

Obviously, if relaxation occurred with no constraints, the solution would be  $\vec{B} = \vec{0}$ .

However, there are constraints, and they turn out to be topological. This follows from the fact that Ideal MHD accepts a topological conserved magnetic quantity, named helicity.

### Helicity

Consider the quantity

$$H \equiv \iiint_V \vec{A} \cdot \vec{B} \, dV$$

where

$\vec{B} = \vec{\nabla} \times \vec{A}$ , and  $\vec{A}$  is the vector potential.

Let's prove some properties of  $H$ .

1. Helicity is well defined.

Not obvious, as we can always shift

$$\vec{A} \rightarrow \vec{A} + \vec{\nabla} \chi \quad \text{and not change } \vec{B}.$$

(a gauge transformation).

If we gauge transform we get

$$H \rightarrow H + \iiint_V \vec{B} \cdot \vec{\nabla} \chi \, dV$$

by parts

$$= H + \iiint_V (\vec{\nabla} \cdot (\vec{B} \chi) - \chi \vec{\nabla} \cdot \vec{B}) \, dV$$

divergence theorem

$$= H + \oint_{\partial V} \chi \vec{B} \cdot d\vec{S}$$

So if our volume encases the entire field  
then  $\vec{B} \cdot d\vec{S} = 0$  and  $H$  is unchanged.

## 2. Helicity is conserved

Induction equation

$$\frac{\partial \vec{B}}{\partial t} = \vec{\nabla} \times (\vec{u} \times \vec{B})$$

$$\therefore \frac{\partial (\vec{\nabla} \times \vec{A})}{\partial t} = \vec{\nabla} \times (\vec{u} \times \vec{B})$$

"uncurl"

$$\frac{\partial \vec{A}}{\partial t} = \vec{u} \times \vec{B} + \vec{\nabla} \chi$$

dot with  $\vec{B}$

$$\vec{B} \cdot \frac{\partial \vec{A}}{\partial t} = \frac{\partial (\vec{A} \cdot \vec{B})}{\partial t} - \vec{A} \cdot \frac{\partial \vec{B}}{\partial t}$$

$$\Rightarrow \frac{\partial (\vec{A} \cdot \vec{B})}{\partial t} = \vec{B} \cdot [\vec{u} \times \vec{B} + \vec{\nabla} \chi] - \vec{A} \cdot [\vec{\nabla} \times (\vec{u} \times \vec{B})]$$

term by term

$$\vec{B} \cdot (\vec{u} \times \vec{B}) = 0 \quad (\text{symmetry})$$

$$\vec{B} \cdot \vec{\nabla} \chi$$

$$= \vec{\nabla} \cdot (\vec{B} \chi) - \chi \vec{\nabla} \cdot \vec{B} = \vec{\nabla} \cdot (\vec{B} \chi)$$

$$\vec{A} \cdot [\vec{\nabla} \times (\vec{u} \times \vec{B})] = A_i \epsilon_{ijk} \partial_j \epsilon_{klm} u_l B_m$$

or  $A_i \epsilon_{ijk} \partial_j B_k$  <sup>by parts</sup>  $= \epsilon_{ijk} \partial_j (A_i B_k) - \epsilon_{ijk} B_k \partial_j A_i$

$$= - \overset{\text{one swap}}{\epsilon_{jik}} \partial_j (A_i B_k) + \overset{\text{three swap}}{\epsilon_{kji}} B_k \partial_j A_i$$

$$= - \vec{\nabla} \cdot (\vec{A} \times (\vec{u} \times \vec{B})) + (\vec{u} \times \vec{B}) \cdot (\vec{\nabla} \times \vec{A})$$

but  $\vec{\nabla} \times \vec{A} = \vec{B}$

so  $(\vec{u} \times \vec{B}) \cdot \vec{B} = 0$

and we are left with

$$= - \vec{\nabla} \cdot [\vec{A} \times (\vec{u} \times \vec{B})]$$

but  $\vec{A} \times (\vec{u} \times \vec{B})_i = \epsilon_{ijk} A_j \epsilon_{klm} u_l B_m$

