

ATS 421/521

Climate Modeling

Spring 2013

Lecture 16

- Ice Sheets (Oerlemans, 1981)
- Ocean Biogeochemistry

May 20, 2013

Reading

- Wednesday: textbook chapter 3.3.4 (Land Surface)
- Friday: Friedlingstein et al. (2006)

HW vs Project

- Ideas ?
- Juan: Ocean Circulation LGM and piControl in CMIP5 models
- Student presentations on June 6th

Ice Sheets

Oerlemans (1981)

J. Oerlemans (1981) developed the following simple vertically-integrated model of a continental ice sheet.

7.2.1 *Perfectly plastic solution for an ice sheet on a flat base*

Assumptions:

- flow is quasi-two dimensional
- normal stress deviations are small
- the surface slope ($s < 0.1$) is small

Balance of forces: $\frac{\partial \tau_{xz}}{\partial z} = \rho g s \Rightarrow \tau_{xz} = \rho g (H - z) s$

vertical gradient of
the shear stress pressure
gradient

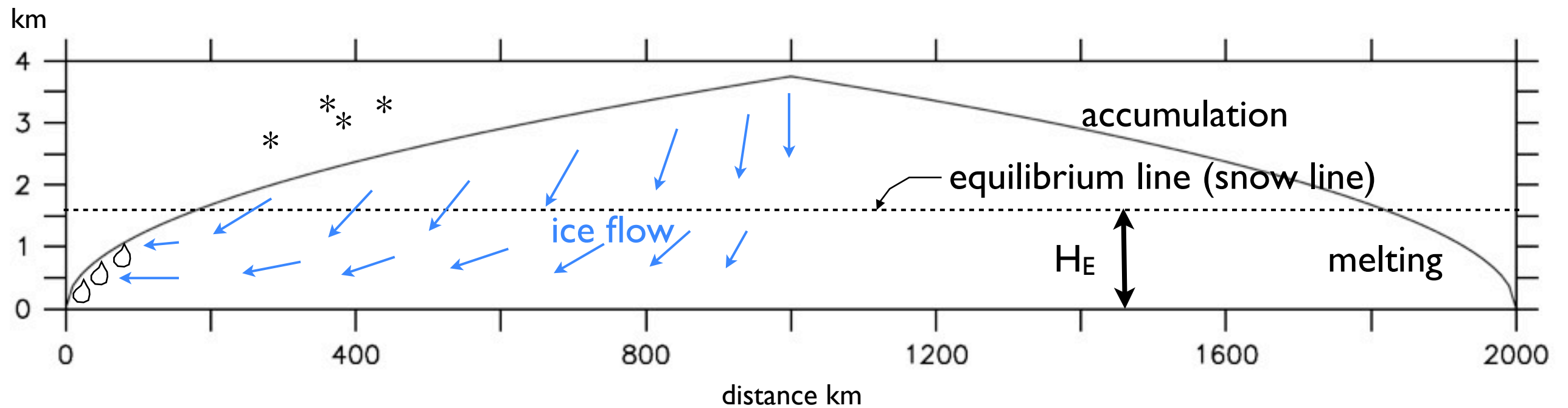
Stress at base: $\Rightarrow \tau_b = \rho g H s = \rho g H \frac{\partial H}{\partial x} = \text{const.} = \tau_0$

$$\Rightarrow \frac{1}{2} \frac{\partial H^2}{\partial x} = \frac{\tau_0}{\rho g} \Rightarrow H = \sqrt{\frac{2\tau_0}{\rho g} x} = \Lambda \sqrt{x} \quad (7.3)$$

$[3.5 \text{ m}^{1/2} < \Lambda < 4 \text{ m}^{1/2}]$

$$\frac{1}{2} \frac{\partial H^2}{\partial x} = \frac{\tau_0}{\rho g} \Rightarrow H = \sqrt{\frac{2\tau_0}{\rho g} x} = \Lambda \sqrt{x}$$

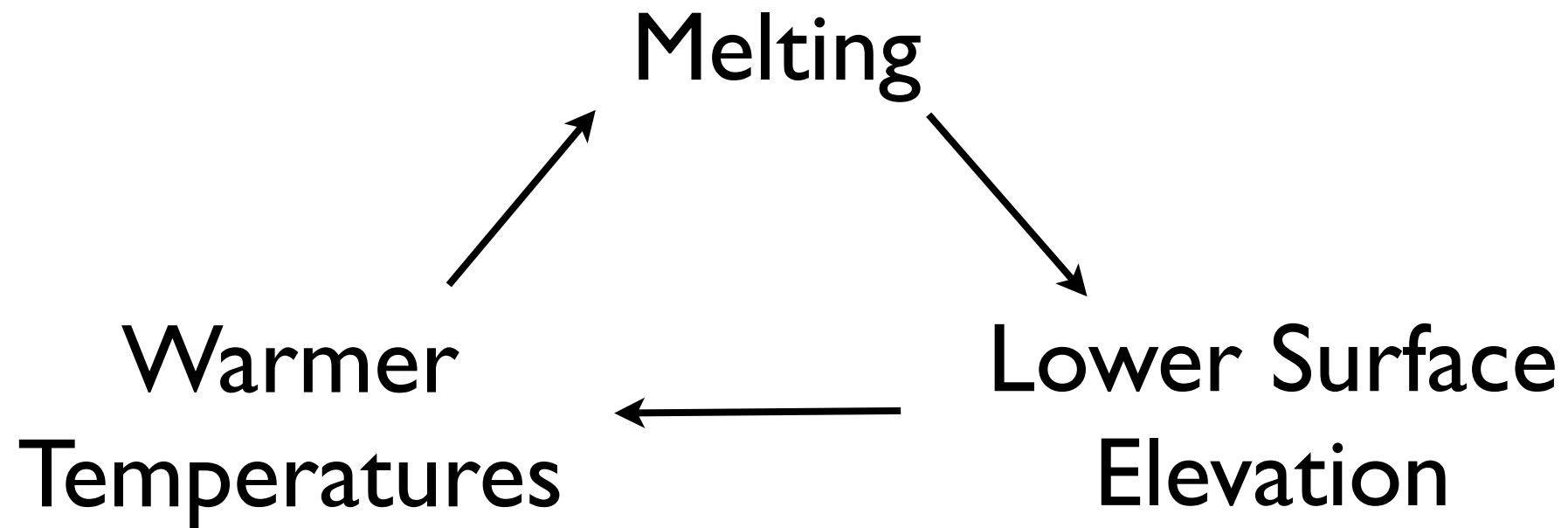
parabolic ice sheet profile



\bar{H} = average ice sheet height

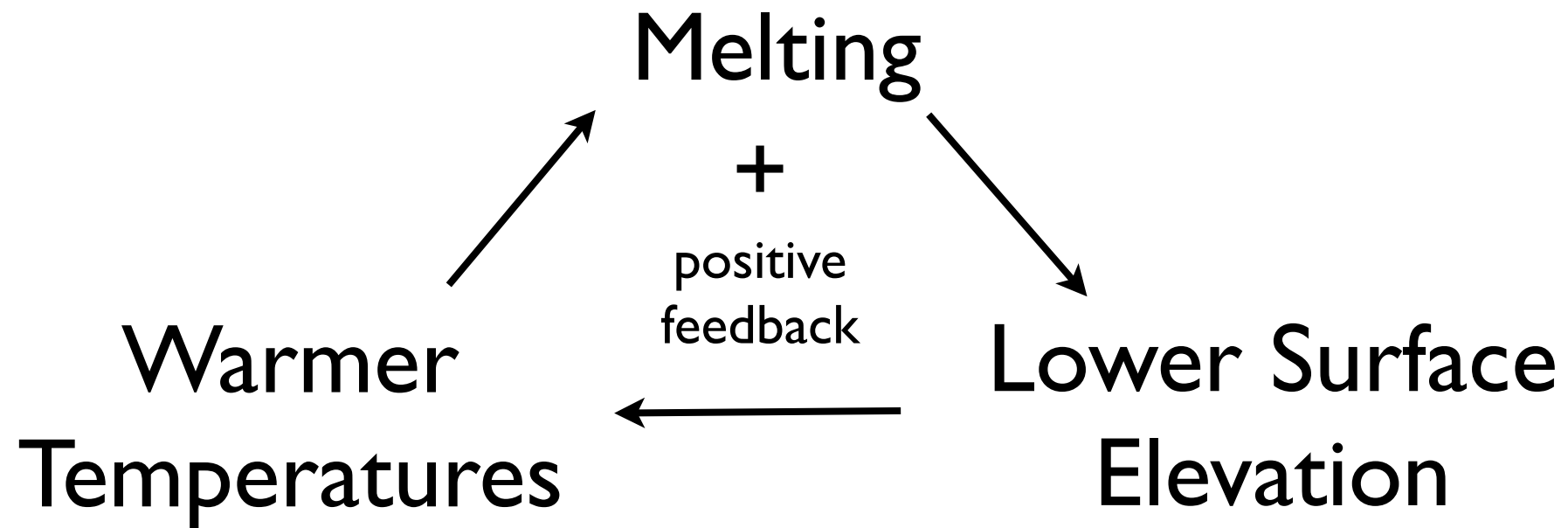
$$\bar{H} = \frac{1}{L} \int_0^L H dx = \frac{\sqrt{2}\Lambda}{3} \sqrt{L} > H_E \quad (7.5)$$

