

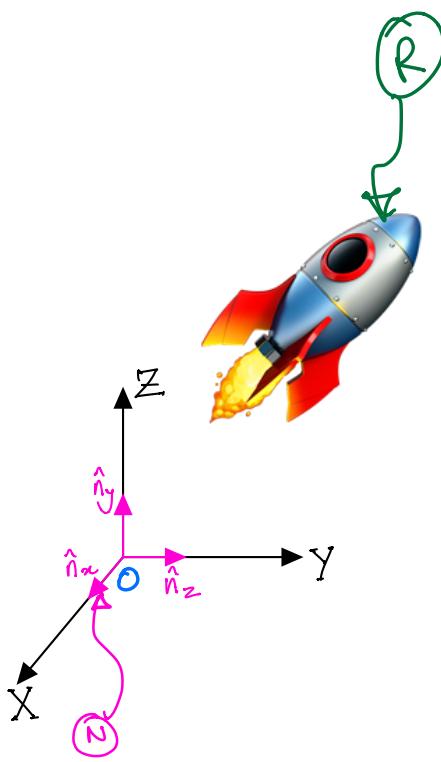
# Key Theorems for computing $[I]$ <sup>s/o</sup>

There are three useful theorems to compute moments of inertia. They are:-

- (i) Rotation theorem
- (ii) Parallel axes theorem (or translation theorem)
- (iii) Composite theorem

Let us examine them in further detail.

(i) Rotation theorem :



- In the figure

X-Y-Z make up a cartesian coordinate system.

O is the origin.

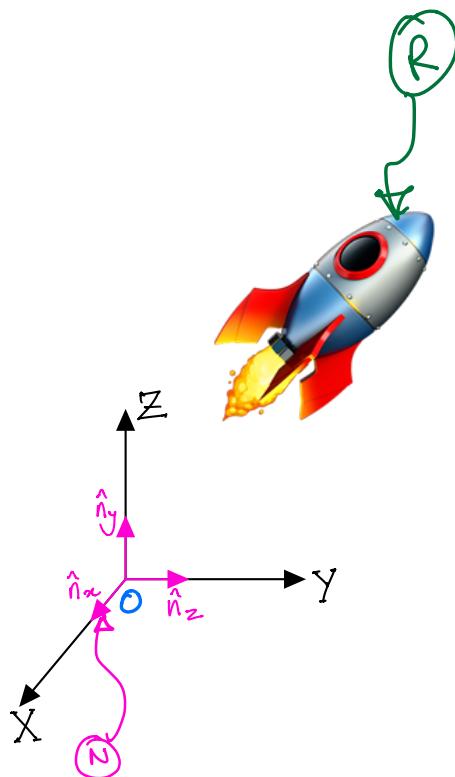
$\hat{n}_x, \hat{n}_y, \hat{n}_z$  are unit vectors directed along X, Y, and Z respectively.

The unit vectors represent a reference frame N.

- Also, the figure shows a rocket which has a reference frame R attached to it.

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- Also, the figure shows a rocket which has a reference frame R attached to it. You are given the inertia matrix of the rocket R about O along the unit vectors of frame N:

$$[I]^{R/O} = \begin{bmatrix} I_{xx}^{R/O} & I_{xy}^{R/O} & I_{xz}^{R/O} \\ I_{yx}^{R/O} & I_{yy}^{R/O} & I_{yz}^{R/O} \\ I_{zx}^{R/O} & I_{zy}^{R/O} & I_{zz}^{R/O} \end{bmatrix}$$

- So far, given:-
- $[I]^{R/I} = \begin{bmatrix} I_{xx}^{R/I} & I_{xy}^{R/I} & I_{xz}^{R/I} \\ I_{yx}^{R/I} & I_{yy}^{R/I} & I_{yz}^{R/I} \\ I_{zx}^{R/I} & I_{zy}^{R/I} & I_{zz}^{R/I} \end{bmatrix}$
- 
- Also, the figure shows a rocket which has a reference frame  $R$  attached to it. Naturally, this reference frame also has 3 mutually orthogonal unit vectors:  $\hat{i}_x$ ,  $\hat{i}_y$ ,  $\hat{i}_z$ .
- Now, we can define another inertia matrix for  $R$  about  $O$  along the newly introduced rotating reference frame's unit vectors  $\hat{i}_x$ ,  $\hat{i}_y$  and  $\hat{i}_z$ . This matrix and its elements are:-
- $$[J]^{R/I} = \begin{bmatrix} J_{xx}^{R/I} & J_{xy}^{R/I} & J_{xz}^{R/I} \\ J_{yx}^{R/I} & J_{yy}^{R/I} & J_{yz}^{R/I} \\ J_{zx}^{R/I} & J_{zy}^{R/I} & J_{zz}^{R/I} \end{bmatrix}$$
- Question: How are the two matrices related?

