

$$\underline{\tilde{S}} = 2 \frac{\partial \Psi(\underline{C})}{\partial \underline{C}} = 2 \left[\left(\frac{\partial \Psi}{\partial I_1} + I_1 \frac{\partial \Psi}{\partial I_2} \right) \underline{I} - \frac{\partial \Psi}{\partial I_2} \underline{C} + I_3 \frac{\partial \Psi}{\partial I_3} \underline{C}^{-1} \right]$$

————— (13)

where Ψ - strain energy function.

$$\underline{\tilde{\sigma}} = \underline{J}^{-1} \underline{F} \underline{\tilde{S}} \underline{F}^T \quad \text{————— (14)}$$

using (13) & (14)

$$\begin{aligned} \underline{\tilde{\sigma}} &= 2 \left[\left(\frac{\partial \Psi}{\partial I_1} + I_1 \frac{\partial \Psi}{\partial I_2} \right) \underline{F} \underline{I} \underline{F}^T - \frac{\partial \Psi}{\partial I_2} \underline{F} \underline{C} \underline{F}^T + I_3 \frac{\partial \Psi}{\partial I_3} \underline{F} \underline{C}^{-1} \underline{F}^T \right] \underline{J}^{-1} \\ &= 2 \left[\left(\frac{\partial \Psi}{\partial I_1} + I_1 \frac{\partial \Psi}{\partial I_2} \right) \underline{b} - \frac{\partial \Psi}{\partial I_2} \underline{F} (\underline{F}^T \underline{F}) \underline{F}^T + I_3 \frac{\partial \Psi}{\partial I_3} \underline{F} (\underline{F}^{-1} \underline{F}^{-T}) \underline{F}^T \right] \underline{J}^{-1} \\ \underline{\tilde{\sigma}} &= 2 \left[\left(\frac{\partial \Psi}{\partial I_1} + I_1 \frac{\partial \Psi}{\partial I_2} \right) \underline{b} - \frac{\partial \Psi}{\partial I_2} \underline{b}^2 + I_3 \frac{\partial \Psi}{\partial I_3} \underline{I} \right] \underline{J}^{-1} \quad \text{————— (15)} \end{aligned}$$

\therefore ~~$\underline{\tilde{\sigma}} = 2 \underline{J}^{-1} \left[\left(\frac{\partial \Psi}{\partial I_1} + I_1 \frac{\partial \Psi}{\partial I_2} \right) \underline{I} - \frac{\partial \Psi}{\partial I_2} \underline{C} + I_3 \frac{\partial \Psi}{\partial I_3} \underline{C}^{-1} \right]$~~ Another form.

$$\underline{\tilde{\sigma}} = 2 \underline{J}^{-1} \left[\left(I_2 \frac{\partial \Psi}{\partial I_2} + I_3 \frac{\partial \Psi}{\partial I_3} \right) \underline{I} + \frac{\partial \Psi}{\partial I_1} \underline{b} - I_3 \frac{\partial \Psi}{\partial I_2} \underline{b}^T \right] \quad \text{————— (15a)}$$

(15) is okay but having a form

$$\underline{\tilde{\sigma}} = 2 \frac{\partial \Psi(\underline{b})}{\partial \underline{b}} \underline{b} \underline{J}^{-1} \quad \text{————— (16)}$$

We know that $\underline{b} = \underline{b}^{1/2}$. Using this relation we can write an alternate relation for $\underline{\sigma}$ as

$$\underline{\sigma} = \underline{J}^{-1} \frac{\partial \Psi(\underline{v})}{\partial \underline{v}} \underline{v} \quad \text{————— (17)}$$

Constitutive eq. in terms of principal stretches

$$\underline{\Psi} = \Psi(\underline{C}) = \Psi(\lambda_1, \lambda_2, \lambda_3)$$

For a Stress free configuration,

$$\Psi = \Psi(1, 1, 1) = 0$$

Thus, using a form of Ψ in terms of λ_α ($\alpha=1, 2, 3$) we can write alternate equations for stress. For this purpose we use - μ form (17) to write

$$\boxed{\underline{\sigma}_\alpha = J^{-1} \lambda_\alpha \frac{\partial \Psi}{\partial \lambda_\alpha}} \quad \{\alpha=1, 2, 3\} \quad \text{--- (18)}$$

$$\text{with } J = \lambda_1 \lambda_2 \lambda_3 \quad \text{--- (19)}$$

Other forms are

$$\boxed{\underline{p} = \frac{\partial \Psi}{\partial \lambda_\alpha} \quad , \quad \underline{s} = \frac{1}{\lambda_\alpha} \frac{\partial \Psi}{\partial \lambda_\alpha}} \quad \{\alpha=1, 2, 3\} \quad \text{--- (20)}$$

Incompressible Hyperelastic Materials

- Several polymeric materials can go under finite deformations without noticeable change in the volume.
- Such materials are treated as incompressible materials and for them only isochoric motions are possible.
- Thus for incompressible materials we have

$$\boxed{J=1} \quad \text{---} \quad (21)$$

- Incompressibility introduces a new constraint.