Ice Sheet Elevation-Mass Balance Feedback



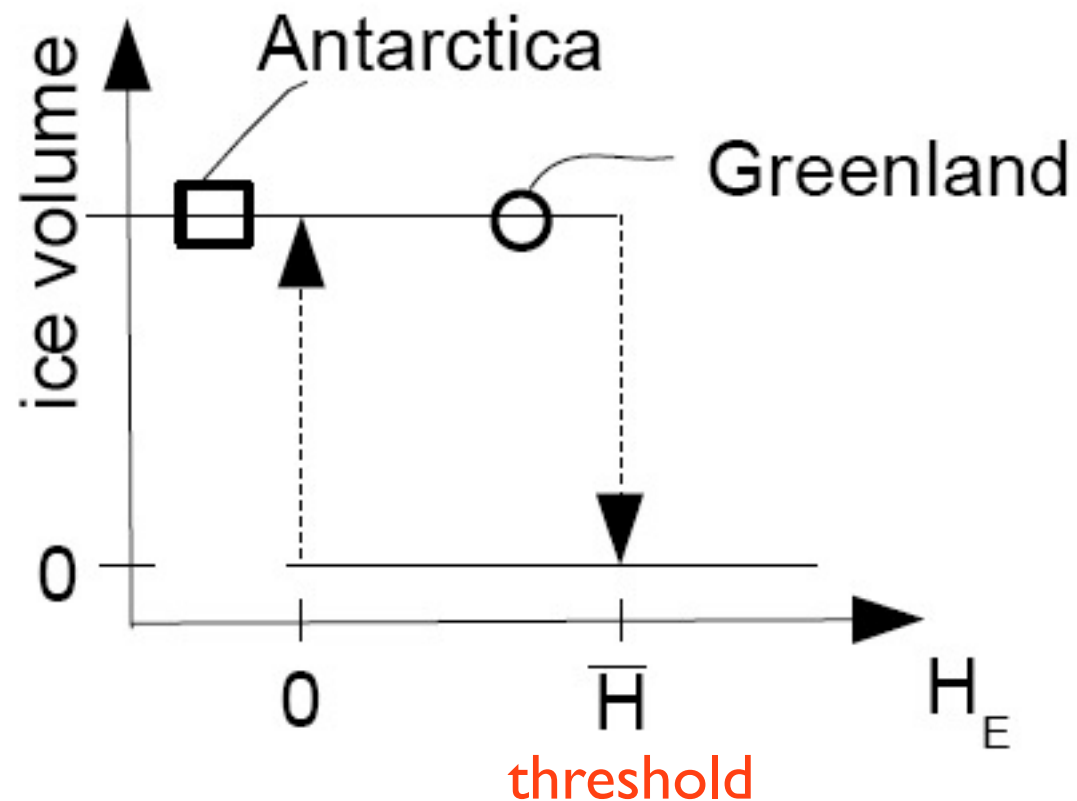
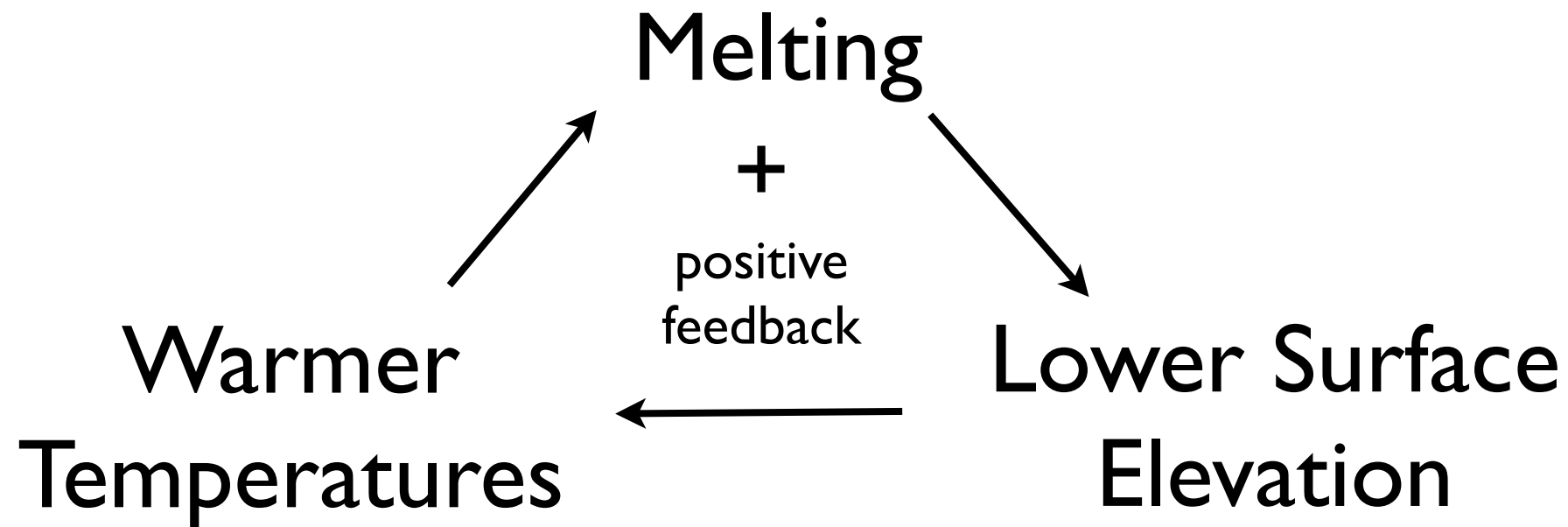
threshold

Ice Sheet Elevation-Mass Balance Feedback

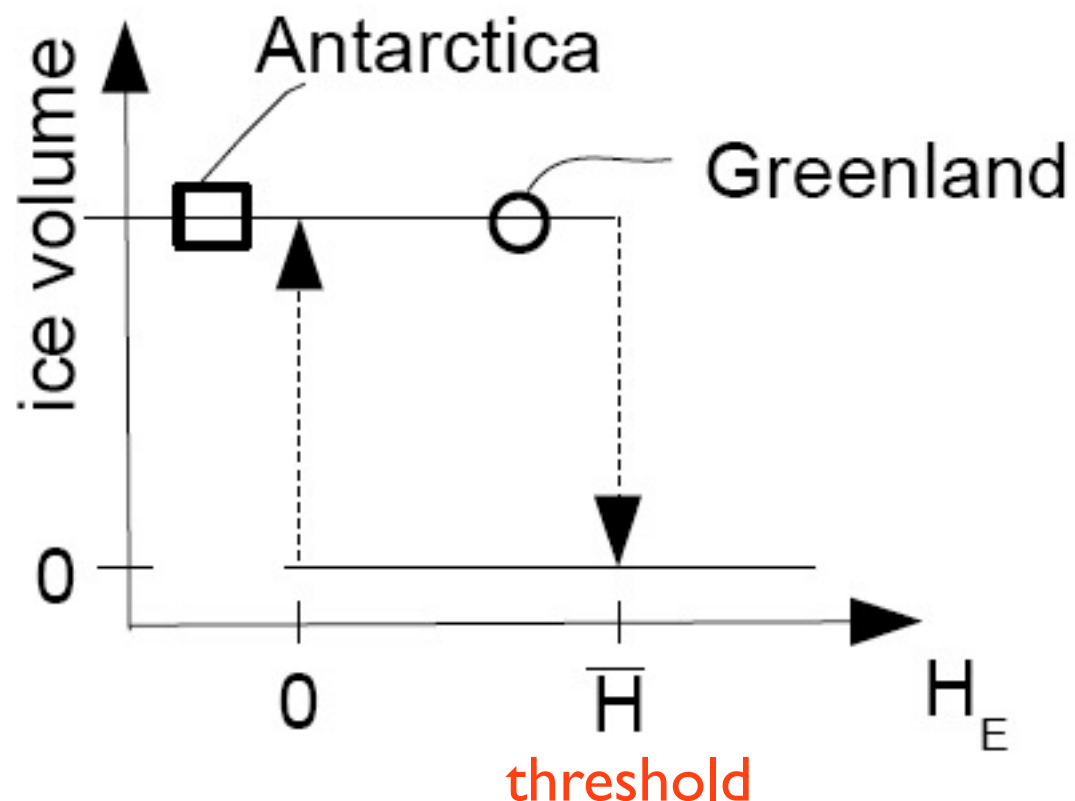
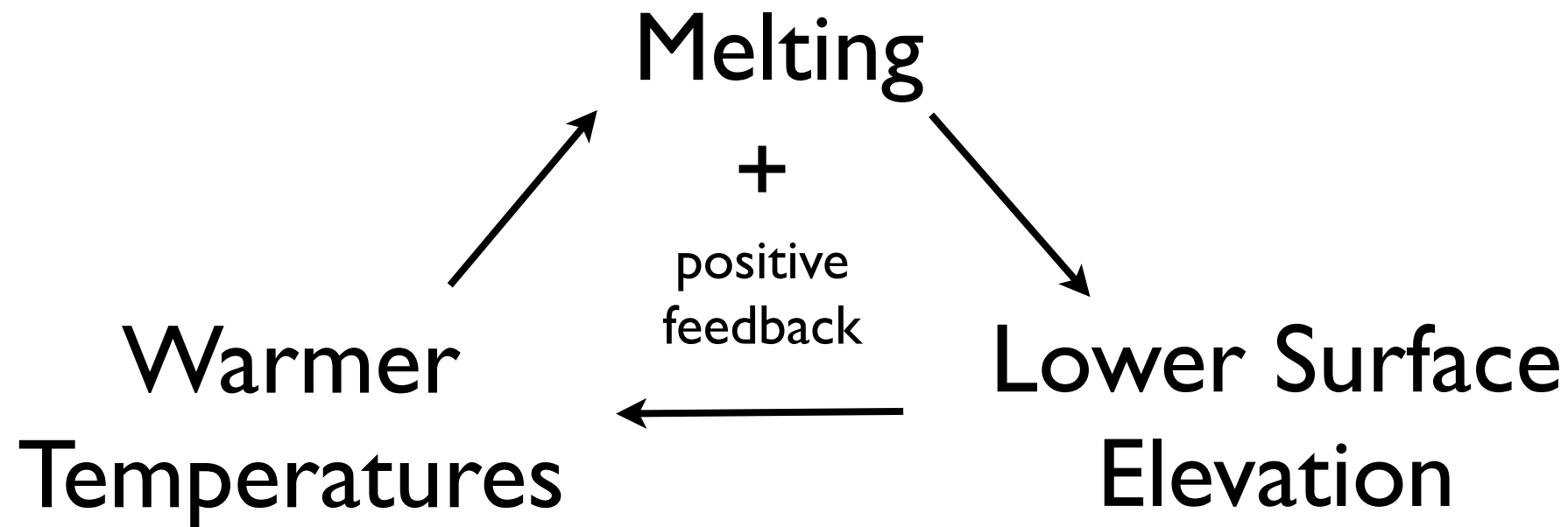


threshold

Ice Sheet Elevation-Mass Balance Feedback

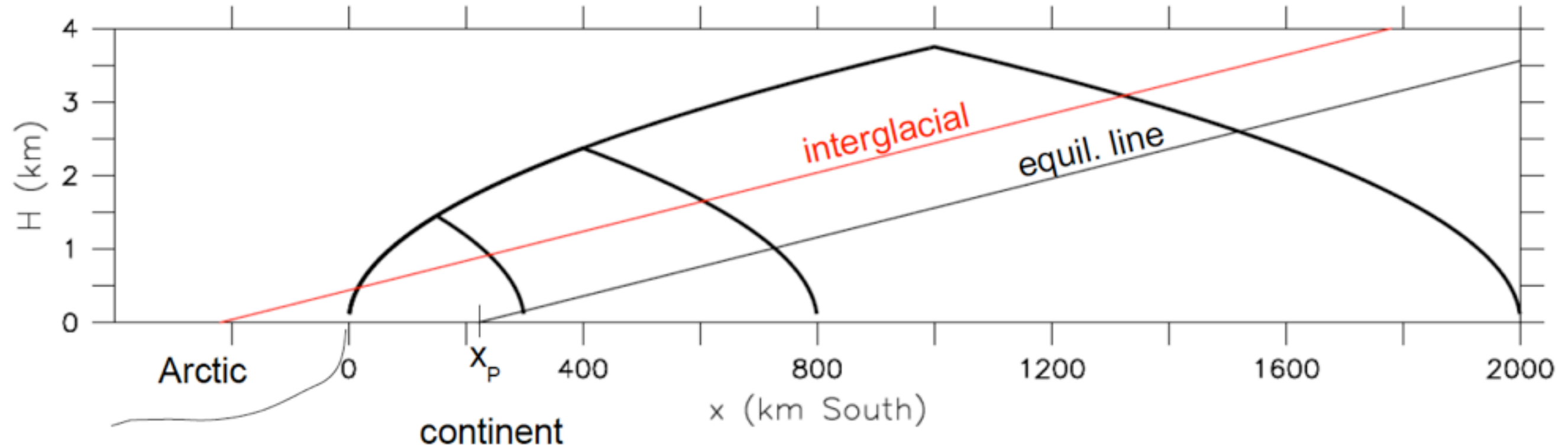


Ice Sheet Elevation-Mass Balance Feedback



- Positive feedback leads to a **threshold** for the equilibrium line.
- If higher than average ice sheet height, the ice sheet will disappear.
- It will only grow back if equilibrium line is decreased below zero (ground), that is below its current elevation. **Irreversibility**.
- **Greenland** is close to threshold. Vulnerable to warming. 2-3°C global mean warming will lead to its irreversible demise with 7 m sea level rise.
- **East Antarctic** ice sheet is not close to the threshold. May even grow due to increased snowfall in warmer climate.