- We begin by assuming that  $R$  is a particle of mass,  $m_R$ .
- Let us consider a product of inertia from each matrix.

$$I_{xy}^{R/O} \triangleq m_R \left( \overset{*}{P} \times \overset{\wedge}{n}_x \right) \cdot \left( \overset{*}{P} \times \overset{\wedge}{n}_y \right)$$

$$J_{xy}^{R/O} \triangleq m_R \left( \overset{*}{P} \times \overset{\wedge}{r}_x \right) \cdot \left( \overset{*}{P} \times \overset{\wedge}{r}_y \right)$$

- $\overset{*}{P}$  is a position vector from O to the origin of the frame  $R$ .

We know from our discussion on direction cosine matrices that the unit vectors of  $R$  can be related to the unit vectors of  $N$  as:-

$$\begin{bmatrix} \hat{r}_x \\ \hat{r}_y \\ \hat{r}_z \end{bmatrix} = {}^R C^N \begin{bmatrix} \hat{n}_x \\ \hat{n}_y \\ \hat{n}_z \end{bmatrix}$$

${}^R C^N$  is the direction cosine matrix of  $R$  in  $N$ . It is a 3-by-3 matrix, which we shall assume has the following elements.

$${}^R C^N = \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix}$$

So, we can now easily derive:-

$$\hat{r}_x = C_{11} \hat{n}_x + C_{12} \hat{n}_y + C_{13} \hat{n}_z$$

$$\hat{r}_y = C_{21} \hat{n}_x + C_{22} \hat{n}_y + C_{23} \hat{n}_z$$

And then, we can rewrite the product of inertia  $J_{xy}^{R/O}$  as:-

$$J_{xy}^{R/O} \triangleq m_R \left( \underset{\omega}{\cancel{P}} \times \hat{r}_x \right) \cdot \left( \underset{\omega}{\cancel{P}} \times \hat{r}_y \right)$$

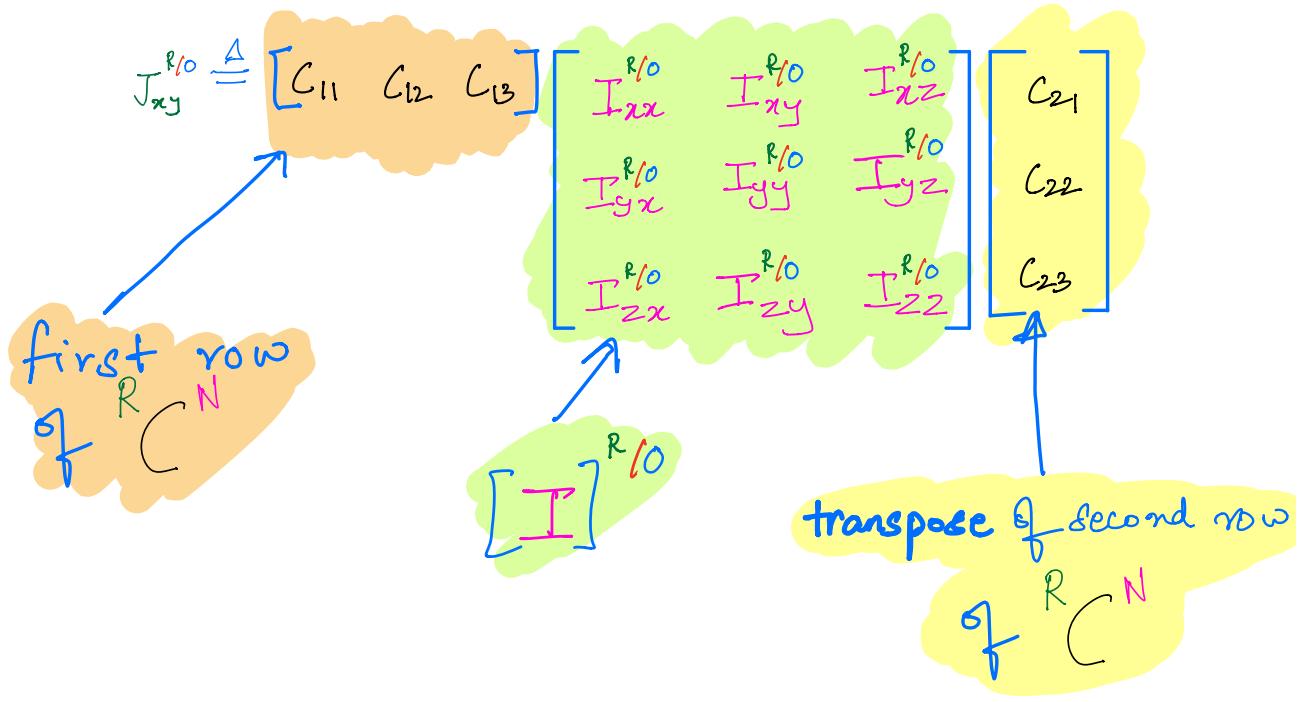
$$J_{xy}^{R/O} \triangleq m_R \left( \underset{\omega}{\cancel{P}} \times (C_{11} \hat{n}_x + C_{12} \hat{n}_y + C_{13} \hat{n}_z) \right) \cdot \left( \underset{\omega}{\cancel{P}} \times (C_{21} \hat{n}_x + C_{22} \hat{n}_y + C_{23} \hat{n}_z) \right)$$

