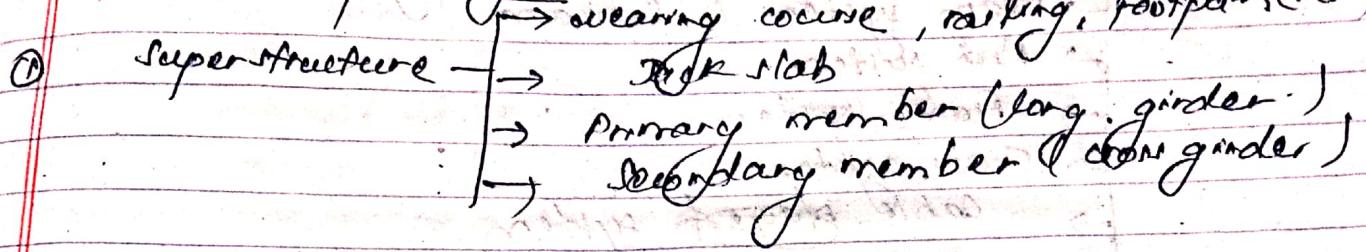
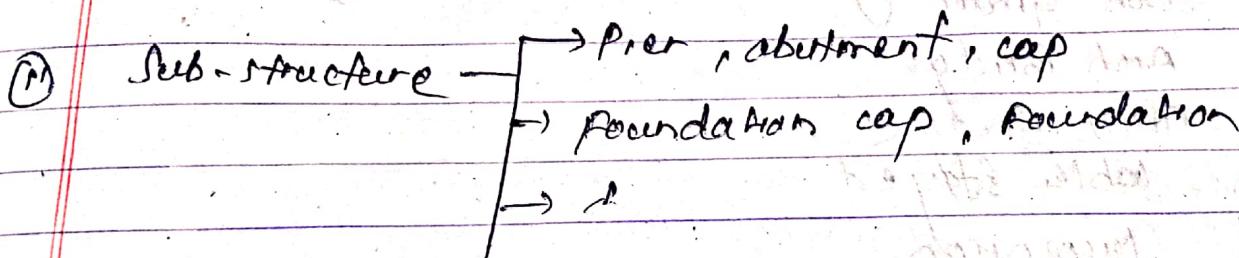


* Component of Bridge



Bearing

It is a mechanical device which safely transmits all vertical and lateral load to substructure-free allowing some translational and rotational movement.



* Various Types of Bridge:

- ① Based upon material used
- Rec, Steel, masonry, timber, prestressed, composite
- ② Based upon span
- As per Nepal Bridge Standard 2087.

Minor bridge: span $\leq 25\text{m}$ no. of span (total) ≤ 5 or

Major Bridge: span $\geq 25\text{m}$ total length $> 50\text{m}$

Special Bridge: (span $> 100\text{m}$)

(iii)

Based upon type of structural system:

- Beam system (T-beam)
- Arch system
- Frame system
- Truss system
- cable stayed system
-

(iv)

Based upon type of superstructure:

- Slab Bridge
- T-beam Bridge
- Box Girder
- Arch Bridge
- Truss Bridge
- cable stayed
- Suspension

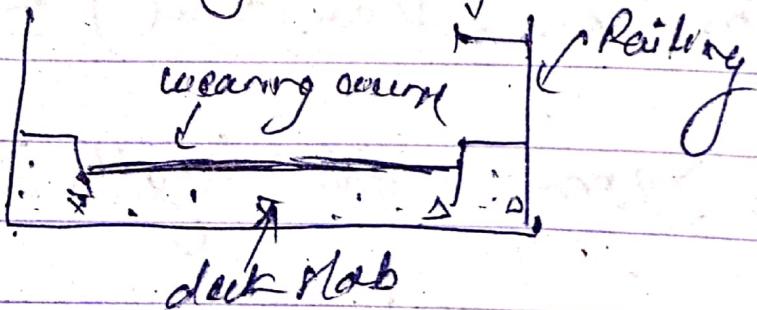
In the context of Nepal?



Reflection of Bridge Type:

(i)

Slab Bridge: Footpath



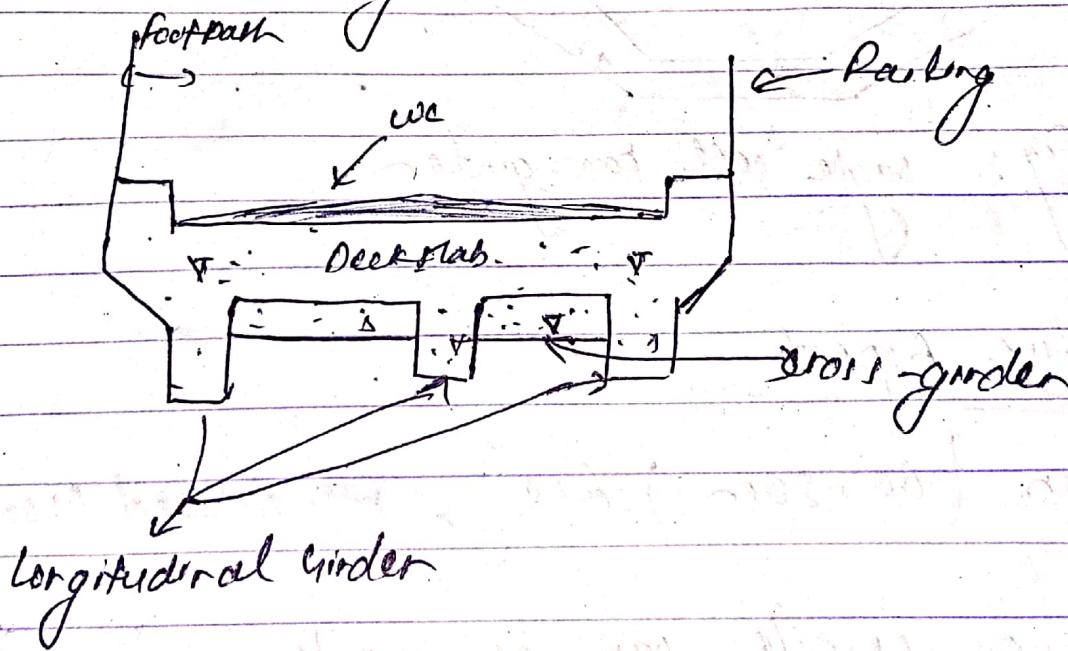
Positive Aspects

- technically feasible and economically viable upto (from RCC) span.
- vertical clearance more (AB)
- uniform lateral load distribution
- good appearance

Negative aspect:

- not feasible for long span.
- no. of lane of bridge more than 2.

(II) T-Beam Bridge:



Positive Aspect:

- technically feasible and economically viable upto (from RCC) span

→ Due to monolithic construction
+ far better rigidity.

- easier to construct
- ~~Negative~~
- less vertical clearance
- bulky in appearance

(iii). Bon Gorder Bridge:
Footpath.

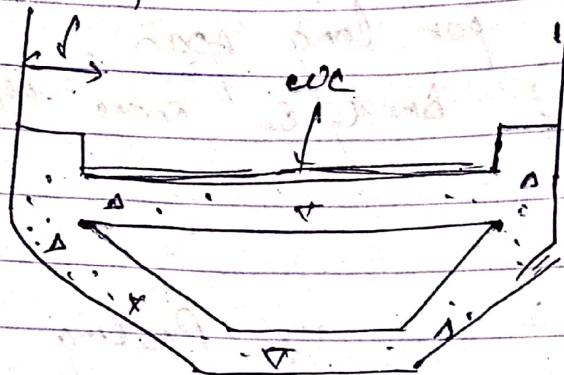


Fig: single cell bon-gorder

Positive Aspect

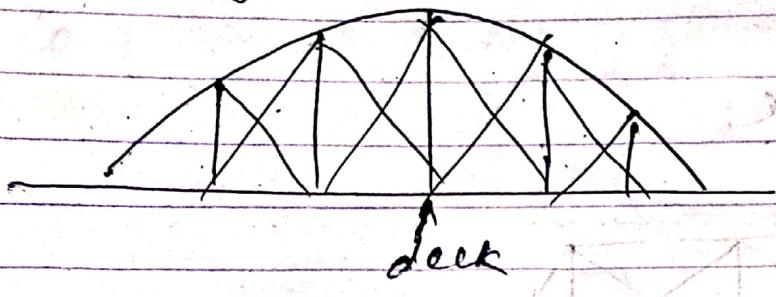
- span (60-80m) Rec, pre-tensioned (100m)
- curve profile can be made
- has good lateral load distribution capacity,
- good appearance
- generally used in Africa

Negative Aspect

- cast in-situ is difficult
- highly skilled manpower needed
- Advance technology.

(iv)

Arch Bridge



(Check Project Q312)

Fig: Through Type Arch

(v)

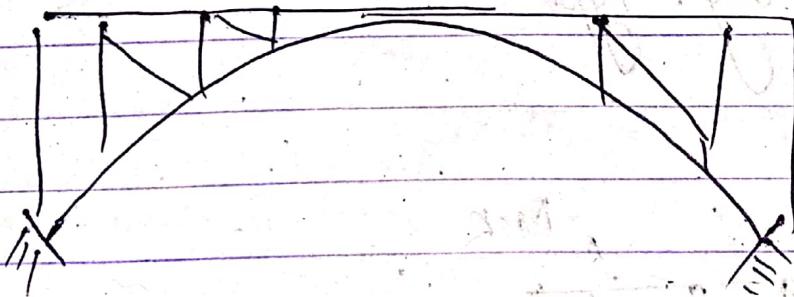


Fig: Deck Type Arch, (A, M, P)

Positive Aspect:

- upt span 600 m for RCC
- aesthetically pleasing.
- economical (section, If small section can resist high loading).

Negative Aspect

- strong abutment con. sub-soil condition
- if required high bearing capacity
- difficult to shape the arch → poor drainage



Tress Bridge:

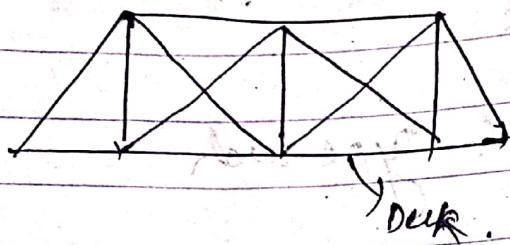


Fig: Through type

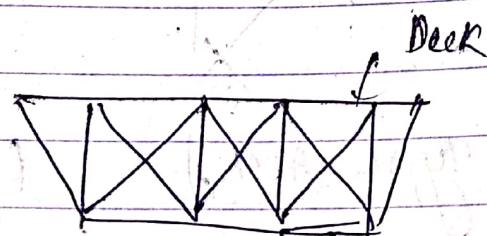


Fig: Deck Type

Positive Aspect:

- economical & viable upto 150 m.
- rigid structure, good lateral load distribution characteristics

→ high speed of fabrication used in emergency case.

