# **Solar Cruiser Total Ionizing Dose**

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## 1 Executive Summary

### 2 Mission Trajectory

The nominal Solar Cruiser location is beyond the Sun-Earth L1 point, called sub-L1, roughly 0.984 AU from the Sun. The sub-L1 location is in interplanetary space with no shielding from any planetary bodies and is exposed to the solar wind. The nominal mission length is 2 years.

#### 3 Materials

The representative material for the Reaction Control Device (RCD) of Solar Cruiser is  $150\mu\text{m}$  of Kapton. Using data from NIST<sup>1</sup>, the composition of Kapton is shown in Table 1, where the density of Kapton is 1.42 g/cm<sup>3</sup>.

Fraction by Weight Atomic # Weight (amu) Fraction by Number Stoichiometry 0.026362 1.008 0.25639 10 6 0.691133 12.011 0.56412 22 7 0.073270 2 14.007 0.05128 8 0.209235 15.999 0.12821 5

Table 1: Composition of Kapton.

### 4 Dose-Depth in Kapton

The SRIM (Stopping and Range of Ions in Solids) software is used to compute the dose in thin materials with no prior shielding. The SRIM software package contains TRIM (the Transport of Ions in Matter), with a screenshot of the setup used in this analysis shown in Figure 1.

The dose deposited in Kapton depends on the energy of the incident protons. As the energy increases, the depth of the deposited dose increases. In Figure 2, the colored solid curves show the percentiles of dose deposited less than a particular depth, as a function of energy for normally incident protons. For example, the purple curve shows the depth vs. energy at which 95% of the dose is deposited. From Figure 2, it is clear that the dose is not deposited uniformly. Thicknesses between the green and blue curves, 45% of the dose is deposited, as well as between the green and purple curves. Therefore, 90% of the dose is deposited between the blue and purple curves. In general, the depth vs. energy profile has a double-power-law shape

$$D(E) = \left(\frac{E}{a}\right)^b + \left(\frac{E}{c}\right)^d,\tag{1}$$

where a is the low-energy scale, c is the high-energy scale, and b & d are the indices for each scale, respectively. As the percentile increases, the values for the energy

<sup>1</sup>https://physics.nist.gov/cgi-bin/Star/compos.pl?matno=179

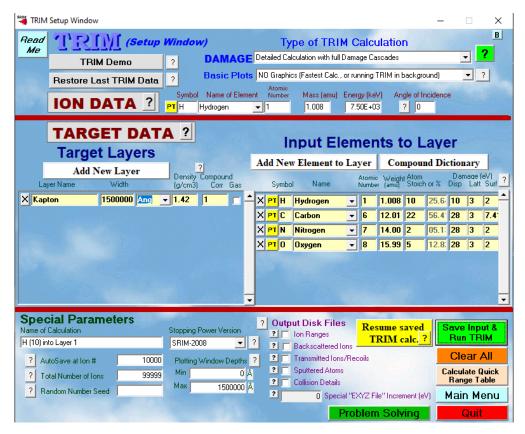


Figure 1: Example of TRIM setup.

scales a and c decreases. For a list of parameter fits, see Table 4 in Appendix A. Observing that b < d, the Kapton material is more effective at stopping lower energy protons ( $<\sim 100~{\rm keV}$ ) than higher energy protons.

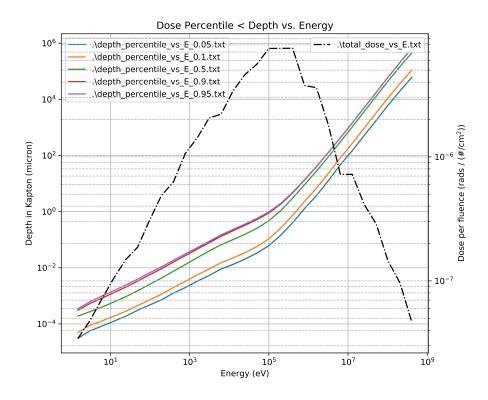


Figure 2: Left axis: Depth in Kapton vs. energy for various dose-depth percentiles. Right axis: Dose per fluence vs. energy.