This leads to

$$\begin{aligned} J_{xy}^{R/O} &\triangleq C_{11} (I_{xx}^{R/O} C_{21} + I_{xy}^{R/O} C_{22} + I_{xz}^{R/O} C_{23}) \\ &+ C_{12} (I_{yx}^{R/O} C_{21} + I_{yy}^{R/O} C_{22} + I_{yz}^{R/O} C_{23}) \\ &+ C_{13} (I_{zx}^{R/O} C_{21} + I_{zy}^{R/O} C_{22} + I_{zz}^{R/O} C_{23}) \end{aligned}$$

or in terms of matrix multiplication.

$$J_{xy}^{R/O} \triangleq [C_{11} \ C_{12} \ C_{13}] \begin{bmatrix} I_{xx}^{R/O} & I_{xy}^{R/O} & I_{xz}^{R/O} \\ I_{yx}^{R/O} & I_{yy}^{R/O} & I_{yz}^{R/O} \\ I_{zx}^{R/O} & I_{zy}^{R/O} & I_{zz}^{R/O} \end{bmatrix} \begin{bmatrix} C_{21} \\ C_{22} \\ C_{23} \end{bmatrix}$$



More generally, it can be shown that

$$[J]^{R/O} = {}^R C^N [I]^{R/O} [{}^R C^N]^T$$

↑  
Rotation theorem.

↑  
transpose of  ${}^R C^N$

teorema huygens

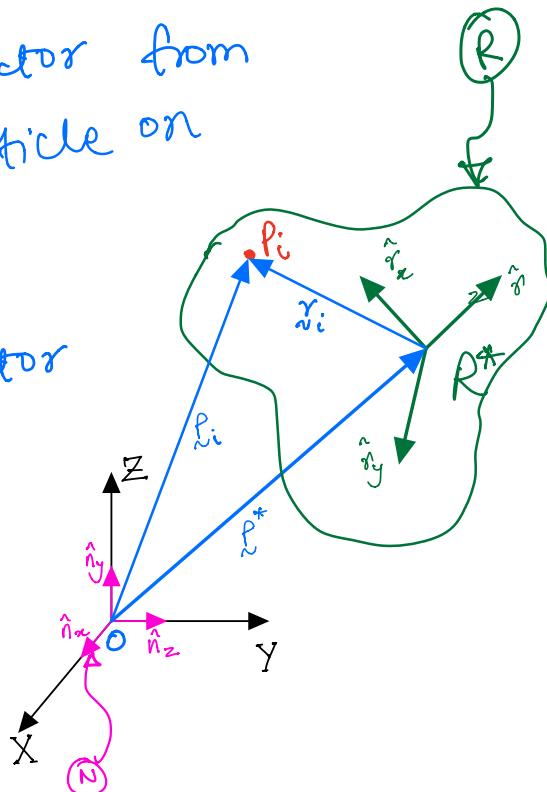
(ii) Parallel axes theorem :-

In the previous section we presumed that the rocket was a point mass.

What happens if this assumption is relaxed and rockets are better approximated as a system of particles?

- $\underline{p}^*$  is a position vector from  $O$  to  $R^*$ , the origin of the frame  $R$ .
- $R^*$  is the mass center of the Rocket.
- $\underline{p}_i$  is a position vector from  $O$  to  $P_i$ , the  $i^{th}$  particle on the rocket body.
- $\underline{\gamma}_i$  is a position vector from  $R^*$  to  $P_i$ . So,

$$\underline{p}_i = \underline{p}^* + \underline{\gamma}_i$$



$I_{rr^*}$  è dato dall'intera massa  $m$  che moltiplica il prodotto dot ( cross( $p^*, O.x$ ), cross( $p^*, O.x$ ) ) per  $I_{xx} \dots$  esattamente come in huygens  $I_a = I_b + mL^2$ ; intera massa per  $I^*_{asse} I$