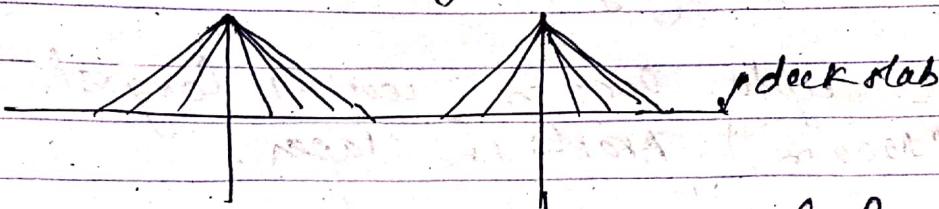
Negative

bulky

→ regular maintenance needed

→ less vertical clearance for deck type.

(vi). Cable Stayed Bridge.



Positive Aspect : ~~horizontal (800 m)~~
~~non-symmetrical~~

→ open upto (800m - 800m) RCC
preferred - 1000 - 1200

→ has good lateral load distribution.

→ main cable anchor set into deck slab.

→ better aesthetic appearance.

→ less no. of piers, foundation.

Negative :

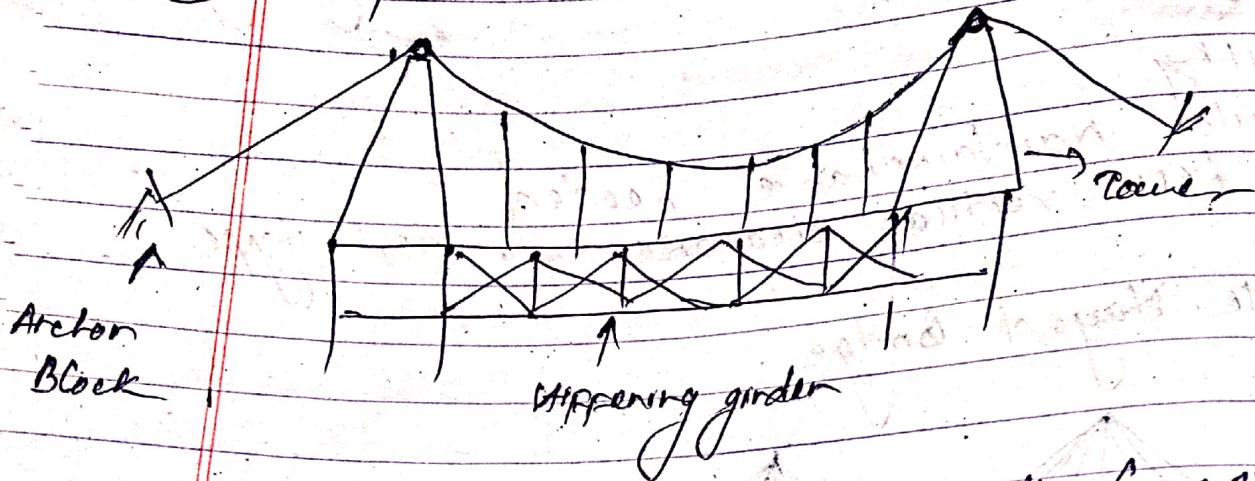
→ taller tower

→ skilled manpower

→ Advanced technology.

VII

Suspension cable Bridge:



→ viable upto 2000 m. world's longest
(1200 m) Akashi in Japan.

- good lateral load distribution
- main cable on top and deck slab.
- better aesthetic

~~Ans~~

What live load are considered for design of bridge in Nepal? Also explain how seismic forces are incorporated in the design of bridge.

- ⇒ Nepal Bridge Standard (2007) : All bridge design are designed as per AASHTO or TPC rules and otherwise specified, TPC can't be used (TPC 6: 2024)
- TPC Bridge Loading

TPC Live Load
(Circular load)

Normal Load
(Wheel vehicle)

- TPC class 'A' Loading
→ TPC class 'B' Loading

Abnormal Load

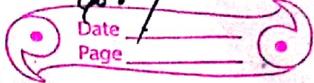
(Military and industrial traffic)

- TPC class 'F' & 'G' Loading
a) wheel loading
b) track loading

- TPC class AA Loading
a) circular loading
b) track loading

Design of Bridge:

lengthy effect on /



(i) Introduction :

- (i) choice of location of bridge site
- (ii) Bridge classification and its selection
- (iii) characteristics of bridge superstructure
- (iv) Data required for Analysis and Design of Bridge
(Bridge Design Data Requirements / Parameters)

Factors Affecting Selection of Bridge Type
component of Bridge

Second Part (Temp.)

- (i) Load calculation and its Structural Analysis
(BM, SF using EAD).

** Temp.*
→ method of lateral load distribution
(Analysis of bridge deck)

- ① coeuron's Method (T-beam Bridge Design)

** Temp. : (70-8.04. T-beam Nepal NT)*

② 3rd Part : Structural Design

→ design of slab bridge

→ design of T-beam bridge

II. Explain briefly how live loads are considered in the design of bridges in Nepal - Also explain the live service forces and moments.

→ Nepal Bridge Standard 80/67

Road Bridge Loading

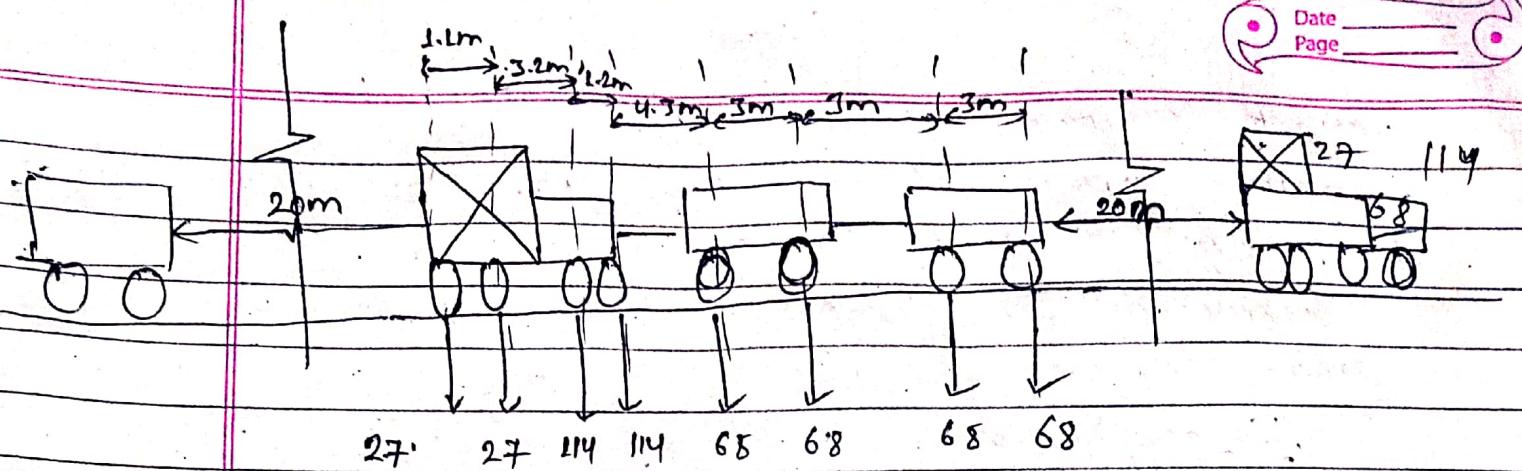
All permanent road bridge in Nepal shall be designed as per IRC loading or AASHTO loading. All design shall be carried out using in accordance to IRC standard for bridge unless otherwise specified.

IRC Live Loading:

① IRC Class A Loading:

If consists of wheel load train comprising a truck (driving unit) and a trailer of specified axle spacing and load.

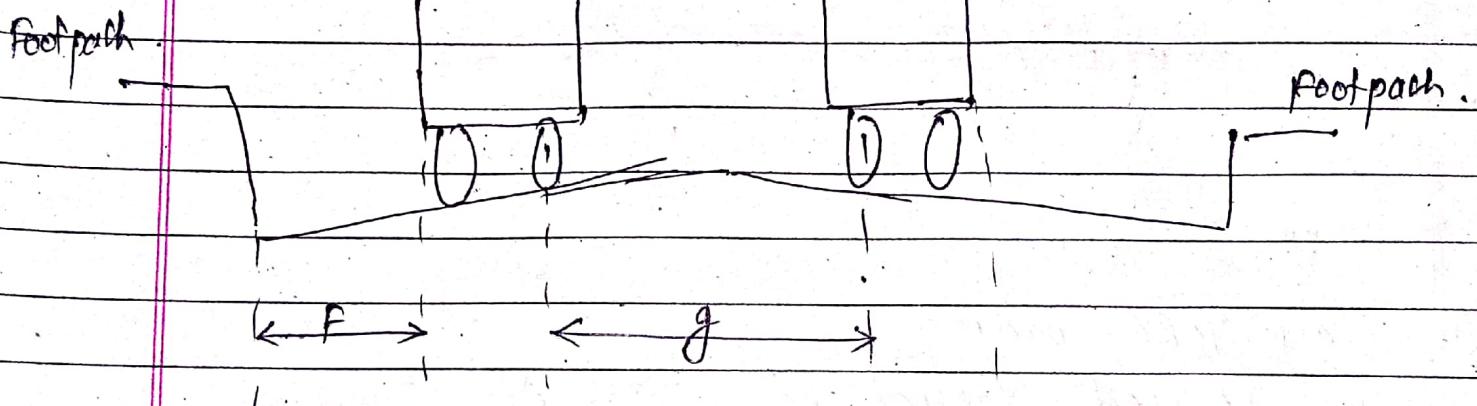
→ normally adopted for design of all roads on which permanent bridge and culvert are constructed.



$$\text{Total load} = 554 \text{ kN}$$

$$= (27 + 27 + 114 + 114 + 68 + 68 + 68 + 68 + 68)$$

Longitudinal positioning of class A vehicle
carriageway width



$$f \geq 150 \text{ mm}$$

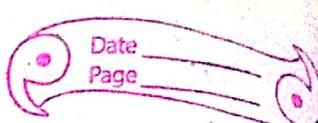
$$g \geq 1.2 \text{ m} \quad \text{for two lane.}$$

→ For one train of class A vehicle occupies
one lane of carriageway of bridge!

→ Bridge designed for class A loading should be checked for class 70R loading and class AA loading. Why? → to identify the most critical loading condition.

