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# Innhold

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# Kapittel 1

## Continuum Mechanics

When studying the dynamics of a medium with fluid or structure properties under the influence of forces, we need in some sense a good description of how these forces act and alter the system itself.

Any medium on a microscopic scale is built up of a structure of atoms, meaning we can observe empty spaces between each atom or discontinuities in the medium. Describing any physical phenomenon on larger scales in such a way are tedious and most often out of bounds due to the high number of particles. Instead we consider the medium to be continuously distributed throughout the entire region it occupies. Hence we want to study some physical properties of the complete volume and not down on atomic scale.

We consider the medium with continuum properties. By a continuum we mean a volume  $V(t) \subset \mathbb{R}^3$  consisting of particles, which we observe for some properties. One property of interest could be the velocity  $\mathbf{v}(x, t)$  for some point  $x \in V(t)$  in time  $t \in (0, T]$ , which would mean the average velocity of the particles occupying this point  $x$  at time  $t$ . The intention of this chapter is not to give a thorough introduction of continuum mechanics, but rather present key concepts needed for the evaluation of fluid-structure interaction.

### 1.1 Coordinate system

We assume that our medium is continuously distributed throughout its own volume, and we start our observation of this medium at some time  $t_0$ . As this choice is arbitrary, we often choose to observe a medium in a stress free initial state. We call this state  $V(t_0)$  of the medium as the *reference configuration*. We let  $V(t)$  for  $t \geq t_0$  denote the *current configuration*.

#### 1.1.1 Lagrangian

As the medium is acted upon by forces, one of the main properties of interest is the deformation. Let  $\hat{x}$  be a particle in the reference configuration  $\hat{x} \in \hat{V}$ . Further let  $x(\hat{x}, t)$  be the new location of a particle  $\hat{x}$  for time  $t$  such that  $x \in V(t)$ . We assume that no two particles  $\hat{x}_a, \hat{x}_b \in \hat{V}$  occupy the same location for some time  $V(t)$ . Hence the map  $\hat{T}(\hat{x}, t) = x(\hat{x}, t)$  maps a particle  $\hat{x}$  from the *reference configuration*  $\hat{V}$  to the *current configuration*  $V(t)$ . Assuming that the path for some  $\hat{x}$  is continuous in time, we can define the inverse mapping  $\hat{T}^{-1}(x, t) = \hat{x}(x, t)$ , which maps  $x(\hat{x}, t)$  back to its initial location at time  $t = t_0$ .

We now have enough background to define the *deformation*

$$\hat{T}(\hat{x}, t) = \mathbf{u}(\hat{x}, t) + \hat{x} = x(\hat{x}, t) - \hat{x} \quad (1.1)$$

and the *deformation velocity*

$$\frac{\partial \hat{\mathbf{T}}(\hat{\mathbf{x}}, t)}{\partial t} = \hat{\mathbf{v}}(\hat{\mathbf{x}}, t) = d_t x(\hat{\mathbf{x}}, t) = d_t \hat{\mathbf{u}}(\hat{\mathbf{x}}, t) \quad (1.2)$$

Such a description of tracking each particle  $\hat{\mathbf{x}} \in \hat{\mathbf{V}}$  is often denoted the *Lagrangian Framework* and is a natural choice of describing structure mechanics.

### 1.1.2 Eulerian

Considering a flow of fluid particles in a river, a *Lagrangian* description of the particles would be tedious as the number of particles entering and leaving the domain quickly rise to a immense number. Instead consider defining a view-point  $V$  fixed in time, and monitor every fluid particle passing the coordinate  $x \in V(t)$  as time elapses. Such a description is defined as the *Eulerian framework*. It is important to mention that the we are not interested in which particle is occupying a certain point in our domain, but only its properties. Such a description falls natural for describing fluid dynamics.