Northern Hemisphere Ice Sheets



Mass Balance

$$B = \alpha(x - x_p) + \beta H \quad \alpha < 0 \quad (7.6)$$

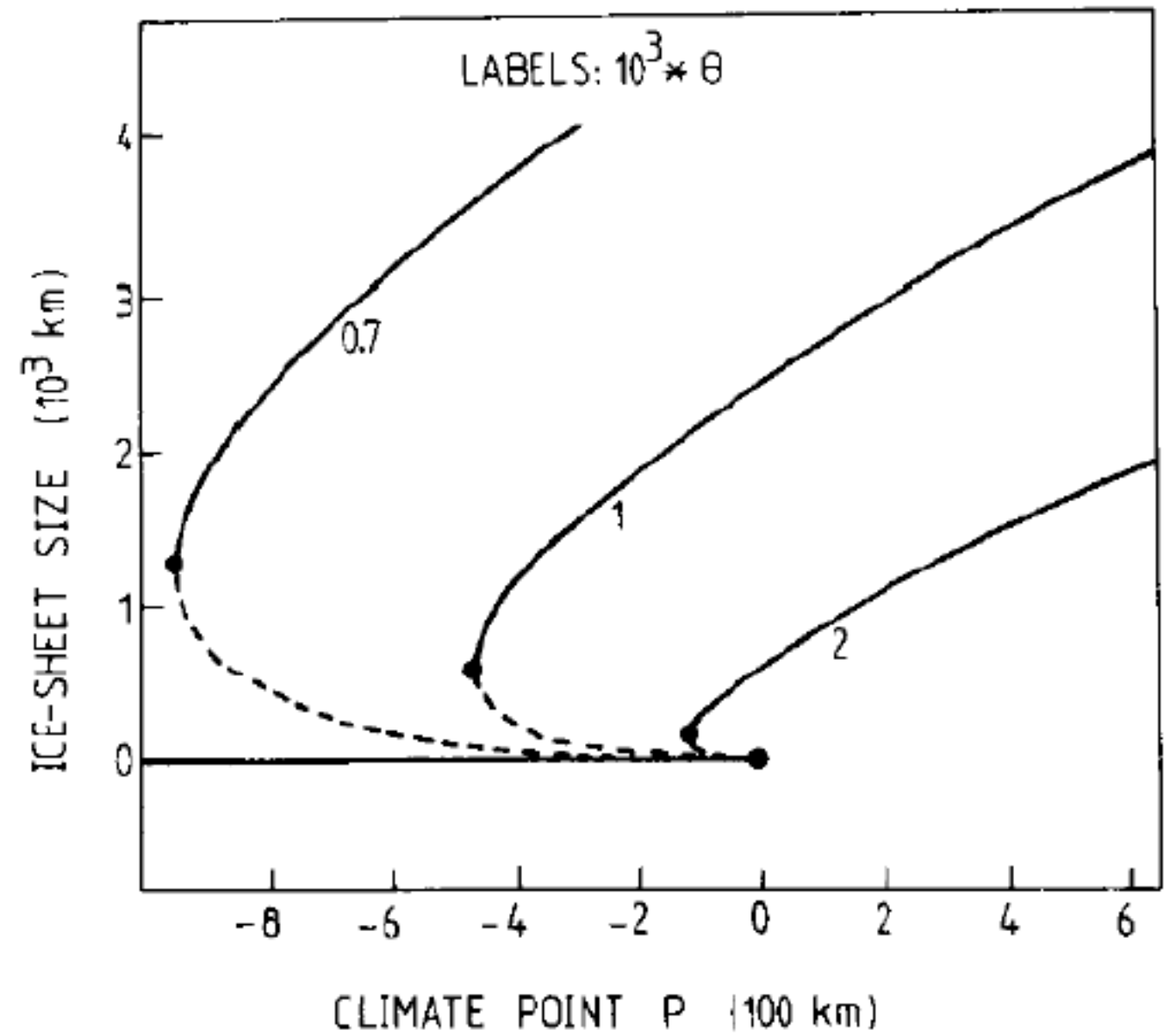
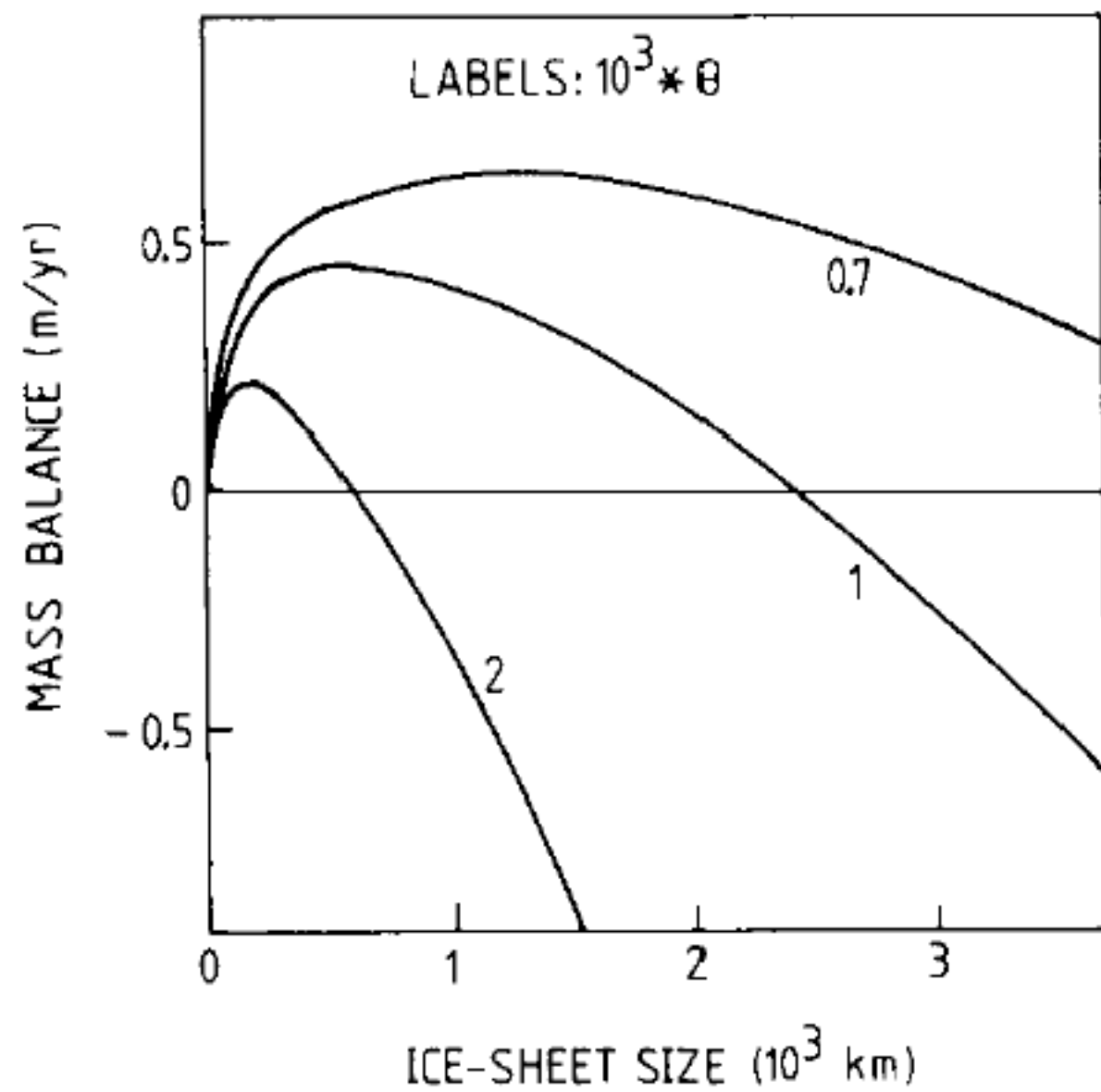
Northern half will lose mass by calving if ice bergs into Arctic.
Equilibrium: mass balance integrated over southern half = zero.

Equil. line slope: $\Theta = -\alpha/\beta$

$$\bar{B}(L) = \frac{2}{L} \int_{L/2}^L B dx = B_1 + B_2 L^{1/2} + B_3 L = 0$$

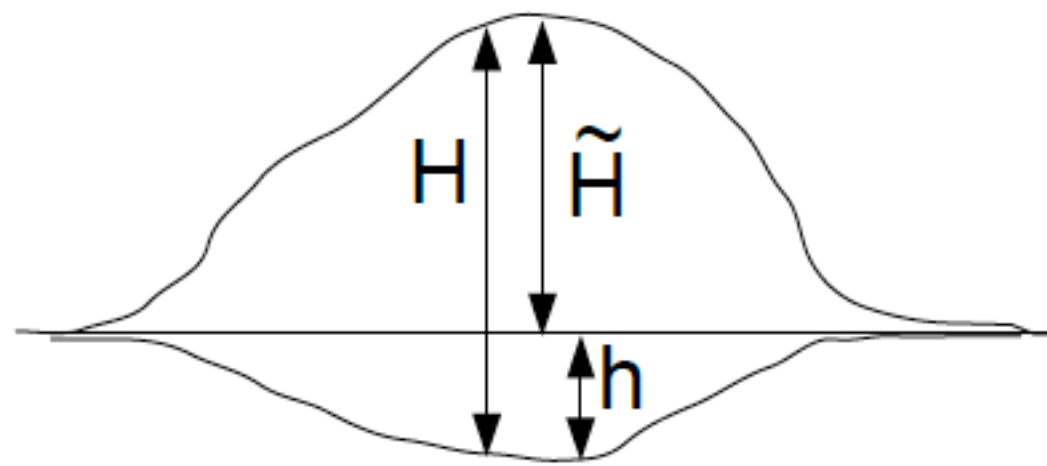
$$B_1 = -\alpha x_p, \quad B_2 = \sqrt{2} \beta \Lambda / 3, \quad \text{and} \quad B_3 = 3\alpha/4$$

The equilibrium is stable if $\partial \bar{B} / \partial L < 0$ and unstable if $\partial \bar{B} / \partial L > 0$



Hysteresis

Bedrock adjustment



$$\frac{\partial h}{\partial t} = \frac{(\rho_i / \rho_B) H - h}{\tau_B} \quad (7.8)$$

$$\tau_B \sim 3\text{-}5 \text{ ka}$$

$$\rho_i / \rho_B \simeq 1/4 - 1/3$$

A numerical model using Glen's law

$$\frac{\partial H}{\partial t} = \vec{\nabla} \cdot \vec{M} + B \quad (7.9)$$

Vertically integrated mass flux: $M = Hu$ $u = C \tau_b^m$ $\tau_b = \rho g H s = \rho g H \frac{\partial \tilde{H}}{\partial x}$ (7.2)

