

ECE 310

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Review Notes for ECE 310 (Digital Signal Processing)

This is in no way comprehensive.

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1 Midterm 1

1.1 DT vs. CT signals

ECE 210 dealt primarily with CT (continuous time) signals. ECE 310 deals with DT (discrete time) signals.

Signals:

- Continuous-domain (analog) $\rightarrow x(t)$ for $(t \in \mathbb{R})$
- Discrete-domain (digital) $\rightarrow x[n]$ for $(n \in \mathbb{Z})$

Notation is technically important, $x[n]$ refers to a singular sample at n . A signal is represented with $\{x[n]\}_n$ for $n \in \mathbb{Z}$, and a system can be represented as $\{y[n]\} = S\{x[n]\}$ for $n \in \mathbb{Z}$. However, I really cannot be bothered to do this, and most problems don't either.

1.2 LTI/LSI Systems

Linear Time Invariant or Linear Shift Invariant (same thing).

- Linear: Superposition of inputs has a corresponding superposition of outputs. Stuff like scaling is preserved.
- Time/Shift Invariant: Time shift in the input results in an equal time shift in the output.

Most of the fancy theorems in this class rely on systems being LTI.

Determining linearity is relatively straightforward (IMO) but time-invariance isn't (again, IMO). But generally the approach seems to be plugging in a time shift n_o into the input. Then apply the same time shift in the output, and see if the two expressions match.

Trivial Example: $y[n] = x[n^2]$

$x[n]$ transforms $x[n] \rightarrow x[n - n_o]$. Thus, $y[n] = x[n^2 - 2nn_o + n_o^2]$. Applying the same time shift to the output, we get $y[n - n_o] = x[n^2 - n_o]$. These are not the same expression, and thus this system is time-variant.

1.3 The Delta Function

Similar to the delta function from ECE 210. Except its not an infinite spike.

$$\delta[n] := \begin{cases} 1 & \text{if } n=0 \\ 0 & \text{otherwise} \end{cases}$$

We can represent a DT signal as a superposition of scaled and shifted delta functions. For example:

- $x[n] = \sum_{k \in \mathbb{Z}} x[k] \delta[n - k]$
- $y[n] = \sum_{k \in \mathbb{Z}} x[k] S\{\delta[n - k]\}$

1.4 Convolution

Thankfully we don't have to do 3D tiled convolution kernels for this class.

In ECE 210, we use convolution to “apply” an impulse response to an input CT signal. In this class its more or less the same, except its with DT signals.

Discrete convolution is defined as the following:

$$y[n] = (x * h)[n] = \sum_{k \in \mathbb{Z}} x[k]h[n - k] = \sum_{k \in \mathbb{Z}} h[k]x[n - k]$$

Some useful properties of convolution:

- start point = (start of $x[n]$)(start of $h[n]$)
- end point = (end of $x[n]$)(end of $h[n]$)
- start index = (start index of $x[n]$) + (start index of $h[n]$)
- end index = (end index of $x[n]$) + (end index of $h[n]$)
- Convolution is associative, distributive, commutative (and linear)

1.5 LCCDEs

Stands for Linear Constant Coefficient Difference Equations, and is a popular way to represent LTI/LSI systems. There are two ways of solving LCCDE's: guess-and-check (painful) and Z-transforms (not painful).

General form of LCCDEs:

$$y[n] = \sum_{i=1}^K b_i y[n - i] + \sum_{j=0}^M c_j x[n - j] \quad (1)$$

for $\{K, M \in \mathbb{Z} \mid 0 \leq K < \infty \text{ and } 1 \leq M < \infty\}$

I may be a little too ECE 210-pilled, but I guess you can think of the left summation as the Zero-Input terms, and the right summation as the Zero-State terms.

1.5.1 FIR/IIR Systems

FIR (Finite Impulse Response) systems occur when you have LCCDEs with $K = 0$ (no feedback terms). IIR (Infinite Impulse Response) systems have $K > 0$.

