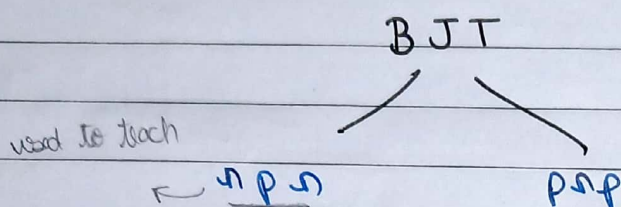


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Module - 5

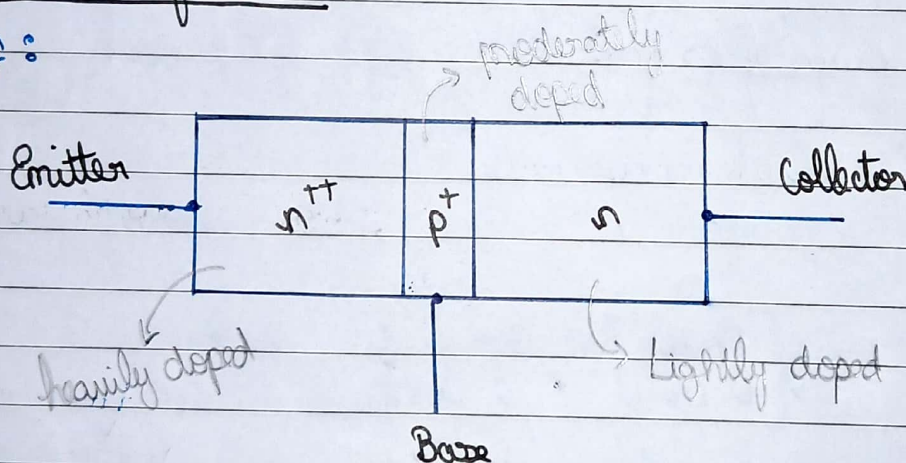
Bipolar Junction Transistor

- Transistor - An active device that transfers charge carriers with a sensitive force. (Transfer resistor)

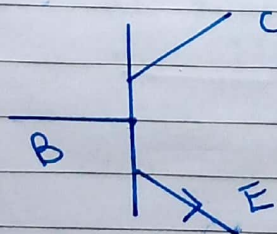


* Structure of BJT:

- n p n:

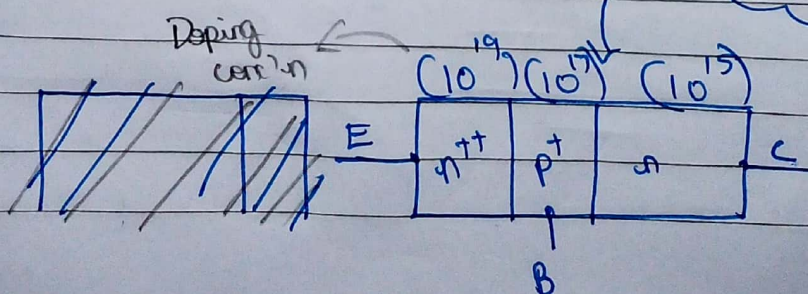


→ Base width is less and the emitter is heavily doped to produce more current.