$m=3$

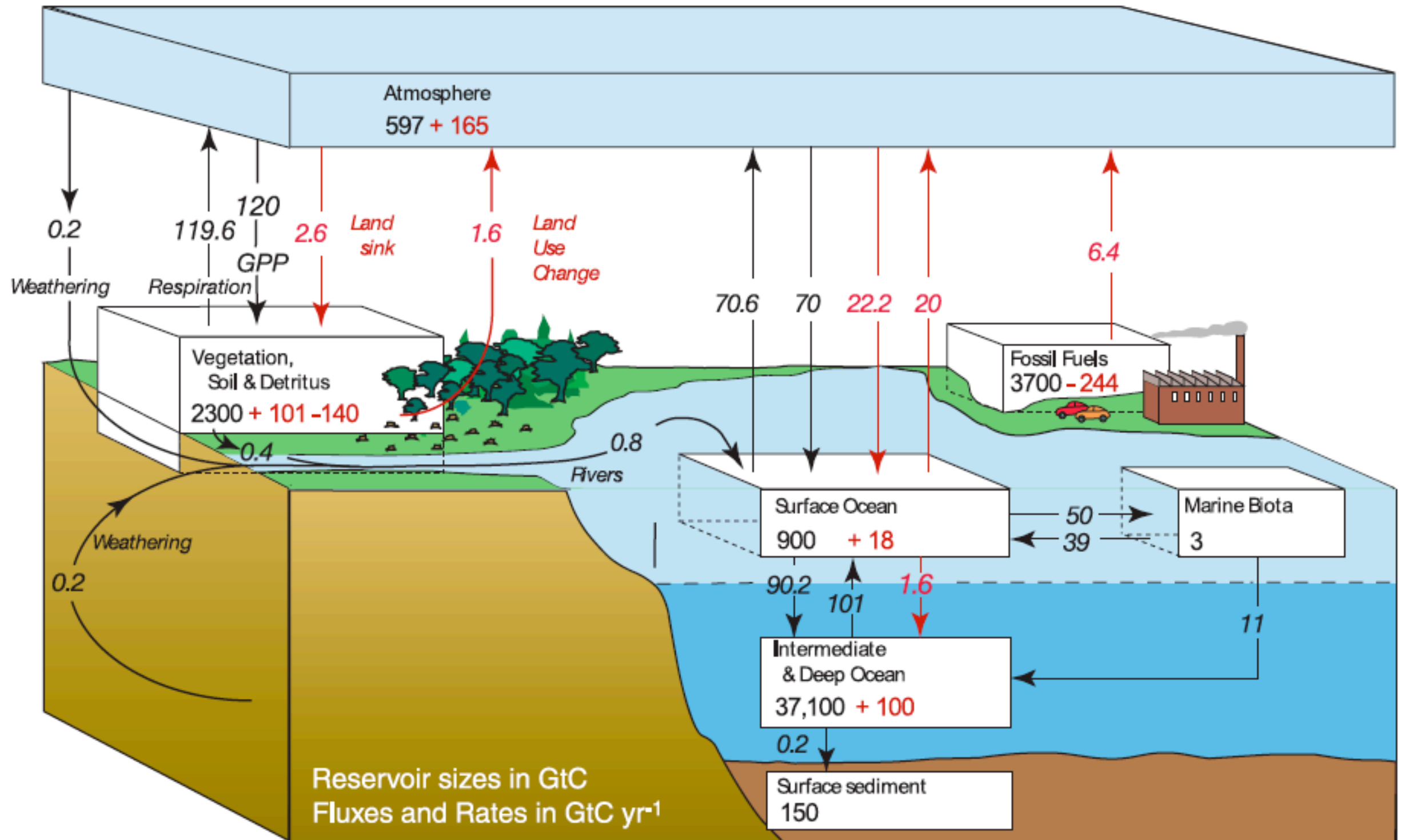
$$\vec{M} = \underbrace{A H^{m+1} |\vec{\nabla} \tilde{H}^{m-1}|}_{D} \vec{\nabla} \tilde{H} \quad (7.10)$$

$$\frac{\partial H}{\partial t} = \vec{\nabla} \cdot (D \vec{\nabla} \tilde{H}) + B \quad (7.11)$$

$$D = A H^{m+1} \left[\left(\frac{\partial \tilde{H}}{\partial x} \right)^2 + \left(\frac{\partial \tilde{H}}{\partial y} \right)^2 \right]^{(m-1)/2} \quad (7.12)$$

Your 2D ice sheet model !

The Global Carbon Cycle

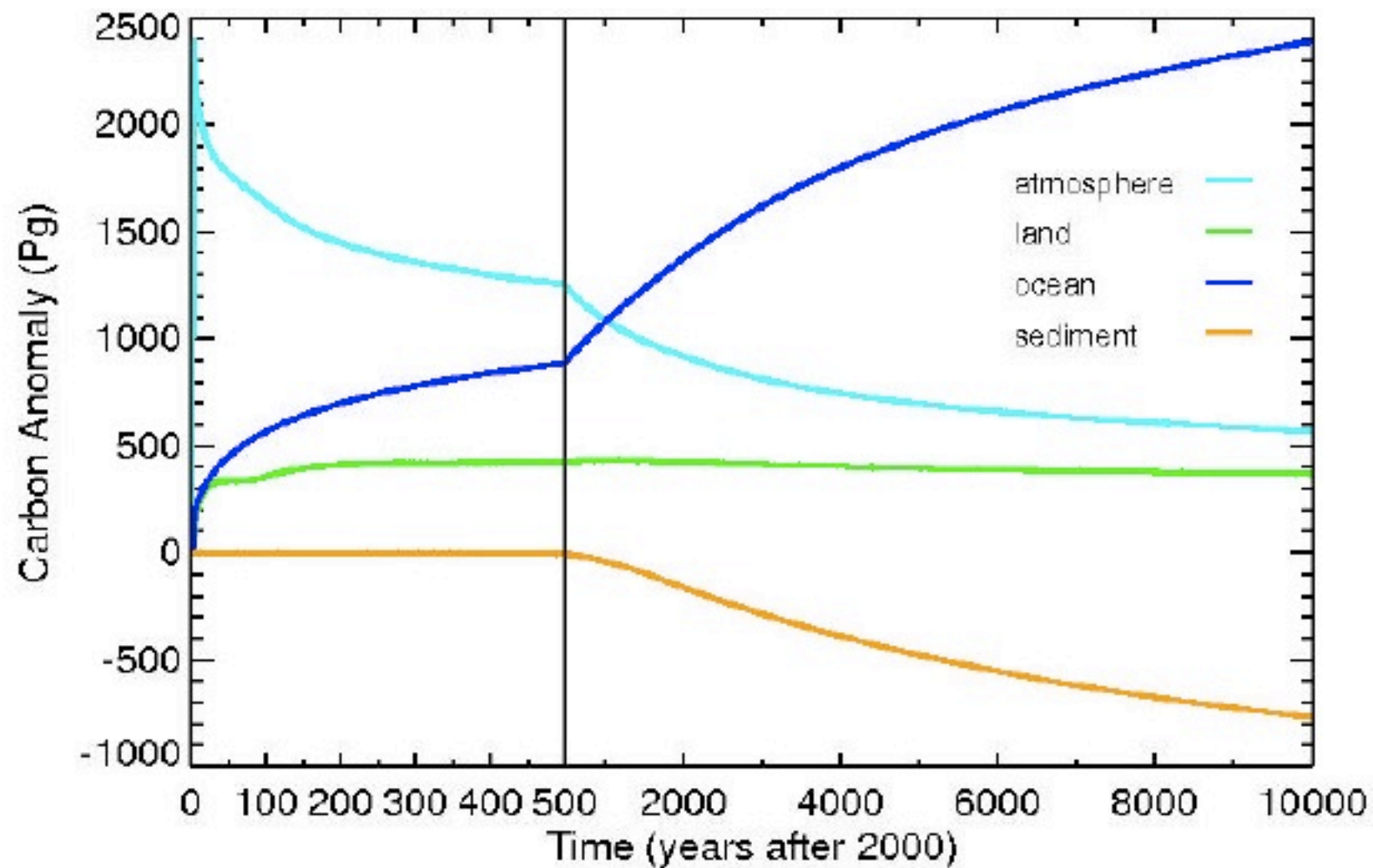


2 GtC = 1 ppmv

IPCC (2007)