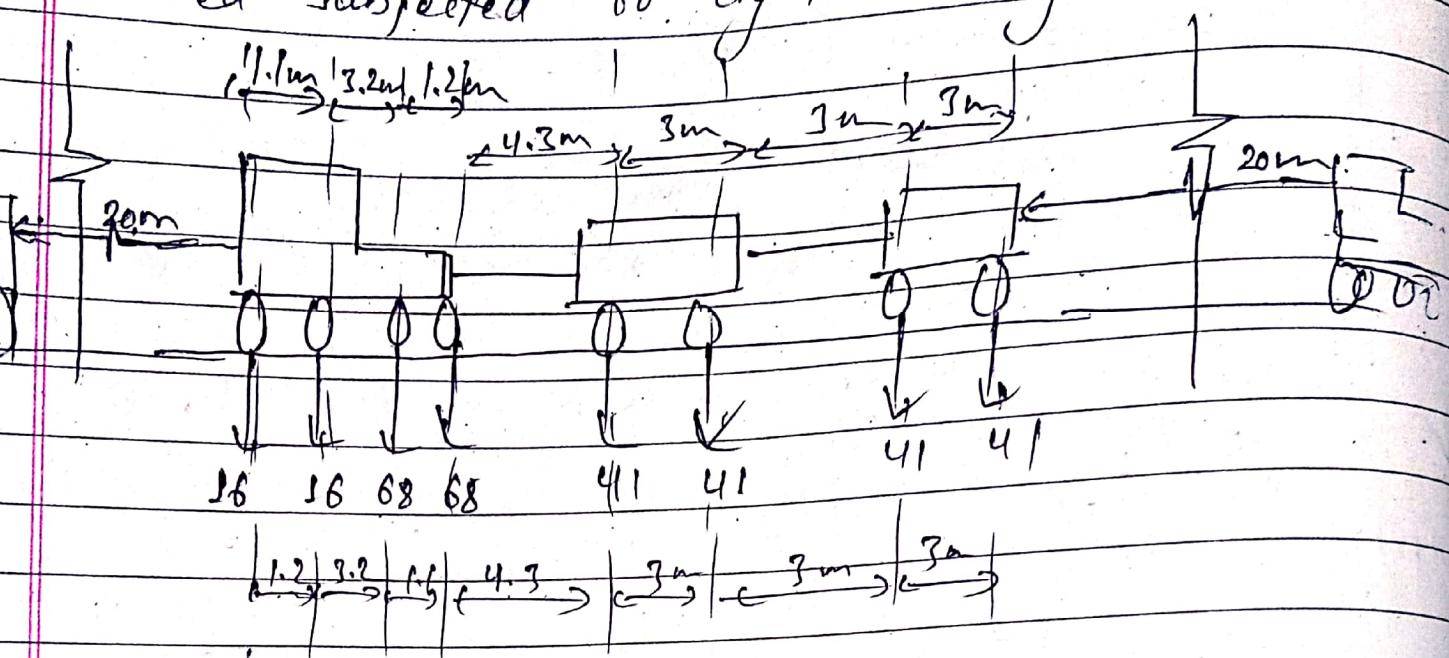
00 00 00 00 00 00 00
 11 11 11 11 11 11 11
 24 7+114 114 63

00 00 00 00 00 00
 H H H H H H
 1.1 3.2 1.2
 11 11 11 11 11 11
 24 7+114 114 63 63



(ii) Class B Loading:

- composed of wheel load train similar to class A loading but with smaller axle load.
- considered for temporary bridge in specified area subjected to light loading.



27 29 114 114

(iii)

Class F0R Loading:

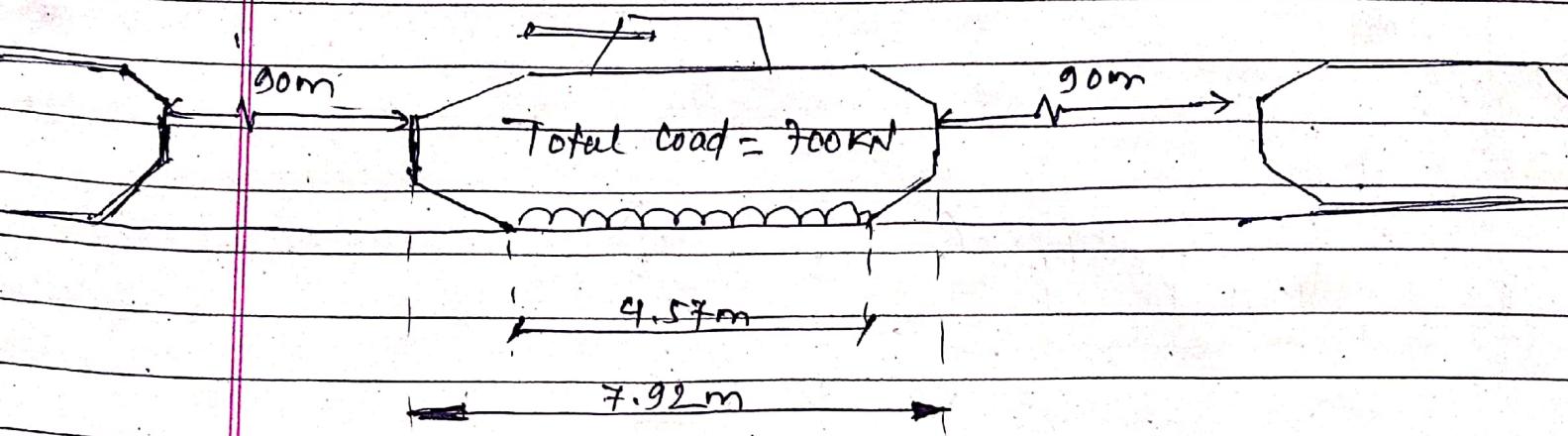
- renamed version of class 'AA' loading and consist of tracked and wheel load.

→ FRC class F0R loading is adopted for all road where permanent bridge is constructed.

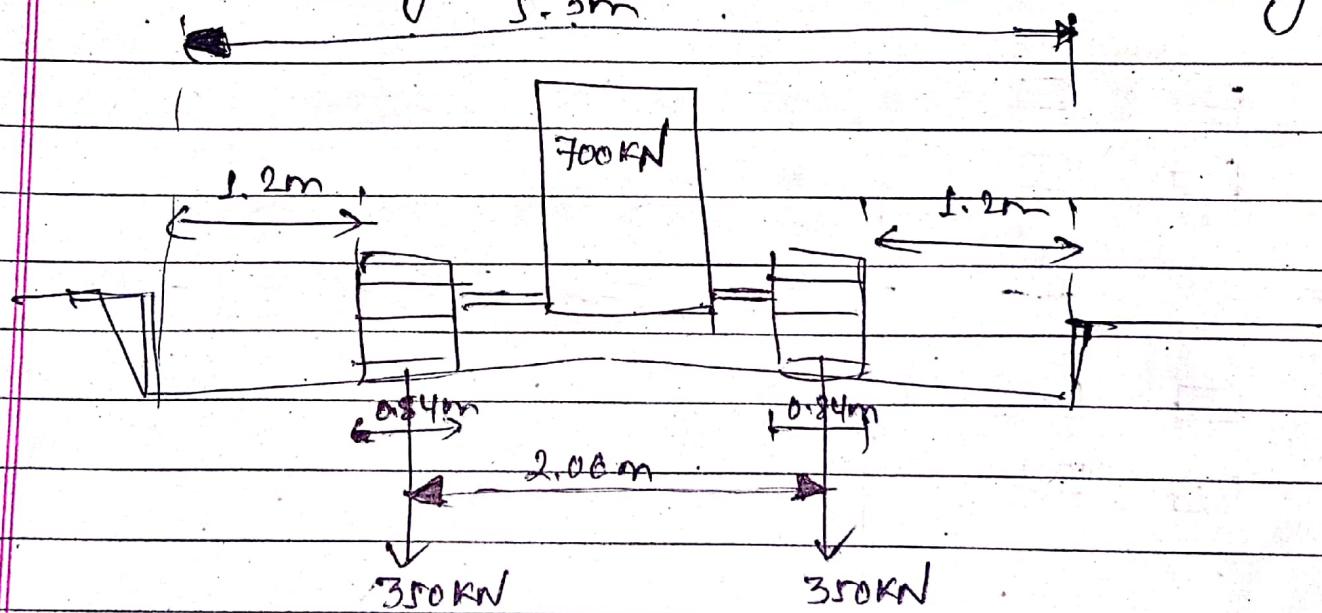
→ Bridge design for FRC class F0R loading should be checked for class A loading.

→ One class of 70 kN loading occupies two lanes of bridge carriageway.

(a) Track ~~dead~~ loading:



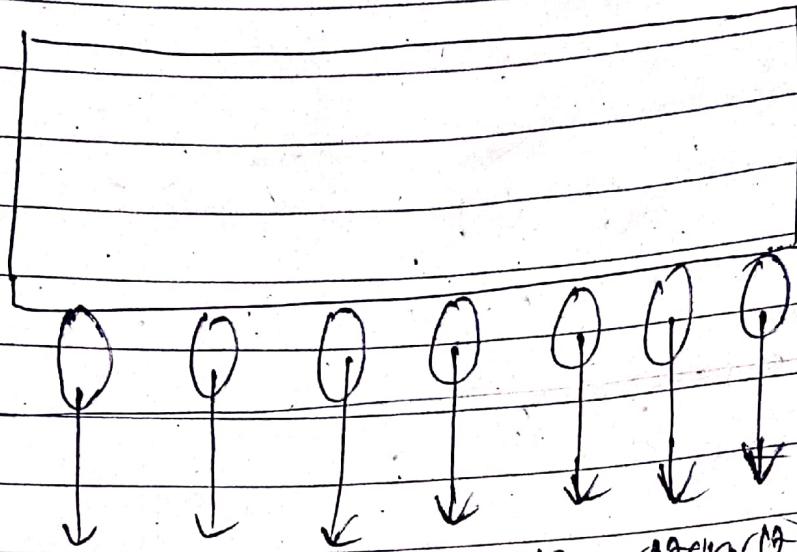
longitudinal section of class 70 kN loading.



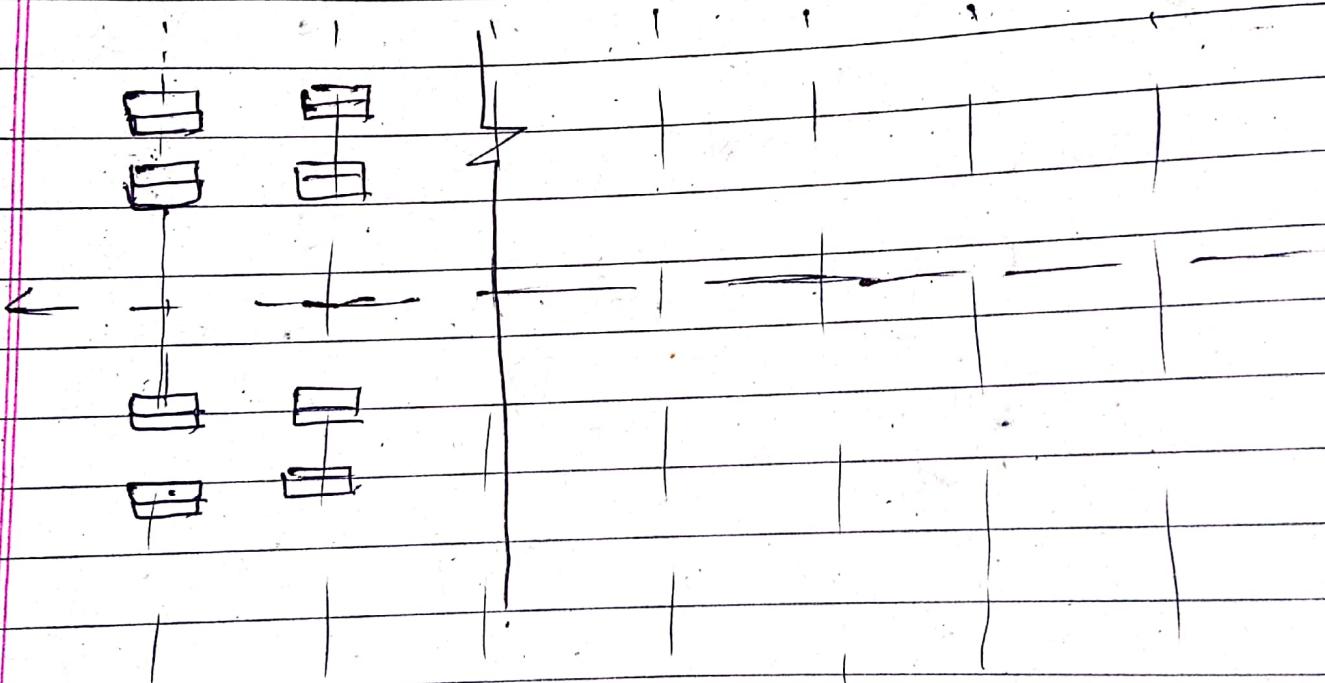
Transverse - section

(11). Class AA loading :

