

@ Steady State :  $\frac{d[Y]}{dt} = 0$

$$Y^* = \frac{[Y^*]}{Y_T}$$

$$Y_T = Y + Y^*$$

$$\frac{dY^*}{dt} = \frac{V_3[Y]}{K_3 + [Y]} - \frac{V_4[Y^*]}{K_4 + [Y^*]}$$

$$V_3 = \gamma_3[X^*]$$

(1) @ S.S.  $0 = K_{on}[R][L] - K_{off}[R^*]$

$$K_{off}[R^*] = K_{on}[R][L] \Rightarrow K_{off}[R^*] = K_{on}(R_T - [R^*])[L]$$

~~$\cancel{K_{off}[R^*] = K_{on}[R][L]}$~~

$$K_{off}[R^*] = (K_{on} R_T - K_{on}[R^*])[L]$$

$$K_{off}[R^*] + K_{on}[R^*][L] = K_{on} R_T [L]$$

$$[R^*](K_{off} + K_{on}[L]) = K_{on} R_T [L]$$

$$[R^*] = \frac{K_{on} R_T [L]}{(K_{off} + K_{on}[L]) / K_{off}}$$

$$[R^*] = \theta_B R_T$$

↓

$$V_1 = \gamma_1 [R^*]$$

$$[R^*] = \frac{\frac{1}{\gamma_1} R_T}{1 + \frac{K_0}{K_D}} \Rightarrow \frac{R_T}{K_D + 1}$$

(2) @ S.S.  $0 = \frac{V_1[X]}{K_1 + [X]} - \frac{V_2[X^*]}{K_2 + [X^*]}$

$$\frac{V_2[X^*]}{K_2 + [X^*]} = \frac{V_1[X]}{K_1 + [X]} \Rightarrow V_2[X^*](K_1 + [X]) = V_1[X](K_2 + [X^*])$$

$$V_2[X^*](K_1 + [X]) = V_1[X]K_2 + V_1[X][X^*]$$

~~$$\frac{V_2[X^*](K_1 + [X])}{V_1[X]} - \frac{V_1[X]}{V_1[X]} = \frac{V_1[X][X^*]}{V_1[X]}$$~~

$$V_1 = \gamma_1 \theta_B * R_T$$

$$v_2[x^*](k_1 + [x]) = v_1[x]k_2 + v_1[x][x^*]$$

$$v_2[x^*]k_1 + v_2[x^*]x = v_1[x]k_2 + v_1[x][x^*]$$

$$v_2[x^*]k_1 - v_1[x]k_2 = [x][x^*](v_1 - v_2)$$

$$v_2[x^*]k_1 - v_1k_2x_T + v_1k_2[x^*] = x_T[x^*](v_1 - v_2) - [x^*]^2(v_1 - v_2)$$

$$[x^*]^2(v_1 - v_2) + [x^*](v_1k_2 - x_T(v_1 - v_2)) - v_1k_2x_T = 0$$

~~$$= (v_1k_2 - x_T(v_1 - v_2)) \pm \sqrt{(v_1k_2 - x_T(v_1 - v_2))^2 - 4(v_1 - v_2)(v_1k_2x_T)}$$~~

~~$$[x^*]_{\text{real}} = -v_1k_2 + x_T(v_1 - v_2) \mp \frac{(v_1k_2)^2 - 2v_1k_2x_T(v_1 - v_2) + x_T^2(v_1 - v_2)^2}{2(v_1 - v_2)} - 4(v_1 - v_2)v_1k_2x_T$$~~

$$[x^*]_{\text{real}}(v_1 - v_2) + x^*(v_1k_2 - x_T(v_1 - v_2)) - v_1v_2 = 0$$

$$x^* \left( \frac{1}{v_2} x_T \right) + x^* (v_1 k_2 - x_T(v_1 - v_2)) - v_1 v_2 = 0$$

(3)  
@ S.S.

$$0 = \frac{V_3[Y]}{K_3 + [Y]} - \frac{V_4[Y^*]}{K_4 + [Y^*]}$$

\* similar process as (2) @ S.S. . .