We can describe the particles occupying the *current configuration*  $V(t)$  for some time  $t \geq t_0$

$$x = \hat{\mathbf{x}} + \hat{\mathbf{u}}(\hat{\mathbf{x}}, t)$$

Since our domain is fixed can define the deformation for a particle occupying position  $x = x(\hat{\mathbf{x}}, t)$  as

$$\mathbf{u}(x, t) = \hat{\mathbf{u}}(\hat{\mathbf{x}}, t) = x - \hat{\mathbf{x}}$$

and its velocity

$$\mathbf{v}(x, t) = \partial_t u(x, t) = \partial_t \hat{\mathbf{u}}(\hat{\mathbf{x}}, t) = \hat{\mathbf{v}}(\hat{\mathbf{x}}, t)$$

## 1.2 Deformation gradients

When studying continuum mechanics we observe continuous mediums as they are deformed over time. These deformations results in relative changes of positions due to external and internal forces acting.. These relative changes of position is called *strain*, and is the primary property that causes *stress* within a medium of interest [?]. We define stress as the internal forces that particles within a continuous material exert on each other.

The equations of mechanics can be derived with respect to either a deformed or undeformed configuration of our medium of interest. The choice of referring our equations to the current or reference configuration is indifferent from a theoretical point of view. In practice however this choice can have a severe impact on our strategy of solution methods and physical of modelling. [?]. We will therefore define the strain measures for both configurations of our medium.

**Definition 1.2.1.** Deformation gradient.

$$\hat{\mathbf{F}} = I + \hat{\nabla} \hat{\mathbf{u}} \quad (1.3)$$

Mind that deformation gradient of  $\hat{\mathbf{u}}$  is which respect to the reference configuration. From the assumption that no two particles  $\hat{\mathbf{x}}_a, \hat{\mathbf{x}}_b \in \hat{\mathbf{V}}$  occupy the same location for some time  $V(t)$ , the presented transformation must be linear. As a consequence from the invertible matrix theorem found in linear algebra, the linear operator  $\hat{\mathbf{F}}$  cannot be a singular. We define the *determinant of the deformation gradient* as  $J$ , which denotes the local change of volume of our domain.

**Definition 1.2.2.** Determinant of the deformation gradient

$$J = \det(\hat{\mathbf{F}}) = \det(I + \hat{\nabla} \hat{\mathbf{u}}) \neq 0 \quad (1.4)$$

By the assumption that the medium can't be selfpenetrated, we must limit  $J$  to be greater than 0 [?]

### 1.3 Measures of Strain and Stress

The equations describing forces on our domain can be derived in accordance with the current or reference configuration. With this in mind, different measures of strain can be derived according to which configuration we are interested in. We will here by [?] show the most common measures of strain. We will first introduce the right *Cauchy-Green* tensor  $\mathbf{C}$ , which is one of the most used strain measures [?].

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Let  $\hat{\mathbf{x}}, \hat{\mathbf{y}} \in \hat{\mathbf{V}}$  be two points in our referemce configuration and let  $\hat{\mathbf{a}} = \hat{\mathbf{y}} - \hat{\mathbf{x}}$  denote the length of the line bewtween these two points. As our domain undergoes deformation let  $\mathbf{x} = \hat{\mathbf{x}} + \hat{\mathbf{u}}(\hat{\mathbf{x}})$  and  $\mathbf{y} = \hat{\mathbf{y}} + \hat{\mathbf{u}}(\hat{\mathbf{y}})$  be the position of our points in the current configuration, and let  $\mathbf{a} = \mathbf{y} - \mathbf{x}$  be our new line segment. By [?] we have by first order Taylor expansion