The dotted-dashed curve in Figure 2 shows the total dose deposited per fluence as a function of energy. Basically, this curve can be thought of as the dose cross-section of Kapton for normally incident protons. One way to find the total dose for a given energy spectrum, one could convolute the dose cross-section with the differential energy spectrum, taking into account the depth percentile for a particular thickness of Kapton material. However, a more direct method to find the total dose is used in the following sections.

#### 5 Natural Environment

The natural environments for the RCD of Solar Cruiser are separated into a midenergy component (solar energetic particles, Section 5.1) and a low-energy component (background solar wind, Section 5.2). The high-energy component (galactic cosmic rays, > GeV) are omitted because of the thin materials studied in this analysis. In general, for an isotropic proton environment with energies greater than  $\sim 6.5$  MeV (see Equation (1)), the particles do not deposit a significant amount of energy in  $150\mu m$  Kapton (i.e., the Bragg peak has not been reached yet).

#### 5.1 Solar Particle Events

The solar particle event (SPE) environment for interplanetary space is derived following the same procedure as outlined in the Cross-Program Design Specification for Natural Environments (DSNE) Section 3.3.1 (see the technical notes at the end of the section). A 2-year trajectory is defined in interplanetary space at the sub-L1 location of 0.984 AU in SPENVIS² under the Coordinate generators tab. Once this is set, the SPE fluence is computed under the Solar particle mission fluences. The following parameters are set:

• Solar particle model: ESP-PSYCHIC (worst event fluence)

· Ion range: H to H

Prediction period: override

• Prediction period [years]: 2.0

· Offset in solar cycle: override

· Offset from solar maximum [years]: 0

• Confidence level [%]: 95.0

Table 2 shows the down-selected energy bins that match DSNE Table 3.3.1.10.2-1. In terms of fluence >100 keV, the 2-year SPE environment shown in Table 2 is only 6% greater than the unshielded SPE environment is DSNE Table 3.3.1.10.2-1, despite the fluence duration doubling. This is why it is important to run the ESP-PSYCHIC model for the required mission length and not multiply Table 3.3.1.10.2-1 by the number of years. Otherwise, a large overestimate occurs.

<sup>&</sup>lt;sup>2</sup>https://www.spenvis.oma.be/

Table 2: ESP-PSYCHIC worst event fluence of protons for 2 years during solar maximum at 0.984 AU. The energy center =  $\sqrt{\text{bin left edge} \times \text{bin right edge}}$ .

Energy Center (keV)	Bin Flux (#/cm <sup>2</sup> )	Bin Width (keV)	Bin Left Edge (keV)
1.58E+02	2.08E+11	1.50E+02	1.00E+02
3.54E+02	1.00E+11	2.50E+02	2.50E+02
7.07E+02	6.83E+10	5.00E+02	5.00E+02
1.41E+03	4.65E+10	1.00E+03	1.00E+03
2.65E+03	2.74E+10	1.50E+03	2.00E+03
4.18E+03	1.46E+10	1.50E+03	3.50E+03
5.96E+03	1.51E+10	2.10E+03	5.00E+03
7.54E+03	4.83E+09	9.00E+02	7.10E+03
8.49E+03	4.23E+09	1.00E+03	8.00E+03
9.49E+03	3.38E+09	1.00E+03	9.00E+03
1.26E+04	1.07E+10	6.00E+03	1.00E+04
1.70E+04	1.88E+09	2.00E+03	1.60E+04
1.90E+04	1.52E+09	2.00E+03	1.80E+04
2.24E+04	3.50E+09	5.00E+03	2.00E+04
2.96E+04	3.77E+09	1.00E+04	2.50E+04
3.74E+04	1.83E+09	5.00E+03	3.50E+04
4.24E+04	1.02E+09	5.00E+03	4.00E+04
4.74E+04	1.15E+09	5.00E+03	4.50E+04
5.96E+04	2.35E+09	2.10E+04	5.00E+04
7.54E+04	5.35E+08	9.00E+03	7.10E+04
8.49E+04	4.18E+08	1.00E+04	8.00E+04
9.49E+04	2.59E+08	1.00E+04	9.00E+04
1.26E+05	6.29E+08	6.00E+04	1.00E+05
1.70E+05	7.92E+07	2.00E+04	1.60E+05
1.90E+05	5.44E+07	2.00E+04	1.80E+05
2.24E+05	7.92E+07	5.00E+04	2.00E+05
3.16E+05	7.33E+07	1.50E+05	2.50E+05
4.47E+05	1.27E+07	1.00E+05	4.00E+05