$$= [\delta_{il} \delta_{jm} - \delta_{im} \delta_{jl}] A_j u_l B_m$$

$$= u_i (A_j B_j) - B_i (A_j u_j)$$

$$\therefore \vec{A} \cdot [\vec{\nabla} \times (\vec{u} \times \vec{B})] = - \vec{\nabla} \cdot (\vec{u} (\vec{A} \cdot \vec{B}) - \vec{B} (\vec{A} \cdot \vec{u}))$$

and so

$$\frac{\partial}{\partial t} (\vec{A} \cdot \vec{B}) = \vec{\nabla} \cdot [\vec{B} \chi + \vec{B} (\vec{A} \cdot \vec{u}) - \vec{u} (\vec{A} \cdot \vec{B})]$$

Integrate over total volume

$$\begin{aligned} \frac{\partial}{\partial t} \iiint_V \vec{A} \cdot \vec{B} dV &= \iiint_V \vec{\nabla} \cdot [\vec{B} (\chi + (\vec{A} \cdot \vec{u})) - \vec{u} (\vec{A} \cdot \vec{B})] dV \\ &= \oint_{\partial V} (\vec{B} \chi + \vec{B} (\vec{A} \cdot \vec{u}) - \vec{u} (\vec{A} \cdot \vec{B})) \cdot d\vec{S} \end{aligned}$$

= 0 as nothing ( $\vec{u}$  or  $\vec{B}$ )  
sticks out of the volume.

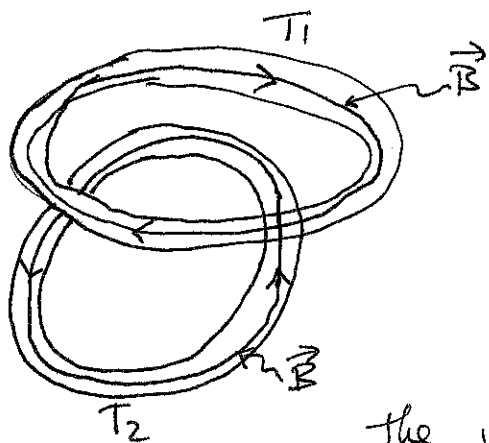
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$$\left( \frac{dH}{dt} = 0 \right)$$

this is the constraint subject to which  
energy may be minimised.

Helicity is a topological invariant

Consider two linked flux tubes [recall from Alfvén's theorem that these tubes forever enclose a field line]



Then the helicity of tube 1 is

$$H_1 = \iiint_{T_1} \vec{A} \cdot \vec{B} \, dV_{T_1}$$

the volume of the tube is  $\underbrace{d\vec{l} \cdot d\vec{S}}_{\substack{\text{unit along tube } \hat{b} \, dl \\ \text{surface of tube } \hat{b} \, dS}}$

thus

$$H_1 = \iiint_{T_1} \hat{b} \, dl \cdot \hat{b} \, dS \, \vec{A} \cdot (\hat{b} \vec{B})$$

$$= \underbrace{\iint_{T_1} \vec{B} \cdot d\vec{S}}_{\substack{\text{flux along tube 1} \\ \equiv \Phi_1}} \int_{T_1} \vec{A} \cdot d\vec{l} = \Phi_1 \int_{T_1} \vec{A} \cdot d\vec{l}$$

by Stoke's theorem  $\int_{T_1} \vec{A} \cdot d\vec{l} = \iint_{S_1} (\vec{\nabla} \times \vec{A}) \cdot d\vec{S}$