$$\begin{aligned} \mathbf{y} - \mathbf{x} &= \hat{\mathbf{y}} + \hat{\mathbf{u}}(\hat{\mathbf{y}}) - \hat{\mathbf{x}} - \hat{\mathbf{u}}(\hat{\mathbf{x}}) = \hat{\mathbf{y}} - \hat{\mathbf{x}} + \hat{\nabla} \hat{\mathbf{u}}(\hat{\mathbf{x}})(\hat{\mathbf{y}} - \hat{\mathbf{x}}) + \mathcal{O}(|\hat{\mathbf{y}} - \hat{\mathbf{x}}|^2) \\ \frac{\mathbf{y} - \mathbf{x}}{|\hat{\mathbf{y}} - \hat{\mathbf{x}}|} &= [I + \hat{\nabla} \hat{\mathbf{u}}(\hat{\mathbf{x}})] \frac{\hat{\mathbf{y}} - \hat{\mathbf{x}}}{|\hat{\mathbf{y}} - \hat{\mathbf{x}}|} + \mathcal{O}(|\hat{\mathbf{y}} - \hat{\mathbf{x}}|) \end{aligned}$$

This detour from [?] we have that

$$\begin{aligned} \mathbf{a} &= \mathbf{y} - \mathbf{x} = \hat{\mathbf{F}}(\hat{\mathbf{x}})\hat{\mathbf{a}} + \mathcal{O}(|\hat{\mathbf{a}}|^2) \\ |\mathbf{a}| &= \sqrt{(\hat{\mathbf{F}}\hat{\mathbf{a}}, \hat{\mathbf{F}}\hat{\mathbf{a}}) + \mathcal{O}(|\hat{\mathbf{a}}|^3)} = \sqrt{(\hat{\mathbf{a}}^T, \hat{\mathbf{F}}^T \hat{\mathbf{F}} \hat{\mathbf{a}}) + \mathcal{O}(|\hat{\mathbf{a}}|^2)} \end{aligned}$$

We let  $\hat{\mathbf{C}} = \hat{\mathbf{F}}^T \hat{\mathbf{F}}$  denote the right *Cauchy-Green tensor*. By observation the Cauchy-Green tensor is not zero at the reference configuration

$$\hat{\mathbf{C}} = \hat{\mathbf{F}}^T \hat{\mathbf{F}} = (I + \hat{\nabla} \hat{\mathbf{u}})^T (I + \hat{\nabla} \hat{\mathbf{u}}) = I$$

Hence it is convenient to introduce a tensor which is zero at the reference configuration. We define the *Green-Lagrange strain tensor*, which arises from the squard rate of change of the linesegment  $\hat{\mathbf{a}}$  and  $\mathbf{a}$ . By using the definition of the Cauchy-Green tensor we have the relation

$$\begin{aligned} \frac{1}{2}(|\mathbf{a}|^2 - |\hat{\mathbf{a}}|^2) &= \frac{1}{2}(\hat{\mathbf{a}}^T \hat{\mathbf{C}} \hat{\mathbf{a}} - \hat{\mathbf{a}}^T \hat{\mathbf{a}}) + \mathcal{O}(|\hat{\mathbf{a}}|^3) = \hat{\mathbf{a}}^T \left( \frac{1}{2}(\hat{\mathbf{F}}^T \hat{\mathbf{F}} - I) \right) \hat{\mathbf{a}} + \mathcal{O}(|\hat{\mathbf{a}}|^3) \\ \hat{\mathbf{E}} &= \frac{1}{2}(\hat{\mathbf{C}} - I) \end{aligned}$$

Both the *right Cauchy-Green tensor*  $\hat{\mathbf{C}}$  and the *Green-Lagrange*  $\hat{\mathbf{E}}$  are refered to the Lagrangian coordinate system, hence the *reference configuration*.

Strain itself is nothing else than the measurement of linesegments under derformation. Therefore strain alone is purley an observation, and it is not dependent on the material of interest. but one expects that a material undergoing strain, will give for forces within the material.

### 1.4 Transformations of conservation laws

To be clear later, transformation of conservation principles from Eulerian coordinates to other coordinate systems are essential for deriving the equations of fluid-structure interaction. These conservation laws often has some spatial or temporal derivaties, and the essence is how to we transform these operators between our coordinate systems.

