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Diaphragm Based Fiber Bragg Grating Acceleration Sensor with Temperature Compensation

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Abstract: A novel fiber Bragg grating (FBG) sensing-based acceleration sensor has been proposed to simultaneously decouple and measure temperature and acceleration in real-time. This design applied a diaphragm structure and utilized the axial property of a tightly suspended optical fiber, enabling improvement in its sensitivity and resonant frequency and achieve a low cross-sensitivity. The theoretical vibrational model of the sensor has been built, and its design parameters and sensing properties have been analyzed through the numerical analysis. A decoupling method has been presented with consideration of the thermal expansion of the sensor structure to realize temperature compensation. Experimental results show that the temperature sensitivity is $8.66 \text{ pm}/^{\circ}\text{C}$ within the range of $30\text{--}90\text{ }^{\circ}\text{C}$. The acceleration sensitivity is 20.189 pm/g with a linearity of 0.764% within the range of $5\text{--}65 \text{ m/s}^2$. The corresponding working bandwidth is $10\text{--}200 \text{ Hz}$ and its resonant frequency is 600 Hz . This sensor possesses an excellent impact resistance for the cross direction, and the cross-axis sensitivity is below 3.31% . This implementation can avoid the FBG-pasting procedure and overcome its associated shortcomings. The performance of the proposed acceleration sensor can be easily adjusted by modifying their corresponding physical parameters to satisfy requirements from different vibration measurements.

Keywords: fiber Bragg grating (FBG); temperature compensation; vibration sensor; diaphragm

1. Introduction

Compared with the traditional electronic vibration detection sensors, Fiber Bragg grating (FBG)-based vibration sensors provide an emerging and practical alternative solution [1–3]. They have offered the advantages of miniature size and light weight, are resistant to electromagnetic interference and corrosion, and easy to perform distributed dynamic measurements [1–5]. In recent years, FBG-derived sensors have aroused increased interest for structural health monitoring in many industrial sectors due to their remarkable attributes [6,7]. FBGs have been increasingly extended to measure seismic and mechanical vibration through designing mechanical structures to convert vibration into strain signals [8]. Au et al. presented a tapered plate FBG accelerometer with a sensitivity of $18.93 \mu\text{e/g}$ (Note: g represents the gravitational acceleration) [9]. However, this sensor suffered from a low resonant frequency of 150 Hz . Some scholars have proposed some FBG accelerometers based on using cantilever beam structures or other improved beam forms to improve their sensing properties [10,11]. Basumallick et al. presented to improve the sensitivity of a FBG-based vibration sensor by changing the distance between the FBG element axis and the neutral axis of the cantilever beam [10]. However, the resonant frequency of this design was still limited to 150 Hz . In order to improve the resonant frequency of the pasted FBG acceleration sensors, Liu et al. presented a novel diaphragm-based FBG accelerometer with the FBG element pasted around the circumferential direction

on the diaphragm [12]. This design provided a linear response over a frequency ranging from 10 to 200 Hz with a sensitivity of 36.6 pm/g. All of the above-mentioned FBG-based vibration sensors involved pasting FBG elements on the surface of mechanical structure elastomers. However, there are several drawbacks associated with these FBG-pasting vibration sensors, such as poor repeatability, chirp failure, and low resonant frequency.

To overcome these limitations, the use of the axial property of a suspended or metal-coated optical fiber has been proposed [13,14]. Antunes et al. proposed an FBG-based accelerometer with a low cross-sensitivity based on the use of axial property, and two optical fibers were arranged in a parallel manner on an improved cantilever beam [14]. The resonant frequency of this design was improved up to 344 Hz. Although the drawbacks of pasted FBG vibration sensors can be overcome by using the axial property of optical fiber to design vibration sensors, these implementations still suffered from poor dynamic properties, such as low resonant frequency and limited bandwidth [13–15]. In our previous work, we have proposed a new method that was based on the use of the transverse property of a suspended optical fiber to design an FBG vibration sensor [16]. This design can also avoid the FBG-pasting process and its accompanied limitations, and provided a higher sensitivity. However, its resonant frequency is 34 Hz, making it difficult to meet the requirements of complex mechanical vibration situations.

