0.00	1.06	1.66	
cB04	0.90	0.15	40.0	1.10		-41%	53%	1.20	0.27	1.41	0.04	0.00	1.16	1.71	
cC01	0.90	0.20	30.0	1.30		-34%	57%	0.52	0.16	1.00	0.06	0.00	1.20	2.18	
cC02	0.90	0.20	32.5	1.20		-30%	61%	0.90	0.27	1.63	0.03	0.00	1.40	2.16	
cC03	0.90	0.20	32.5	1.25		-37%	54%	1.01	0.27	1.51	0.06	0.00	1.27	2.25	
cC04	0.90	0.20	32.5	1.30	30 / 70 / 0	-32%	58%	1.12	0.27	1.39	0.14	0.00	1.30	2.34	
cC05	0.90	0.20	35.0	1.15	30 / 70 / 0	-36%	54%	1.32	0.35	1.98	0.03	0.00	1.46	2.21	
cC06	0.90	0.20	35.0	1.20		-35%	56%	1.24	0.29	1.60	0.01	0.00	1.28	2.31	
cC07	0.90	0.20	45.0	1.00		-54%	39%	1.30	0.31	1.61	0.06	0.00	1.74	2.37	
cC08	0.90	0.20	50.0	1.00		-76%	20%	3.16	0.65	2.84	0.37	0.00	2.02	2.57	
fA01	0.90	0.20	30.0	1.30		-28%	64%	0.95	0.29	1.50	0.37	0.00	1.40	2.16	
fA02	0.90	0.20	35.0	1.20		-28%	63%	1.18	0.26	1.20	0.13	0.00	1.55	2.28	
fA03	0.90	0.20	32.5	1.25	50 / 50 / 0	-31%	62%	1.16	0.29	1.41	0.25	0.00	1.48	2.23	
fA04	0.90	0.20	35.0	1.25		-24%	67%	1.33	0.29	1.22	0.26	0.00	1.57	2.38	
fA05	0.90	0.20	40.0	1.10		-33%	59%	1.17	0.29	1.56	0.09	0.00	1.68	2.34	
fB01	0.90	0.10	30.0	1.35		-23%	74%	0.03	0.02	0.08	0.05	0.00	0.74	1.01	
fB02	0.90	0.10	35.0	1.30		-28%	69%	0.38	0.11	0.37	0.30	0.00	0.78	1.12	
fB03	0.90	0.10	40.0	1.10		-25%	73%	0.31	0.10	0.46	0.16	0.00	0.85	1.06	
fB04	0.90	0.10	45.0	1.00	70 / 30 / 0	-19%	78%	0.39	0.11	0.59	0.12	0.00	0.89	1.06	
fB05	0.90	0.10	48.0	1.00		-33%	64%	0.72	0.18	0.51	0.54	0.00	0.97	1.12	
fB06	0.90	0.20	30.0	1.30		-19%	75%	1.48	0.37	1.40	0.68	0.00	1.47	2.13	
fB07	0.90	0.20	30.0	1.35		-18%	76%	1.63	0.38	1.38	0.71	0.00	1.48	2.21	

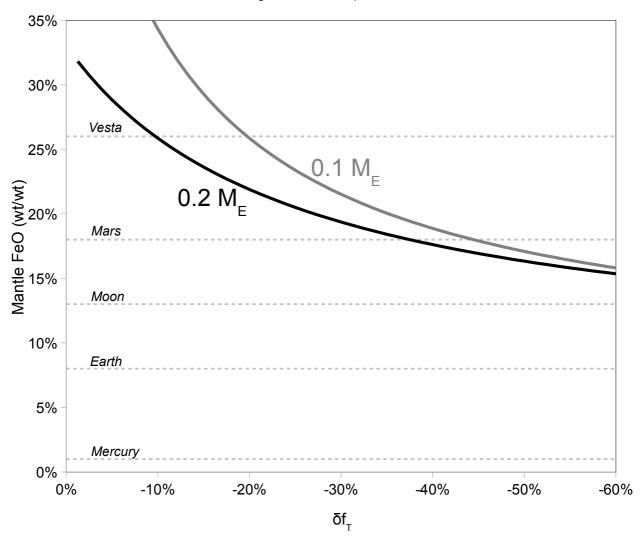
SOM Table 1.: Simulation results. Note that $L_{\scriptscriptstyle D}$ and $M_{\scriptscriptstyle moon}$ estimated according to (Kokubo 2000) considers all disk material, including any present iron and water ice.