With this in mind, we will derive these transformations with the help of a new arbitrary fixed reference system  $\hat{\mathbf{W}}$ . We will throughout this subsection follow the ideas and approaches found in [?]. Further we denote its deformation gradient as  $\hat{\mathbf{F}}_w$  and its determinant  $\hat{\mathbf{J}}_w$ . Then the invertibale mapping  $\hat{\mathbf{T}}_w : \hat{\mathbf{W}} \rightarrow V(t)$  exists.

For  $\hat{\mathbf{V}} = \hat{\mathbf{W}}$ ,  $\hat{\mathbf{W}}$ , simply denotes the familiar Lagrangian description. In the case  $\hat{\mathbf{V}} \neq \hat{\mathbf{W}}$ ,  $\hat{\mathbf{W}}$  have

no direct physical meaning. Hence it is important to notice that the physical velocity  $\frac{\partial \hat{\mathbf{v}}}{\partial t}$  and the velocity of arbitrary domain  $\frac{\partial \hat{\mathbf{W}}_w}{\partial t}$  doesn't necessarily coincide. This observation is essential, as we will soon see.

We will first consider the transformation of spatial derivatives from  $V(t)$  to  $\hat{W}$

**Lemma 1.4.1.** Let  $f$  be a function  $f : V(t) \rightarrow \mathbb{R}$  and  $\mathbf{w} : \mathbb{R}^d \rightarrow \mathbb{R}^d$  be a vectorfield. Then the spatial transformation from  $V(t)$  to  $\hat{W}$  is defined as

$$\nabla f = \hat{\mathbf{F}}_W^{-T} \hat{\nabla} \hat{f}, \quad \nabla \mathbf{w} = \hat{\nabla} \hat{\mathbf{f}} \hat{\mathbf{F}}_W^{-1}$$

**Lemma 1.4.2.** Let  $f$  be a function  $f : V(t) \rightarrow \mathbb{R}$ . Then the temporal transformation from  $V(t)$  to  $\hat{W}$  is defined as

$$\frac{\partial f}{\partial t} = \frac{\partial \hat{f}}{\partial t} - (\hat{\mathbf{F}}_W^{-1} \hat{\mathbf{v}} \cdot \hat{\nabla}) \hat{f} + \hat{\mathbf{F}}_W^{-T} \hat{\nabla} \hat{f} \cdot \hat{\mathbf{v}}$$

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## 1.5 Conservation laws

### 1.5.1 Conservation of continuum

### 1.5.2 Conservation of momentum

## 1.6 The fluid

We assume an incompressible Newtonian fluid, described by the usual Navier-Stokes equations. We define the fluid density as  $\rho_f$  and fluid viscosity  $\nu_f$  to be constant in time. Our physical unknowns fluid velocity  $v_f$  and pressure  $p_f$  both live in the time-dependent fluid domain  $\hat{\Omega}_f(t)$ . Let any Dirichlet boundary conditions be defined as  $v_f^D, p_f^D$  on the boundaries of  $\hat{\Omega}_f(t)$ , and let  $g_1$  denote the Neumann conditions of  $\sigma_f \cdot n$  defined on the boundaries of  $\hat{\Omega}_f(t)$ .

## 1.7 The solid

For the structure we use the Saint-Venant-Kirchhoff (STVK) model of deformation of solids. We usually describe the material elasticity by two parameters, Lamé coefficients  $\lambda_s$  and  $\mu_s$  or the Poisson ratio  $\nu_s$  and the Young modulus  $E_s$  [?]. INSERT RELATIONS

### 1.7.1 Material models, St. Venant Kirchhoff material, incomp neo-Hookean material



## Kapittel 2

# Fluid Structure Interaction

The concepts of Fluid-structure interaction are often introduced in several engineering fields, for example biomechanics and hydrodynamics. As we will see throughout this chapter, one of the main challenges of this field is that our governing equations describing fluid and solids are defined on different coordinate systems. Recall from chapter 1, that the solid equations are often described in the *Lagrangian coordinate system*, while the fluid equations are on the contrary described in the *Eulerian coordinate system*.