$$[Y^*]^2(V_3 - V_4) + [Y^*](V_3 K_4 - Y_T(V_3 - V_4)) - V_3 K_4 Y_T = 0$$

$$[Y^*] Y^*(V_3 - V_4) + Y^*(V_3 K_4 - Y_T(V_3 - V_4)) - V_3 K_4 = 0$$

$$[Y^*] Y^*(V_3 - V_4) + Y^* V_3 K_4 - Y^* Y_T(V_3 - V_4) - V_3 K_4 = 0$$

$$Y^*(V_3 - V_4) + Y^* V_3 K_4 - Y^*(V_3 - V_4) - V_3 K_4 = 0$$

$$Y^{*2} V_3 - Y^{*2} V_4 + Y^{*2} V_3 K_4 - Y^* V_3 + Y^* V_4 - V_3 K_4 = 0$$

$$Y^{*2} V_3 V_4 - Y^{*2} + Y^{*2} V_3 V_4 K_4 - Y^* V_3 V_4 + Y^* - V_3 V_4 K_4 = 0$$

$$Y^{*2}(V_3 V_4 - 1) + Y^*(V_3 V_4 K_4 - V_3 V_4 + 1) - V_3 V_4 K_4 = 0$$

~~Wrote down~~

$$Y^{*2}[(Y_3 X^*/V_4)^* X_T - 1] + Y^*[K_3 + (Y_3 X^*/V_4) X_T K_4 - (Y_3 X^*/V_4) X_T^*]$$

$$- (Y_3 X^*/V_4) X_T K_4 = 0$$

$$X^{*2}[(Y_1 \theta_B/V_2) R_T - 1] + X^*[K_1 + (Y_1 \theta_B/V_2) R_T K_2 - (Y_1 \theta_B/V_2) R_T^*]$$

$$- (Y_1 \theta_B/V_2) R_T K_2 = 0$$

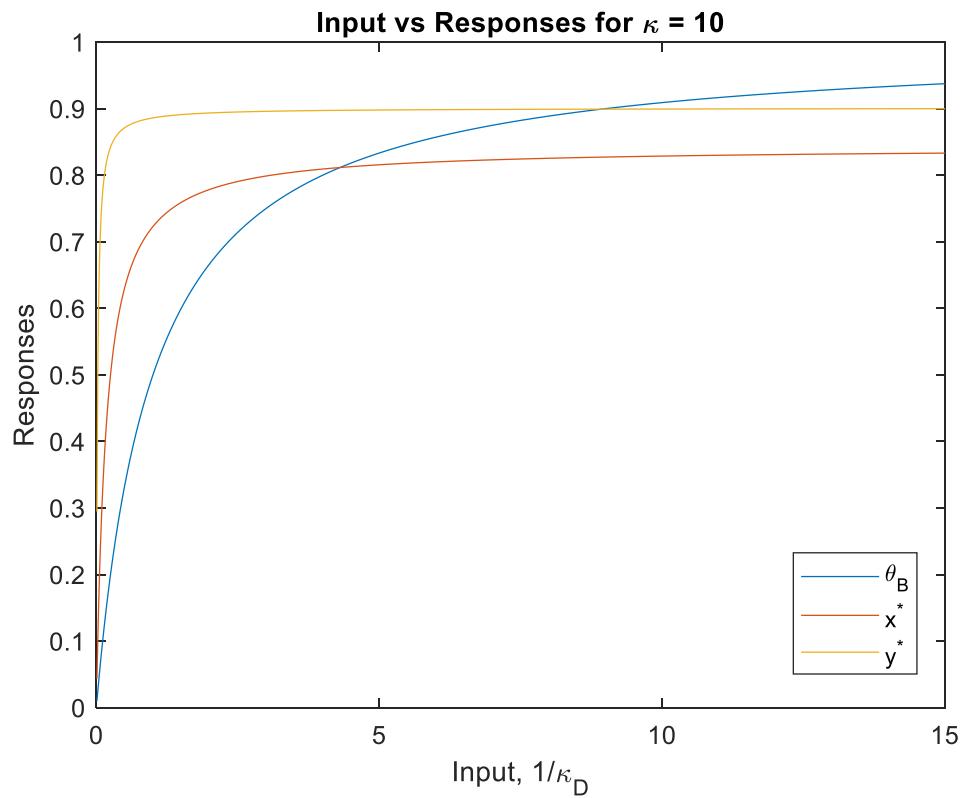
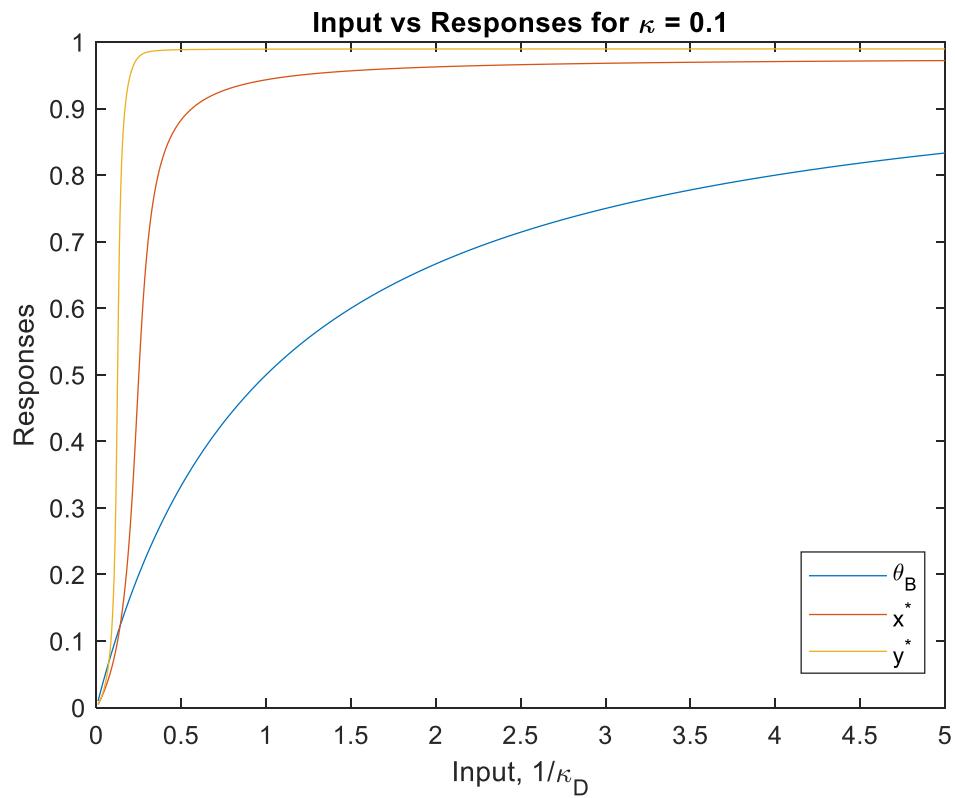
$$\theta_B = \frac{1}{K_0 + 1} \quad \text{-OR-} \quad \theta_B = \frac{K_0}{1 + K_0}$$