Fate of Anthropogenic CO₂

Pulse of 2560 PgC released

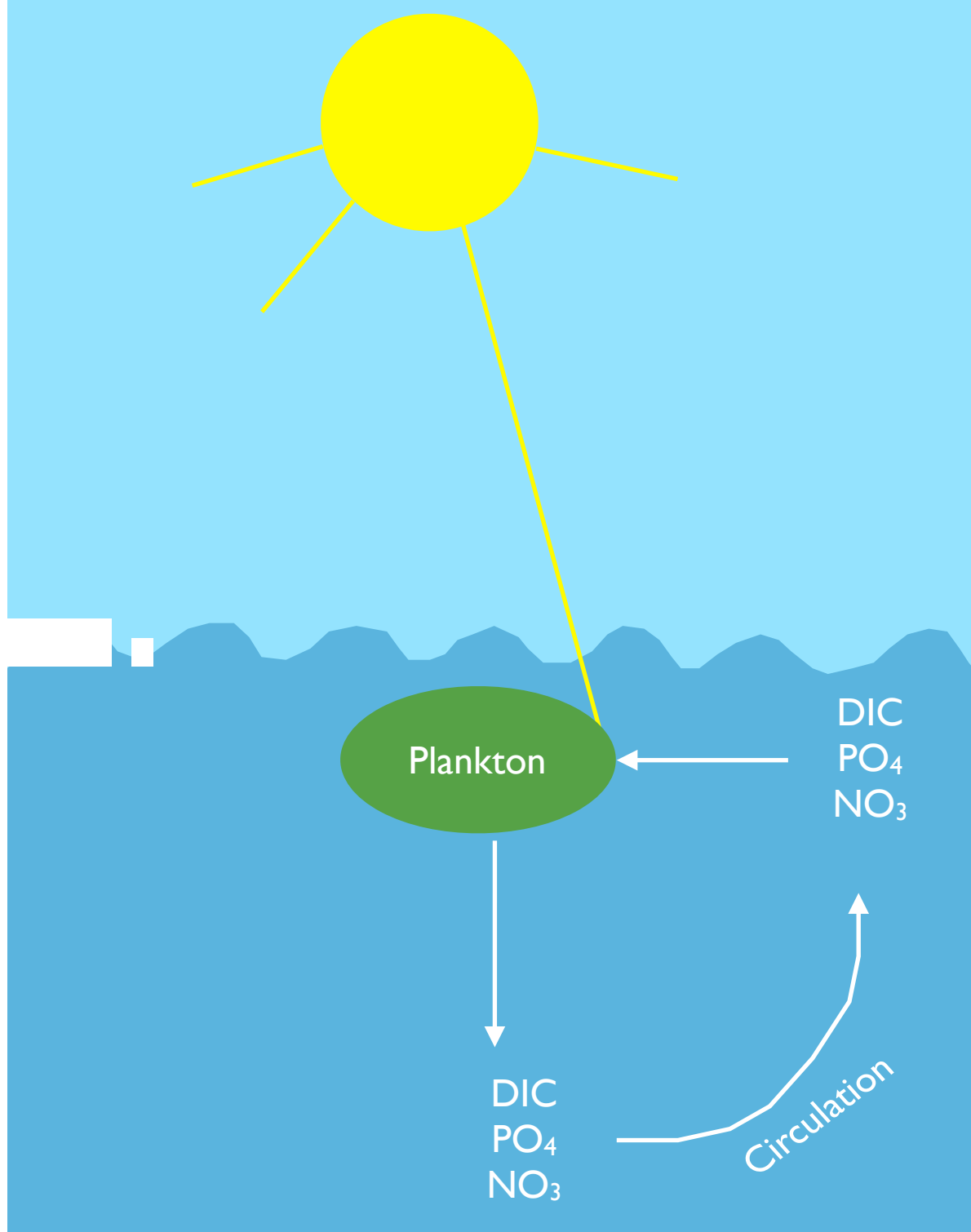


Eby et al. (2009) J. Climate 22, 2501-2511

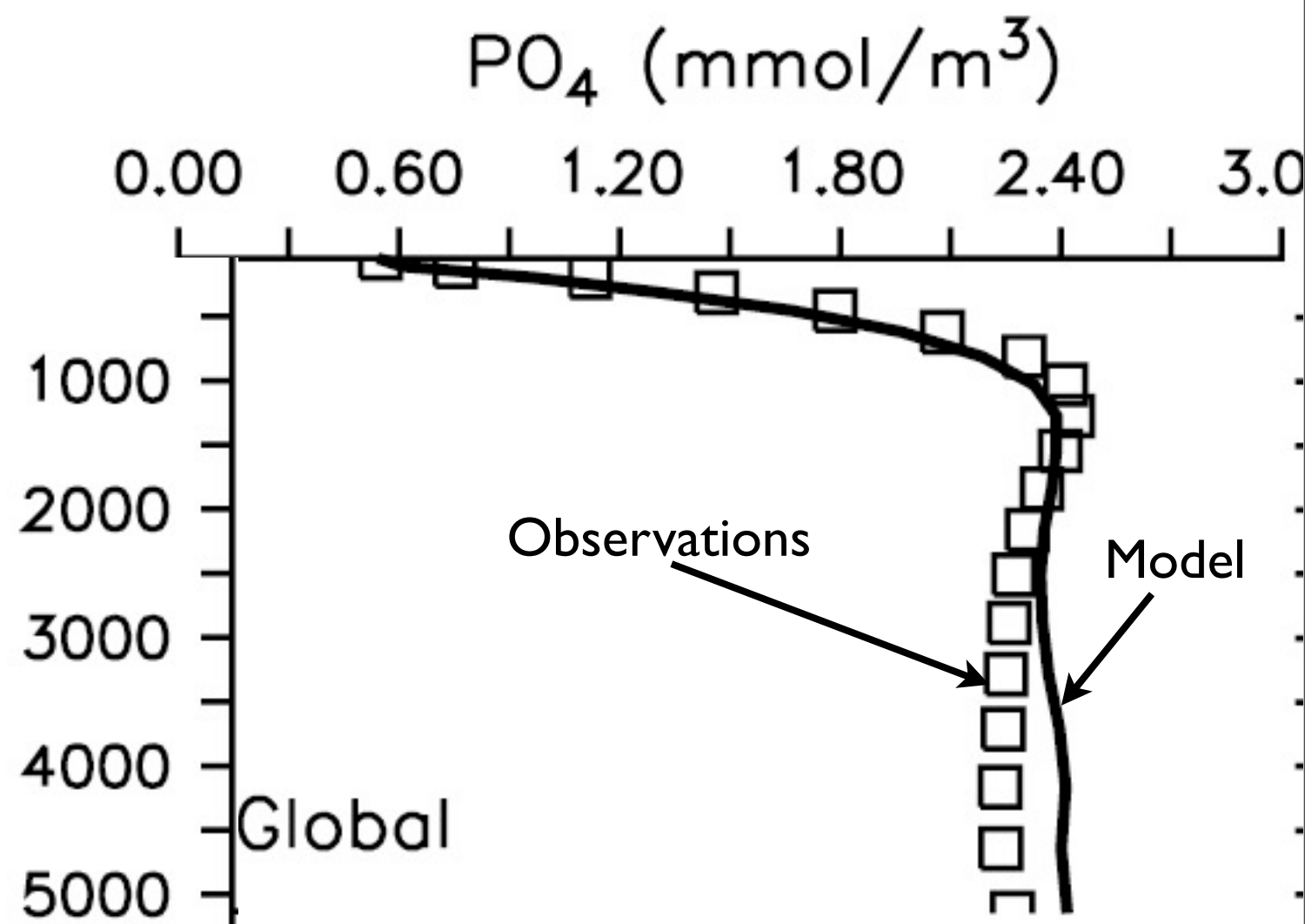
The Biological Pump

I. The Soft Tissue (Organic Matter) Pump

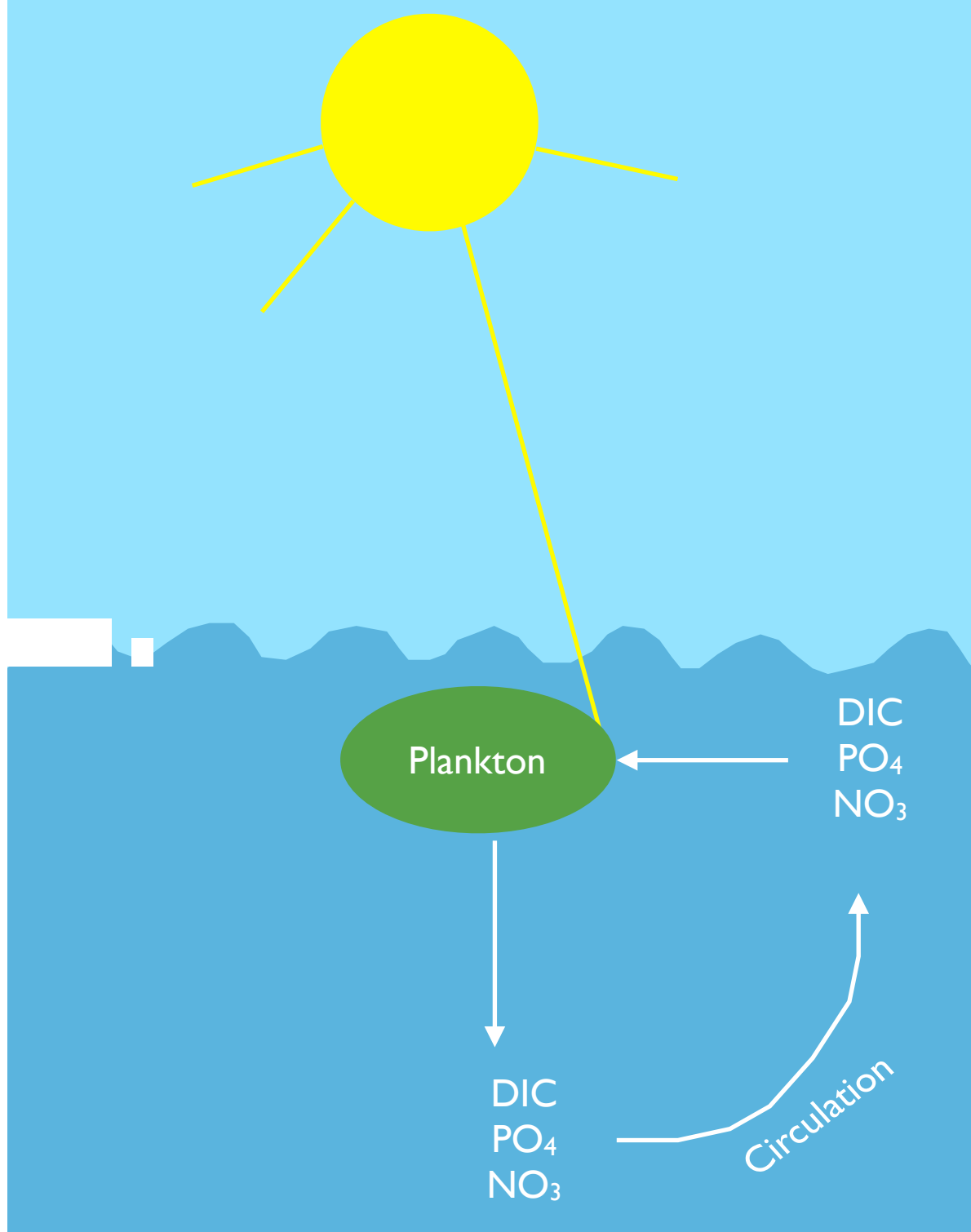