#### 5.2 Low-Energy Solar Wind

To compute the low-energy solar wind plasma contribution of the environment (assumed at 1 AU), the L2-CPE V1.3 software package was used. The proton fluence was computed with the setup shown in Figure 3. Other percentiles that are automatically calculated are 5%, 50%, 95%, and the maximum, mean, and minimum fluxes for each energy bin (see Listing 1 in Appendix B). Table 3 shows the reduced data in the same format as Table 2. The 95% is used in accordance with DSNE (see the technical notes at the end of Section 3.3.1). The sunward facing flux is used and assumed isotropically as worst-case.

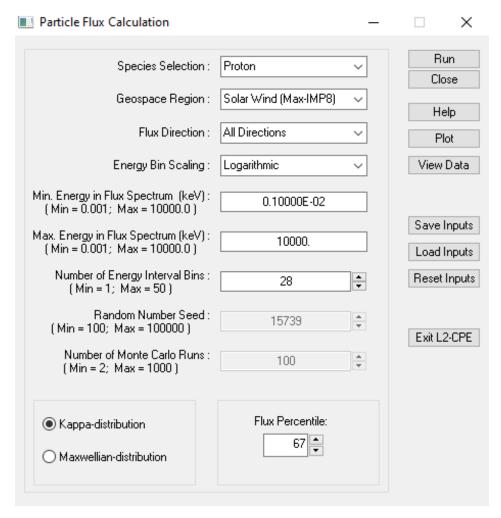


Figure 3: Screen shot of the setup used in computing the low-energy proton flux environment in L2-CPE.

Table 3: The 95% sunward solar wind environment from L2-CPE for 2 years.

Energy Center (keV)	Bin Flux (#/cm <sup>2</sup> )	Bin Width (keV)	Bin Left Edge (keV)
1.34E-03	4.97E+09	8.00E-04	1.00E-03
2.40E-03	8.36E+09	1.40E-03	1.80E-03
4.23E-03	1.38E+10	2.40E-03	3.20E-03
7.48E-03	2.24E+10	4.40E-03	5.60E-03
1.33E-02	3.50E+10	7.80E-03	1.00E-02
2.37E-02	5.29E+10	1.38E-02	1.78E-02
4.21E-02	7.66E+10	2.46E-02	3.16E-02
7.50E-02	1.05E+11	4.38E-02	5.62E-02
1.33E-01	1.37E+11	7.78E-02	1.00E-01
2.37E-01	1.64E+11	1.38E-01	1.78E-01
4.22E-01	1.86E+11	2.46E-01	3.16E-01
7.50E-01	1.94E+11	4.38E-01	5.62E-01
1.33E+00	1.88E+11	7.78E-01	1.00E+00
2.37E+00	1.68E+11	1.38E+00	1.78E+00
4.22E+00	1.40E+11	2.46E+00	3.16E+00
7.50E+00	1.10E+11	4.38E+00	5.62E+00
1.33E+01	8.21E+10	7.78E+00	1.00E+01
2.37E+01	5.75E+10	1.38E+01	1.78E+01
4.22E+01	3.91E+10	2.46E+01	3.16E+01
7.50E+01	2.56E+10	4.38E+01	5.62E+01
1.33E+02	1.65E+10	7.78E+01	1.00E+02
2.37E+02	1.04E+10	1.38E+02	1.78E+02
4.22E+02	6.43E+09	2.46E+02	3.16E+02
7.50E+02	3.91E+09	4.38E+02	5.62E+02
1.33E+03	2.35E+09	7.78E+02	1.00E+03
2.37E+03	1.43E+09	1.38E+03	1.78E+03
4.22E+03	8.50E+08	2.46E+03	3.16E+03
7.50E+03	5.05E+08	4.38E+03	5.62E+03

### Total lonizing Dose

- 6.1 Solar Particle Events
- 6.2 Low-Energy Solar Wind

### **Results**

### Dose Percentile-Depth vs. Energy Parameters Fits

Table 4: Parameter fits to Equation (1) for various dose percentiles using normally incident protons.

