

Assign #1 Soln. Guide - F'16

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1. N-S eqn. tensor notation: (incompressible, $\mu = \text{const.}$)

(+5)
$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = \rho g_i - \frac{\partial P}{\partial x_i} + \mu \left(\frac{\partial^2 u_i}{\partial x_j \partial x_j} \right)$$

• scales: vel. = U

press. = $\frac{\mu U}{L}$

$\frac{L}{U}$ = time, t

replace $u_i = U u_i^*$

$P = \frac{\mu U}{L} P^*$

$t = \frac{L}{U} t^*$

$x_i = L x_i^*$

insert into N-S eqn. and rearrange:

(+10) result:
$$\frac{\partial u_i^*}{\partial t^*} + u_j^* \frac{\partial u_i^*}{\partial x_j^*} = \frac{1}{Fr} + \frac{1}{Re} \left(-\frac{\partial P^*}{\partial x_i^*} + \frac{\partial^2 u_i^*}{\partial x_j^* \partial x_j^*} \right)$$

There are two parameters: $Re = \frac{\rho U L}{\mu} = \frac{\text{inertia}}{\text{visc. force}}$

(+5)
$$Fr = \frac{U^2}{gL} = \frac{\text{inertia}}{\text{body force}}$$

2. If you mult. by Re then let $Re \rightarrow 0$.

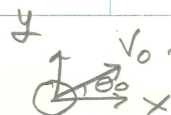
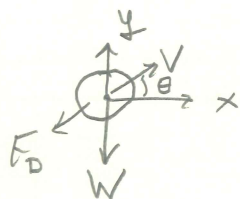
(+5)
$$0 = \left(-\frac{\partial P^*}{\partial x_i^*} + \frac{\partial^2 u_i^*}{\partial x_j^* \partial x_j^*} \right)$$

eliminates inertia terms (no accel.) or body

(+5) force terms; Left with balance of Press. & visc. forces.

3. Trajectory Problem

FBD



F_D opposite to V

W always in neg. y
(x is horizontal, y vertical)

$$D = Lm = L$$

$$W = 1 \text{ kg} (9.8 \text{ m/s}^2) = 9.8 \text{ N}$$

$$\rho_{\text{fluid}} = \rho = 10 \text{ kg/m}^3$$

V_0 = initial vel. at 45°

$$F_D = C_D \frac{\rho V^2}{2} A_f \quad A_f = \frac{\pi D^2}{4}$$

C_D = const. in 3. C.

a. $\Sigma F = m \frac{dV}{dt} = \vec{F}_D + \vec{W}$ (sign of F_D is shown pos. here but direction is imposed when writing component eqns.)

(+8) nondimensionalize:

$$m \frac{V_0^2}{D} \frac{dV^*}{dt^*} = - \left(\frac{C_D \rho A_f V_0^2}{2} \right) V^{*2} + \frac{\vec{W}}{W}$$

in nondim. form:

(+8) $\frac{dV^*}{dt^*} = \left(\frac{\rho C_D A_f g D V_0^2}{2 W V_0^2} \right) V^{*2} + \frac{\vec{W}}{W} \quad m = W/g$

$$\frac{dV^*}{dt^*} = \left(\frac{1}{F_r} \cdot F_D^* \right) V^{*2} + \frac{\vec{W} D g}{W V_0^2}$$

(+4) where: $F_r = \frac{V_0^2}{g D} \quad F_D^* = \frac{C_D \rho V_0^2 A_f}{2 W}$
(ratio inertia/body force)

ratio of
(drag coes. at
initial time to)
weight

b. (+5) $P_i = \frac{F_D^*}{F_r} = \frac{\text{initial drag coef}}{\text{body force}} \cdot \frac{\text{body force}}{\text{inertia}} \equiv \frac{\text{initial drag inertia}}{\text{inertia}} = \left[\frac{C_D \rho A_f g D}{2 W} \right]$
(Physical meaning)