(b) wheel loading (class 70R)
→ seven axle wheel load

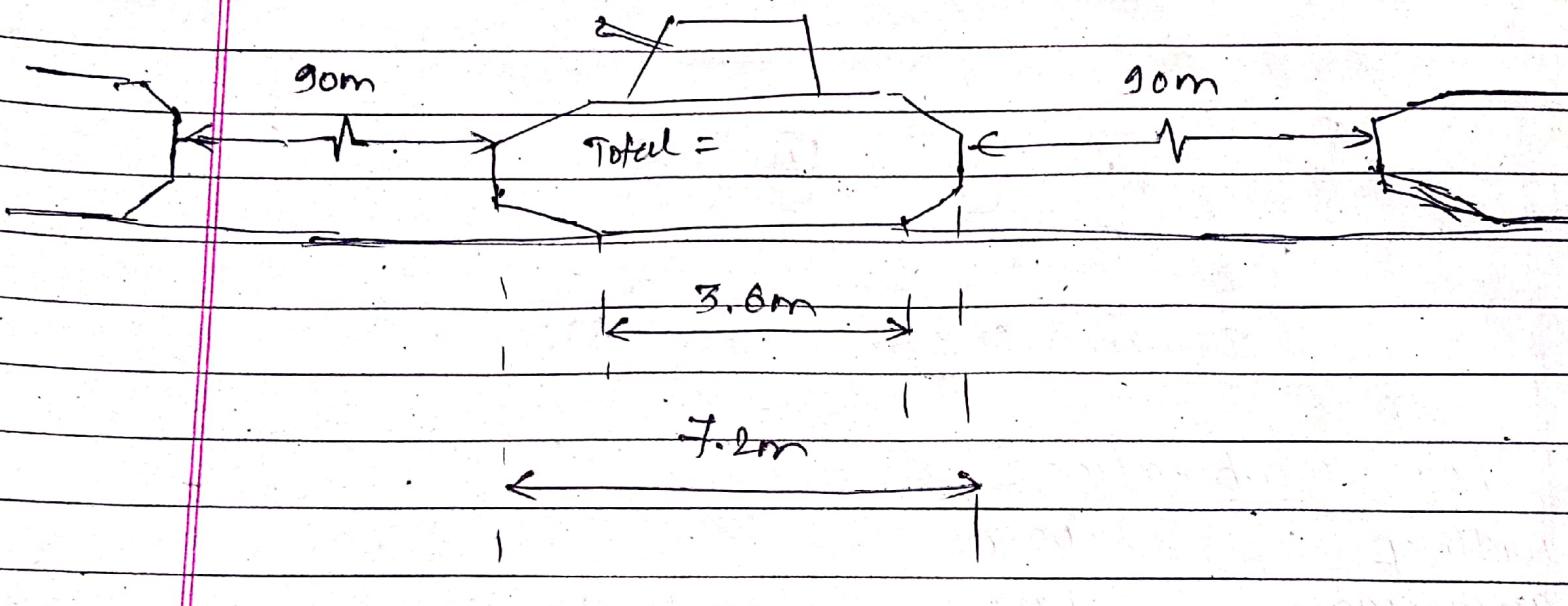


80kN 120kN 120kN 120kN 120kN 120kN 120kN

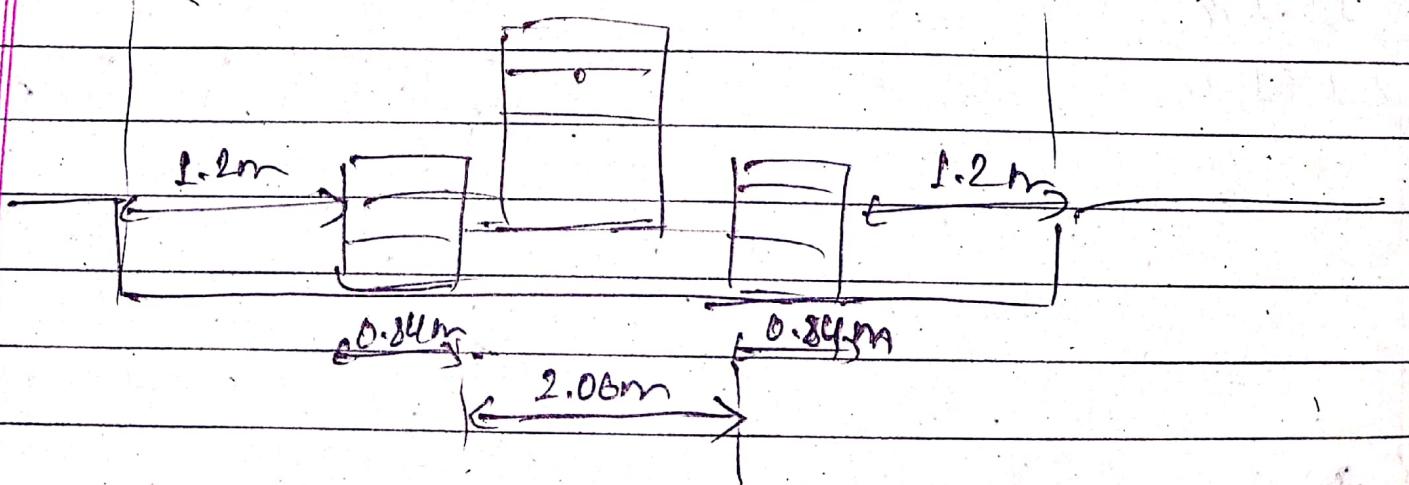


(iv) class AA Loading:

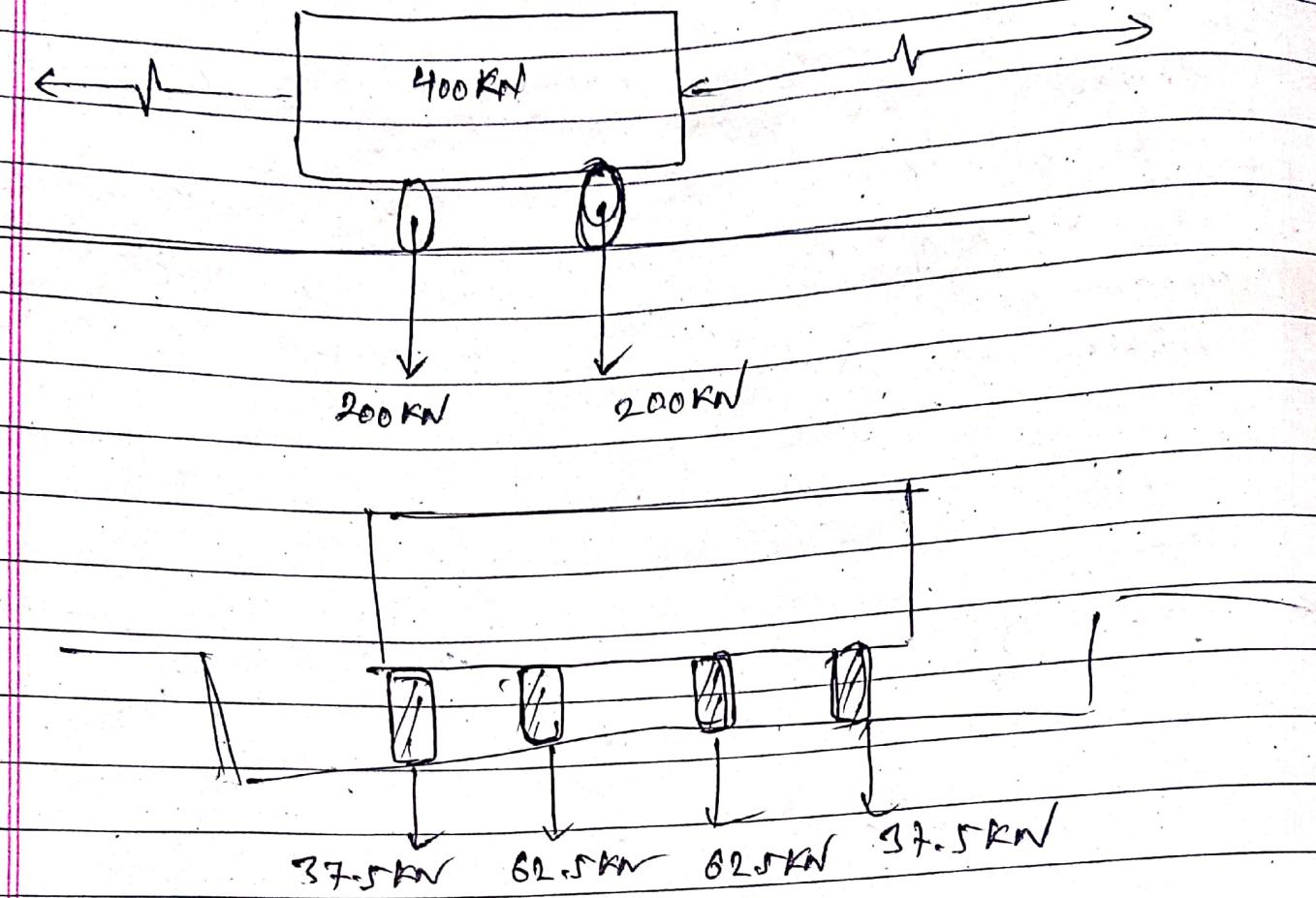
- ⑨. → consists of either a tracked vehicle or wheeled vehicle
 → normally bridge on national highways are designed for class 'AA' loads.
 → Bridge design for class AA loading should be checked for class A loading (unless certain condition, heavier stress might be obtained under class A loading).



longitudinal positioning of class AA loading
 $\geq 5.3 \text{ m}$

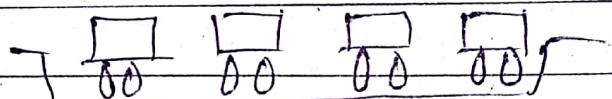


(b) Wheeled vehicle.