Recall the expression for internal dissipation

$$D_{int} = P : \dot{\underline{\underline{F}}} - \dot{\Psi} = \theta \left(P - \frac{\partial \Psi}{\partial \underline{\underline{F}}} \right) : \dot{\underline{\underline{F}}} = 0 \quad \text{---} \quad (22)$$

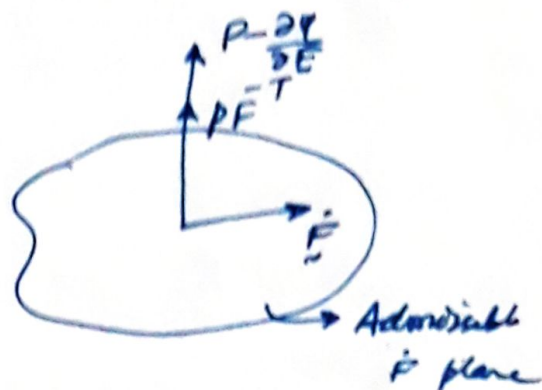
- For hyperelastic materials we derived an expression for stress by using the argument that $\underline{\underline{F}}$ and $\dot{\underline{\underline{F}}}$ are independent and hence $\dot{\underline{\underline{F}}}$ is arbitrary.
- However when ~~is~~ incompressibility enters then we have

$$J=1$$
$$\therefore \dot{J}=0 = \dot{\underline{\underline{F}}}^{-T} : \dot{\underline{\underline{F}}}, \quad \text{---} \quad (23)$$

which suggest that $\underline{\underline{F}}$ and $\dot{\underline{\underline{F}}}$ are now not independent. Hence, the argument given earlier ~~to~~ ~~that~~ is not valid now.

Hence, (22) & (23) combined gives us the condition that

$$\left(p - \frac{\partial \Psi}{\partial F} \right) = -p \bar{F}^{-T}$$



Hence,

$$\boxed{p = \frac{\partial \Psi}{\partial F} - p \bar{F}^{-T}} \quad \left\{ p \text{ is a scalar constant} \right\} \quad (24)$$

Other definitions of stress can be derived using (24) as

$$\boxed{\underline{S} = 2 \frac{\partial \Psi(\underline{C})}{\partial \underline{C}} - p \underline{C}^{-1} \underline{I}} \quad (25) \quad \left\{ \begin{array}{l} J=1 \\ \text{isotropic} \end{array} \right.$$

$$\boxed{\underline{T} = \underline{F} \left(\frac{\partial \Psi(\underline{F})}{\partial \underline{F}} \right)^T - p \underline{I}} \quad (26)$$

From (26), we can identify that the term involving the constant p is the hydrostatic part of the stress, hence p is nothing but the pressure term.

Hence, the other part is the deviatoric part of the stress

$$\therefore \boxed{\begin{aligned} \underline{S}' &= 2 \frac{\partial \Psi(\underline{C})}{\partial \underline{C}} \quad \text{or} \quad \underline{\sigma}' = \underline{F} \left[\frac{\partial \Psi(\underline{F})}{\partial \underline{F}} \right]^T \\ &\text{or} \quad p' = \frac{\partial \Psi}{\partial F} \end{aligned}} \quad (27)$$

* Constant p is determined from boundary conditions in a given problem.

Considering above constraints, we can write a suitable form of strain energy function ψ as

$$\psi = \psi[I_1(\underline{c}), I_2(\underline{c})] - \frac{1}{2}p(I_3 - 1)$$
$$\psi = \psi[I_1(\underline{b}), I_2(\underline{b})] - \frac{1}{2}p(I_3 - 1)$$

Some forms of strain-energy function

Ogden model for rubber-like materials :-

$$\psi = \psi(\lambda_1, \lambda_2, \lambda_3) = \sum_{i=1}^N \frac{\mu_i}{\alpha_i} (\lambda_1^{\alpha_i} + \lambda_2^{\alpha_i} + \lambda_3^{\alpha_i} - 3)$$

Mooney Rivlin model $\{ N=2, \alpha_1=2, \alpha_2=-2 \}$

$$\psi = C_1 (\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3) + C_2 (\lambda_1^{-2} + \lambda_2^{-2} + \lambda_3^{-2} - 3)$$