1.6 Z-Transforms

Motivation for Z-Transforms: Can we find a class of signals which do not change shape once passed through an LTI/LSI system?

The Z-Transform $X(z)$ of a DT signal $x[n]$ is defined as:

$$X(z) = \sum_{n=-\infty}^{\infty} x[n]z^{-n} \text{ where } z \in \mathbb{C} \quad (2)$$

The ROC (region of convergence) is the range of values in the z -domain in which the Z-transform converge. **Any particular Z-transform may have multiple ROCs which correspond to different inverse Z-transforms.**

A Few Reoccurring Z-Transforms:

- $\alpha^n u[n] \rightarrow \frac{1}{1-\alpha z^{-1}}$ (Right-handed signal, ROC: $|z| > \alpha$)
- $-\alpha^n u[-n-1] \rightarrow \frac{1}{1-\alpha z^{-1}}$ (Left-handed signal, ROC: $|z| < \alpha$)
- $\delta[n-m] \rightarrow z^{-m}$

A Few Reoccurring Z-Transform properties

- Linearity
- Time Shifting: $x[n-k] \rightarrow z^{-k} X(z)$
- Convolution: $x_1[n] * x_2[n] \rightarrow X_1(z)X_2(z)$. Note: this is a reoccurring property of FTs and LTs as well. Pretty sure thats why a lot of convolution algo's use FFT so that convolution becomes an $O(n \log(n))$ operation

Due to the convolution property, we can express LTI systems in the Z-domain as follows:

$$y[n] = (x * h)[n] \rightarrow Y(z) = X(z)H(z) \quad (3)$$

Alternatively, we can write $H(z) = \frac{Y(z)}{X(z)}$ and inverse Z-transform to recover the impulse response $h[n]$. This is probably the best way of determining the impulse response for LCCDEs (for now, at least).

Inverse Z-transforming often devolves into a lot of partial fraction decomposition, so review that.

1.7 Causality

Pretty much the same as introduced in ECE 210.

Output depends solely on current/past inputs \rightarrow **Causal**

Output depends on future inputs \rightarrow **Not Causal**

An anticausal system relies **solely** on future inputs.

A system is causal if impulse response $h[n] = 0$ for $n < 0$.

Both causal and non-causal systems have their merits. Causal systems are used often in real-time systems. Example application of non-causal systems would be in image post-processing, and (generally) signal processing on data which has been stored in some memory unit.

1.8 BIBO Stability

A system is BIBO (Bounded-Input Bounded-Output) stable if for some $\{y[n]\}_n = S\{x[n]\}_n$, whenever $|x[n]| \leq B_{\text{in}} < \infty$, it holds that $|y[n]| \leq B_{\text{out}} < \infty$.

Because of convolution properties, a finite length impulse response is indicative of a BIBO stable system.

What if $h[n]$ is infinite-length? Then it must converge.

$S\{h[n]\}$ is BIBO stable iff $\sum_{k=-\infty}^{\infty} |h[k]| < \infty$.

1.8.1 Z-domain and Stability

In general, a system with transfer function $H(z)$ and associated ROC_H is stable if it contains $|z| = 1$ (the unit circle).

With problems with multiple terms within the transfer function, the ROC is at least the intersection of all terms. For problems that ask to find a bounded input which will result in a bounded output for a non-bounded system, use pole-zero cancellation. For problems that ask to find a bounded input which results in an unbounded output, try to make divergent terms non-zero (delta function does the trick usually).

An LTI system is **marginally stable** if its ROC is open at the unit circle $|z| = 1$.