* Load combination:-

| width of carriage way off bridge | No. of lanes | Load combination |
|-------------------------------------|--------------|---------------------|
| $\geq 15.1\text{ m}$ | 4 | combination ① |
| $< 16.1\text{ m}$ | | class A vehicle (4) |



combination ①.

no. 2 class A vehicle +

class 70R or class AA

② no. 1
combo ③

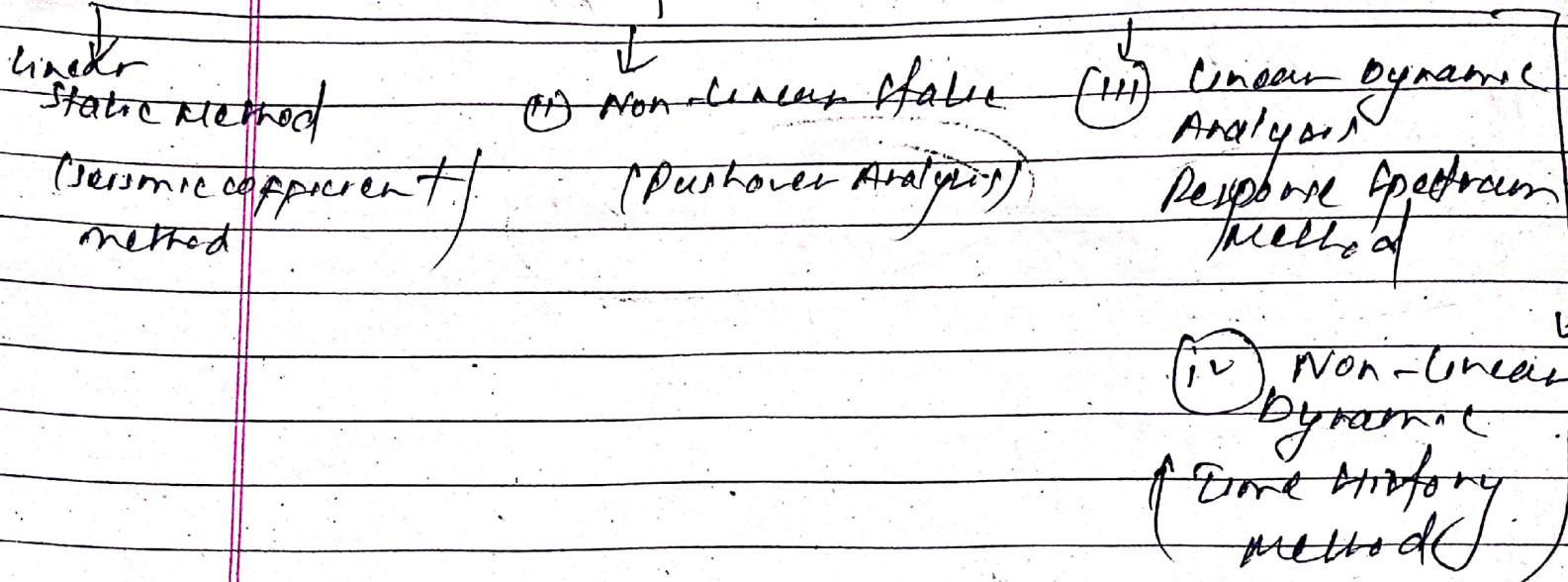
5.18 m

Class 7 or class A

2nd year.

most critical taken.

Seismic wave consideration:



Linear static method:

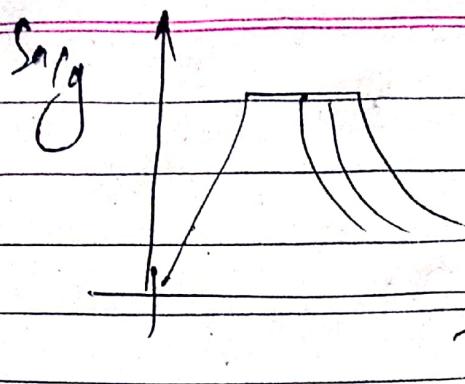
$$V_B = A_h w$$

$$A_h = \left(\frac{\pi}{2} \right) \left(\frac{S_a}{g} \right) \left(\frac{I}{R} \right)$$

I = importance factor = 1.5 for national highway bridge
 $= 1$ for other bridge.

R = Response Reduction Factor = 2.5
 (ductile detailing).

Z = ① depends on seismic zone.

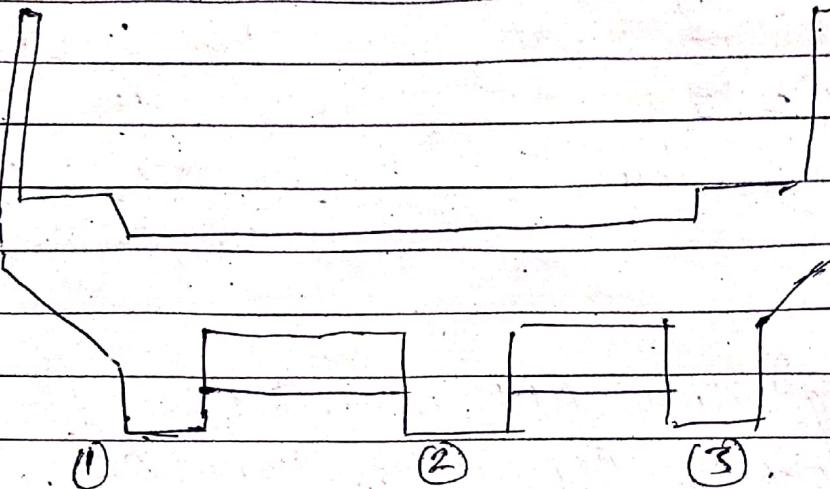


depends on fundamental time period.

Theorem, slab body

Courton's

- * Structural Analysis of T-beam and Slab Bridge:
- method of lateral load distribution in deck slab and girder. (long. girder π with load $311.3 \text{ kN}/\text{m}$)



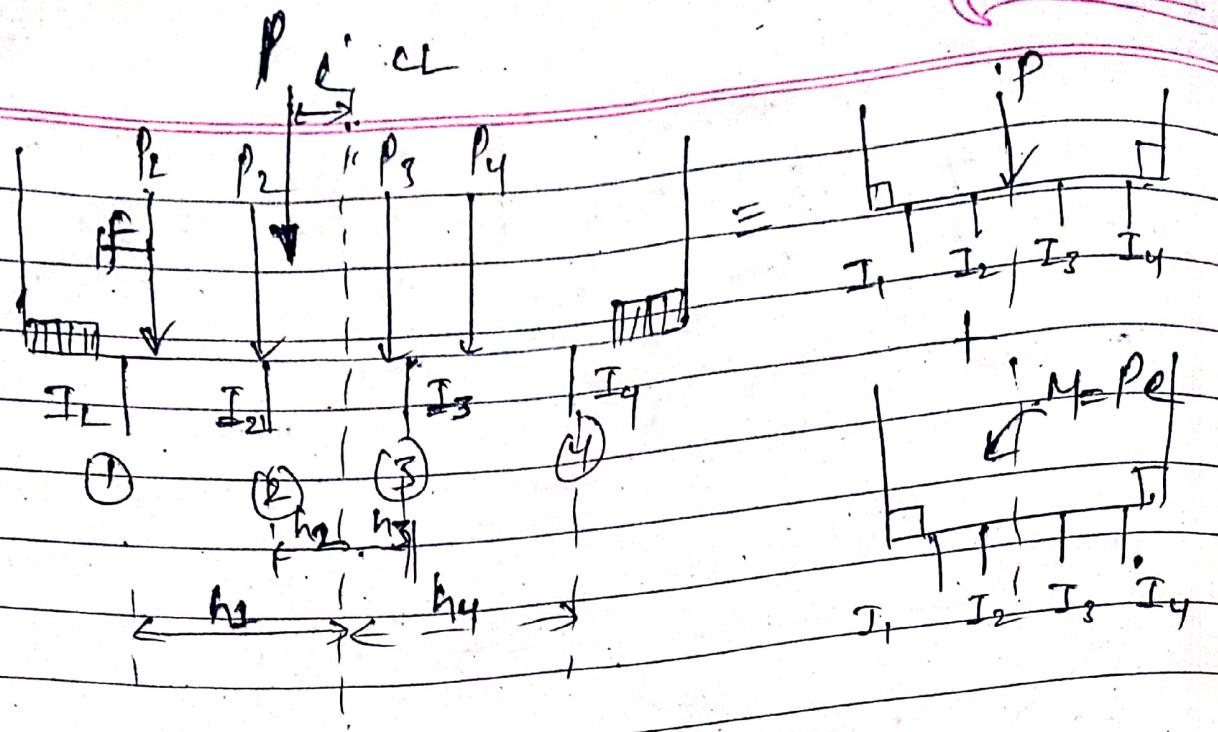
- ① Courbion's method of lateral load distribution:
- used in the analysis of T-beam and composite bridge

Requirement:

(I) ratio of spans to width > 2
 (II) \wedge No. of cross-beams interconnecting the longitudinal girder slab = 5 (adequate stiffeners)

(III). Depth of cross girder should at least be $3/4 (0.75)$ of the depth of longitudinal beam girder.

Simple, highly popular and powerful tool
 for lateral load distribution in T-beam



Analysis:

→ mon. longitudinal BM, mon. SF along SF.

→ mon. transverse BM, mon. SF

To get mon longitudinal BM and SF due to live load, transverse positioning of live load is such that it produces maximum eccentricity.

Load shared by each girder:

$$1^{\text{st}} \text{ girder } R_1 = \frac{P_{I1}}{\sum I} + \frac{M I_{1h_1}}{\sum I h_1^2}$$

$$R_2 = \frac{P_{I2}}{\sum I} + \frac{M I_{2h_2}}{\sum I h_2^2}$$

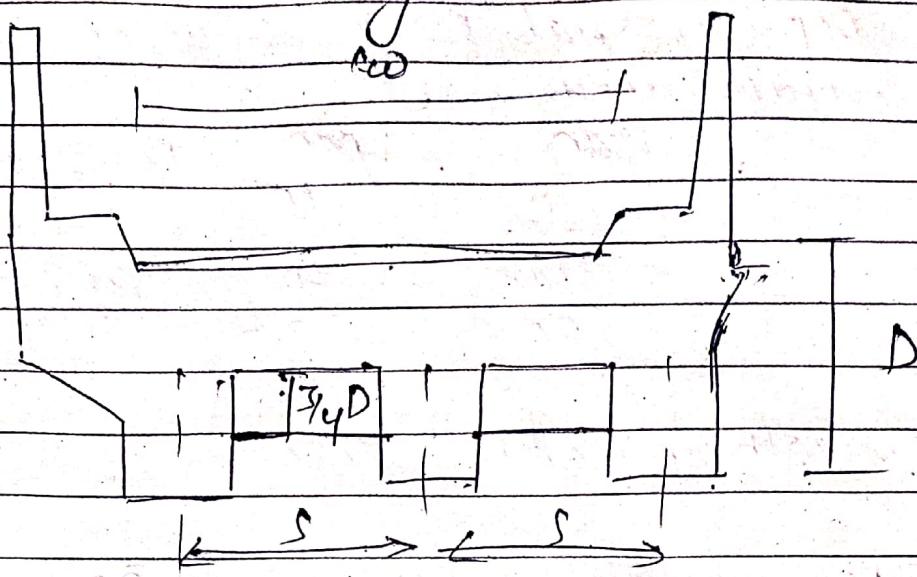
$$R_3 = \frac{P_{I3}}{\sum I} - \frac{M I_{3h_3}}{\sum I h_3^2}$$

$$R_4 = \frac{P_{I4}}{\sum I} - \frac{M I_{4h_4}}{\sum I h_4^2}$$

$$R_2 = \frac{P I_y}{C_2} + \frac{M_{2,2n}}{C_2 L_n}$$

$$R_1 = \frac{P I_y}{C_1 L_n} - \frac{M_{1,2n}}{C_1 L_n}$$

* Design of T-beam bridge :



→ Main load Resisting member

(i) Deck slab

(ii) Main girder

(iii) cross girder.

