

**Q1) What is a Gimbal lock?**

In case 2 axes (about which the rotation is capable of happening) get aligned exactly with each other, the problem of gimbal lock arises. In such a case, there is no way to rotate around one of the axes.

This problem becomes particularly evident while representing rotations using EULER angles as similar to the case of a gyroscope gimbal (where the inner gimbals move whenever the external gimbal moves), when we are using **INTRINSIC EULER ANGLES** (let's say Z-Y-X), then coordinate axes X and Y also rotate when Z rotates, thus displacing them from their original location and transporting them to a location where rotation has already taken place before.

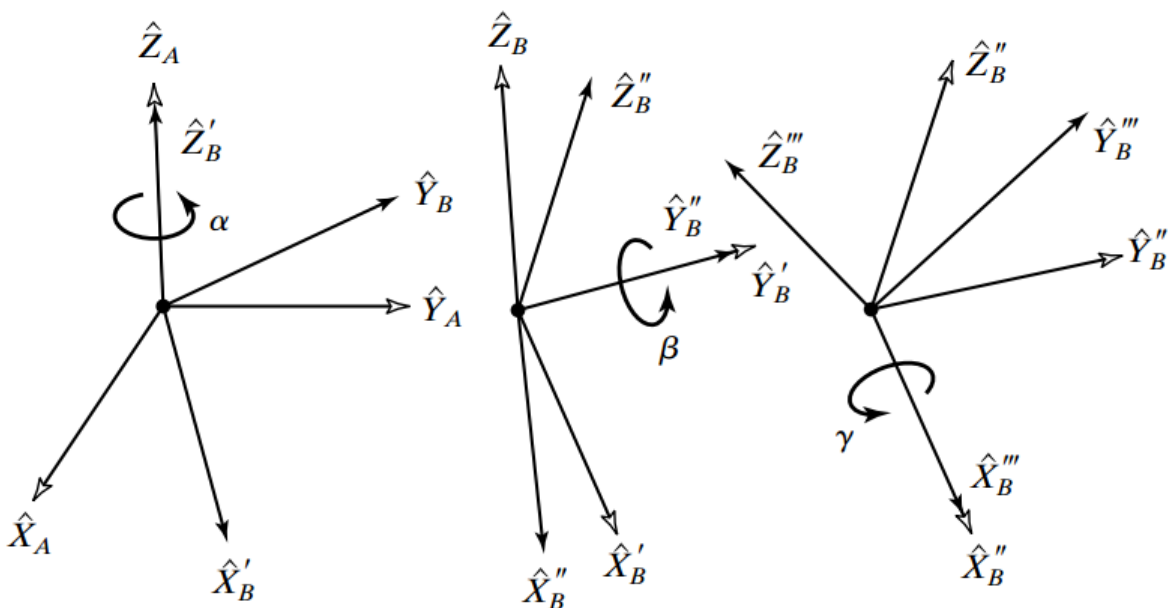
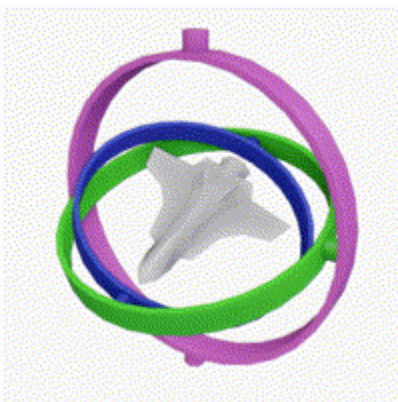


FIGURE 2.18: Z–Y–X Euler angles.

In case of a gimbal lock, it is NOT possible to uniquely determine the euler angles from the rotation matrix.

The gimbal lock leads to a loss in a degree of freedom.

I have elaborated more in the BETA = 90 degree case.

**Q2) Why is  $\beta=90^\circ$  a “certain problematic value”?**

Consider an intrinsic rotation (X->Y->Z).

Then, the rotation matrix will be a multiplication of  $R_x$ ,  $R_y$  and  $R_z$ .

Then,

$$R_x = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta_x & -\sin \theta_x \\ 0 & \sin \theta_x & \cos \theta_x \end{bmatrix} \quad R_y = \begin{bmatrix} \cos \theta_y & 0 & \sin \theta_y \\ 0 & 1 & 0 \\ -\sin \theta_y & 0 & \cos \theta_y \end{bmatrix} \quad R_z = \begin{bmatrix} \cos \theta_z & -\sin \theta_z & 0 \\ \sin \theta_z & \cos \theta_z & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Final rotation matrix will be (in the case when  $\theta_y=90$  degrees):

$$\begin{bmatrix} 0 & 0 & 1 \\ \cos \theta_z \sin \theta_x + \cos \theta_x \sin \theta_z & \cos \theta_x \cos \theta_z - \sin \theta_x \sin \theta_z & 0 \\ -\cos \theta_x \cos \theta_z + \sin \theta_x \sin \theta_z & \cos \theta_z \sin \theta_x + \cos \theta_x \sin \theta_z & 0 \end{bmatrix}$$