where  $S_1$  is the surface bounded by  $l_1$

as  $\vec{\nabla} \times \vec{A} = \vec{B}$

$$\int_{T_1} \vec{A} \cdot d\vec{l} = \iint_{S_1} \vec{B} \cdot d\vec{S}$$

Flux through middle of loop 1 =  $\Phi_2$

$$\Rightarrow H_1 = \Phi_1 \Phi_2$$

by the same token, in a system of many linked tubes, the helicity of tube  $i$  is

$$H_i = \Phi_i \Phi_{\text{through hole, } i} = \Phi_i \sum_{j \neq i} \Phi_j N_{ij}$$

flux of  $j^{\text{th}}$  tube  
↙  
number of linkages between  $i$  &  $j$

and thus the total helicity is

$$H = \sum_i \sum_{j \neq i} \Phi_i \Phi_j N_{ij}$$

Thus helicity measures the number of linkages of the flux tubes weighted by the field strength in each tube.

The physical insight is the following: if one thinks of the magnetic field as a tangled mess of field lines, while you can change this mess by moving field lines around, you cannot easily undo linkages, knots, etc.

[This is Alfvén's theorem again], Basically any operation which would require field lines to have "ends".

## Taylor Relaxation

We can now work out which equilibrium an MHD system will relax to by minimising its energy subject to constant helicity. This is a classic lagrange multiplier problem, with "action"

$$S = \iiint_V (B^2 - \alpha \vec{A} \cdot \vec{B}) dV$$

↑ lagrange multiplier.

then  $\delta S = 0$

implies

$$\delta \left[ \iiint_V (B^2 - \alpha \vec{A} \cdot \vec{B}) dV \right] = 0$$

first term

$$\begin{aligned} \delta \iiint_V B^2 dV &= 2 \iiint_V \vec{B} \cdot \delta \vec{B} dV \\ &= 2 \iiint_V \vec{B} \cdot (\vec{\nabla} \times \delta \vec{A}) dV \end{aligned}$$

$$\vec{B} \cdot (\vec{\nabla} \times \delta \vec{A}) = B_i \epsilon_{ijk} \partial_j \delta A_k =$$

$$= \epsilon_{ijk} \partial_j (B_i \delta A_k) - \epsilon_{ijk} \delta A_k \partial_j B_i$$

$$= \overset{\text{one swap}}{-\epsilon_{jik}} \partial_j (B_i \delta A_k) + \overset{\text{three swap}}{\delta A_k \epsilon_{kji}} \partial_j B_i$$

$$= -\vec{\nabla} \cdot (\vec{B} \times \delta \vec{A}) + \delta \vec{A} \cdot (\vec{\nabla} \times \vec{B})$$

$$\Rightarrow \delta \iiint_V B^2 dV = -2 \iiint_V \vec{\nabla} \cdot (\vec{B} \times \delta \vec{A}) dV + 2 \iiint_V \delta \vec{A} \cdot (\vec{\nabla} \times \vec{B}) dV$$



divergence theorem

$$= -2 \oint_{\partial V} (\vec{B} \times \delta \vec{A}) \cdot d\vec{S} + 2 \iiint_V (\vec{\nabla} \times \vec{B}) \cdot \delta \vec{A} dV$$

and

$$\begin{aligned} \delta \iiint_V \vec{A} \cdot \vec{B} dV &= \iiint_V \delta \vec{A} \cdot \vec{B} dV + \iiint_V \vec{A} \cdot \delta \vec{B} dV \\ &= \iiint_V \delta \vec{A} \cdot \vec{B} dV + \iiint_V \vec{A} \cdot (\vec{\nabla} \times \delta \vec{A}) dV \end{aligned}$$

identical manipulation to before on second term

$$= \iiint_V \delta \vec{A} \cdot \vec{B} dV - \iiint_V \vec{\nabla} \cdot (\vec{A} \times \delta \vec{A}) dV + \underbrace{\iiint_V (\vec{\nabla} \times \vec{A}) \cdot \delta \vec{A} dV}_{\vec{B}}$$

divergence theorem + combine 123

$$= 2 \iiint_V \vec{B} \cdot \delta \vec{A} dV - \oint_{\partial V} (\vec{A} \times \delta \vec{A}) \cdot d\vec{S}$$

we must worry about surface terms.

