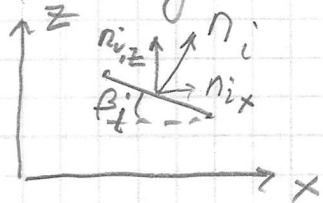


# MORE NOTES ON PANEL METHOD

A slightly more general form: cambered plate  
(X is along chord line)



• if  $n_i$  is on a tilted panel relative to  $z$ :

•  $\beta$  is angle from chord line.

So here the outward normal,  $n_i$ , is a

vector with  $x$  comp. =  $\sin \beta_i$

$z$  comp =  $\cos \beta_i$

if no camber  $\beta = 0$  &  $n_i$  is in  $z$  direction

Our general B.C. eqn. at the collocation pt.

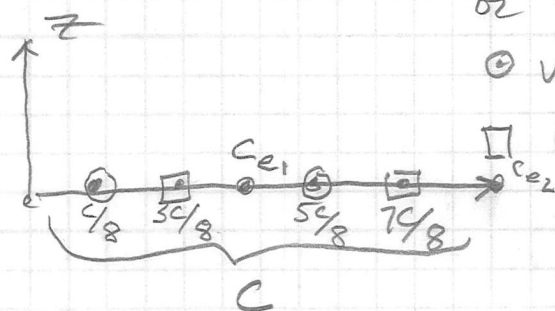
$$g \cdot n = -U \cdot n$$

(here  $g$  is induced flow by vortices)

induced flow by all vortices.

Flow from free stream

Two panels - no camber; each panel length =  $\frac{C}{2}$   
or  $C_e = \frac{C}{2}$



○ vortex centers

□ collocation pts

Write eqn. for  $g$  (or  $v$ ) in general:

note here:  $\eta(x)$  = surface location = 0 ( $z=0$ )

In general the surface may have some  $x_s, z_s$  curve:  
curve:  $\eta(x) = f(x)$  for curve:

Gen. eqn. For  $(u, w)$

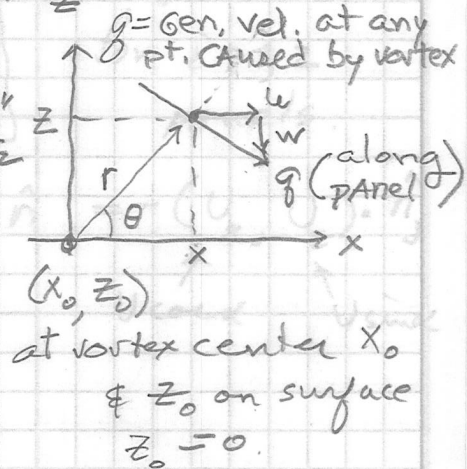
5

$$u = \frac{\Gamma}{2\pi} \frac{(z - z_0)}{(x - x_0)^2 + (z - z_0)^2}$$

$$w = \frac{-\Gamma}{2\pi} \frac{(x - x_0)}{(x - x_0)^2 + (z - z_0)^2}$$

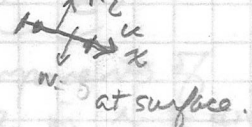
$$\frac{r \sin \theta}{r^2} = \frac{z}{r^2}$$

$$\frac{r \cos \theta}{r^2} = \frac{x}{r^2}$$



We are interested in pts. on surface where  $z = z_0$   
or we end up with:

$$\begin{pmatrix} u \\ w \end{pmatrix} = \frac{\Gamma}{2\pi r^2} \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \begin{pmatrix} x - x_0 \\ z - z_0 \end{pmatrix} \quad \text{on surface:}$$



We write  $\begin{pmatrix} u \\ w \end{pmatrix}$  for "unit gamma"  $\Gamma = 1$  at  $z = z_0$  (on surface).

with vortex located at  $1/4$  of each element

Note: Vortex generates no  $x$  comp. of vel. on surface!!

Define  $u_{ij}$  &  $w_{ij}$  ( $\Gamma = 1$ )  $i$  = vel. at collocation  $i$   
 $j$  = vel. from vortex at  $j$

$$u_{11}, w_{11} = \left(0, -\frac{1}{2\pi c}\right) = \left(0, -\frac{z}{\pi c}\right) \quad \text{For } \frac{1}{4} \text{ PANEL}$$

$$u_{11} = 0 \text{ since } z = z_0 \text{ (see above eqn.)}$$

$$\rightarrow w_{11} = \frac{-1}{2\pi (x - x_0)^2} = \frac{-1}{2\pi (x - x_0)} = \frac{-1}{2\pi \left(\frac{3c}{8} - \frac{c}{8}\right)} = \frac{-1}{2\pi c} = \frac{-z}{\pi c}$$

$$w_{21} = \frac{-z}{3\pi c}$$

$$w_{12} = \frac{z}{\pi c}$$

$$w_{22} = \frac{-z}{\pi c}$$

← positive because  $(x - x_0)$  is neg. along  $x$  axis.

define:  $a_{ij} = g_{ij}(\Gamma = 1) \cdot \hat{n}_i$

We use this in our B.C. at the surface:

define:  $\bar{g} \cdot \hat{n} = \sum_{j=1}^2 a_{ij} \Gamma_j$  for  $i=1, 2$  panels.