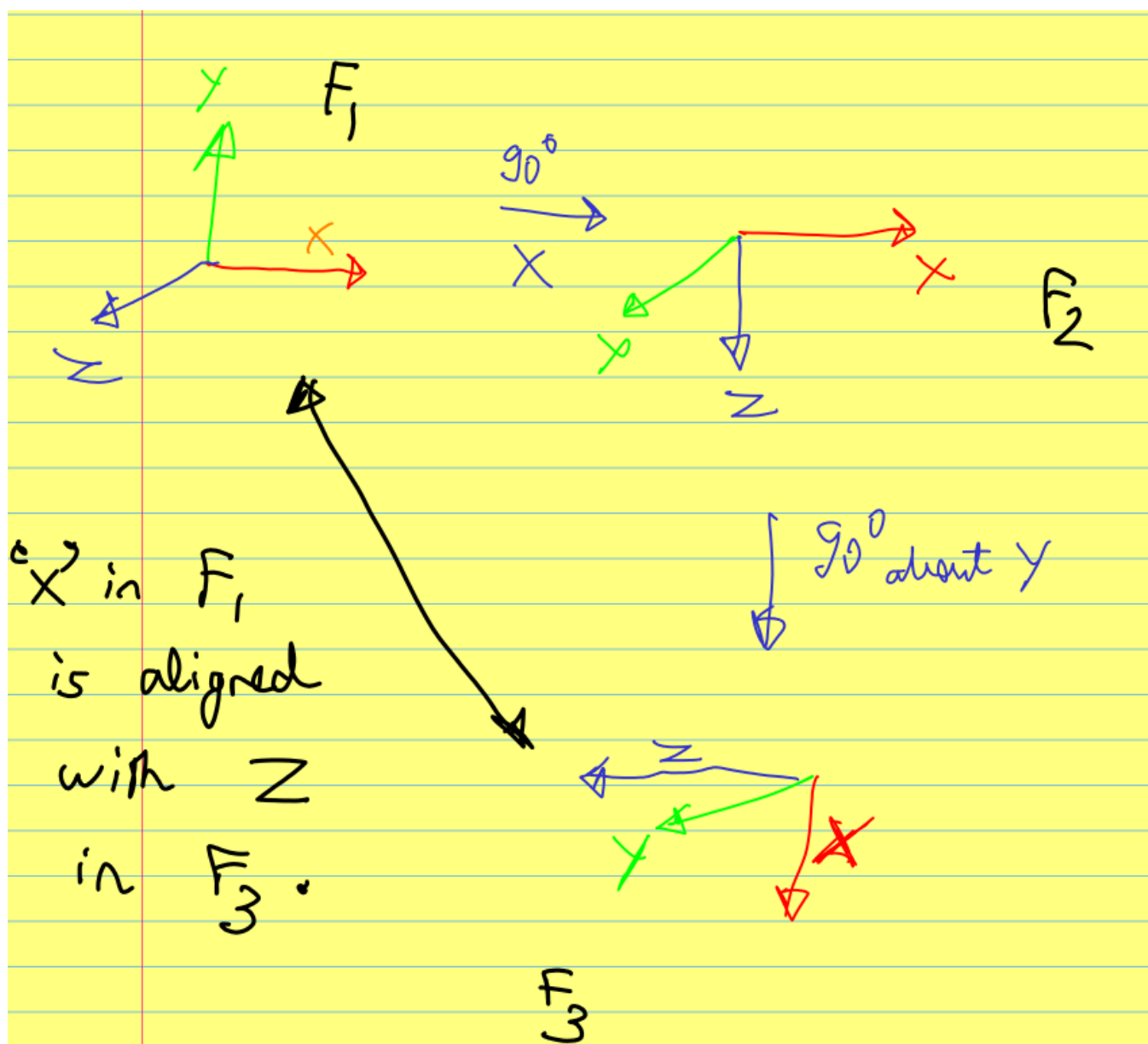
This simplifies to:

$$\begin{bmatrix} 0 & 0 & 1 \\ \sin(\theta_x + \theta_z) & \cos(\theta_x + \theta_z) & 0 \\ -\cos(\theta_x + \theta_z) & \sin(\theta_x + \theta_z) & 0 \end{bmatrix}$$

Here, no matter how we adjust  $\theta_x$  and  $\theta_z$ , we will be able to rotate in one plane only.

So, in addition to the previous rotation about the “y” axis: we have just one more DOF, leading to a total of 2 DOFs.