The Biological Pump



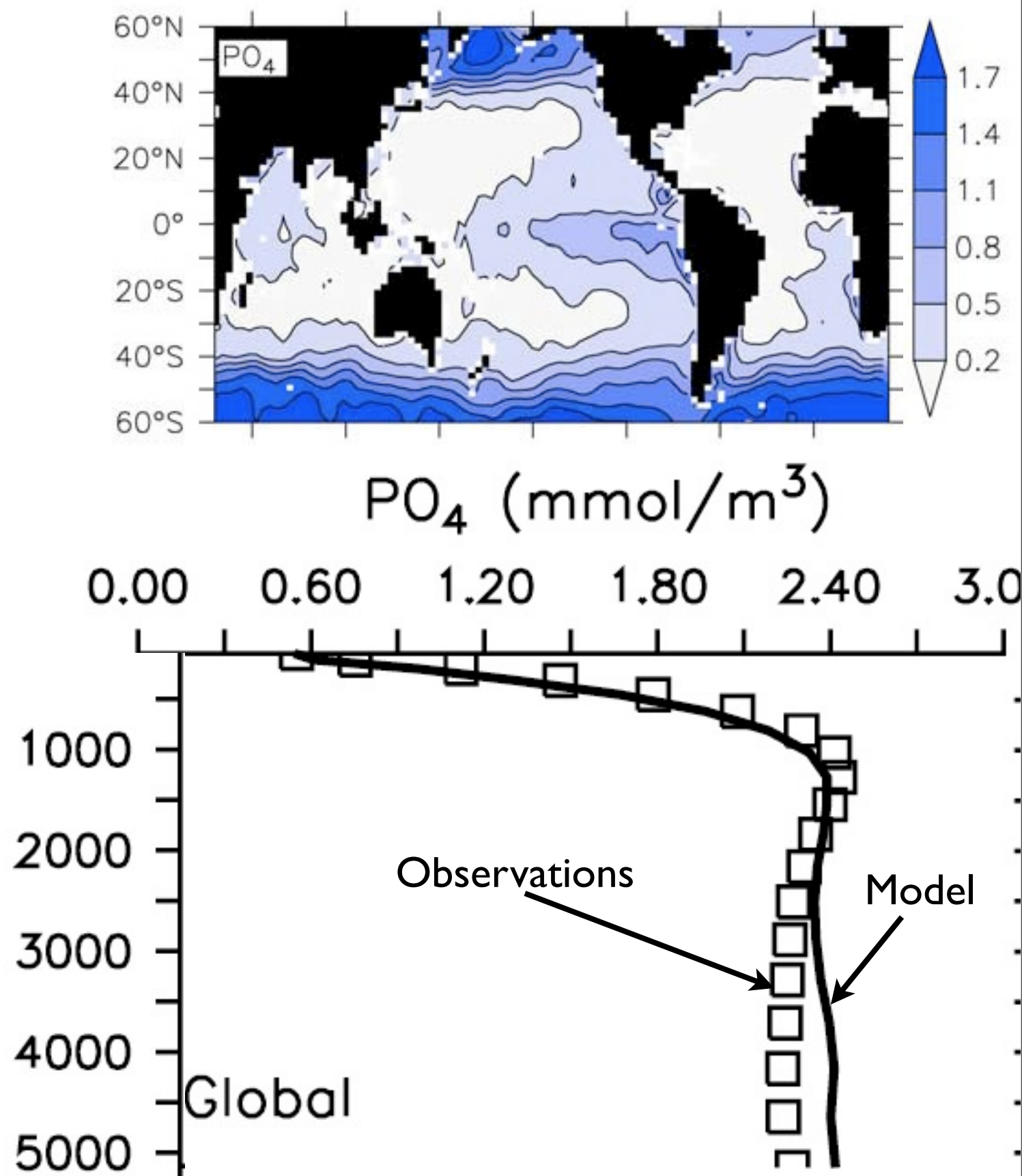
Surface Nutrients



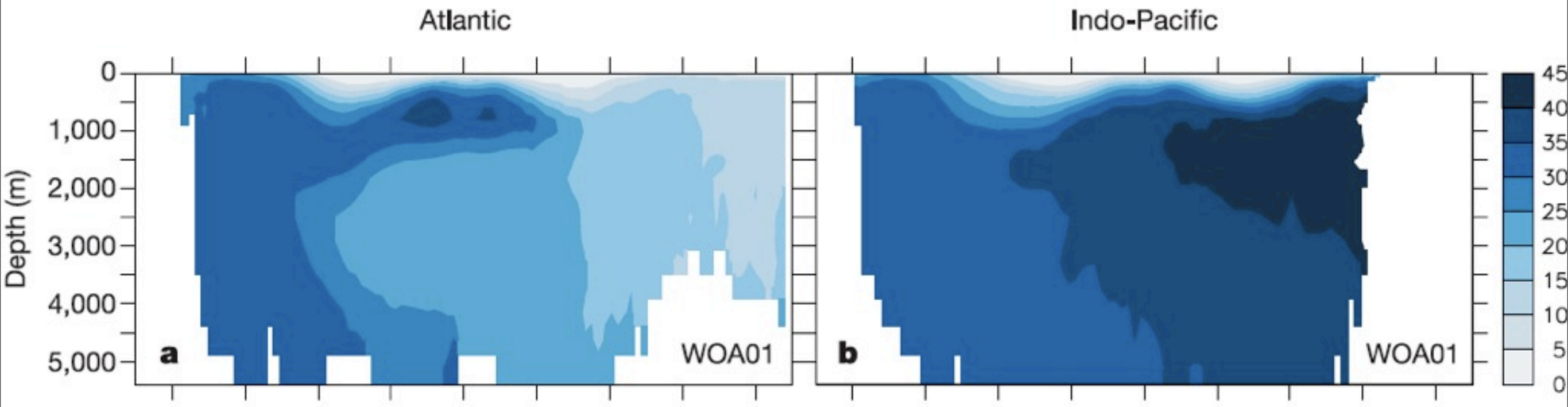
The Biological Pump



Surface Nutrients

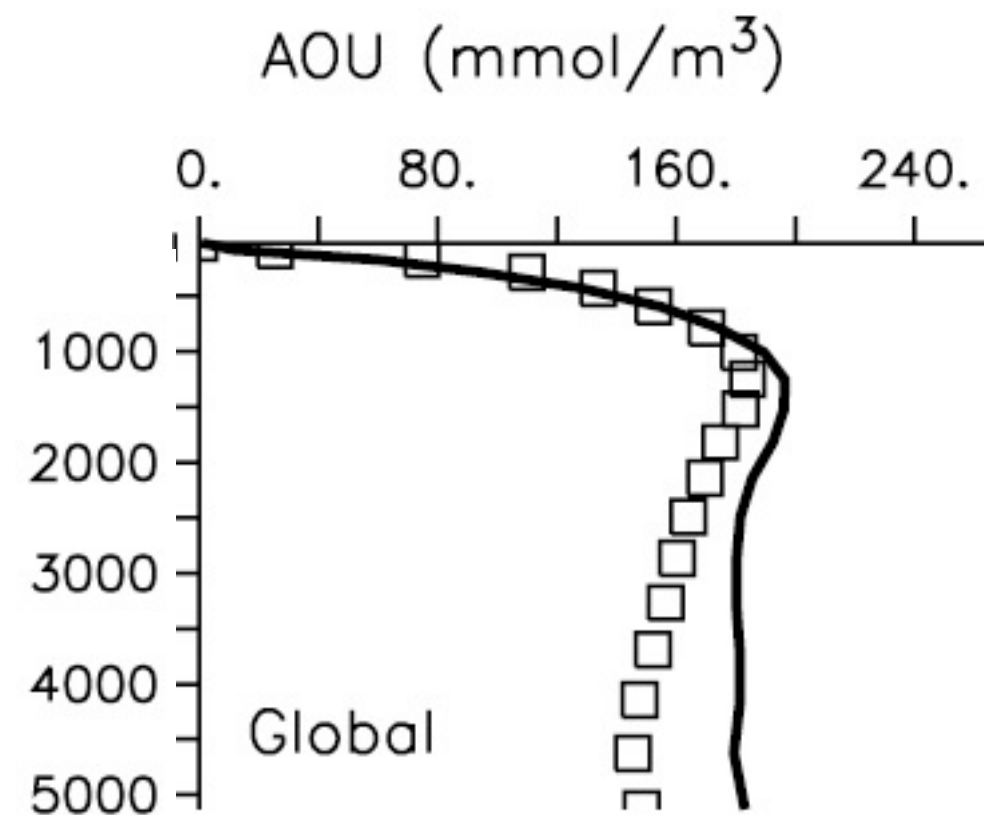
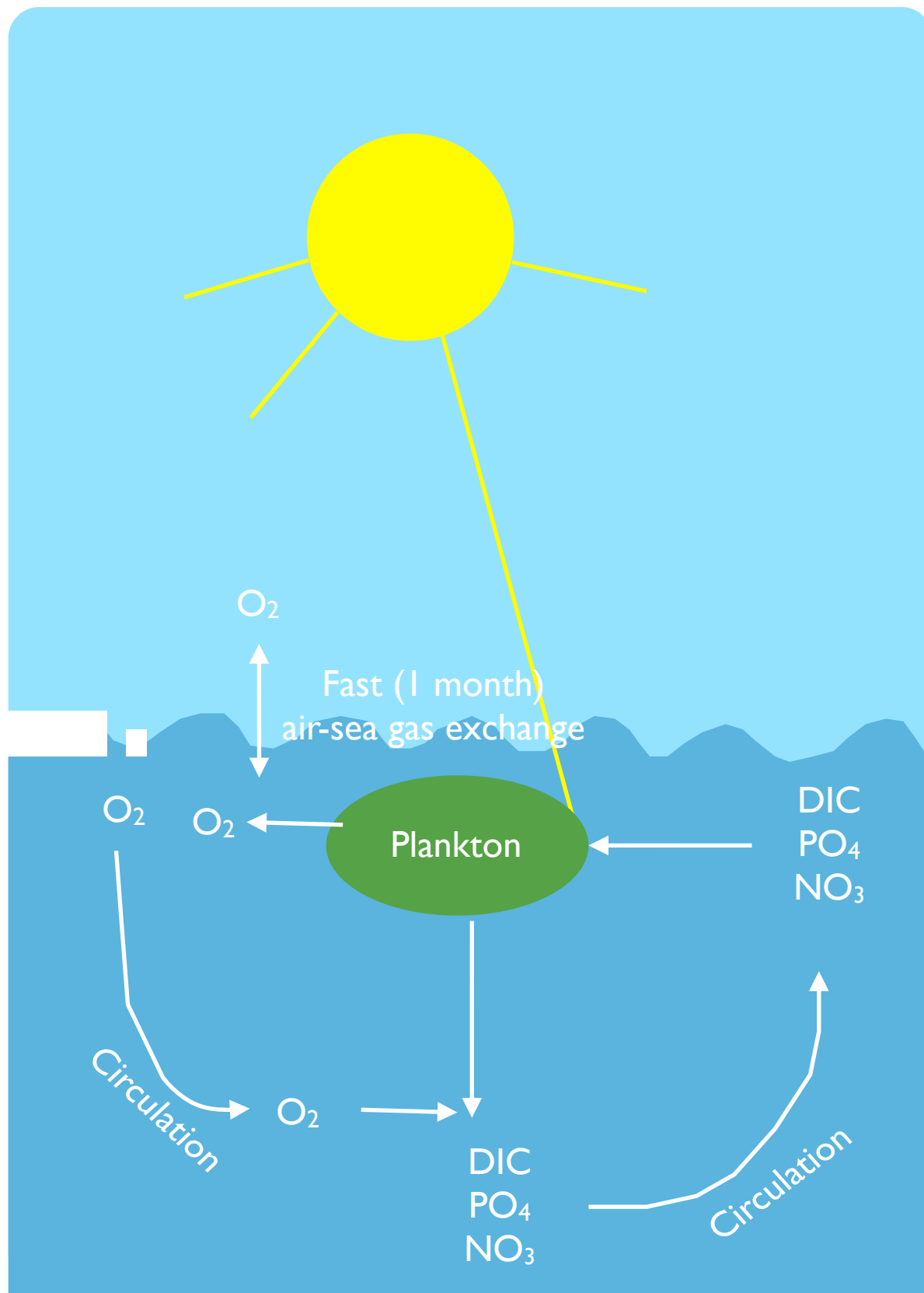