To address these issues, this paper has proposed an FBG sensing-based acceleration sensor to simultaneously measure temperature and medium-high frequency vibration with a high resonant frequency, and support multi-point distributed sensing. The axial property of a tightly suspended optical fiber has been utilized as elastomer together with the suspended diaphragm to sense the acceleration of target. The optical fiber inscribed with FBG elements was compressed and stretched to sense the strain caused by vibration. Such combined configuration can effectively overcome the limitations accompanied with the pasting process and improve the sensitivity and resonant frequency, leading to achieving a low cross-sensitivity and avoiding the chirping failure. The designed sensor consists of a diaphragm and an optical fiber that was fixed between the diaphragm center and the sensor housing base. Two FBGs were inscribed in the same optical fiber to decouple vibration and temperature. The working principle and theoretical modeling of the proposed sensor have been introduced and derived, and the corresponding numerical and experimental analyses have been performed to improve and validate the proposed design. This paper is organized as the following sections: working principle and modeling of the proposed sensor, numerical analysis and structure design, experiments and discussion, and conclusion.

2. Working Principle and Modeling of the Proposed Sensor

The schematic design of the proposed sensor and its simplified model are shown in Figure 1. This sensor mainly consists of a mass, a diaphragm, and a suspended optical fiber embedded with two FBGs, as shown in Figure 1a. The mass was assembled in the center of the suspended diaphragm, and the optical fiber was suspended with two ends fixed on the sensor housing frame and the upper surface of the mass. While measuring the vibration, the inertial force of the mass can compress or stretch #1FBG, which was embedded in the optical fiber and arranged between the sensor frame and the mass. Thus, vibration can be detected using the relative center wavelength shift of #1FBG. The other FBG element of #2FBG in the optical fiber was suspended in interior of the sensor frame, and it was used to measure and decouple the temperature effect.

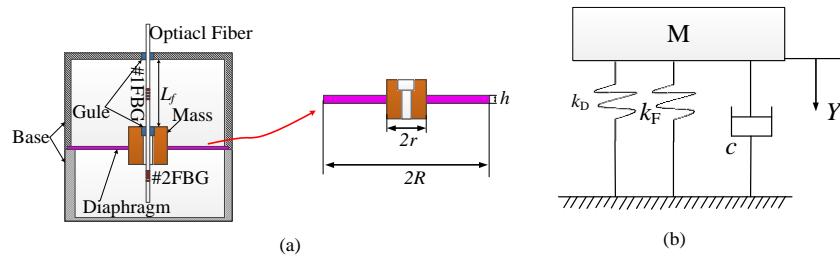


Figure 1. Schematic and modeling of the proposed sensor: (a) the schematic design of the FBG-based vibration sensor; and (b) the vibrational modeling of this proposed sensor.

2.1. Temperature Sensing Model

According to the working principle of FBG sensing, the relationship between the center wavelength shift of #2FBG and temperature can be written as:

$$\frac{\Delta\lambda_2}{\lambda_2} = (\alpha_f + \xi_f)\Delta T \quad (1)$$

where $\Delta\lambda_2$ is the center wavelength shift of #2FBG; λ_2 represents the center wavelength of #2FBG. ξ_f denotes the thermo-optic coefficient of the used optical fiber. α_f expresses the thermal expansion coefficient of FBG, and ΔT is the temperature variation.

The suspended optical fiber possesses a small diameter, and will be compressed or stretched along the axial direction with temperature variation. Therefore, the thermal expansion effect of this sensor can be simplified as a linear model along the axial direction of the optical fiber. The equivalent linear thermal expansion coefficient of the sensor base and the diaphragm along the axial direction of optical fiber can be denoted as α_M . Consequently, the relationship among the center wavelength shift of #1FBG, temperature and strain can be expressed as [17]:

$$\frac{\Delta\lambda_1}{\lambda_1} = (1 - \rho_e)\Delta\varepsilon + (\alpha_f + \alpha_M + \xi_f)\Delta T \quad (2)$$

where $\Delta\lambda_1$ is the center wavelength shift of #1FBG; λ_1 represents the center wavelength of #1FBG. ρ_e denotes the strain-optic coefficient of the optical fiber, and $\Delta\varepsilon$ is the axial strain increment of #1FBG under the inertial force. α_M expresses the equivalent linear thermal expansion coefficient of the sensor base and the diaphragm along the y direction.