Define: $x[n] = a^n u[n]$ and $h[n] = b^n u[n]$ where $|a| = |b| = 1$. We can thus expand $a = e^{j\varphi}$ and $b = e^{j\theta}$, respectively. The system output $y[n] = \sum_{k=-\infty}^{\infty} x[n-k]h[k] = \sum_{k=-\infty}^{\infty} e^{j\varphi(n-k)} e^{j\theta(k)} u[n-k]u[k]$. We factor out $\exp(j\varphi n)$ and simplify the summation bounds to rewrite this as:

$$y[n] = e^{j\varphi n} \sum_{k=0}^n e^{jk(\theta-\varphi)} = e^{j\varphi n} \left(\frac{1 - e^{j(\theta-\varphi)(n+1)}}{1 - e^{j(\theta-\varphi)}} \right) u[n].$$

When $\varphi = \theta$, the indeterminate expression can be written as:

$$y[n] = e^{j\varphi n} \sum_{k=0}^n (1) = (n+1) e^{j\varphi n} u[n].$$

We can see this expression is unbounded due to the $(n+1)$ term.

When $\varphi \neq \theta$, $y[n]$ oscillates, but remains bounded.

Thus, in a marginally stable system, only inputs that match at least one unit circle pole of the system will produce unbounded outputs. Otherwise, it will be bounded.

2 Midterm 2.

2.1 CTFT and DTFT

Continuous-Time Fourier Transform (CTFT): $\{x(t)\}_{t \in \mathbb{R}} \leftrightarrow \{X_c(\Omega)\}_{\Omega \in \mathbb{R}}$ where:

$$X_c(\Omega) = \int_{-\infty}^{\infty} x(t)e^{-j\Omega t} d\Omega \quad (4)$$

Discrete-Time Fourier Transform (DTFT): $\{x[n]\}_{n \in \mathbb{Z}} \leftrightarrow \{X_d(\omega)\}_{\omega \in \mathbb{R}}$ where:

$$X_d(\omega) = \sum_{-\infty}^{\infty} x[n]e^{-j\omega n} \quad (5)$$

Important Things to keep in mind about **both** CTFT and DTFT:

- CTFT converts a continuous input into a continuous output. DTFT converts a discrete input into a continuous output.
- DTFT is a special case of the Z-transform, CTFT is a special case of the Laplace transform.
- Both DTFT/CTFT provide a representation of a signal as a linear combination of complex exponentials (which can be thought of as 2D vectors in the complex plane)

DTFT properties

- $X_d(\omega)$ is 2π -periodic
- **If $\{x[n]\}_{n \in \mathbb{Z}}$ is real-valued**, $|X_d(-\omega)| = |X_d(\omega)|$ and $\angle X_d(-\omega) = -\angle X_d(\omega)$ (Magnitude is symmetric, phase is anti-symmetric)
- Convolution in n -domain is multiplication in the ω -domain. Thus, LTI systems have a corresponding frequency response $H_d(\omega)$
- Most CTFT properties have an analogue for the DTFT
- Inverse DTFT: $x(t) = (2\pi)^{-1} \int_{-\pi}^{\pi} X_d(\omega)e^{j\omega n} d\omega$

2.2 Sampling and ADC/DAC

Idea: We have a **continuous** signal $x_c(t)$, and every T seconds, we take a sample of it. We then end up with a **discrete** signal $x[n] = x_c(nT)$. Our sampling period is T , and our sampling frequency is $f_s = \frac{1}{T}$.

Question: What is the relationship between $X_c(\Omega)$ and $X_d(\omega)$? In other words, what effect does sampling have in the Fourier domain?

Quick lil' derivation:

By definition, we know $x[n] = x_c(nT) = (2\pi)^{-1} \int_{-\infty}^{\infty} X_c(\Omega)e^{j\Omega(nT)} d\Omega$. Furthermore, $x[n] = (2\pi)^{-1} \int_{-\pi}^{\pi} X_d(\omega)e^{j\omega n} d\omega$.