Percentile/100	a	b	c	d
0.05	8.445E+00	6.539E-01	4.543E+03	1.785E+00
0.10	4.414E+00	6.654E-01	3.267E+03	1.786E+00
0.15	2.923E+00	6.729E-01	2.682E+03	1.787E+00
0.20	2.171E+00	6.793E-01	2.339E+03	1.788E+00
0.25	1.723E+00	6.845E-01	2.109E+03	1.789E+00
0.30	1.429E+00	6.894E-01	1.947E+03	1.790E+00
0.35	1.216E+00	6.937E-01	1.826E+03	1.792E+00
0.40	1.057E+00	6.976E-01	1.732E+03	1.793E+00
0.45	9.332E-01	7.013E-01	1.658E+03	1.794E+00
0.50	8.296E-01	7.043E-01	1.598E+03	1.795E+00
0.55	7.407E-01	7.067E-01	1.549E+03	1.796E+00
0.60	6.660E-01	7.089E-01	1.510E+03	1.798E+00
0.65	6.006E-01	7.109E-01	1.479E+03	1.799E+00
0.70	5.423E-01	7.128E-01	1.456E+03	1.800E+00
0.75	4.868E-01	7.140E-01	1.438E+03	1.801E+00
0.80	4.309E-01	7.141E-01	1.423E+03	1.802E+00
0.85	3.744E-01	7.131E-01	1.412E+03	1.803E+00
0.90	3.140E-01	7.104E-01	1.402E+03	1.804E+00
0.95	2.441E-01	7.046E-01	1.396E+03	1.804E+00
0.99	1.554E-01	6.904E-01	1.393E+03	1.805E+00
0.999	9.998E-02	6.752E-01	1.394E+03	1.807E+00
0.9999	7.282E-02	6.638E-01	1.385E+03	1.806E+00

## Raw L2-CPE output of the Interplanetary Proton Environment

Listing 1: The sunward facing flux (worst-case) during solar maximum from IMP8 using L2-CPE.

```
- FLUX SUMMARY -
   L2-CPE V1.3
                       Kappa-distribution
   Cartesian (LRAD) Algorithm
3
4
   Phenomenological Region => Solar Wind at SolMax (IMP-8)
8
   Species => Protons
10
11
   Positive X direction flux calculated.
13
                     0.0010 keV
14
   Minimum Energy =
   Maximum Energy = 10000.0000 keV
15
16
   Number of Energy Bins =
17
18
   50% Total Flux
                      = 0.6109E+03 (\#/cm^2/sec)
19
   95% Total Flux
                      = 0.2986E+05 (\#/cm^2/sec)
20
    5% Total Flux
                      = 0.6493E+01 (\#/cm^2/sec)
21
   67% Total Flux

Maximum Total Flux =

Minimum Total Flux =

Total Flux =
                          0.1896E+04 (\#/cm^2/sec)
                          0.5679E+07 (#/cm<sup>2</sup>/sec)
23
                          0.1387E-02 (#/cm^2/sec)
24
                          0.7319E+04 (#/cm<sup>2</sup>/sec)
   Std. Dev. Total Flux = 0.4616E+05 (\#/cm^2/sec)
27
28
                       Differential Energy Flux Table (#/cm^2/sec/keV)
29
30
      E1(keV)
               E2(keV)
                                   95%
                                                        67%
                                              5%
      Maximum
               Minimum
                          Mean
                                    Std. Dev.
               0.0010
      +08  0.2333E-01  0.2406E+05  0.1700E+06
               0.0018
33
      +08 0.2121E-01 0.2272E+05 0.1597E+06
      0.0032
              0.0056  0.3597E+04  0.8902E+05  0.6892E+02  0.9277E+04  0.3526E
34
      +08  0.1871E-01  0.2109E+05  0.1472E+06
      0.0056
             0.0100 0.3200E+04 0.8097E+05 0.5914E+02 0.8297E+04 0.3125E
35
      +08  0.1588E-01  0.1914E+05  0.1324E+06
               0.0100
36
      +08 0.1282E-01 0.1688E+05 0.1155E+06
              0.0316  0.2252E+04  0.6065E+05  0.3763E+02  0.5959E+04  0.2182E
      0.0178
      +08 0.9715E-02 0.1437E+05 0.9709E+05
      0.0316
               0.0562 0.1746E+04 0.4935E+05 0.2715E+02 0.4692E+04 0.1685E
38
      +08 0.6801E-02 0.1173E+05 0.7806E+05
      0.0562
              0.1000  0.1268E+04  0.3808E+05  0.1798E+02  0.3485E+04  0.1216E
39
      +08  0.4322E-02  0.9100E+04  0.5960E+05
      0.1000
               40
      +07 0.2350E-02 0.6656E+04 0.4296E+05
      0.1778
              0.3162  0.5214E+03  0.1882E+05  0.5686E+01  0.1526E+04  0.4940E
41
      +07 0.1078E-02 0.4558E+04 0.2909E+05
      42
      +07 0.4226E-03 0.2905E+04 0.1846E+05
              1.0000 0.1428E+03 0.7016E+04 0.1063E+01 0.4634E+03 0.1357E
      0.5623
      +07 0.1060E-03 0.1717E+04 0.1096E+05
```