We define  $\Omega$  in the *reference configuration* be partitioned in a fluid domain  $\hat{\Omega}_f$  and a structure domain  $\hat{\Omega}_s$  such that  $\Omega = \hat{\Omega}_f \cup \hat{\Omega}_s$ . Further we define the interface  $\hat{\Gamma}$  as the intersection between these domains such that  $\Gamma_i = \partial\hat{\Omega}_f \cap \partial\hat{\Omega}_s$ . A natural dilemma arises as the domain  $\Omega$  undergoes deformation over time. If the natural coordinate system are used for  $\hat{\Omega}_f$  and  $\hat{\Omega}_s$ , the domains doesn't match and the interface  $\hat{\Gamma}$  doesn't have a general description for both domains. As such only one of the domains can be described in its natural coordinate system, while the other domain needs to be defined in some transformed coordinate system.

The scope of FSI methods can formally be divided into *interface-tracking* and *interface-capturing* methods.[?]. In the *interface-tracking* literature, the *arbitrary Lagrangian-Eulerian* formulation is dominant approach [3], [?]. In this approach the structure is given in its natural *Lagrangian coordinate system*, while the fluid is transformed into an artificial *Lagrangian* coordinate system. From this approach tracking of the interface  $\hat{\Gamma}$  is more trivial, as it is fixed on a *reference system* and can be tracked by mappings defined in Chapter 2.

While *interface-capturing* are also defined on a fixed mesh, the interface  $\hat{\Gamma}$  is now moving over the mesh element. Hence by its name, the interface must be tracked as it is moving in time.

Initially one of the *interface-capturing* methods, the *fully Eulerian approach* was considered, but difficulty in tracking the interface in time was unsuccessful. Therefore ALE approach was finally chosen for this thesis. As such both the *fully Eulerian* and *ALE* concepts will be introduced following sub-chapters.

### 2.0.1 Fully Eulerian

This method keeps the fluid in its *Eulerian coordinates*, and such can be seen as the natural counterpart of the ALE method [?]. First proposed by [2].

### 2.0.2 Arbitrary Lagrangian Eulerian

The ALE method was initially developed to combine the strengths of the *Lagrangian* and *Eulerian* coordinate systems. As pointed out in chapter 2, the *Lagrangian* description is useful for tracking particles as they are acted upon by forces. Hence its main contribution is the ability to track interfaces and materials with history. We choose to keep the structure in its *Lagrangian coordinate system*, and to transform the fluid domain into an artificial coordinate system similar to the *Lagrangian coordinate*

*system*. It is however important to note that there is no natural displacement in the fluid domain, hence this domain has no directly physical meaning [3], [1].

### **Strong and weak coupling**

One of the major aspects of Fluid-structure interaction is the coupling of the fluid and solid equations. As the total system is exerted by external forces, the interface  $\hat{\Gamma}$  must fulfill the physical equilibrium of forces given by the two domains. Therefore, it is critical that the transmission of forces from the two domains are fulfilled in a consistent way.

# Bibliografi

- [1] J Donea, A Huerta, J.-Ph Ponthot, and A Rodríguez-Ferran. Arbitrary Lagrangian-Eulerian methods. (1969):1–38, 2004.
- [2] Th Dunne. An Eulerian approach to uid – structure interaction and goal-oriented mesh adaptation. *International Journal for Numerical Methods in Fluids*, (December 2005):1017–1039, 2006.
- [3] Thomas Dunne and Rolf Rannacher. Adaptive Finite Element Approximation of Fluid-Structure Interaction Based on an Eulerian Variational Formulation. *Fluid-Structure Interaction*, 53:110–145, 2006.
- [4] T. Richter and T. Wick. Finite elements for fluid-structure interaction in ALE and fully Eulerian coordinates. *Computer Methods in Applied Mechanics and Engineering*, 199(41-44):2633–2642, 2010.
- [5] Thomas Richter. Fluid Structure Interactions. 2016.
- [6] P. Wriggers. *Computational contact mechanics, second ed.*, Springer. 2006.