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\*Everything not done on lined paper was done with MATLAB code

1. A) \*on lined paper

B)



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C)  $\kappa = 0.1$   $\Theta_B$  Hill coefficient:  $n = 1$ , (other parameter in eq:  $c = 1$ )

X\* Hill coefficient:  $n = 3.053$ , (other parameter in eq:  $c = 0.251$ )

Y\* Hill coefficient:  $n = 7.315$ , (other parameter in eq:  $c = 0.124$ )

$\kappa = 10$   $\Theta_B$  Hill coefficient:  $n = 1$ , (other parameter in eq:  $c = 1$ )

X\* Hill coefficient:  $n = 0.642$ , (other parameter in eq:  $c = 0.260$ )

Y\* Hill coefficient:  $n = 0.608$ , (other parameter in eq:  $c = .0202$ )

D)  $\kappa = 0.1$   $\Theta_B$  % change:  $43.478\%$

X\* % change:  $101.826\%$

Y\* % change:  $402.580\%$

$\kappa = 10$   $\Theta_B$  % change:  $43.478\%$

X\* % change:  $27.966\%$

Y\* % change:  $5.6566\%$

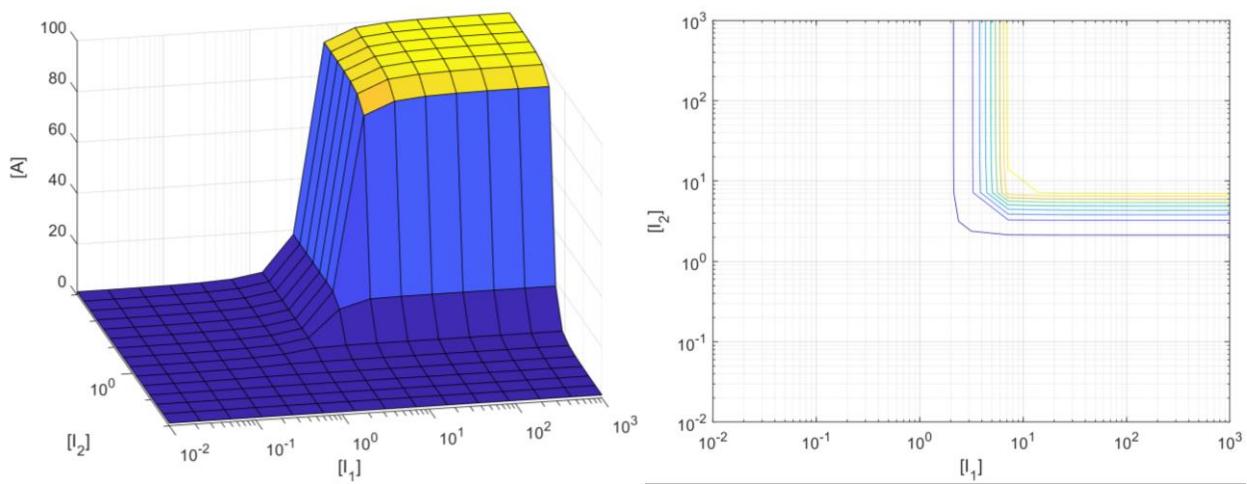
E) \*on lined paper

2. A)  $[A] = 1.1097$

$[B] = 49.4451$

$[C] = 49.4451$

B)

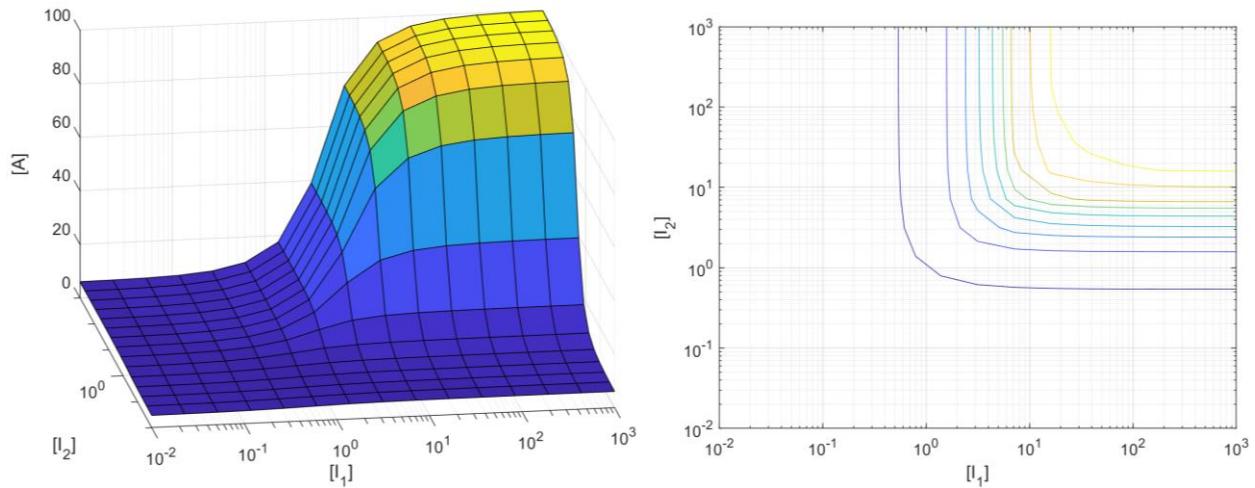


C) AND Logic Gate

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\*Everything not done on lined paper was done with MATLAB code

D)



This might be referred to as a “fuzzy” operator since the  $[A]$  values are not as close to 0 as they were when  $K_{si}$  values were 5 units. Plus, as the concentrations of the inhibitors reached higher values, the switch-like response with the AND logic operation was less defined when  $K_{si}$  values were 35 units.

E) \*on lined paper