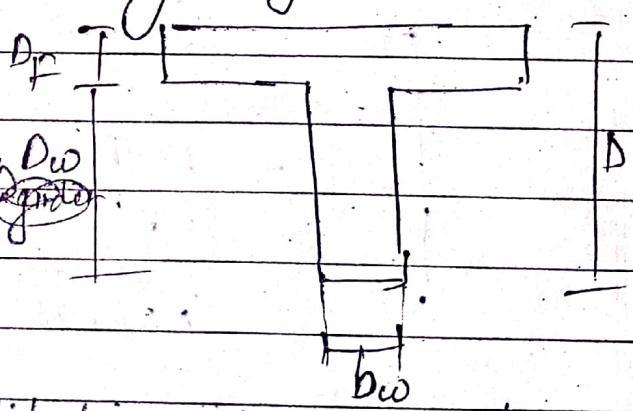
STEP (I) : planning and preliminary design

Planning :

For single lane : 4.25m

For double lane : 7-7.5m

width of carriageway :



Ht. of railing $\Rightarrow \geq 1.1$ - half width of railing

width of kerb $\Rightarrow \geq 0.225$ m

depth of kerb = 0.225 m

width of footpath ≥ 0.6 m

Preliminary design:

a) Depth of slab/plating $\geq 200\text{mm}$

b) overall depth =

$$= \frac{\text{span}}{10} - 1\text{ step}$$
 For simply supported.

$= \frac{\text{span}}{20} - \frac{\text{span}}{25}$ for continuous.

c) breadth of web (b_w) $\geq 250\text{mm}$

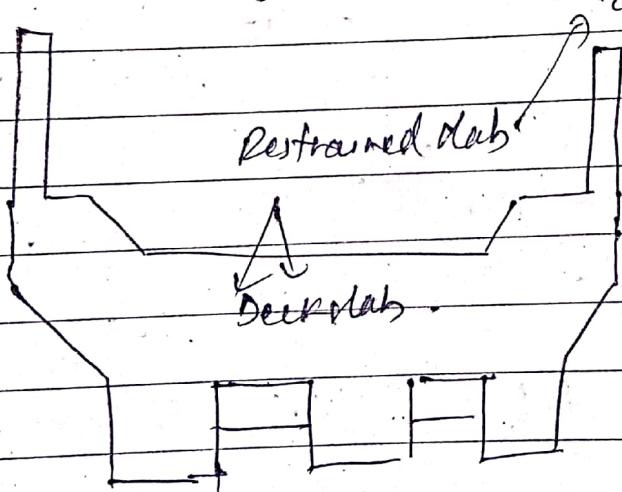
d) spacing of main girder = 2-3m

e) spacing of cross girder = 3-5m

f) min. no. of cross girder = ≥ 5 nos.

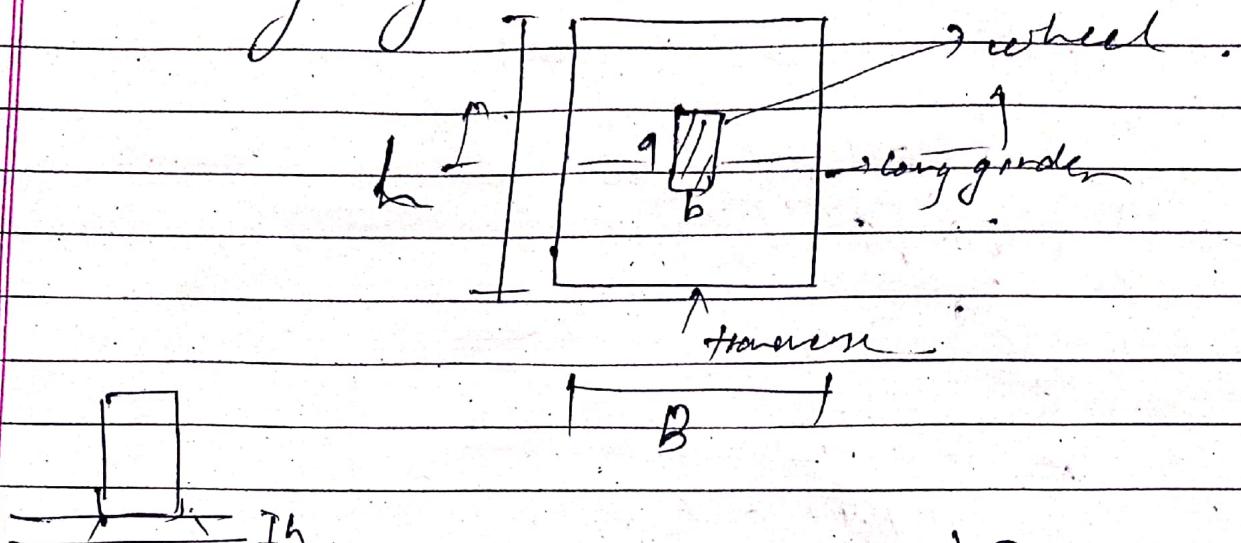
g) depth of cross girder = $\geq \frac{3}{4} D$

Confidence
STEP ② : Analysis of ~~deck~~ slab and its design.
 w.r.t support.



→ using effective width method

STEP 3: Analysis and design of restrained slab.
→ Using Pigeaud method.



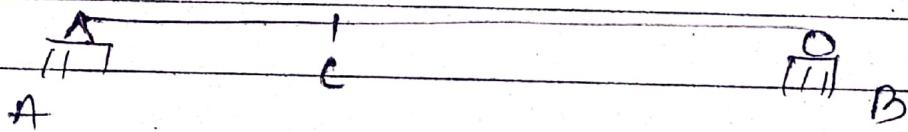
$$M_1 = (m_1 + \mu m_2) P$$

$$M_2 = (m_2 + \mu m_1) P$$

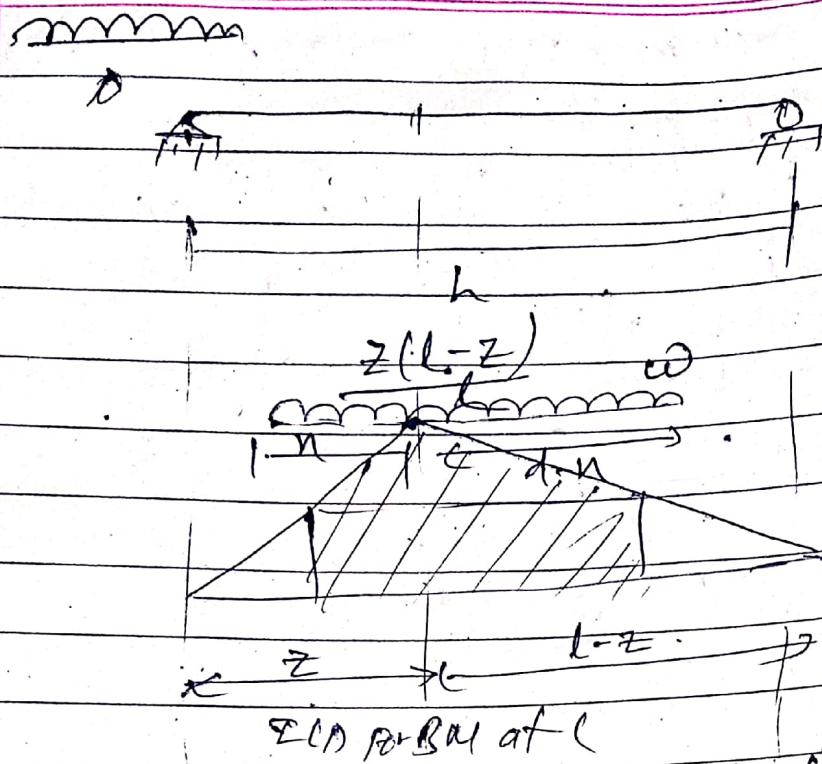
$m_1, m_2 \Rightarrow$ coeff. for moments along short and long spans

$M_1, M_2 \Rightarrow$ moment along short and long spans

STEP 4: Analysis and Design of main girder due to moving load:



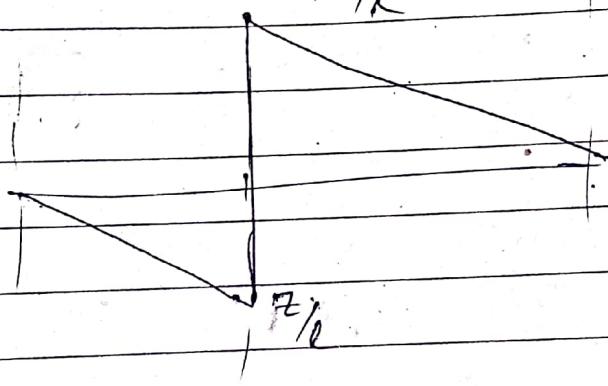
main. B.S. of section C. per
a) track load.



\rightarrow Using ICD we have to calculate mean value of BM and MF

Top BM and MF

$$L - z/r$$



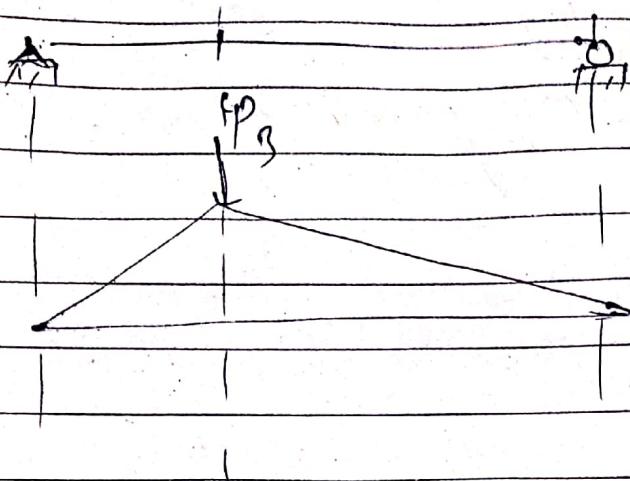
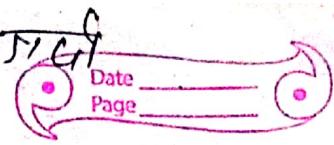
BM max at C occurs when $\frac{d}{d} = \frac{z}{r}$

Mean = $\omega \times \text{Area of shaded part}$.

(b) wheel load

P_4 P_3 P_2 P_1

Span after moment
calculator done.



Now when one of the load at C and . Eg.

B2 P_3 is 604

B2 P_3 C AT BISER 316E

$$\left(\frac{P_y}{z} \right) > \frac{R_2}{(L-z)}$$

It changes sign.

$$\left(\frac{R_2}{z} \right) < \frac{R_2}{(L-z)}$$

$$M_{mom} = P_1 y_1 + P_2 y_2 + P_3 y_3 + P_4 y_4$$

similarly if

STEPS :- Calculation of steel reinforcement.