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{[L_{E-M}]}{1.35}$
iA01 0.90 0.20 15.0 1.50 -6% 84% -0.13 0.02 0.21 0.00 0.08 0.75	
iA02 0.90 0.20 25.0 1.30 -26% 66% 0.17 0.09 0.47 0.00 0.19 1.12	1.92
iA03 0.90 0.20 25.0 1.35 -23% 69% 0.15 0.08 0.41 0.00 0.18 1.08	1.99
iA04 0.90 0.20 25.0 1.50 -16% 76% 0.07 0.07 0.47 0.00 0.16 0.92	2.21
iA05 0.90 0.20 25.0 1.75 -24% 71% 0.17 0.07 0.38 0.01 0.11 0.60	2.58
iA06 0.90 0.20 30.0 1.00 -20% 71% 0.20 0.10 0.20 0.00 0.52 1.28	1.74
iA07 0.90 0.20 30.0 1.15 -52% 43% 0.76 0.21 0.62 0.00 0.65 1.36	2.01
iA08 0.90 0.20 30.0 1.20 -62% 34% 0.91 0.23 0.75 0.00 0.59 1.35	2.09
iA09 0.90 0.20 30.0 1.25 -20% 72% 0.36 0.11 0.33 0.00 0.35 1.15	2.18
iA10 0.90 0.20 30.0 1.30 -10% 81% 0.60 0.17 0.73 0.00 0.33 1.12	2.27
iA11 0.90 0.20 30.0 1.32 -14% 78% 0.26 0.09 0.26 0.00 0.37 1.00	2.30
iA12 0.90 0.20 30.0 1.35 -10% 82% 0.32 0.11 0.45 0.00 0.30 0.96	2.36
iA13 0.90 0.20 32.5 1.25 -15% 77% 0.71 0.19 0.56 0.00 0.56 1.01	2.34
iA14 0.90 0.20 32.5 1.30	2.44
iA15 0.90 0.20 32.5 1.35 137 337 30 -54% 42% 2.19 0.45 1.50 0.26 0.48 1.06	2.53
iA16 0.90 0.20 35.0 1.00 -60% 36% 1.35 0.32 0.70 0.00 1.03 1.51	2.00
iA17 0.90 0.20 35.0 1.10 -30% 63% 1.61 0.37 0.92 0.00 1.07 1.42	2.20
iA18 0.90 0.20 35.0 1.15 -60% 36% 3.03 0.59 1.50 0.00 1.23 1.57	2.30
iA19 0.90 0.20 35.0 1.20 -60% 36% 2.89 0.52 1.23 0.00 0.95 1.55	2.40
iA20 0.90 0.20 35.0 1.25 -56% 40% 2.26 0.50 1.73 0.16 0.74 1.23	2.50
iA21 0.90 0.20 35.0 1.30 3% 98% -0.01 0.00 0.02 0.00 0.02 0.48	2.60
iA22 0.90 0.20 40.0 1.15 -70% 27% 8.14 1.39 2.80 0.80 1.97 2.03	2.58
iA23 0.90 0.20 45.0 1.00 -67% 30% 2.04 0.49 1.28 0.01 1.39 1.71	2.47
iA24 0.90 0.20 45.0 1.15 -61% 37% 0.09 0.04 0.09 0.00 0.19 1.14	2.84
iA25 0.90 0.20 45.0 1.20 -1% 97% 0.01 0.01 0.03 0.00 0.05 0.35	2.96
iA26 0.90 0.20 45.0 1.25 -10% 89% 0.01 0.01 0.03 0.00 0.04 0.35	3.08
iA27 0.90 0.20 60.0 1.00 -73% 24% 0.96 0.28 0.75 0.01 0.99 1.41	3.02
iA28 0.90 0.20 60.0 1.15 0% 100% 0.00 0.00 0.01 0.00 0.02 0.16	3.48

SOM Table 1. (continued)

Impactor Mantle FeO

vs. target material depletion in disk



SOM Figure 1: The FeO content of the impactor's mantle (in wt%), if the Moon's content of 13wt% FeO is a mixture of Earth mantle (fixed at 8wt% FeO) and impactor mantle material, for an impactor of 0.2 (black line) and 0.1 (gray line) Earth masses. Note that an impactor with FeO = 18wt% (equal to Mars) yields a δf_T of -35% to -40%, a typical outcome of simulations as presented here. The mantle compositions of Mercury, Earth, Moon, Mars and Vesta are shown for comparison (Righter et al., 2006).