Now, we know that the product of inertia for this system of particles along the  $\hat{A}_x$  and  $\hat{A}_y$  directions is given by:-

$$I_{xy}^{R/O} \triangleq \sum_i m_i (\underline{\rho_i} \times \hat{A}_x) \cdot (\underline{\rho_i} \times \hat{A}_y)$$

or...

$$I_{xy}^{R/O} \triangleq \sum_i m_i ((\underline{\rho^*} + \underline{\gamma_i}) \times \hat{A}_x) \cdot ((\underline{\rho^*} + \underline{\gamma_i}) \times \hat{A}_y)$$

or...

$$\begin{aligned} I_{xy}^{R/O} &= \sum_i m_i (\underline{\rho^*} \times \hat{A}_x) \cdot (\underline{\rho^*} \times \hat{A}_y) + (\underline{\rho^*} \times \hat{A}_x) \cdot \left( \sum_i m_i \underline{\gamma_i} \times \hat{A}_y \right) \\ &\quad + \left( \sum_i m_i \underline{\gamma_i} \times \hat{A}_x \right) \cdot (\underline{\rho^*} \times \hat{A}_y) + \sum_i m_i (\underline{\gamma_i} \times \hat{A}_x) \cdot (\underline{\gamma_i} \times \hat{A}_y) \end{aligned}$$

The terms highlighted in green go to zero because

$\sum_i m_i \underline{\gamma_i} = 0$  by the definition of mass centers.

$$I_{xy}^{R/O} = I_{xy}^{R/R^*} + I_{xy}^{R/O}$$

$I_{xy}^{R/R^*}$  is the product of inertia of  $R$  about the mass center  $R^*$ .

$I_{xy}^{R/O}$  is the product of inertia of  $R^*$  about  $O$ .

Some comments:-

1. This result extrapolates to the moment of inertia scalars. For example,

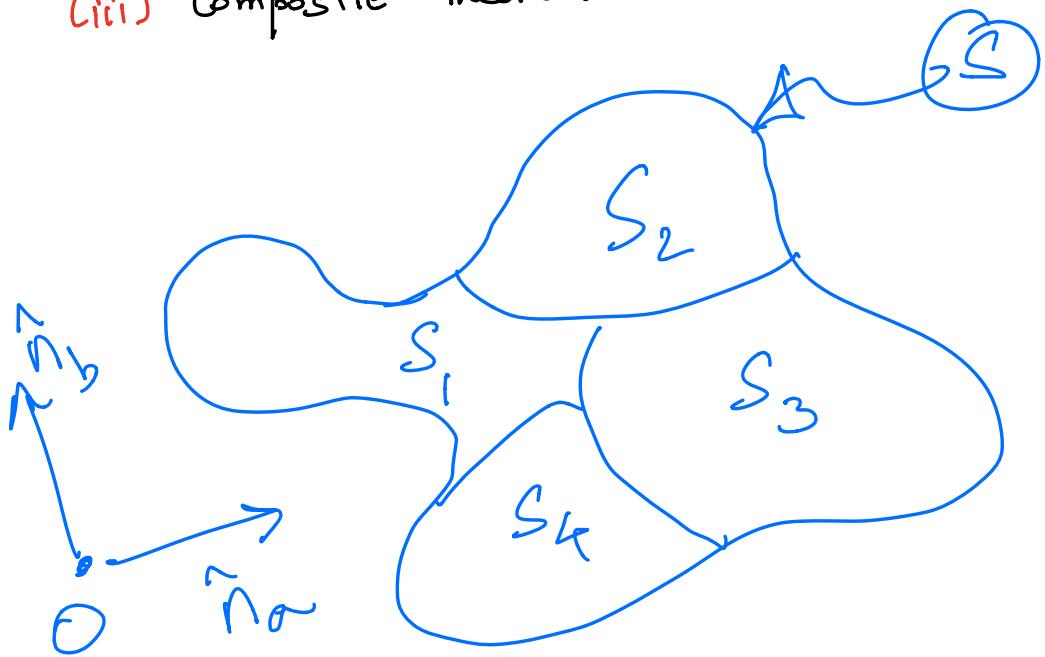
$$I_{xx}^{R/O} = I_{xx}^{R/R^*} + I_{xx}^{R^*}$$

2. This result extrapolates to the inertia matrix.

$$[I]^{R/O} = [I]^{R/R^*} + [I]^{R^*}$$

3. This rule is only valid when going through the mass centre.

(iii) Composite theorem



$$I_{ab}^{S/0} = \sum_i I_{ab}^{S_i/0}$$