

At each simulation step  $t$  and for each  $\iota$ , the path length reflected by the  $\iota$ -th scatter  $l_t^{(\iota)} = |(x_t^\iota, y_t^\iota) - (0, 0)| + |(x_t^*, y_t^*) - (x_t^\iota, y_t^\iota)|$  and its derivative with respect to time  $\frac{d}{dt}l_t^{(\iota)}$  are computed. The corresponding transmission delay time  $\sigma_t^{(\iota)}$ , the constant phase offset  $\theta_t^{(\iota)}$ , and the Doppler frequency  $f_{D_t}^{(\iota)}$  caused by the  $\iota$ -th scatterer following the rules  $\sigma_t^{(\iota)} = l_t^{(\iota)}/c_0$ ,  $\theta_t^{(\iota)} = ((-l_t^{(\iota)} f_{\text{carrier}}/c_0) \bmod 1) \cdot 2\pi$ , and  $f_{D_t}^{(\iota)} = -\frac{d}{dt}l_t^{(\iota)} f_{\text{carrier}}/c_0$ , respectively, as well as the received signal amplitude  $a_t^{(\iota)}$  computed using the free-space propagation model  $a_t^{(\iota)} = c_0/(4\pi f_{\text{carrier}} l_t^{(\iota)})$  (cf.) are recorded for each scatterer  $\iota$ . (Here,  $c_0$  refers to the speed of light in vacuum.) In a setting without line of sight, using linearisation of the phase offset with respect to the Doppler frequency, the time-variant channel impulse response evaluated at time  $t + \tau$  for each simulation step  $t$  and small  $\tau$  resulting from the multipath transmission simulated using the above parameters can be approximated by

$$h(\cdot, t + \tau) = \frac{1}{\sqrt{\sum_{\iota=0}^{255} (a_t^{(\iota)})^2}} \sum_{\iota=0}^{255} a_t^{(\iota)} \exp(i\theta_t^{(\iota)} + i2\pi f_{D_t}^{(\iota)} \tau) \delta_{\sigma_t^{(\iota)}}(\cdot).$$

For any signal  $\{S_\tau\}_{0 \leq \tau < T}$  being transmitted in the block beginning at time step  $t$  through the simulated channel, this consideration leads to a received signal  $\{R_\tau\}_{0 \leq \tau < T}$  in the form of

$$\begin{aligned} R_\tau &= (h(\cdot, t + \tau) * S)(\tau) \\ &= \frac{1}{\sqrt{\sum_{\iota=0}^{255} (a_t^{(\iota)})^2}} \sum_{\iota=0}^{255} a_t^{(\iota)} \exp(i\theta_t^{(\iota)} + i2\pi f_{D_t}^{(\iota)} \tau) (\delta_{\sigma_t^{(\iota)}}(\cdot) * S)(\tau). \end{aligned} \quad (1)$$

This parametrisation is used in and delivers a realistic approximation of real-world scenarios for numbers of summands greater than 100. In order to allow continuous time delays to be applied to discrete time signals, the impulse function  $\delta_{\sigma_t^{(\iota)}}(\cdot)$  in (1) is convolved with a windowed sinc( $\cdot$ ) function scaled with a given bandwidth. Overall, the channel transmission including pulse shaping with bandwidth restricted to half the sample rate and additive noise is approximated by replacing the  $\delta_{\sigma_t^{(\iota)}}(\cdot)$  in (1) by  $\sin(\pi(\cdot/2))/(\pi(\cdot/2))\mathbf{1}_{[-8,8]}$  and adding independent and identically distributed Gaussian white noise  $\sim \mathcal{N}(0, \sigma^2)$  to the transmitted signal with power  $\sigma^2$  resulting in a signal-to-noise ratio of 12dB.

## 1 Channel Estimation

The time-variant channel transfer functions  $\mathcal{F}h(\cdot, t + \tau)$  for  $t = 0, \dots, 4095T$  and  $0 \leq \tau < T$  simulated in Section are approximated by a time series of block wise time-invariant transfer functions  $\{\mathcal{F}h^t\}_{t=0, \dots, 4095}$  based on which the estimation and prediction of the channel transmission are conducted. For each transmission block beginning at time step  $t$ , in order to estimate the corresponding channel transfer function  $\mathcal{F}h^t$ , a complex-valued (white noise) test signal  $\{\hat{S}_\tau^t\}_{\tau=0, \dots, N-1}$  whose Fourier transform has constant amplitude and random phases  $\sim \mathcal{U}(-\pi, \pi)$  is generated and then transmitted through the channel simulated in Section resulting in a received signal  $\{R_\tau^t\}_{\tau=0, \dots, N-1}$ .