44	1.0000 1.7783 +06 0.2191E-04	0.6332E+02 0.9409E+03	0.3824E+04 0.6094E+04	0.3668E+00	0.2177E+03	0.6088E
45	1.7783 3.1623	0.2496E+02	0.1928E+04	0.1092E+00	0.9264E+02	0.2900E
46	+06 0.3786E-05 3.1623 5.6234	0.4789E+03 0.8762E+01	0.3183E+04 0.9028E+03	0.2810E-01	0.3574E+02	0.1467E
47	+06 0.5546E-06 5.6234 10.0000	0.2276E+03 0.2794E+01	0.1569E+04 0.3977E+03	0.6305E-02	0.1251E+02	0.7069E
48	+05 0.7017E-07 10.0000 17.7828	0.1018E+03 0.8167E+00	0.7351E+03 0.1673E+03	0.1265E-02	0.4048E+01	0.3331E
49	+05 0.7825E-08 17.7828 31.6228	0.4326E+02 0.2200E+00	0.3295E+03 0.6582E+02	0.2297E-03	0.1225E+01	0.1518E
50	+05 0.7849E-09 31.6228 56.2341	0.1764E+02 0.5576E-01	0.1422E+03 0.2516E+02	0.3830E-04	0.3482E+00	0.6881E
51	+04 0.7220E-10 56.2341 100.0000	0.6967E+01 0.1341E-01	0.5949E+02 0.9267E+01	0.5868E-05	0.9401E-01	0.2985E
52	+04 0.6195E-11 100.0000 177.8279	0.2690E+01 0.3090E-02	0.2427E+02 0.3361E+01	0.8546E-06	0.2441E-01	0.1249E
53	+04 0.5030E-12 177.8279 316.2278 +03 0.3913E-13	0.1023E+01 0.6874E-03	0.9707E+01 0.1191E+01 0.3827E+01	0.1201E-06	0.6135E-02	0.5097E
54	+03 0.3913E-13 316.2278 562.3413 +03 0.2944E-14	0.3849E+00 0.1495E-03 0.1441E+00	0.4141E+00 0.1493E+01	0.1598E-07	0.1510E-02	0.2056E
55	562.3413 1000.0000 +02 0.2159E-15	0.3152E-04 0.5386E-01	0.1416E+00 0.5782E+00	0.2079E-08	0.3623E-03	0.8160E
56	1000.0000 1778.2794 +02 0.1552E-16	0.6590E-05 0.2013E-01	0.4795E-01 0.2229E+00	0.2656E-09	0.8677E-04	0.3197E
57	1778.2794 3162.2776 +02 0.1100E-17	0.1354E-05 0.7536E-02	0.1634E-01 0.8573E-01	0.3325E-10	0.2047E-04	0.1240E
58	3162.2776 5623.4131 +01 0.6855E-19	0.2765E-06 0.2829E-02	0.5473E-02 0.3294E-01	0.4064E-11	0.4813E-05	0.4777E
59	5623.4131 10000.0000 +01 0.3413E-20			0.4980E-12	0.1122E-05	0.1829E
60 61						
62		Particle F	Flux per Enerç	gy Bin Table	(#/cm^2/sec	;)
64	E1(keV) E2(keV)	50%	95%	5%	67%	
	Maximum Minim		Std. D		0.00075.04	۰ ۵۵۵۵۶
65	0.0010 0.0018 +05 0.1815E-04	0.3291E+01 0.1873E+02	0.7883E+02 0.1323E+03	0.6563E-01	0.8387E+01	0.3229E
66	0.0018 0.0032	0.5458E+01	0.1326E+03	0.1070E+00	0.1397E+02	0.5352E
67	+05 0.2935E-04 0.0032 0.0056	0.3145E+02 0.8853E+01	0.2211E+03 0.2191E+03	0.1696E+00	0.2283E+02	0.8678E
	+05 0.4606E-04	0.5190E+02	0.3623E+03			
68	0.0056 0.0100 +06 0.6950E-04	0.1400E+02 0.8375E+02	0.3544E+03 0.5794E+03	0.2588E+00	0.3631E+02	0.1368E
69	0.0100 0.0178 +06 0.9978E-04	0.2134E+02 0.1314E+03	0.5552E+03 0.8989E+03	0.3779E+00	0.5581E+02	0.2079E
70	0.0178	0.3117E+02 0.1989E+03	0.8393E+03 0.1344E+04	0.5209E+00	0.8248E+02	0.3019E
71	0.0316 0.0562 +06 0.1674E-03	0.4296E+02 0.2887E+03	0.1344E+04 0.1215E+04 0.1921E+04	0.6682E+00	0.1155E+03	0.4147E
72	0.0562 0.1000 +06 0.1891E-03	0.5549E+02 0.3983E+03	0.1666E+04 0.2608E+04	0.7870E+00	0.1525E+03	0.5322E
73	0.1000 0.1778 +06 0.1829E-03	0.6622E+02 0.5180E+03	0.2169E+04 0.3343E+04	0.8392E+00	0.1871E+03	0.6310E