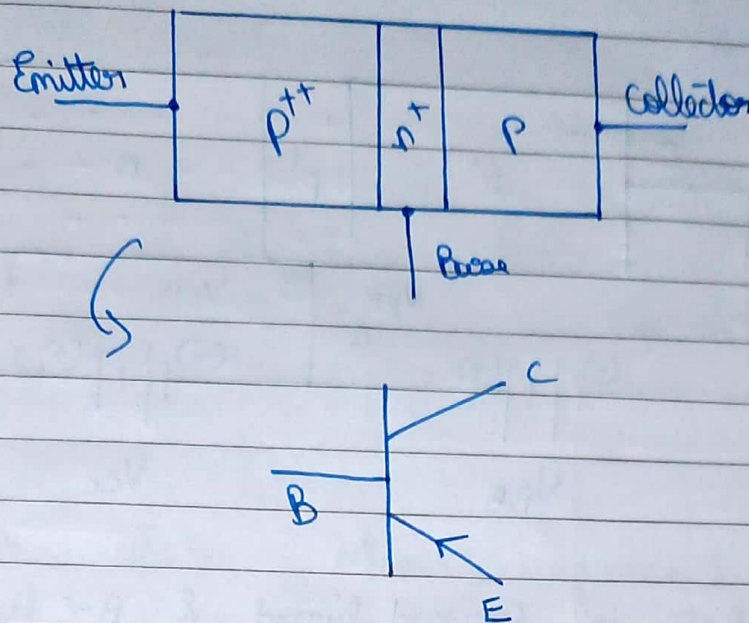


- E → heavily doped, less area
- B → moderately doped, very less area
- C → lightly doped, more area

Ideally:



PNP:



* Configuration of BJT:

- Common Base
- Common Emitter (Standard configuration)
- Common Collector

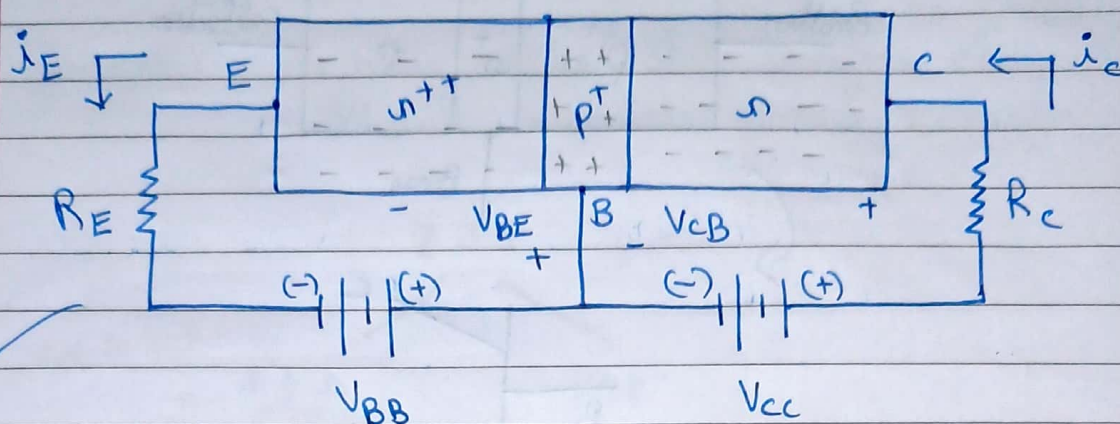
NOTE:

- Base - input
- Emitter - output
- V_{BE} (voltage between base & emitter) controls output current.
- C-E configuration provides voltage & current amplification.

* Operation of BJT:

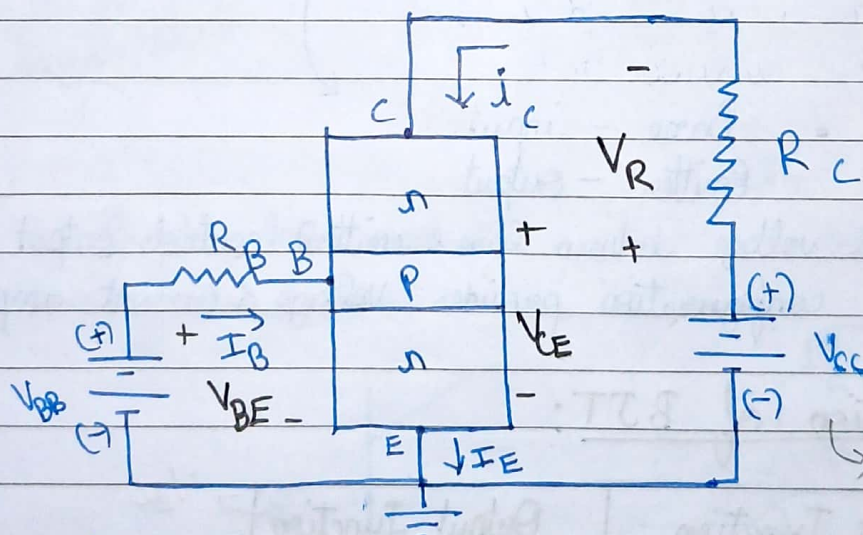
$V_{BE} \leftarrow$	Input Junction	Output Junction	$\rightarrow V_{BC}$
1.	Forward	Forward	→ Saturation → on switch
2.	Reverse	Reverse	→ Cut-off → off switch
3.	Forward	Reverse	→ Forward active mode → amplification
4.	Reverse	Forward	→ Reverse operation mode ↳ NOT USED OFTEN