Eqn. becomes:

$$\frac{dV^*}{dt^*} = -P_i V^{*2} + \frac{1}{F_r} \frac{\vec{W}}{W}$$

note if $P_i \rightarrow 0$ we have no drag force

(+5) let $P_2 = \frac{1}{F_r} = \frac{\text{body force}}{\text{inertia}} = \frac{g D}{V_0^2}$

Component Eqs.

$$\underline{x}: \quad (+5) \quad \frac{dV_x^*}{dt} = -P_1 V^{*2} \cos \theta = \frac{d^2 x^*}{dt^{*2}} \quad x^* = x/D$$

note: P_1 is initial drag force/inertia; here we use x comp.

$$\left\{ \begin{array}{l} (P_1 V^*)^z_x = P_1 V^{*2} \cos \theta; \text{ use } V^* \text{ not } V_x^* \text{ to find } F_D, \text{ then take } x \text{ component} \\ \text{also } W_x = 0 \end{array} \right.$$

• Integrate (numerically) from $t=0$: $V=V_0$ $\theta_0=45^\circ$ $x=0$

$$(+5) \quad (\text{note } V_x^*(t=0) = V_0 \cos 45^\circ) \quad P_1 = .001 \text{ \& } .01$$

$$\underline{y}: \quad (+5) \quad \frac{dV_y^*}{dt} = -P_1 V^{*2} \sin \theta - P_2 = \frac{d^2 y^*}{dt^{*2}} \quad y^* = y/D$$

where P_1 is same as in x eqn. (scalar)

$$P_2 = 2D/V_0^2 \text{ (scalar)}$$

$$V_y^* = V^* \sin \theta$$

$$W_y = W$$

$$\text{at } t=0 \quad V_y^* = 1 \sin 45^\circ, \quad y=0$$

(+5) Integrate for 2 values of P_1 \& 2 values of P_2
interpret

• as $P_1 \uparrow$ (increased drag) expect trajectory to be less (x_{end} decreases \& y_{max} decreases)

(+5) • as $P_2 \uparrow$ (less inertia) expect trajectory to be less.

Results show greater sensitivity to P_2

d. To convert to actual variables:

$$x = x^* D$$

$$y = y^* D$$

$$t = t^* \frac{D}{V_0}$$

if D is same for 2 cases then

trajectories look the same and all

values of x^* & y^* are multiplied by $D=1$

$$\text{for } P_1 = .01 = \frac{C_D \rho A V_0^2 D}{2W}$$

(+3)

$$C_D = P_1 2W / \rho \frac{\pi D^2}{4} V_0^2 = (.01) 2(9.8) / 10 \frac{\pi (.1)^2}{4} 9.8 (1)$$

$$= 2.54 \text{ (very high)}$$

$$\text{for } P_1 = .001 \quad C_D = 0.254 : C_D \sim P_1, \text{ all else given as constant}$$

(+3)

(This is very close to the drag coef. of a sphere at high Re).

$$\text{for } V_0: 5 \rightarrow 25 \text{ then } P_2 = \frac{g D}{V_0^2} \text{ ranges: } .0392 \rightarrow .0016.$$

(+5) So let $P_1 = .01$ (or .001) & solve for range of P_2 to find x_{\max}^* & y_{\max}^* then $x_{\max} = x_{\max}^* \times (.1)$; $y_{\max} = y_{\max}^* \times (.1)$

Example values

$$\begin{array}{ll} P_1 = .01 & \\ \bullet P_2 = .04 & x_{\max}^* = 21.25 \quad y_{\max}^* = 5.81 \end{array}$$

$$\bullet P_2 = .001 \quad \text{"} = 61. \quad \text{"} = 20.01$$

$$\bullet P_2 = .0016 \quad x_{\max}^* = 136 \quad y_{\max}^* = 58.0$$

interpret: decreasing P_2 means greater initial inertia so

(+4) expect x to increase & y to increase.

Typical results: Using nondimensional variables of x^* and y^* for the four set of P_1 and P_2 values.

