

11.4 CASE 4: - find shear stress at wall
- relate stress to body force.

Flow down along a rod (gravity forced flow)

$$v_z = \frac{ga^2}{2\nu} \left[\frac{b^2}{a^2} \ln\left(\frac{r}{a}\right) + \frac{1}{2} \left(1 - \frac{r^2}{a^2}\right) \right] \quad (11.11)$$

Can take $\frac{dv_z}{dr} \Big|_{r=a}$ or let's start from

the differential N-S eqn: (simplified)

$$\frac{1}{r} \frac{d}{dr} \left(r \frac{dv}{dr} \right) = - \frac{g}{\nu}$$

$$\text{integrate: } \int_a^b d\left(r \frac{dv}{dr}\right) = \int_a^b -\frac{g}{\nu} r dr$$

$$- a \frac{dv}{dr} \Big|_a = - \frac{g}{\nu} \left(\frac{b^2}{2} - \frac{a^2}{2} \right)$$

$$\tau_a = \mu \frac{dv}{dr} \Big|_a = \gamma \left(\frac{b^2}{2a} - \frac{a}{2} \right)$$

$$\tau_a = \frac{\gamma}{2a} (b^2 - a^2)$$

Over length l along the rod:

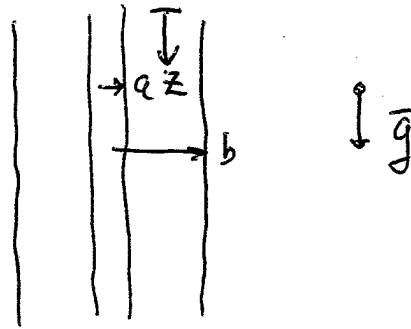
$$\text{Friction force} = \tau_a 2\pi a l$$

$$\text{fluid Weight} = \gamma V_{\text{fluid}} = \gamma \pi l (b^2 - a^2)$$

$$F_{\text{shear}} = \tau_a 2\pi a l = W = \gamma \pi l (b^2 - a^2)$$

insert expression for τ_a - they match

11.9



Fully developed flow
 $P = \text{const.}$
(gravity driven flow).

Reduce N-S eqn. & give B.C.

- Use cylindrical coord. z direction (down)

$$\rho \left(\frac{\partial v_z}{\partial t} + v_r \frac{\partial v_z}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_z}{\partial \theta} + v_z \frac{\partial v_z}{\partial z} \right) = - \frac{\partial P}{\partial z} + \rho g_z + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2} + \frac{\partial^2 v_z}{\partial z^2} \right]$$

From given conditions:

$$v_r = v_\theta = 0$$

$$\frac{\partial v_z}{\partial z} = 0 \quad \frac{\partial v_z}{\partial t} = 0$$

$$\frac{\partial P}{\partial z} = 0$$

so: no accel. terms

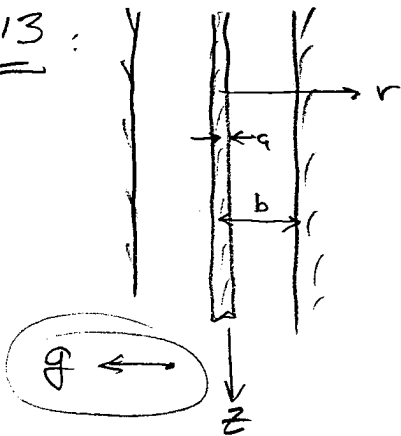
$$0 = \rho g_z + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) \right]$$

can also write as:

$$0 = \gamma + \mu \left[\frac{\partial^2 v_z}{\partial r^2} + \frac{1}{r} \frac{\partial v_z}{\partial r} \right]$$

by expanding visc. term derivative

11.13 :



• Thin wire drawn down the centerline of a pipe.

• Steady, incompressible, laminar fully developed flow.

• Use cylindrical coordinates for flow in a pipe.

• z mom. eqn: (10.22)

0 (horizontal)

$$\underbrace{\frac{\partial v_z}{\partial t}}_{0 \text{ (steady)}} + \underbrace{v_r \frac{\partial v_z}{\partial r}}_0 + \underbrace{\frac{v_\theta}{r} \frac{\partial v_z}{\partial \theta}}_0 + \underbrace{v_z \frac{\partial v_z}{\partial z}}_{0 \text{ (fully developed)}} = -\gamma \frac{\partial h}{\partial z} - \frac{\partial P}{\partial z} + \mu \nabla^2 v_z$$

$$0 = -\frac{\partial P}{\partial z} + \mu \left(\underbrace{\frac{\partial^2 v_z}{\partial r^2}}_{0 \text{ (stated as zero)}} + \underbrace{\frac{1}{r} \frac{\partial v_z}{\partial r}}_0 + \underbrace{\frac{1}{r^2} \frac{\partial^2 v_z}{\partial \theta^2}}_0 + \underbrace{\frac{\partial^2 v_z}{\partial z^2}}_0 \right)$$

Final Form

$$0 = \mu \left(\frac{\partial^2 v_z}{\partial r^2} + \frac{1}{r} \frac{\partial v_z}{\partial r} \right)$$

$$0 = \mu \left(\frac{1}{r} \frac{d}{dr} \left(r \frac{dv_z}{dr} \right) \right)$$

B.C. :

$$r = b \quad v_z = 0$$

$$r = a \quad v_z = V_w \quad (\text{velocity of moving wire}).$$

11.15

$$F = \int_0^l \zeta_w z \pi a dz = 2 \pi a l \zeta_w$$

$$\zeta_w = -\mu \frac{\partial v_z}{\partial r} = -\mu \frac{C_1}{r} = -\mu \frac{V_w}{r \ln(r_b)}$$

$$F = 2 \mu \pi l \frac{V_w}{\ln(a/b)}$$

C_1 is from integration const. (see 11.14)

$$\frac{\partial}{\partial r} \left(r \frac{\partial v_z}{\partial r} \right) = 0$$

$$r \frac{\partial v_z}{\partial r} = C_1 \rightarrow v_z = C_1 \ln r + C_2$$

$$\text{at } r=a \quad v_z = V_w$$

$$\text{at } r=b \quad v_z = 0 \quad \text{so } C_2 = -C_1 \ln b.$$