• Structure and working of npn: (common-emitter config.)

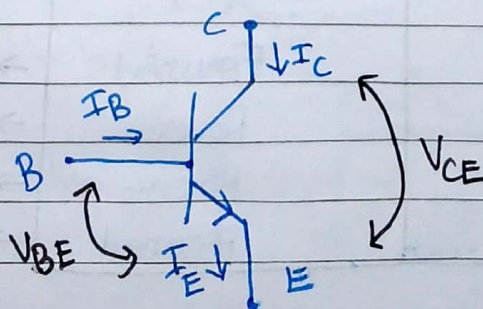


Here, B-E is forward biased & B-C is reverse biased to operate npn in (amplification) forward active mode.

- $R_E / R_C \rightarrow$ helps to minimize current flow to protect the transistor.
(current limiting resistor)



(Transistor can also be rep. as)



- Common Emitter (CE) config. $I_B \rightarrow$ input current, $I_C \rightarrow$ output current
 $V_{BE} \rightarrow$ input voltage, $V_{CE} \rightarrow$ output voltage

The electrons from the emitter (produced due to Forward bias) is injected into the base, which creates an excess conc'n of minority carriers in the base (minority since the base is p-type).

The Base-collector junction is reverse biased, hence conc'n of e^- is very less

due to the large gradient in e^- conc'n, the electrons from the base will diffuse across to the collector.

→ The width of the base is very small to prevent recombination of e^- & holes (recombination cannot be totally prevented but can be prevented to the maximum level)