+06 0.1492E-03 0.6308E+03 0.4026E+04 0.3162 0.5623 0.7079E+02 0.2952E+04 0.6500E+00 0.2173E+03 0.6712 +06 0.1040E-03 0.7149E+03 0.4543E+04 0.5623 1.0000 0.6250E+02 0.3071E+04 0.4650E+00 0.2028E+03 0.594 +06 0.4638E-04 0.7516E+03 0.4797E+04 1.0000 1.7783 0.4928E+02 0.2976E+04 0.2854E+00 0.1694E+03 0.4738 +06 0.1705E-04 0.7323E+03 0.4743E+04 1.7783 3.1623 0.3454E+02 0.2669E+04 0.1511E+00 0.1282E+03 0.4014 +06 0.5240E-05 0.6628E+03 0.4405E+04 3.1623 5.6234 0.2156E+02 0.2222E+04 0.6916E-01 0.8797E+02 0.361 +06 0.1365E-05 0.5602E+03 0.3862E+04 5.6234 10.0000 0.1223E+02 0.1741E+04 0.2760E-01 0.5475E+02 0.3094 +06 0.3071E-06 0.4456E+03 0.3217E+04 10.0000 17.7828 0.6356E+01 0.1302E+04 0.9842E-02 0.3150E+02 0.2593 +06 0.6090E-07 0.3367E+03 0.2564E+04	Ε
+06 0.1040E-03 0.7149E+03 0.4543E+04 0.5623 1.0000 0.6250E+02 0.3071E+04 0.4650E+00 0.2028E+03 0.5945   +06 0.4638E-04 0.7516E+03 0.4797E+04   1.0000 1.7783 0.4928E+02 0.2976E+04 0.2854E+00 0.1694E+03 0.4738   +06 0.1705E-04 0.7323E+03 0.4743E+04   1.7783 3.1623 0.3454E+02 0.2669E+04 0.1511E+00 0.1282E+03 0.4014   +06 0.5240E-05 0.6628E+03 0.4405E+04   3.1623 5.6234 0.2156E+02 0.2222E+04 0.6916E-01 0.8797E+02 0.3615   +06 0.1365E-05 0.5602E+03 0.3862E+04   5.6234 10.0000 0.1223E+02 0.1741E+04 0.2760E-01 0.5475E+02 0.3094   +06 0.3071E-06 0.4456E+03 0.3217E+04   10.0000 17.7828 0.6356E+01 0.1302E+04 0.9842E-02 0.3150E+02 0.2593	_
76         0.5623         1.0000         0.6250E+02         0.3071E+04         0.4650E+00         0.2028E+03         0.5943           77         1.0000         1.7783         0.4928E+02         0.2976E+04         0.2854E+00         0.1694E+03         0.4738           78         1.7783         3.1623         0.3454E+02         0.2669E+04         0.1511E+00         0.1282E+03         0.4014           79         3.1623         5.6234         0.2156E+02         0.2222E+04         0.6916E-01         0.8797E+02         0.3613           +06         0.1365E-05         0.5602E+03         0.3862E+04         0.2760E-01         0.5475E+02         0.3094           80         5.6234         10.0000         0.1223E+02         