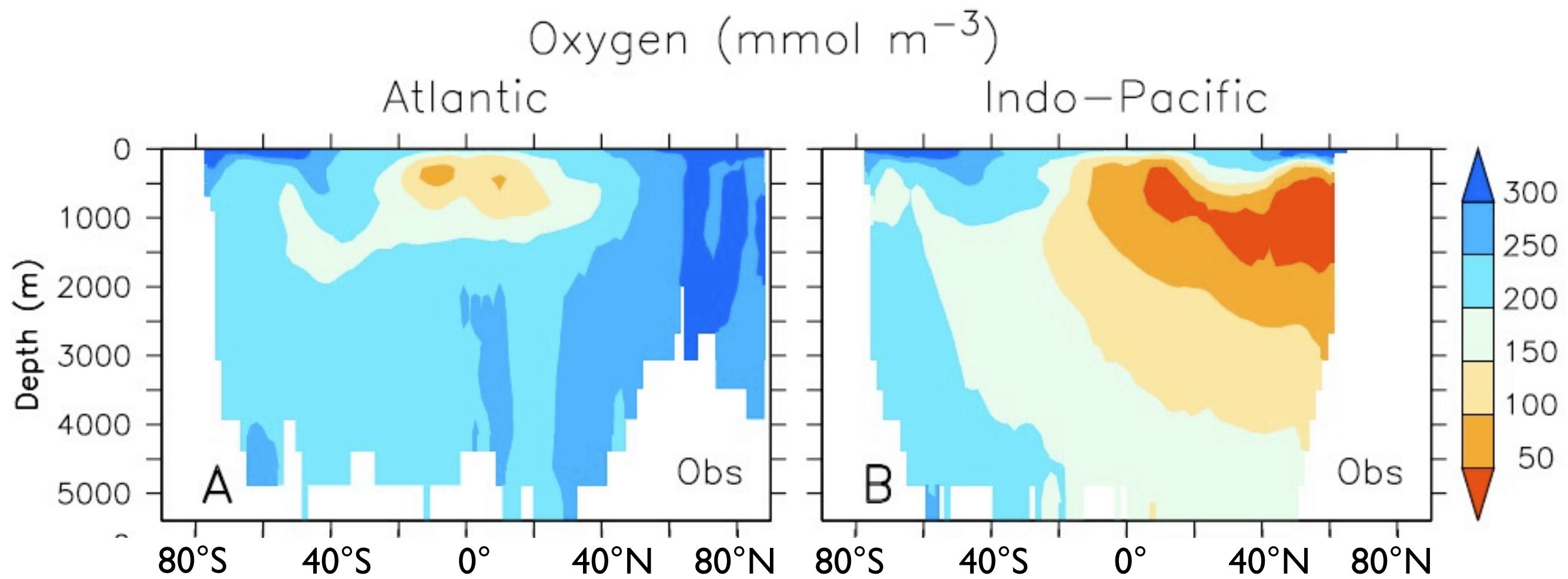
NO₃ in the deep ocean

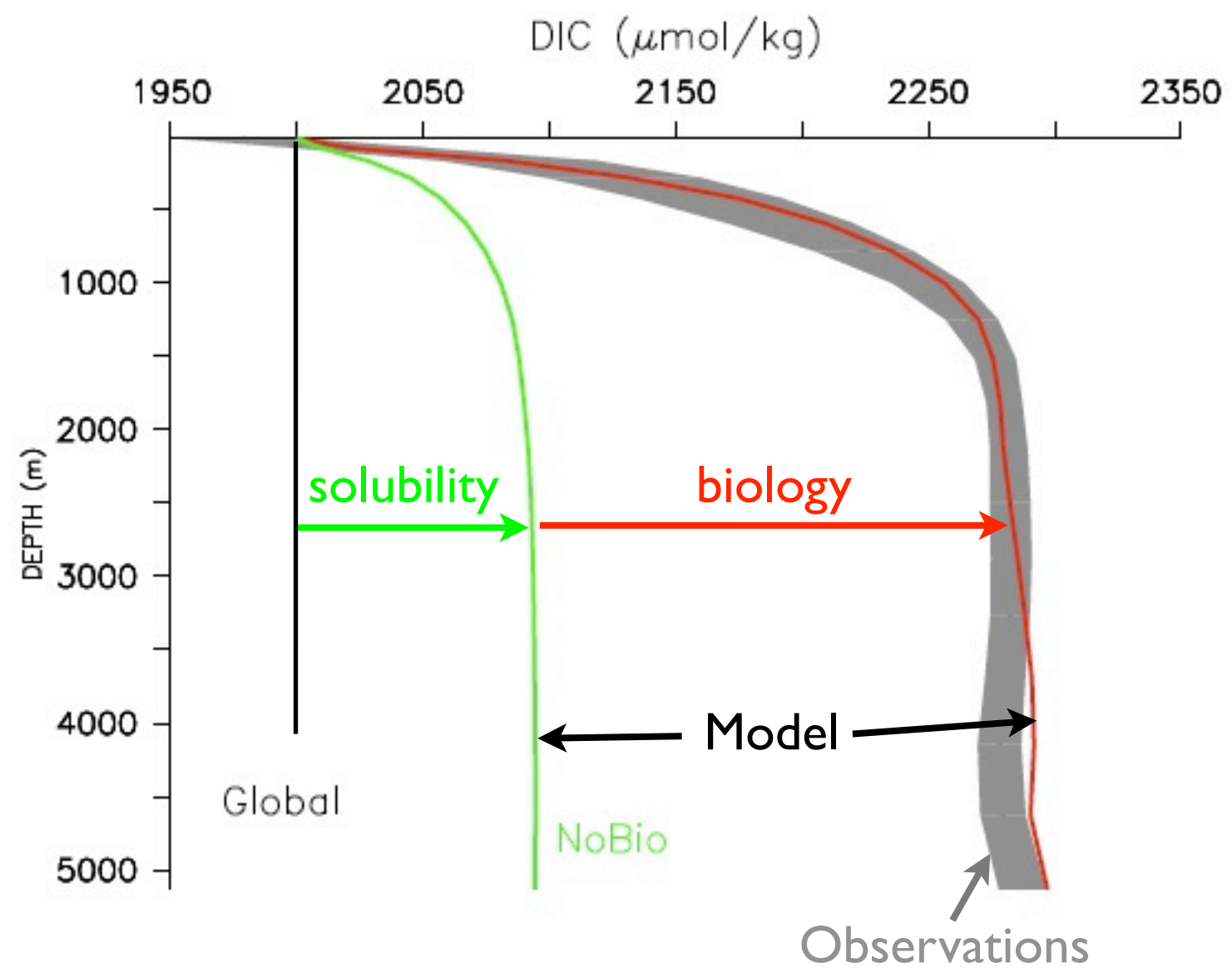
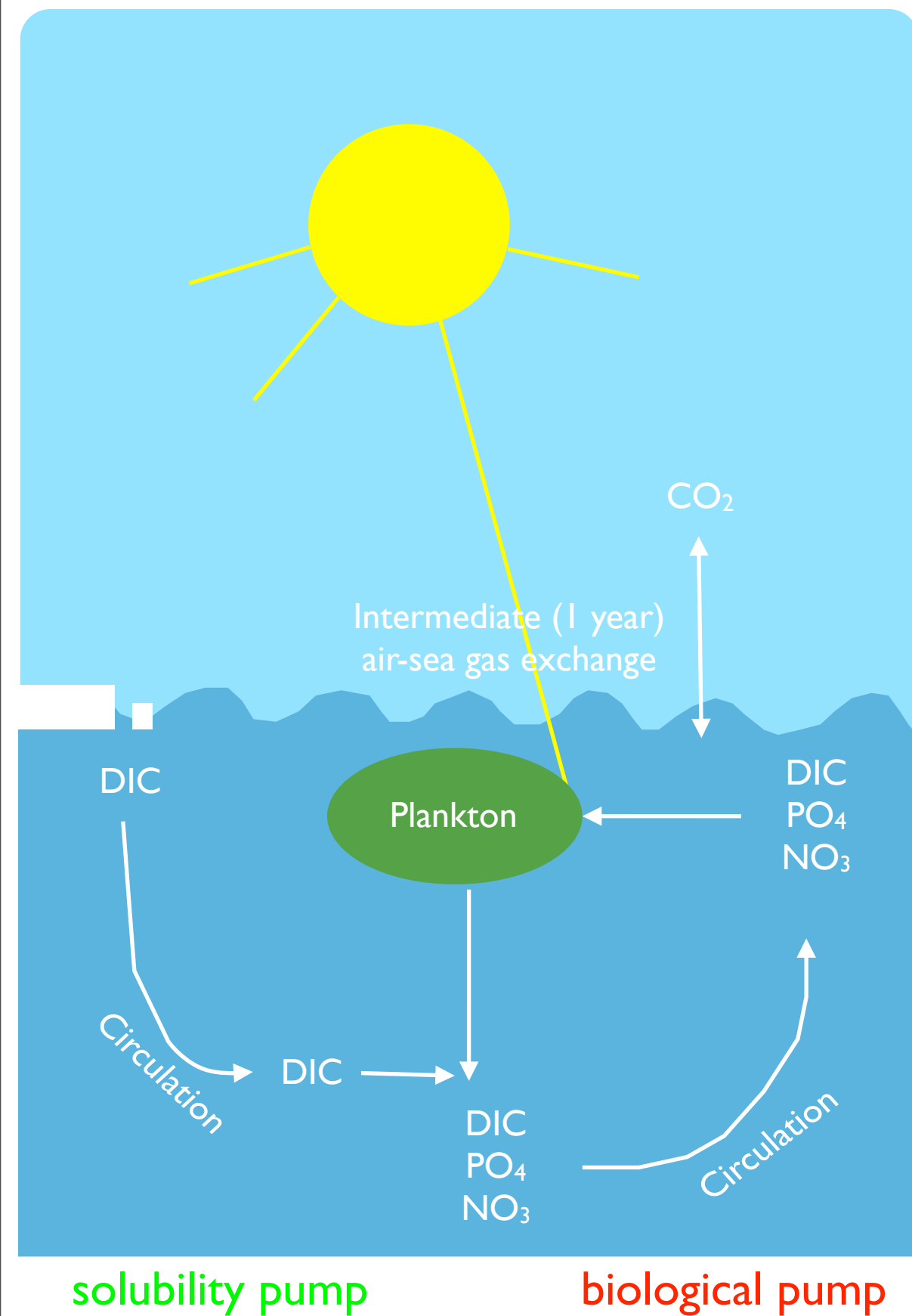


Oxygen and Apparent Oxygen Utilization (AOU)

$$\text{AOU} = \text{satO}_2(T) - \text{O}_2$$







Air sea gas exchange:

$$q = -K(|v|, T, S)(p\text{CO}_2^{\text{atm}} - p\text{CO}_2^{\text{ml}})$$

$$p\text{CO}_2^{\text{ml}} = [\text{CO}_2]^{\text{ml}} / \alpha(T, S)$$

↑
Solubility

Chemistry



Total Carbon

Dissolved Inorganic
Carbon

$$\text{DIC} = \sum \text{CO}_2 = [\text{HCO}_3^-] + [\text{CO}_3^{2-}] + [\text{CO}_2]$$

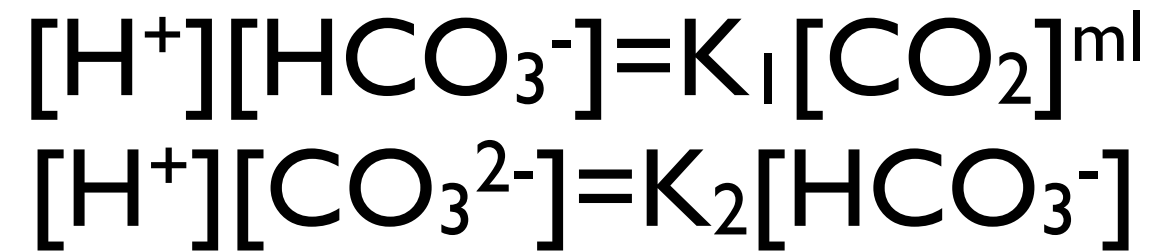
bicarbonate

carbonate

1%

The Biological Pump

2.The Hard Tissue (Inorganic Matter/Alkalinity) Pump



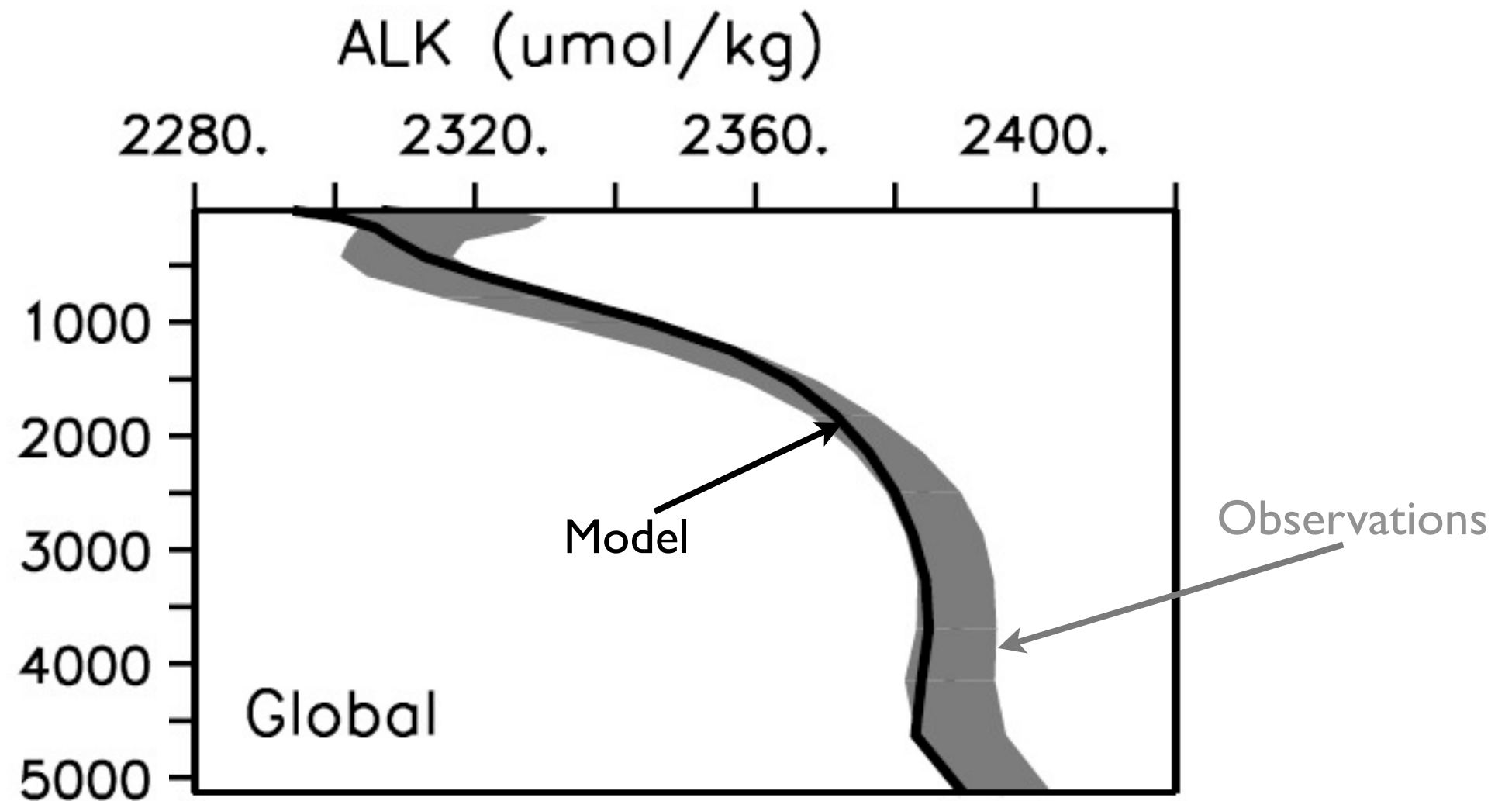
$$\Rightarrow [CO_2]^{ml} = K_2 [HCO_3^-]^2 / (K_1 [CO_3^{2-}])$$