$$\text{As } \frac{\partial \delta \vec{B}}{\partial t} = \vec{\nabla} \times \left( \frac{\partial \vec{\xi}}{\partial t} \times \vec{B} \right) \quad \left[ \text{reintroducing } \delta \vec{u} = \frac{\partial \vec{\xi}}{\partial t} \right]$$

uncurling

$$\delta \vec{A} = \vec{\xi} \times \vec{B}$$

$$\begin{aligned} \text{As } \vec{A} \times \delta \vec{A} &= \vec{A} \times (\vec{\xi} \times \vec{B}) = \epsilon_{ijk} A_j \epsilon_{klm} \xi_l B_m \\ &= [\delta_{ie} \delta_{jm} - \delta_{im} \delta_{je}] A_j \xi_l B_m \\ &= (\vec{A} \cdot \vec{B}) \vec{\xi} - (\vec{A} \cdot \vec{\xi}) \vec{B} \end{aligned}$$

also

$$\vec{B} \times \delta \vec{A} = \epsilon_{ijk} B_j \epsilon_{klm} \delta B_l B_m$$

same argument

$$= B^2 \frac{\delta \vec{B}}{\delta B} - (\vec{B} \cdot \frac{\delta \vec{B}}{\delta B}) \vec{B}$$

and so all surface terms come with  $\frac{\delta \vec{B}}{\delta B} \cdot d\vec{S}$  or  $\vec{B} \cdot d\vec{S}$ , which will vanish if  $\delta V$  encloses both the magnetic field and the plasma.

Thus, we are left with

$$\delta \iiint_V (B^2 - \alpha \vec{A} \cdot \vec{B}) dV = 2 \iiint_V [\vec{\nabla} \times \vec{B} - \alpha \vec{B}] \cdot \delta \vec{A} dV$$
$$= 0$$

$$\therefore \vec{\nabla} \times \vec{B} = \alpha \vec{B} \Rightarrow \nabla^2 \vec{B} = -\alpha^2 \vec{B}$$

and we have recovered the

linear force free field.

So our system will relax to a linear force free state with system-specific boundary conditions.

The boundary conditions come in through the initial helicity, and our lagrange multiplier  $\alpha$  is a function  $\alpha = \alpha(H)$ , which enforces this

This linear force free state has a particularly simple helicity, which follows from

$$\vec{\nabla} \times \vec{B} = \alpha \vec{B} = \alpha \vec{\nabla} \times \vec{A} \Rightarrow \vec{B} = \alpha \vec{A} + \vec{\nabla} \chi$$

$$H(\alpha) = \iiint_V \vec{A} \cdot \vec{B} \, dV = \frac{1}{\alpha} \iiint_V B^2 \, dV - \frac{1}{\alpha} \iiint_V \vec{B} \cdot \vec{\nabla} \chi \, dV$$

Final term vanishes under volume integral

$$\begin{aligned} \iiint_V \vec{B} \cdot \vec{\nabla} \chi \, dV &= \iiint_V \vec{\nabla} \cdot (\vec{B} \chi) \, dV - \iiint_V \chi \vec{\nabla} \cdot \vec{B} \, dV \\ &= \oint_{\partial V} \chi \vec{B} \cdot d\vec{S} = 0 \quad [\text{enclose field}]. \end{aligned}$$

$\therefore$  Constant ' $\alpha$ ' set by

$$H = \frac{1}{\alpha} \iiint_V B^2 \, dV.$$

General procedure:

- solve  $\nabla^2 \vec{B} = -\alpha^2 \vec{B}$ , get  $\vec{B}(\vec{r}, \alpha)$ .
- Calculate  $H(\alpha) = \frac{1}{\alpha} \iiint_V B^2(\vec{r}, \alpha) \, dV$
- Set  $H(\alpha) = H_0$ , the initial value of helicity
- Set  $\alpha$  by inverting to  $\alpha = \alpha(H_0)$
- Then relaxed state  $\vec{B} = \vec{B}(\vec{r}, \alpha[H_0])$ .