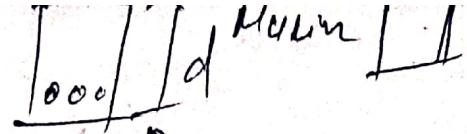
$$M_{mom} = 0.87 f_y (A_{st}) d \left[1 - \frac{f_y A_{st}}{f_{ck} b d} \right]$$

$$A_{st} = - - - -$$

f_{ck} = 500 N/mm²

$$\text{Also, check } M_{mom} = 0.133 f_{ck} b d^2$$

$$d_{min} = \sqrt{\frac{M}{0.133 f_{ck} b}}$$



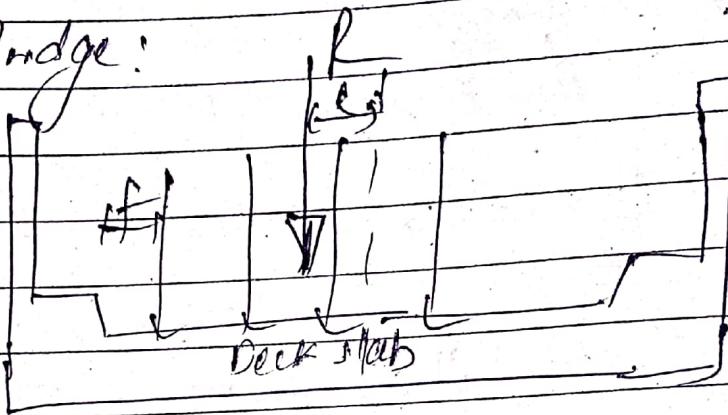
$d > d_{\text{base}}$ \Rightarrow singly reinforced.

$d \leq d_{\text{base}}$ \Rightarrow doubly reinforced.

STEP 6: Detailing:

see notes).

(II) Slab Bridge:



main loading taken by slab ..

Planning and preliminary design:

1 lane \Rightarrow 4.25 m

2 lane = 7 - 7.5 m.

Kerb width = 0.225 m

height of footpath = 0.225 m ..

Preliminary Design:

Depth of slab (Deflection control considered)

$$D = \frac{\text{span}}{15} - \frac{\text{span}}{12} \quad \text{simply supported}$$

$$= \frac{\text{span}}{20} - \frac{\text{span}}{25} \quad \text{continuous.}$$

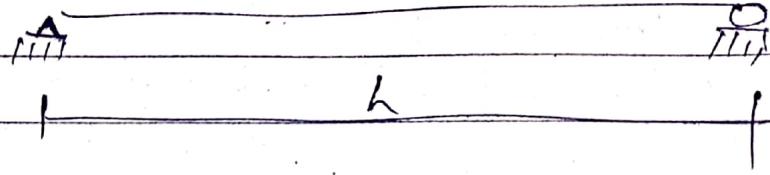
STEP (E) : Analysis of deck slab

Positioning of one load ~~at center~~

$\Rightarrow M_{\text{max}} \rightarrow$ end of long

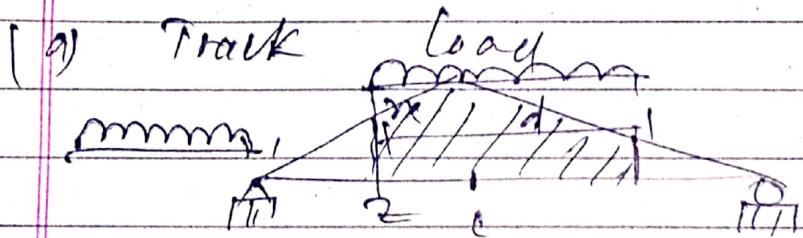
$M_{\text{max transverse}} \Rightarrow e_{\text{min}}$.

assume unit (1m)
width beam.



unit effective width multiply

using IED determine B_{max} and S_{max}
per (a) track load and (b) wheel load..



$B_{\text{max}} \text{ when } \frac{w}{l} = \frac{2}{3}$

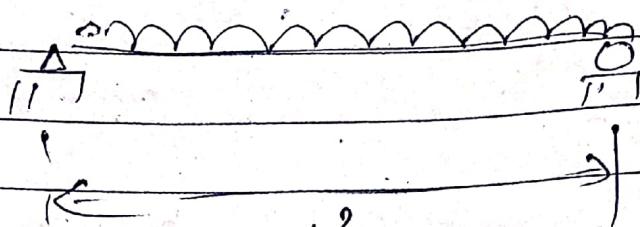
$B_{\text{max}} = w \times \text{Area of shaded}$.

(b) wheel load

Term reinforcement. H/T & A/C

Date _____
Page _____

Dead load



$$M_{\text{dead}} = \frac{\omega l^2}{8} \quad (\text{long})$$

b) Toy. Reinforcement.

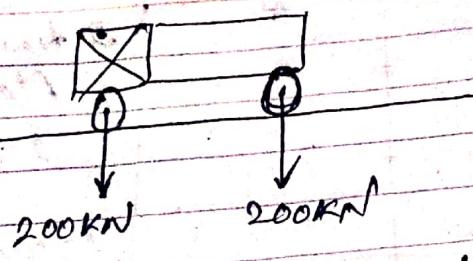
For Bending in framework

$$(M_{\text{frame}})_{\text{dead}} = 0.3 \text{ LLBM} + 0.2 \text{ DCBM}$$

$$= 0.3(M_{\text{dead}})_{\text{LL}} + 0.2(M_{\text{dead}})_{\text{DC}}$$

y
toy reinforcement :

Span



Ag: Longitudinal section.

* Bridge Load combination:

| carriageway width (m) | No. of lane. | Live load | |
|--|--------------|-----------------------------------|---|
| $\leq 5.3 \text{ m}$ $> 4.75 \text{ m}$ | 1 | class 'A' loading per 2.3 m width | |
| $5.3 \leq n < 9.6 \text{ m}$ | 2 | class 'A' train 2 number | class 70R / class AA load one train |
| $9.6 \leq n < 13.1 \text{ m}$ | 3 | class 'A' train 3 number | class 70R / class AA load one train + class A one train |
| $13.1 \leq n < 16 \text{ m}$ | 4 | class A train 4 no. | 2 trains of class 70R / AA or or 1 train class 70R / AA + 2 class A |

⑤. $\geq 16.6 \text{ m} < 20.1 \text{ m}$

5

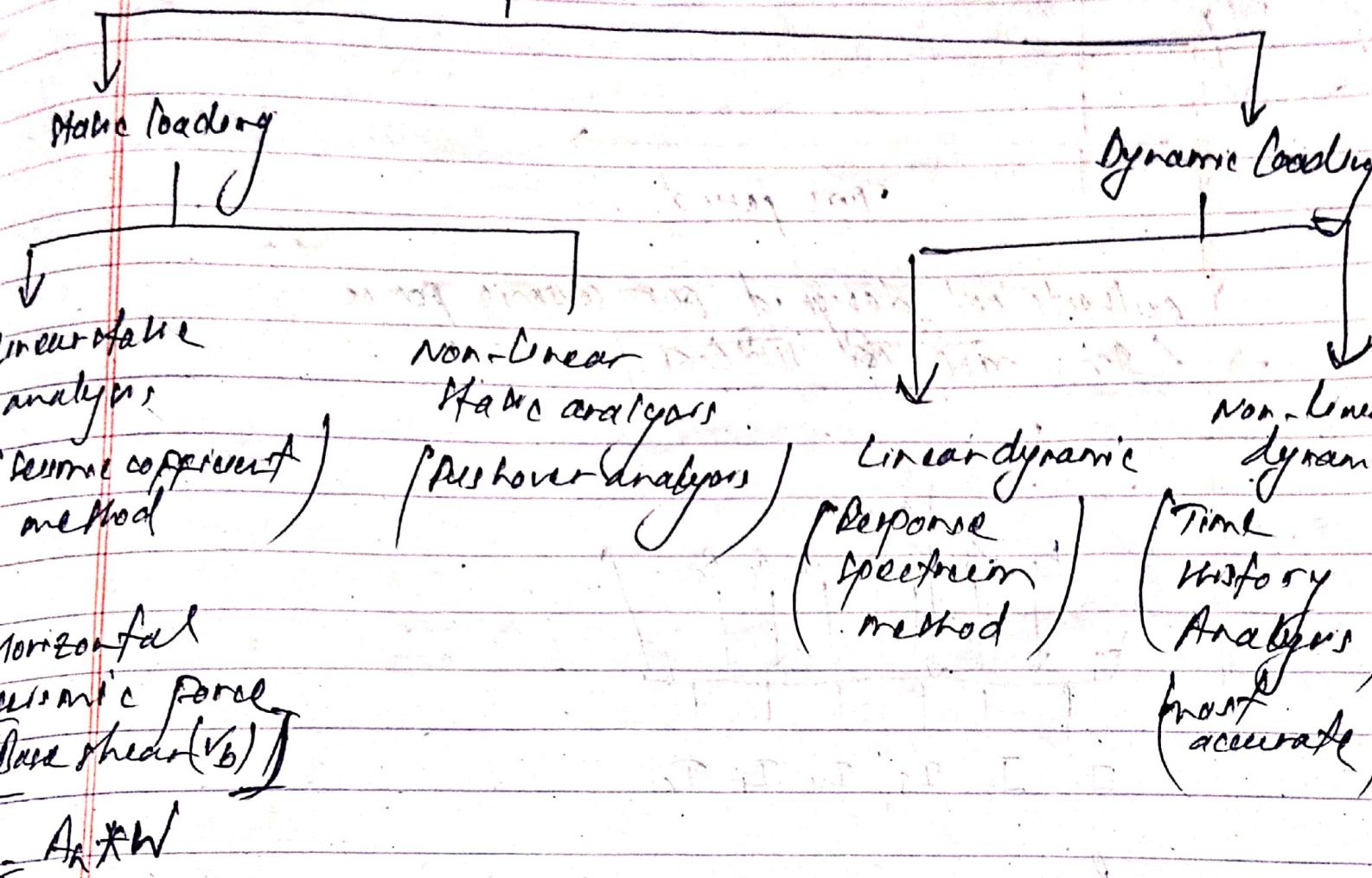
2 train of class ~~AOR~~
1 train of class AA +
1 train of class A
~~AOR~~

1 train of class AA ~~AOR~~
+ 3 train of class
A ~~AOR~~

⑥. $\geq 20.1 \text{ m} < 28.6 \text{ m}$

6

* Seismic Analysis of Bridge:



$$V_b = \frac{f_1}{g} * \left(\frac{\pi}{2}\right) * \left(\frac{I}{R}\right)$$

f_1) Zone factor.

\approx) Importance factor (1.65 for natural road 1 for feeder)

\approx) Response reduction factor (2.5)

\approx) Spectral acceleration at 5% damping,

* List out and discuss the loads, forces and stresses which are to be considered in the designing of a road bridge.