CaCO₃ production increases [CO₂]
because [CO₃²⁻] is taken up by organisms:

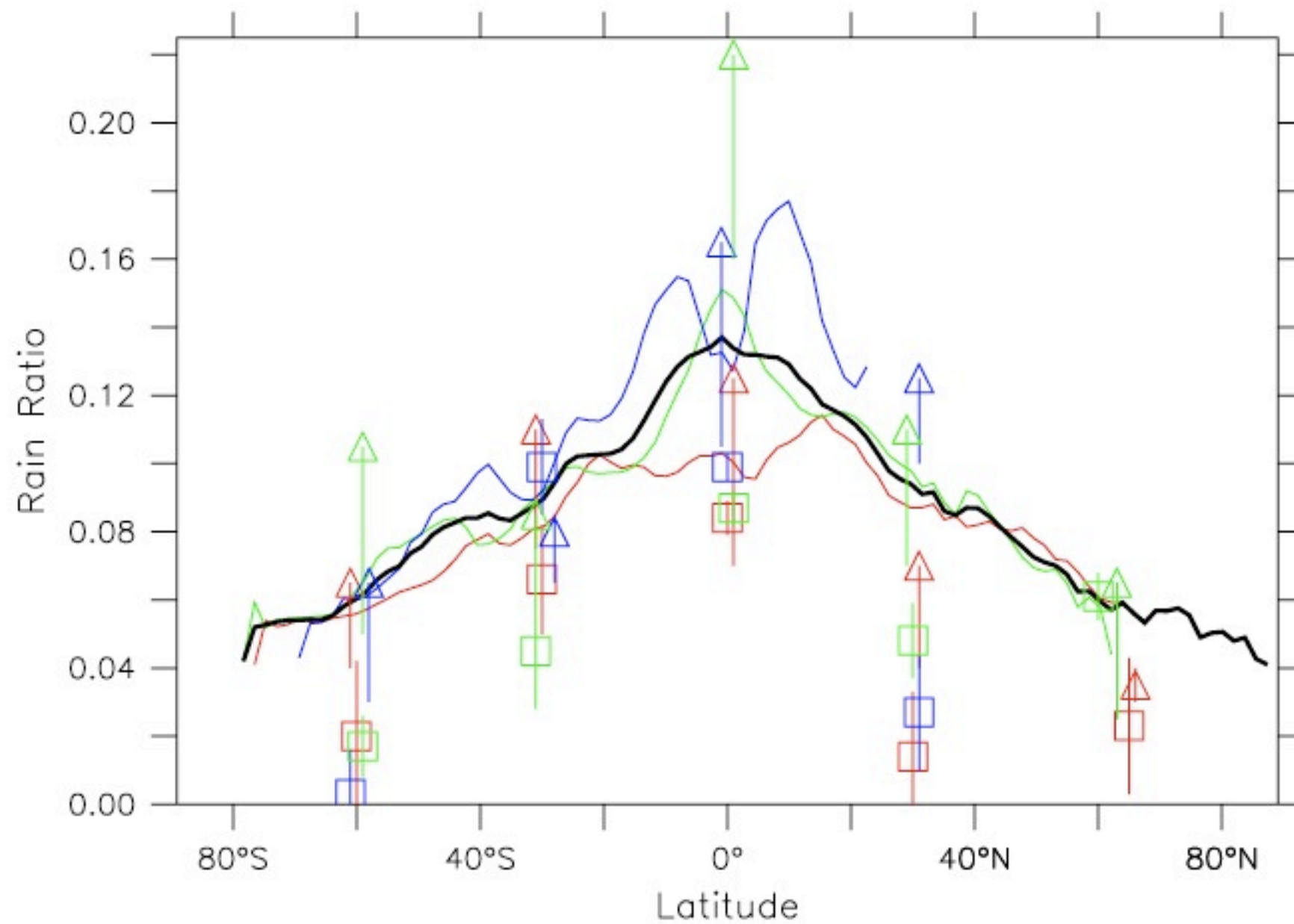
- Coccolithophorids (phytoplankton)
 - Foraminifera (zooplankton)
 - Pteropods (zooplankton)
- } Calcite
 Aragonite

Carbonate Alkalinity

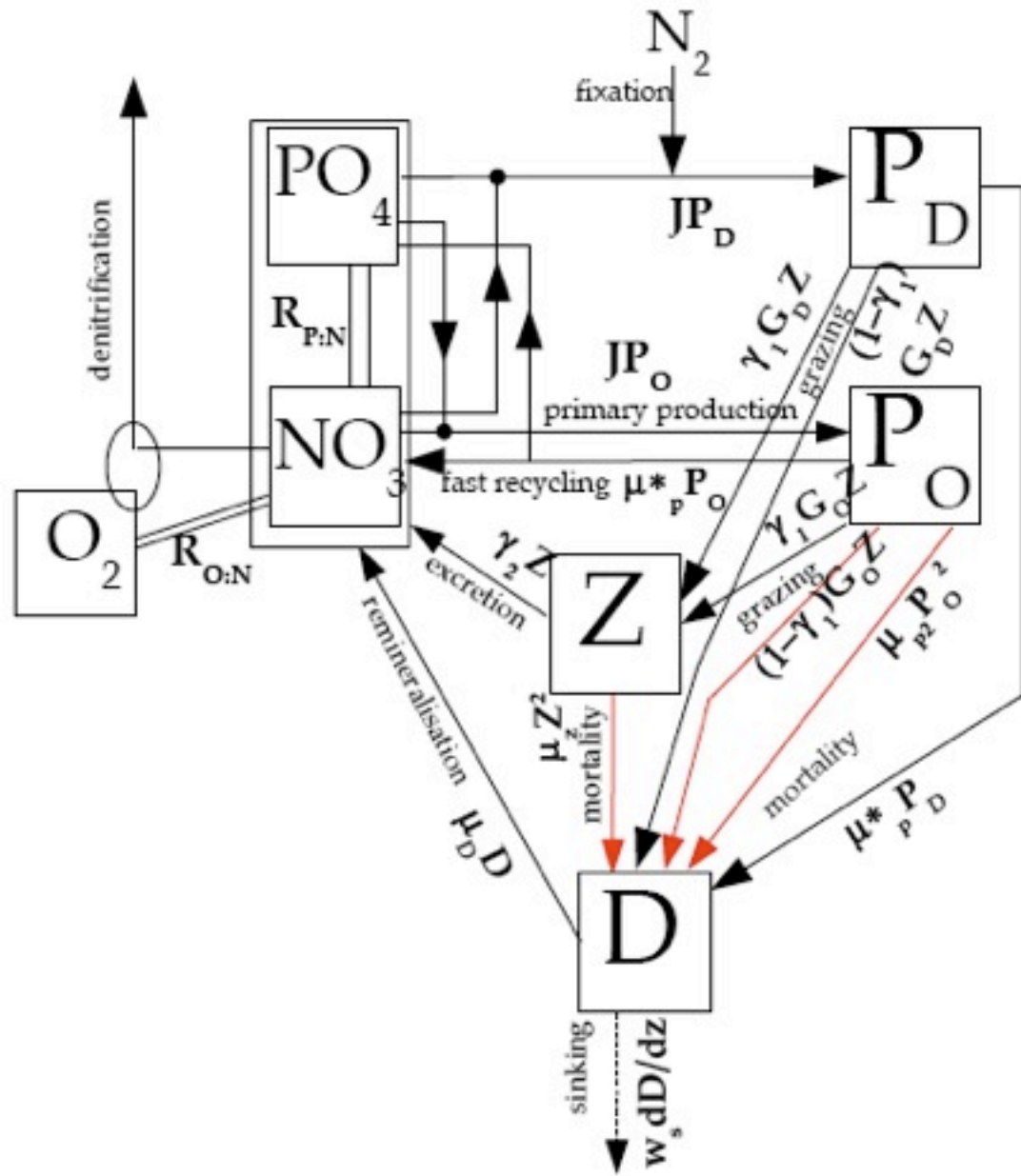
$$\text{ALK} = [\text{HCO}_3^-] + 2[\text{CO}_3^{2-}] = 2\text{DIC} - [\text{HCO}_3^-]$$



Rain Ratio = Export of CaCO_3 / Export of POC



Details of Ecosystem and Carbon Cycle Model



$$\frac{\partial C}{\partial t} = T + S,$$

Transport Biological Sources/Sinks

$$S(DIC) = S(PO_4)R_{C:P} - S(CaCO_3)$$

$$S(ALK) = -S(NO_3) \times 10^{-3} - 2S(CaCO_3).$$

$$S(PO_4) = (\mu_D D + \mu_P^* P_O + \gamma_2 Z - J_O P_O - J_D P_D) R_{P:N}$$

$$S(NO_3) = (\mu_D D + \mu_P^* P_O + \gamma_2 Z - J_O P_O - u_N J_D P_D) \cdot (1 - 0.8 R_{O:N} r_{sox}^{NO_3})$$

$$S(P_O) = J_O P_O - \mu_P^* P_O - G(P_O) Z - \mu_{P_2} P_O^2$$

$$S(P_D) = J_D P_D - G(P_D) Z - \mu_P P_D$$

$$S(Z) = \gamma_1 [G(P_O) + G(P_D)] Z - \gamma_2 Z - \mu_Z Z^2$$

$$S(D) = (1 - \gamma_1) [G(P_O) + G(P_D)] Z + \mu_P P_D + \mu_{P_2} P_O^2 + \mu_Z Z^2 - \mu_D D - w_D \partial D / \partial z$$

$$J(I, NO_3, PO_4) = \min(J_{OI}, J_{Omax} u_N, J_{Omax} u_P), \quad u_P = PO_4 / (k_P + PO_4),$$

$$J_{OI} = \frac{J_{Omax} \alpha I}{[J_{Omax}^2 + (\alpha I)^2]^{1/2}} \quad J_{Omax} = a \times \exp(T/T_b)$$

$$w_D = \begin{cases} w_{D0} + m_w z, & z \leq 1000m \\ w_{D0} + m_w 1000m, & z > 1000m \end{cases},$$

$$\mu_D = \mu_{D0} \exp(T/T_b) [0.65 + 0.35 \tanh(O_2 - 6)]$$

$$S(O_2) = F_{sfc} - S(PO_4) R_{O:P} r_{sox}^{O_2}$$

$$Pr(CaCO_3) = ((1 - \gamma_1) G(P_O) Z + \mu_{P_2} P_O^2 + \mu_Z Z^2) R_{CaCO_3/POC} R_{C:P},$$

$$Di(CaCO_3) = \int Pr(CaCO_3) dz \cdot \frac{d}{dz} \left(e^{-z/D_{CaCO_3}} \right)$$

Schmittner et al. 2008 GBC