1. e) Parameter tuning is important because parameter tuning allows for dimensionality reduction, meaning that random variables are reduced to obtain a set of principal variables. For example, parameter tuning was important to help obtain the Hill coefficients that fit the  $\beta_3$ ,  $x^*$ ,  $\xi$ ,  $y^*$  plots. In order to fit properly with the Hill equation, parameter tuning was needed. Then, zero-order ultrasensitivity is important because it is a great representation of signal responses that are operating close to saturation and are very sensitive to subtle changes for the input. The Hill equation curve fits ~~with~~ when  $n > 1$  would be ultrasensitive. These two components (parameter tuning & zero-order ultrasensitivity) allow for accurate amplification of input signals since random variables that might be magnified will be reduced with parameter tuning, and any important change in the input signal will be amplified into a large change in output with zero-order ultrasensitivity. The same circuit can amplify signals based on parameter values by changing the input protein concentrations or manipulating reaction rates via the environment (changing temperature, pH, etc.)

2.e) Zero-order ultrasensitivity is important in the operation of the gate since such sensitivity provides a switch-like response that can be easily represented with logic gates like "AND" or "OR." As discussed in Goldbeter & Koshland (1981), sigmoidal, ultrasensitive responses are commonplace in cell signaling, and with zero-order (or close to saturation), the response shows both a threshold and an abrupt leveling off at maximal response, resulting in a steeply sigmoidal input-output relationship.