This is set equal to  $-U \cdot \hat{n} = -(U_x, U_z) \cdot \hat{n}_j$   
to satisfy B.C. of zero flow across the boundary  
 $U \cos \alpha$   $U \sin \alpha$

So we end up with:

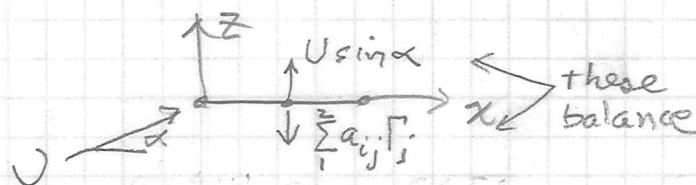
$$\sum_{j=1}^2 a_{ij} \Gamma_j = -(U_x, U_z) \cdot (n_{ix}, n_{iz})$$

components of  $n_i$  in  $x, z$  directions

For our 2 panels with  $\eta=0$

$$\begin{pmatrix} w_{11} & w_{12} \\ w_{21} & w_{22} \end{pmatrix} \begin{pmatrix} \Gamma_1 \\ \Gamma_2 \end{pmatrix} = U \sin \alpha \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

for the case of outward normal in  $z$  direction.



Solve for  $\Gamma_1, \dots, \Gamma_N$

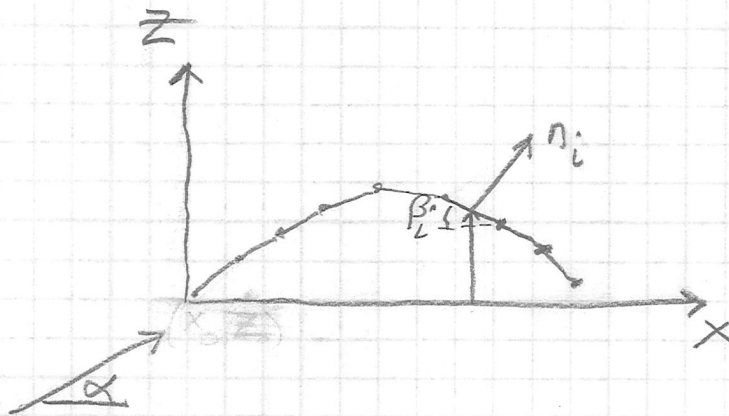
Lift from each panel:  $\Delta L_i = \rho U_\infty \Gamma_i$

here  $\rho U_\infty$  so no neg. sign.

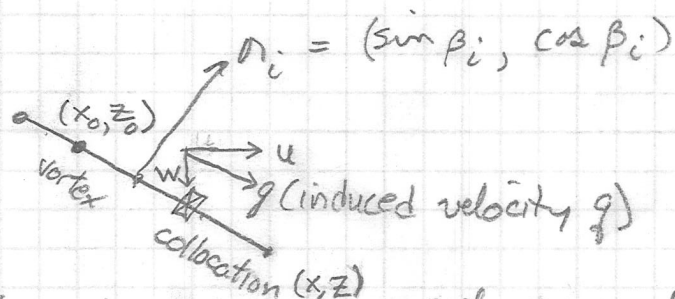
Total Lift  $L = \sum_{i=1}^N \Delta L_i$

and  $C_L = \frac{L}{\frac{1}{2} \rho U^2 c}$  also  $M_o = - \sum_{i=1}^N \Delta L x_{oij}$

# General Diagram for B.C.



- define panel end pts in terms of  $(x, z)$
- locate vortex & collocation pts for each panel



at panel  $i = j$

$$a_{ij} = (u, w)_{ij} \cdot n_i \rightarrow \text{vel. normal to surface by induced vortex flow at collocation } i \text{ by vortex element } j.$$

$(x_0, z_0)$  is at vortex location

which is  $\frac{1}{2}$  length of panel from start of panel.

$(x, z)$  is at collocation pt. (where velocity is evaluated)

So, must determine  $(u, w)_{ij}$  for  $i = j$ ; then take dot product with  $n_i$  to find  $a_{ij}$