0.1741E+04         0.2760E-01         0.5475E+02         0.3094           +06         0.3071E-06         0.4456E+03         0.3217E+04         0.9842E-02         0.3150E+02         0.2593           81         10.0000         17.7828         0.6356E+01         0.1302E+04         0.9842E-02         0.3150E+02         0.2593	E
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79 3.1623 5.6234 0.2156E+02 0.222E+04 0.6916E-01 0.8797E+02 0.361 +06 0.1365E-05 0.5602E+03 0.3862E+04 5.6234 10.0000 0.1223E+02 0.1741E+04 0.2760E-01 0.5475E+02 0.3094 +06 0.3071E-06 0.4456E+03 0.3217E+04 10.0000 17.7828 0.6356E+01 0.1302E+04 0.9842E-02 0.3150E+02 0.2593	_
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81 10.0000 17.7828 0.6356E+01 0.1302E+04 0.9842E-02 0.3150E+02 0.2593	_
	_
+UD U.DUBUE-U/ U.33D/E+U3 U.23D4E+U4	_
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	_
01.0000 50.0011 0.10705 01 0.01005 00 0.01055 00 0.05715 01 0.1000	_
	_
	_
56.2341 100.0000 0.5868E+00 0.4056E+03 0.2568E-03 0.4114E+01 0.1306 +06 0.2711E-09 0.1177E+03 0.1062E+04	_
	_
85   100.0000 177.8279 0.2405E+00 0.2616E+03 0.6651E-04 0.1900E+01 0.9718 +05 0.3915E-10 0.7958E+02 0.7555E+03	_
177 0070 010 0070 0 05105 01 0 10105 00 0 10005 01 0 01015 00 0 7051	_
+05 0.5415E-11 0.5327E+02 0.5296E+03 0.1662E-04 0.8491E+00 0.7058	_
87 316.2278 562.3413 0.3678E-01 0.1019E+03 0.3933E-05 0.3717E+00 0.506	_
+05 0.7245E-12 0.3547E+02 0.3674E+03	_
562.3413 1000.0000 0.1380E-01 0.6197E+02 0.9101E-06 0.1586E+00 0.357	=
+05 0.9447E-13 0.2357E+02 0.2531E+03	_
1000.0000 1778.2794 0.5129E-02 0.3732E+02 0.2067E-06 0.6753E-01 0.2488	F
+05 0.1208E-13 0.1567E+02 0.1735E+03	_
90 1778.2794 3162.2776 0.1874E-02 0.2261E+02 0.4601E-07 0.2833E-01 0.1717	F
+05 0.1522E-14 0.1043E+02 0.1186E+03	_
91 3162.2776 5623.4131 0.6804E-03 0.1347E+02 0.1000E-07 0.1185E-01 0.1176	F
+05 0.1687E-15 0.6963E+01 0.8106E+02	_
92 5623.4131 10000.0000 0.2443E-03 0.8000E+01 0.2180E-08 0.4910E-02 0.800	7E
+04 0.1494E-16 0.4665E+01 0.5541E+02	_
93	
TOTALS: 0.5836E+03 0.2937E+05 0.6244E+01 0.1811E+04 0.697	
+07 0.1260E-02 0.7319E+04 0.5040E+05	Ε