Thus, $\int_{-\infty}^{\infty} X_c(\Omega)e^{j\Omega(nT)} d\Omega = \int_{-\pi}^{\pi} X_d(\omega)e^{j\omega n} d\omega$. Substituting $\omega = \Omega T$, we get:

$$\left(\frac{1}{T}\right) \int_{-\infty}^{\infty} X_c\left(\frac{\omega}{T}\right) e^{j\omega n} d\omega = \int_{-\pi}^{\pi} X_d(\omega)e^{j\omega n} d\omega \quad (6)$$

Lastly, because X_c is 2π -periodic, we can expand the LHS as the following.¹

$$\left(\frac{1}{T}\right) \int_{-\infty}^{\infty} X_c\left(\frac{\omega}{T}\right) e^{j\omega n} d\omega = \frac{1}{T} \sum_{k \in \mathbb{Z}} \int_{-\pi+2\pi k}^{\pi+2\pi k} X_c\left(\frac{\omega+2\pi k}{T}\right) e^{j\omega n} d\omega \quad (7)$$

Matching the integrands of this expanded expression and the DTFT integral, we determine:

$$X_d(\omega) = \frac{1}{T} \sum_{k \in \mathbb{Z}} X_c\left(\frac{\omega+2\pi k}{T}\right) \quad (8)$$

2.2.1 Aliasing and Nyquist Frequency

Suppose we have a **band-limited** signal whose Fourier transform is $X_c(\Omega)$. Thus, $X_c(\Omega) = 0$ for $|\Omega| > B$, where B is the bandwidth (highest-frequency) of the signal.

If we sample this signal, we get that $X_d(\omega) = \frac{1}{T} \sum_{k \in \mathbb{Z}} X_c\left(\frac{\omega+2\pi k}{T}\right)$. Graphically, this looks like an infinite series of scaled & shifted versions (aliases) of $X_c(\Omega)$, each of which centered at some $2\pi k$. To find where the bandwidth gets “mapped” to after sampling, we use the relation $\omega = \Omega T$ where $\Omega \rightarrow B$.

We know B is highest-frequency in our original signal, and has units rad/s, so $B = 2\pi f_B$. We also know $T = \frac{1}{f_s}$. Thus, we can express ω_B (the bandwidth of the signal **after** sampling) as $\omega_B = BT = 2\pi \frac{f_B}{f_s}$

Each of the aliases is centered at $2\pi k$ for $k \in \mathbb{Z}$. They have the potential to overlap if the bandwidth of each alias in the ω -domain exceeds π (think about it graphically). This overlap is called **aliasing**, and it causes us to lose information about the original signal.

Thus, if we don’t want aliasing to occur, the bandwidth in the ω -domain must be less than or equal to π .

Equivalently, $\omega_B = 2\pi \frac{f_B}{f_s} \leq \pi \rightarrow f_s \geq 2f_B$

This condition is called the Nyquist Criterion, and the **Nyquist Frequency** is $2f_B$, which is the lowest sampling frequency in which you will observe no aliasing.

In general there are two ways to resolve aliasing for ADC conversion:

- Increase f_s to at least Nyquist Frequency.
- Use a low-pass filter (LPF) on $X_c(\Omega)$ to artificially reduce f_B .²

¹Note: Omitted the shift of ω in the complex exponential term because a shift by $2\pi k$ in the exponent corresponds to a 360 degree rotation (thus leaving the complex term unchanged).

2.2.2 Ideal ADC and DAC

The process of sampling converts a CT signal to a DT one, and so that process is called Analog-to-Digital Conversion (ADC).

Ideal Digital-to-Analog conversion basically consists of two steps:

- Apply a LPF to remove the higher-frequency aliases, and just retain the frequency spectrum centered at $\omega = 0$.
- Properly scale/resize the resulting frequency spectrum to obtain that of $X_c(\Omega)$

3 Final

Will update this when midterm 3 rolls around :D

²This comes at a cost of losing information about the original signal. However, often times the information lost by low-passing is much less than the potential information lost by aliasing. In other scenarios however, we can actually just allow aliasing to occur, and then use a digital LPF in the ω -domain to select the range of frequencies we need. There was a homework problem about this.