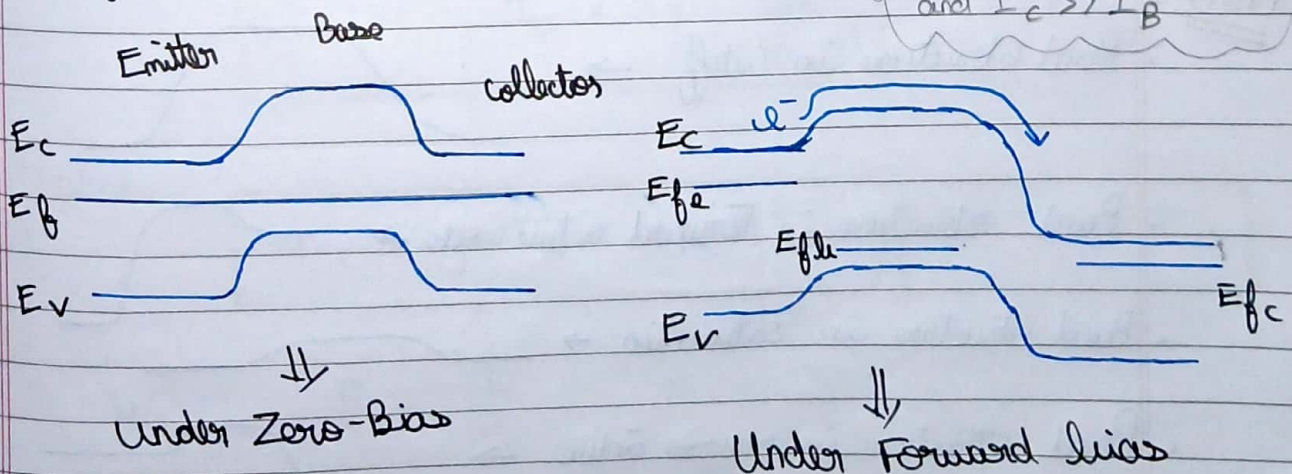
Because of this,

$$I_E \approx I_C$$

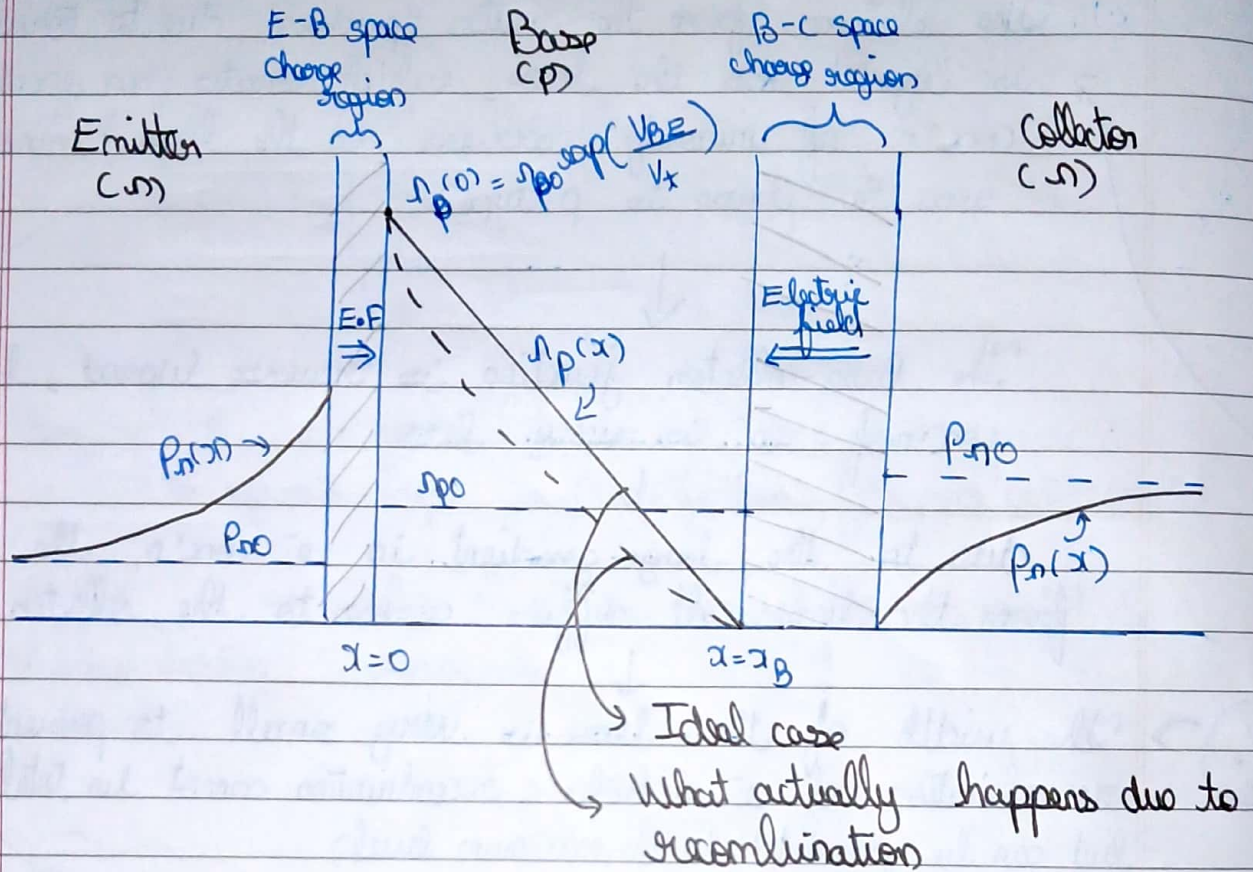
$$\text{since } I_E = I_C + I_B$$

$$\text{and } I_C \gg I_B$$

• Energy Band diagrams:



Note: From the Energy band diagram, it can be observed that more no. of e^- move from emitter to collector in forward bias due to the shortened height of the potential barriers.