→ Loads to be considered for appropriate combination to carry out the necessary checks for the design of road bridges as per IRC, 6-2017 are as follows:

- 1) Dead Load
 - 2) Snow Load
 - 3) Superimposed dead load such as hand rail, crash barriers, footpath & service loads.
 - 4) Surfacing or Wearing coat
 - 5) Back fill weight
 - 6) Earth Pressure
 - 7) Primary and secondary effect of prestress
 - 8) Secondary effects such as creep, shrinkage and settlement
 - 9) Temperature effects including restraint and bearing forces
 - 10) Carriage way live load, footpath live load, construction live load
 - 11) Associated carriageway live load such as braking, tractive and centrifugal forces.
 - 12) Accidental forces such as vehicle collision load, barge impact due to floating bodies and accidental wheel load on mountable footway
 - 13) Wind
 - 14) Seismic Effect
 - 15) Construction dead loads such as weight of launching girder, truss or cantilever construction equipments
 - 16) Water current forces
 - 17) Wave Pressure
 - 18) Buoyancy
 - 19) Hydrodynamic Effect
- } Hydraulic loads.

1. Dead Load

→ It is the self weight of the structure and any permanent loads fixed thereon.
 → The dead load of a member depends upon the type of materials made of.

2. Live Load

→ Road bridges are divided into classes according to the loadings they are designed to carry.

- (i) IRC Class 70R Loading (Wheeled and Tracked Type)
- (ii) IRC Class AA Loading (Wheeled and Tracked Type)
- (iii) IRC Class A Loading
- (iv) IRC Class B Loading → timber bridges
- (v) IRC Class Special Vehicle (SV) Loading

For bridges classified above, the design live load shall consist of standard wheeled or tracked vehicles or trains of vehicles as illustrated below.

(i)

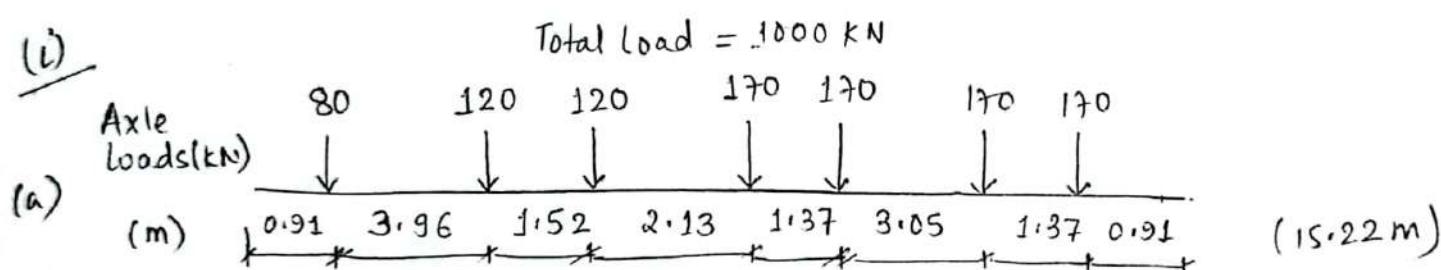


fig: Class 70R (Wheeled) - longitudinal Position.

(b)

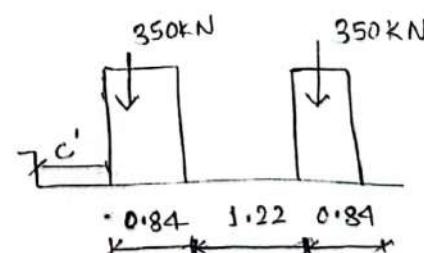
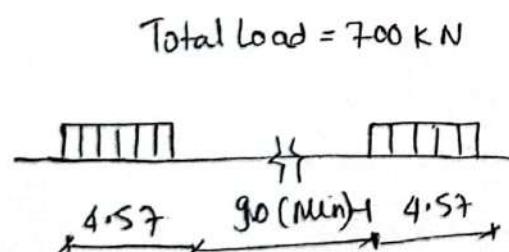
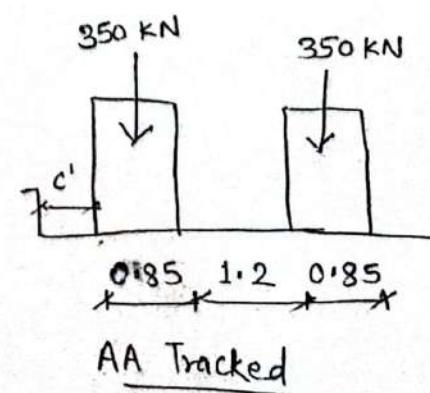
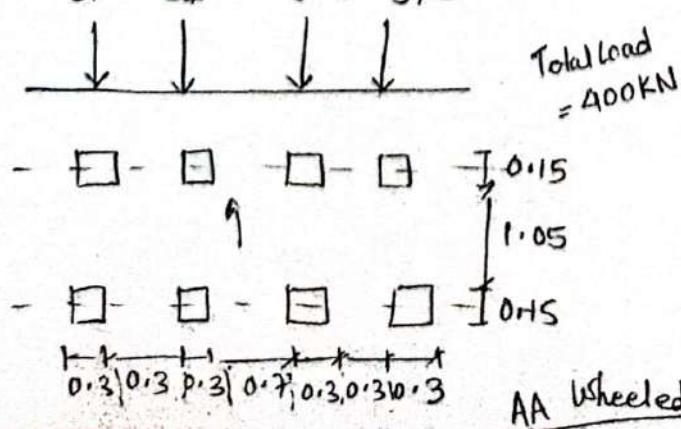


fig: Class 70R (Tracked) Vehicle

(ii)



(iii)

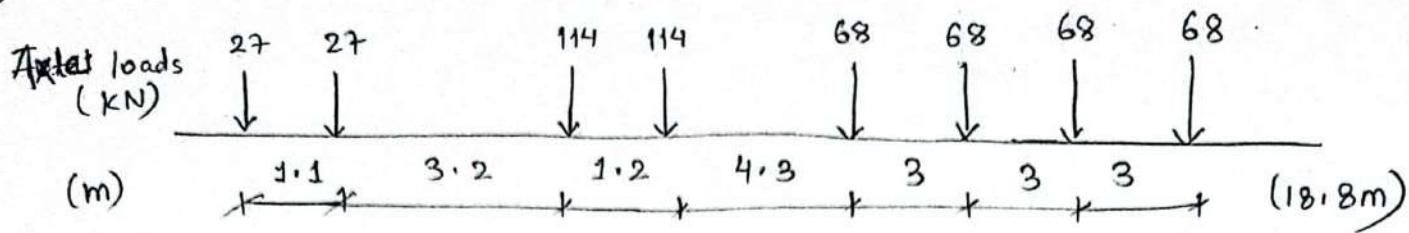


fig : Class A Vehicle (Longitudinal Position)

→ Bridges designed for class AA loading and class 70 R loading should be checked for class A loading also, as under certain conditions, heavier stresses may occur under class A loading.

3. Impact

→ Provision for impact or dynamic action shall be made by an increment of the live load by an impact allowance expressed as a fraction or a percentage of applied live load.

For Class A or B Loading (3m to 45m)

(i) Impact factor fraction for RCC bridges = $\frac{4.5}{6+L}$

(ii) Impact factor fraction for steel bridges = $\frac{9}{13.5+L}$
where; L is span in meters.

For 70R Loading or Class AA Loading

i) for span less than 9m

Tracked vehicles = 25% for span up to 5m & linearly reducing to 10% for span up to 9m.

Wheeled Vehicles = 25%.

ii) for span of 9m or more

RCC Bridges

Tracked vehicles = 10% up to span of 40m

Wheeled Vehicles = 25% up to span of 12m

} for greater, in accordance with curve of IRC code

Steel Bridges

Tracked Vehicles = 10% for all spans

Wheeled Vehicles = 25% up to span of 23m.

Economic Span Length

→ depend upon cost of substructure & Superstructure

Total cost of bridge = Cost of superstructure + total cost of sub-structure.

→ When the span length of bridge increases, cost of sub str. decreases while cost of super str. increases.

→ Cost. of main girders & cross girders per unit length, directly proportional to span.

→ Economic span is span for which overall cost of bridge is minimum. For this, cost of super str. = cost of sub str.

Total cost of bridge = cost of abutments + no. of pier * cost of each pier + length * cost of flooring per unit length + length * cost of main & cross girders per meter length.

$$\therefore C = CA + nC_p + LCF + LTC \quad L = \text{total length}$$

Here,

$$C_T \propto l$$

$$C_T = Kl$$

$$\text{Also, } n = \frac{L}{l} - 1$$

$n = \text{no. of piers}$.

$l = \text{length of one span}$

$$\therefore C = CA + C_p \left(\frac{L}{l} - 1 \right) + LCF + L \cdot K \cdot l = CA + \frac{L}{l} C_p + LCF + LKl - C_p$$

$$\text{for total cost to be min}^m; \quad \frac{dc}{dl} = 0$$

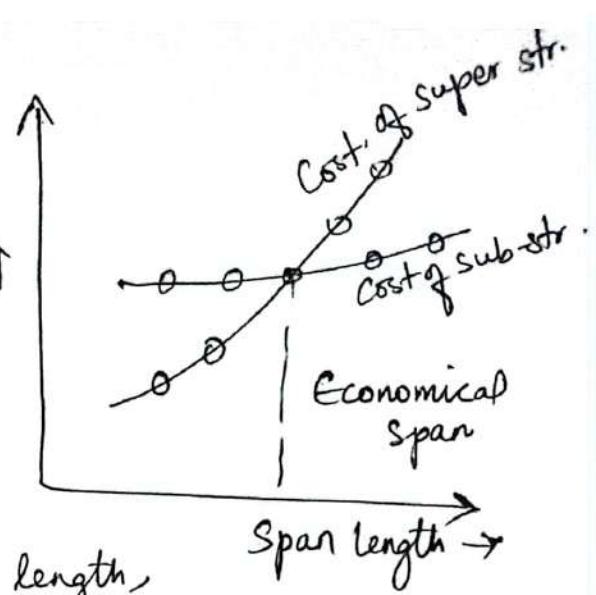
$$0 = 0 - \frac{L}{l^2} C_p + 0 + LK$$

$$\text{or, } K = \frac{C_p}{l^2} \quad \text{or, } lk = \frac{C_p}{l}$$

$$\therefore l = \sqrt{\frac{C_p}{K}}$$

$$\text{or, } C_p = l C_T$$

thus, we can conclude that, most economical span length is that for which cost of superstructure equals the cost of sub-structure.



So when cost of pier is equal to cost of main girders & cross girder of the span, the total cost of bridge will be minimum.

* Selection of bridge type

① Geometric condition of site

→ depend on horizontal and vertical alignment of the highway route and on clearances above and below the roadway.

e.g. alignment is on curve, box & slab type bridges are best option

② Subsurface conditions of site

→ foundations soils

} governs the type of substructure & foundation.

→ Scour depth
→ Weak subsoil = Simply supported spans instead of continuous spans

③ functional requirements

→ future widening or replacement of bridge deck is a concern, girder type bridge is best option.

→ type of traffic - restrict the choice of bridge type.

④ Aesthetics

⑤ Economic and ease* of maintenance

⑥ Construction and erection considerations

→ Availability of skilled & unskilled labours, specified materials.

⑦ legal considerations

→ environmental consideration