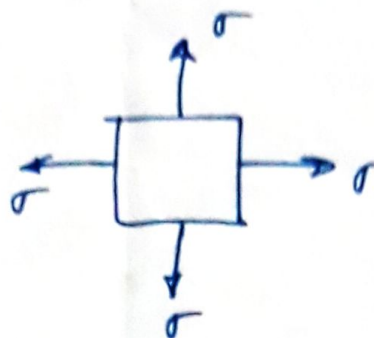
$$\psi = C_1 (I_1 - 3) + C_2 (I_2 - 3)$$

Neo-hookean model $\{ N=1, \alpha_1=2 \}$

$$\psi = C_1 (\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3) = C_1 (I_1 - 3)$$

and several others - - -

Example - Inflation of a spherical balloon



$$\sigma_1 = \sigma_2 = \sigma$$

$$\sigma_3 = 0$$

{ plane stress }

Let us derive expression of stresses for Ogden model

$$\Psi = \sum_{i=1}^N \frac{\mu_i}{\lambda_i} \left(\frac{\lambda_i}{\lambda_1} + \frac{\lambda_i}{\lambda_2} + \frac{\lambda_i}{\lambda_3} - 3 \right) + \frac{p}{2} (I_3 - 1)$$

We start with the form (159),

$$\underline{\underline{\sigma}} = 2 \underline{\underline{J}}^{-1} \left[\left(I_2 \frac{\partial \Psi}{\partial I_2} + I_3 \frac{\partial \Psi}{\partial I_3} \right) \underline{\underline{I}} + \frac{\partial \Psi}{\partial I_1} \underline{\underline{b}} + I_3 \frac{\partial \Psi}{\partial I_2} \underline{\underline{b}}^{-1} \right]$$

~~At / isochoric / isochoric~~

$$\frac{\partial \Psi}{\partial I_3} = -\frac{p}{2}, \quad I_3 = 1 \quad \& \quad J = 1$$

$$\therefore \underline{\underline{\sigma}} = 2 \underline{\underline{J}}^{-1} \left[\left(I_2 \frac{\partial \Psi}{\partial I_2} - \frac{p}{2} \right) \underline{\underline{I}} + \frac{\partial \Psi}{\partial I_1} \underline{\underline{b}} - \frac{\partial \Psi}{\partial I_2} \underline{\underline{b}}^{-1} \right]$$

$$= \cancel{2 \underline{\underline{J}}^{-1}} - p \underline{\underline{I}} + 2 \frac{\partial \Psi}{\partial I_1} \underline{\underline{b}} + 2 I_2 \frac{\partial \Psi}{\partial I_2} \underline{\underline{I}} - 2 \frac{\partial \Psi}{\partial I_2} \underline{\underline{b}}^{-1}$$

$$\therefore \underline{\underline{\sigma}} = \underbrace{\left\{ 2 I_2 \frac{\partial \Psi}{\partial I_2} - p \right\}}_{-p'} \underline{\underline{I}} + 2 \frac{\partial \Psi}{\partial I_1} \underline{\underline{b}} - 2 \frac{\partial \Psi}{\partial I_2} \underline{\underline{b}}^{-1}$$

$$\therefore \boxed{\underline{\underline{\sigma}} = -p' \underline{\underline{I}} + 2 \frac{\partial \Psi}{\partial I_1} \underline{\underline{b}} - 2 \frac{\partial \Psi}{\partial I_2} \underline{\underline{b}}^{-1}}$$

It can be shown using chain rule of differentiation that in terms of $\lambda_1, \lambda_2, \lambda_3$ above relation can be written as

$$\sigma_a = -p + \lambda_a \frac{\partial \Psi}{\partial \lambda_a}$$

Now, using this equation with Ogden energy function we get

$$\sigma_a = -p + \sum_{i=1}^N \mu_i \lambda_a^{\alpha_i} \quad \{a=1, 2, 3\}$$

as discussed constant p will be determined from B.C. In this case we have $\sigma_3 = 0$.

$$\therefore \sigma_3 = 0 = -p + \sum_{i=1}^N \mu_i \lambda_3^{\alpha_i}$$

$$\therefore p = \sum_{i=1}^N \mu_i \lambda_3^{\alpha_i}$$

\therefore we get

$$\sigma_1 = \sum_{i=1}^N \mu_i \left[\lambda_1^{\alpha_i} - (\lambda_1 \lambda_2)^{-\alpha_i} \right]$$

$$\sigma_2 = \sum_{i=1}^N \mu_i \left[\lambda_2^{\alpha_i} - (\lambda_1 \lambda_2)^{-\alpha_i} \right]$$

for our case $\lambda_1 = \lambda_2 = \lambda$, hence

$$\sigma_1 = \sigma_2 = \sigma = \sum_{i=1}^N \left(\lambda^{\alpha_i} - \lambda^{-2\alpha_i} \right)$$