It is for the same reason, that in this case, the EULER angles cannot be uniquely determined from the rotation matrix. In such a case, one can only determine the value of  $(\theta_x + \theta_z)$  but will not be able to derive the individual values uniquely.



## Q2) Part 2

Let  $R_x, R_y, R_z$  be rotation matrices about  $R_x, R_y, R_z$  respectively.

$$R_x(\theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{bmatrix}$$

$$R_y(\theta) = \begin{bmatrix} \cos\theta & 0 & \sin\theta \\ 0 & 1 & 0 \\ -\sin\theta & 0 & \cos\theta \end{bmatrix}$$

$$R_z(\theta) = \begin{bmatrix} \cos(\theta) & -\sin(\theta) & 0 \\ \sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

P.T.D.

Since rotation convention hasn't been mentioned in the question,

I will present my working with both the conventions:-

1st convention  $\rightarrow$

Convention 1: (ZYX intrinsic)

Let A be the initial frame and B be the frame after rotation.

Then,

$${}^A R_B^{ZYX} = R_Z(\alpha) R_Y(\beta) R_X(\gamma)$$

$$\Rightarrow {}^A R_B^{ZYX} = \begin{bmatrix} C_\alpha C_\beta & C_\alpha S_\beta S_\gamma - S_\alpha C_\gamma & C_\alpha S_\beta C_\gamma + S_\alpha S_\gamma \\ S_\alpha C_\beta & S_\alpha S_\beta S_\gamma + C_\alpha C_\gamma & S_\alpha S_\beta C_\gamma - C_\alpha S_\gamma \\ -S_\beta & C_\beta S_\gamma & C_\beta C_\gamma \end{bmatrix}$$

When  $\beta = 90^\circ$ ,

$$\Rightarrow {}^A R_B^{ZYX} = \begin{bmatrix} 0 & -\sin(\alpha - \gamma) & \cos(\alpha - \gamma) \\ 0 & \cos(\alpha - \gamma) & \sin(\alpha - \gamma) \\ -1 & 0 & 0 \end{bmatrix}$$

Let  $\alpha - \gamma = \theta$

$\uparrow$   $R_{\text{global}}$

$$\Rightarrow {}^A R_B^{ZYX} = \begin{bmatrix} 0 & -\sin\theta & \cos\theta \\ 0 & \cos\theta & \sin\theta \\ -1 & 0 & 0 \end{bmatrix}$$

P.T.O.

Q2)

$$a) \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix} \begin{bmatrix} -\sin(\theta) & \cos(\theta) \\ \cos(\theta) & \sin(\theta) \\ 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \\ 0 \end{bmatrix}$$

$$\Rightarrow \theta = 90^\circ \text{ works}$$

$$\Rightarrow \gamma - \alpha = 90^\circ \text{ works}$$

b) Let  $p_{\text{new}}$  lie on x-y unit circle

$\Rightarrow p_{\text{new}}$  can be parametrized as  $(\cos t, \sin t)$

$$i. \begin{pmatrix} \cos t \\ \sin t \\ 0 \end{pmatrix} = \begin{bmatrix} 0 & -\sin(\theta) & \cos(\theta) \\ 0 & \cos(\theta) & \sin(\theta) \\ -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

$$\Rightarrow \begin{bmatrix} \cos(t) \\ \sin(t) \\ 0 \end{bmatrix} = \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \\ 0 \end{bmatrix}$$

$$\text{Now, } \sin(t) = \cos(\theta)$$

$$\text{and } \cos(t) = -\sin(\theta)$$

$$\Rightarrow \theta = 90^\circ - t$$

$\Rightarrow$  There does exist some  $(\alpha, \gamma)$  for each

point on x-y unit circle such that it

can be mapped to  $\begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}$ .

P.T.O.

$$P = (0, \cos t, \sin t)$$

$$c) \begin{bmatrix} 0 \\ \cos(t) \\ \sin(t) \end{bmatrix} = \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \\ 0 \end{bmatrix}$$

$\Rightarrow$  again a soln exists:  $\theta = 0^\circ$   
works

$\Rightarrow$  when  $t = 0, 180^\circ$

$$\Rightarrow p_{\text{new}} = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix}$$

and  $\boxed{\gamma = \alpha}$

This is because here, when  $\beta = 90^\circ$ ,  
the Z-axis's rotation and the  
'x' axis rotation take place along  
the same real world axis and  
are able to compensate for each other.

P.T.O.