## Example

Let us consider the case of cylindrical & axial symmetry once again. We know  $B_r = 0$ , and  $B_\theta, B_z \neq 0$ .

Z-component of  $\nabla^2 \vec{B} = \alpha^2 \vec{B} \Rightarrow \frac{\partial^2 B_z}{\partial r^2} + \frac{1}{r} \frac{\partial B_z}{\partial r} + \alpha^2 B_z = 0.$

This is a Bessel equation, with solution

$$B_z(r) = B_0 J_0(\alpha r)$$

↑  
Bessel function of order 0.

This solution satisfies the b.c.  $B_z(0) = B_0, B_z(r \rightarrow \infty) \rightarrow 0.$

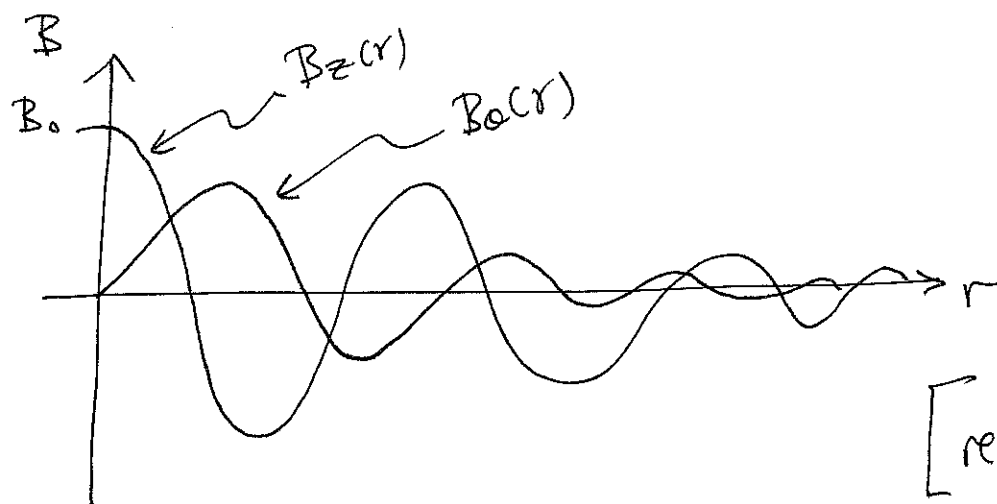
We can use

$$\vec{\nabla} \times \vec{B} = \alpha \vec{B} \Rightarrow \alpha B_\theta = (\vec{\nabla} \times \vec{B})_\theta = -\frac{\partial B_z}{\partial r}$$

using Bessel identities

$$B_\theta(r) = B_0 J_1(\alpha r)$$

↑  
Bessel function of order 1.



[recall  $J(x) \sim \frac{1}{\sqrt{x}} \sin(x)$   
for large  $x$ .]

which is an interesting twisted field geometry  
which can maintain itself in equilibrium.

Enforce helicity constraint

$$H = \frac{1}{\alpha} \iiint_V B^2 dV$$

Assume volume is of a cylinder of length  $L$  and  
radius  $R$

$$H = \frac{1}{\alpha} \cdot B_0^2 \cdot 2\pi \cdot L \cdot \int_0^R r [J_0^2(\alpha r) + J_1^2(\alpha r)] dr$$

$$H = \frac{B_0^2 \pi R^2 L}{\alpha} \left[ J_0^2(\alpha R) + 2J_1^2(\alpha R) + J_2^2(\alpha R) - \frac{2}{\alpha R} J_1(\alpha R) J_2(\alpha R) \right]$$

picking  $H_0$  and inverting for  $\alpha = \alpha(H_0)$  gives us  
our final field state.