$x_B \rightarrow$ width of base after depletion region

NOTE:

- Band structure in cutoff \rightarrow
- Band structure in Forward active mode \rightarrow
- Band structure in saturation \rightarrow
- Band structure in reverse active \rightarrow

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* Transistor Current Relations:

• Collector current:

We know,

$$J_n \equiv I_n = q D_n \frac{dn}{dx} = \frac{I_n}{A}$$

$$\Rightarrow I_n = q D_n \times A \frac{dn}{dx}$$

Here, in a npn transistor,

$$I_c = q D_n A_{BE} \times \left[\frac{n_p(x) - 0}{0 - x_B} \right]$$

$$= q D_n A_{BE} \times \left[\frac{n_{p0} \exp\left(\frac{V_{BE}}{V_T}\right)}{-x_B} \right]$$

$$I_s = - \left(\frac{q D_n A_{BE} n_{p0}}{x_B} \right) \exp\left(\frac{V_{BE}}{V_T}\right)$$

$$I_c = I_s \times \exp\left(\frac{V_{BE}}{V_T}\right)$$

also,

$$I_c = \beta I_B + (\beta + 1) I_{CBO}$$

$$I_c = \alpha I_E + I_{CBO}$$

where, $\beta = \frac{I_c}{I_B}$, $\alpha = \frac{I_c}{I_E}$

$I_{CBO} \rightarrow$ reverse saturation current

• Base current:

↳

$$I_B = (1 - \alpha) I_E - I_{CBO}$$

• Emitter current:

↳

$$I_E = I_C + I_B$$

$$I_C = \alpha I_E + I_{CBO}$$

Note:

$$\alpha \approx \frac{I_C}{I_E}$$

↓

Common Base Current gain

$$\beta \approx \frac{I_C}{I_B}$$

↓

Common Collector Current gain

• Output Voltage →

$$V_{CC} = (I_C R_C) + (V_{CB} + V_{BE})$$

(or)

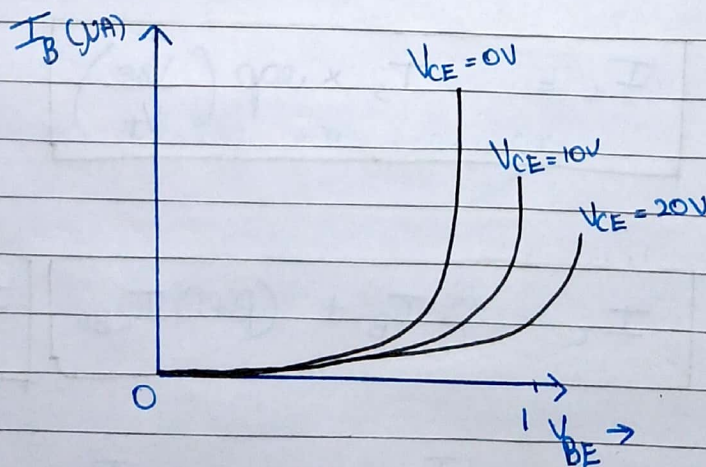
$$V_{CC} = V_R + V_{CE}$$

Refer circuit of npn transistor

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* Transistor Characteristics:

• Input characteristic:



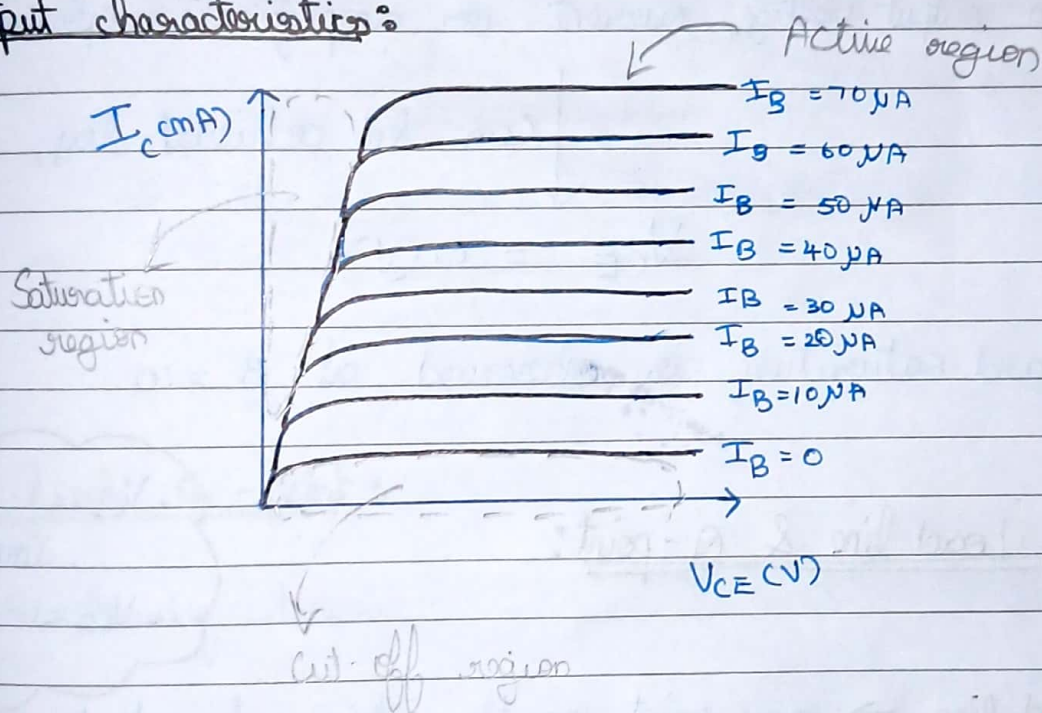
→ I_B Input current (V_{BE}) vs Input voltage (I_B) with Output voltage (V_{CE}) as constant.

Note:

- The constant V_{CE} supply makes sure the base region is present to maintain neutrality by providing extra charge carriers to the base.

↳ This is the reason for shifting in x/p characteristics for different V_{CE} values.

Output characteristics:



→ Output voltage (V_{CE}) Vs Output current (I_C) with input current (I_B) as constant.

* Non-Ideal Effects :-

• Base-Width Modulation:

↳ aka Early effect.

↳ refers to the change in width of the base region (x_b) w.r.t V_{CE} .

- Reduction in x_b increases diffusion current

↳ reduction in x_b (base width) will occur when V_{CB} increases, which increases the Base-collector space charge region.

• Hard Saturation:

↳ a state of transistor which cannot provide further increase in output voltage, current or amplification. (provides max current)

↓ can be achieved by,

$$V_{CE} = 0(V)$$

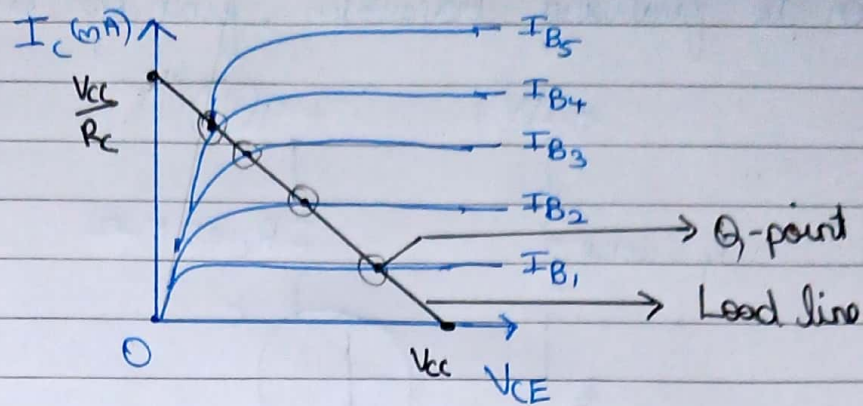
- Hard saturation is observed at $\beta = 10$.