2<sup>nd</sup> convention 2  
 b) Convention 2: XYZ intrinsic

$$\Rightarrow {}^A_R{}^B_{XYZ} = R_x(\alpha) R_y(\beta) R_z(\gamma)$$

(Details in my doc pdf)

When  $\beta = 90^\circ$

$$\Rightarrow {}^A_R{}^B_{XYZ} = \begin{bmatrix} 0 & 0 & 1 \\ \sin(\alpha+\gamma) & \cos(\alpha+\gamma) & 0 \\ -\cos(\alpha+\gamma) & \sin(\alpha+\gamma) & 0 \end{bmatrix}$$

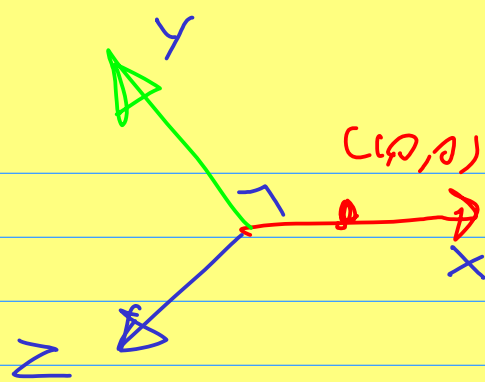
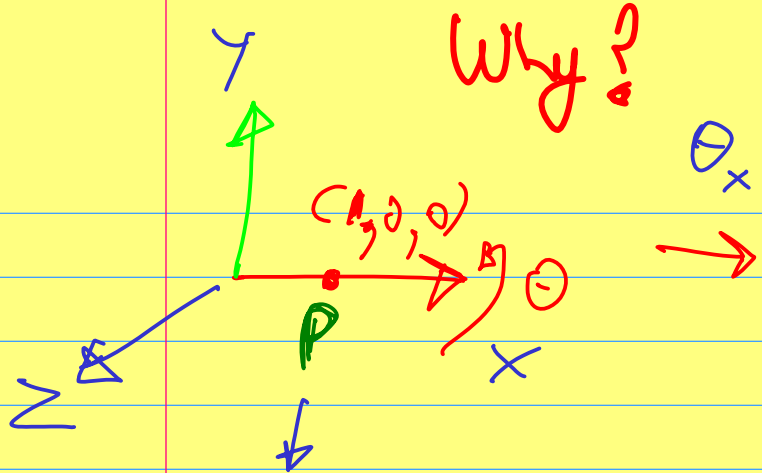
Let  $\Theta = (\alpha + \gamma)$

$$a) \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 \\ \sin(\Theta) & \cos(\Theta) & 0 \\ -\cos(\Theta) & \sin(\Theta) & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}$$

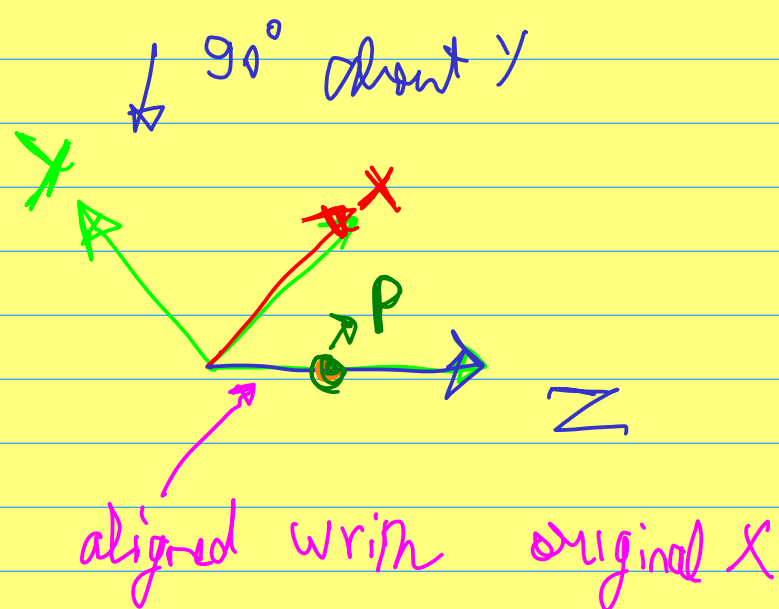
$$\Rightarrow \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ \cos \Theta \\ \sin \Theta \end{bmatrix}$$

$\Rightarrow$  No soln exists.

P.T.O.



Point is fixed  
in space and  
is not  
moving.



'P' lies on the axis around which  
the rotation is happening

→ there is no possible rotation  
about 'z' which can make

→ lie on P.

b) 
$$\begin{bmatrix} \cos t \\ \sin t \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ \cos(\theta) \\ \sin(\theta) \end{bmatrix} \Rightarrow \text{Soln. exists}$$

c) 
$$\begin{bmatrix} 0 \\ \cos(t) \\ \sin(t) \end{bmatrix} = \begin{bmatrix} 0 \\ \cos(\theta) \\ \sin(\theta) \end{bmatrix} \Rightarrow \text{Soln. exists}$$

P.T.O.