* DC Load line & Q-point:

- $V_{CE} = 1$ for amplification
- $V_{CE} < 1$ for saturation

- Load line → any point on the line of output characteristics where a circuit acts as an amplifier, present in the active region.
- Q-point → point on the loadline where faithful amplification is achieved by the transistor.

• Faithful amplification → perfect amplification of the input signal



Here, at $I_C = 0$, we get the cut-off region.

$$\Rightarrow \boxed{V_{CE} = V_{CC}} \quad \leftarrow \quad \{ \because V_{CC} = V_{CE} + I_C R_C \}$$

at $V_{CE} = 0$, we get the saturation point (Max. current)

$$\Rightarrow \boxed{I_C = \frac{V_{CC}}{R_C}} \quad \leftarrow$$

• To find Q-point:

We already know,

$$I_C = \beta I_B$$

$$\Rightarrow \boxed{I_{CQ} = \beta I_B}$$

$$\text{and, } \boxed{V_{CEQ} = V_{CC} - I_{CQ} R_C}$$

and finally,

$$\boxed{(V_{CEQ}, I_{CQ})} \text{ gives the Q-point //}$$

To find I_B ,

$$I_B = \frac{V_{BB} - V_{BE}}{R_B}$$

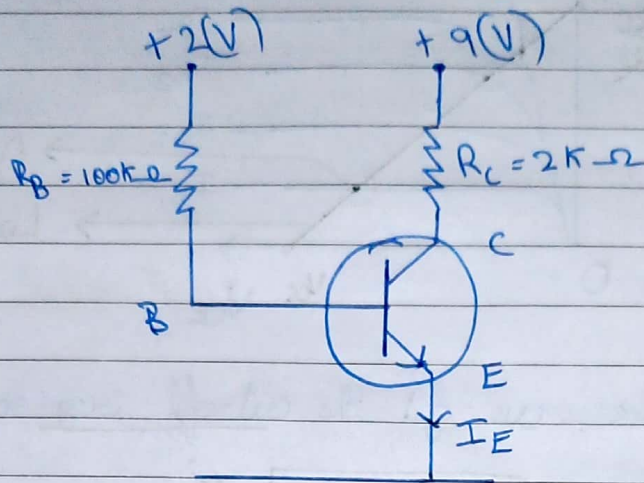
Assume $V_{BE} = 0.65V$
if not given in Q

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Ex: ① For the following transistor, find the Q-point given $\beta = 50$.



Ans: Given,

$$V_{CC} = 9V$$

$$V_{BB} = 2V$$

$$\beta = 50$$

$$\text{Now, } I_C = \frac{V_{CC}}{R_C} = \frac{9}{2000} = 4.5 \text{ mA}$$

$$\text{also, } I_B = \frac{V_{BB} - V_{BE}}{R_B} = \frac{2 - 0.65}{100 \times 10^3} = 13.5 \mu A$$

To find the Q-point,

$$I_{CQ} = \beta \times I_B = (50)(13.5 \times 10^{-6}) \\ = 0.675 \text{ mA}$$

$$\text{and } V_{CEQ} = V_{CC} - I_{CQ} R_C = 9 - (0.675 \times 10^{-3})(2000) \\ = 7.65 \text{ V}$$

∴ Required Q-point is $(7.65 \text{ V}, 0.675 \text{ mA}) //$