Combing Equations (1) and (2), the temperature variation ΔT can be obtained through $\Delta\lambda_2$, but the strain $\Delta\varepsilon$ cannot be decoupled by using these two equations. Assuming that there is no vibration stimulation, the center wavelength shifts $\Delta\lambda_{10}$ of #1FBG will only be affected by temperature. Therefore, a new relationship between the $\Delta\lambda_1$ and strain $\Delta\varepsilon$ can be derived as:

$$\Delta\lambda_1 = (1 - \rho_e)\Delta\varepsilon\lambda_1 + \frac{\lambda_1(\alpha_f + \alpha_M + \xi_f)}{\lambda_2(\alpha_f + \xi_f)}\Delta\lambda_2 \quad (3)$$

2.2. Vibration Sensing Model

The mechanical vibration model of this sensor can be simplified as a mass-spring-damper system with one degree of freedom (refer to Figure 1b). According to Newton's second law, the kinetic equation of this sensor can be expressed as [18]:

$$M\ddot{Y} + c\dot{Y} + (k_D + k_F)Y = F\sin(\omega t) \quad (4)$$

where, Y represents the deformation of the diaphragm, and k_D is the transverse stiffness of the diaphragm. c denotes the damping ratio. F and w are the amplitude and frequency of the stimulation forces, respectively. M represents the mass weight, and k_F is the axial stiffness of the optical fiber, which can be formulated as [19]:

$$k_F = \frac{E_f A_f}{L_f} \quad (5)$$

where, E_f and A_f are Young's modulus and the cross-section area of the optical fiber, respectively. L_f represents the effective working length of the optical fiber.

According to elastic mechanics, the relationship between diaphragm deformation Y and the stimulation force F can be determined as [19,20]:

$$Y = \frac{3(1-\mu^2)}{4\pi} \frac{FR^2}{Eh^3} \left[1 - \left(\frac{r}{R} \right)^2 \frac{1 - (\frac{r}{R})^2 + 4\ln^2(\frac{r}{R})}{1 - (\frac{r}{R})^2} \right] \quad (6)$$

where, μ and E represent Poisson ratio and Young's Modulus of the diaphragm. h , R , and r denote the thickness, radius, and hard core radius of the diaphragm, respectively. According to Equation (6), the stiffness k_D can be described as [19]:

$$\frac{1}{k_D} = \frac{3(1-\mu^2)}{4\pi} \frac{R^2}{Eh^3} \left[1 - \left(\frac{r}{R} \right)^2 \frac{1 - (\frac{r}{R})^2 + 4\ln^2(\frac{r}{R})}{1 - (\frac{r}{R})^2} \right] \quad (7)$$

According to the definition of resonant frequency in mechanical vibrations, the resonant frequency w_n of this sensor can be expressed as [18]:

$$w_n = \sqrt{\frac{K}{M}} = \sqrt{\frac{k_D + k_F}{M}} \quad (8)$$

Consequently, the steady-state solution of Equation (4) can be determined as:

$$Y = \frac{F/K}{\sqrt{4\xi^2 \frac{w^2}{w_n} + \left(1 - \frac{w^2}{w_n}\right)^2}} \quad (9)$$

The stimulation force F is equal to the inertial force Ma . When $w \ll w_n$, Equation (9) can be simplified as:

$$Y = \frac{a}{w_n} \quad (10)$$

where, a represents the measured acceleration along the y direction. The incremental length ΔL of #1FBG is equal to the diaphragm deformation Y , consequently the strain $\Delta\varepsilon$ of #1FBG can be expressed as:

$$\Delta\varepsilon = \frac{\Delta L}{L_f} = \frac{Ma}{E_f A_f + K_D L_f} \quad (11)$$

Combining Equations (3) and (11), the center wavelength shift $\Delta\lambda_1$ of #1FBG can be reformulated as:

$$\Delta\lambda_1 = \frac{M\lambda_1(1-\rho_e)}{E_f A_f + K_D L_f} a + \frac{\lambda_1(\alpha_f + \alpha_M + \xi_f)}{\lambda_2(\alpha_f + \xi_f)} \Delta\lambda_2 \quad (12)$$

Based on Equation (12), the temperature and acceleration can be decoupled and simultaneously detected by using two FBGs. Also according to Equation (12), the peak-valley sensitivity of this sensor for detecting acceleration a can be expressed as:

$$S = \frac{M\lambda_1(1 - \rho_e)}{E_f A_f + K_D L_f} \quad (13)$$

3. Numerical Analysis for Structure Design

The relationship between the sensitivity/resonant frequency and the configuration parameters of this sensor should be investigated to support the design improvement and structural optimization. According to Equations (8), (12) and (13), the relationship between the parameters, such as diaphragm radius, radius of the hard-core diaphragm, diaphragm thickness, and effective working length of the optical fiber, and the sensor's sensitivity and resonant frequency has been determined, as shown in Figure 2. The results indicate that: (i) the sensitivity of this sensor increases with the increment of the diaphragm radius, but its resonant frequency decreases with the increase of the diaphragm radius. When the diaphragm radius is larger than 15 mm, both of the sensor's sensitivity and resonant frequency are close to a constant, as illustrated in Figure 2a. Consequently, the diaphragm radius should be kept below 15 mm for performance adjustment; (ii) when the radius of the hard core diaphragm is less than 5 mm, the resonant frequency is almost unchanged, as demonstrated in Figure 2b. Therefore, the sensitivity of this sensor can be adjusted without sacrificing the resonant frequency when this radius value is less than 5 mm; (iii) when the diaphragm thickness resides in the range of less than 0.05, the sensing properties are difficult to be improved, as shown in Figure 2c; (iv) when the thickness is larger than 0.05 mm, the changing rate of the sensitivity and resonant frequency are greater than these in the other ranges; and (v) compared with the above parameters, the variation of the optical fiber length produces more significant influences on the sensor's sensitivity and resonant frequency, as shown in Figure 2d.

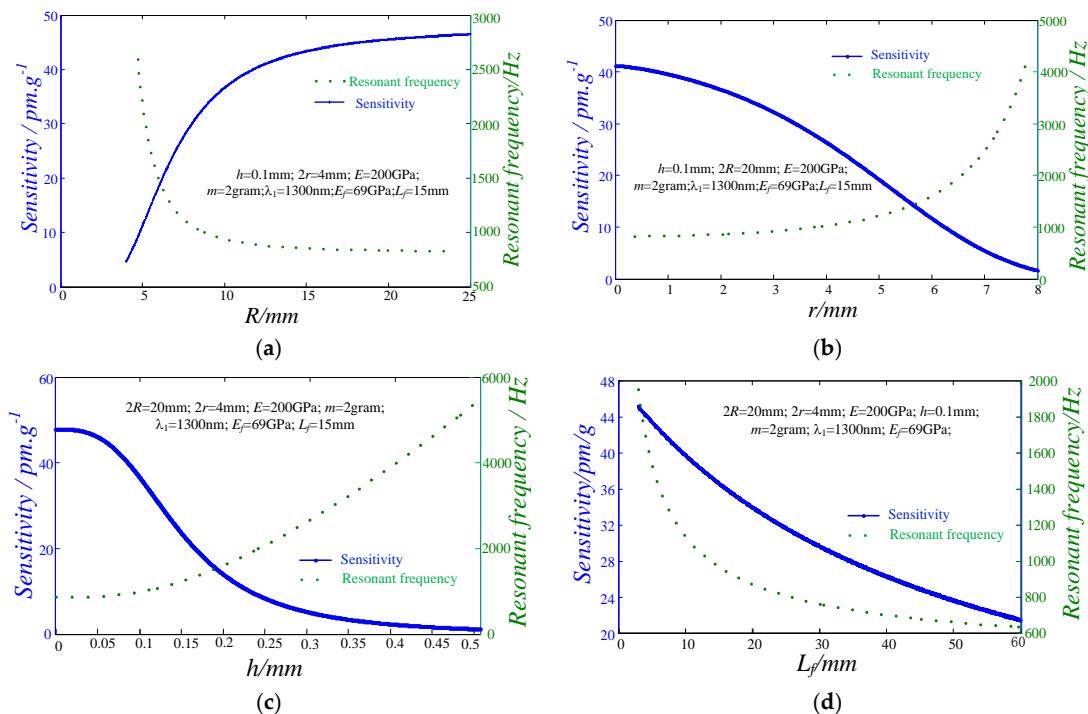


Figure 2. Relationship between the peak-valley sensitivity/resonant frequency and the configuration parameters of this sensor. (a) The effects of diaphragm radius on the sensor's sensitivity and resonance frequency; (b) The effects of radius of the hard-core diaphragm on the sensor's sensitivity and resonance frequency; (c) The effects of diaphragm thickness on the sensor's sensitivity and resonance frequency; (d) The effects of the effective length of the optical fiber on the sensor's sensitivity and resonance frequency.

Based on the above analysis, a stainless steel diaphragm was chosen, and it has an external diameter of 20 mm, a hard core diameter of 4 mm and a thickness of 0.1 mm. The mass weight is 2 g, and the effective working length of optical fiber is determined as 15 mm. The initial center wavelengths of the #1FBG and #2FBG are 1297.989 nm and 1307.881 nm, respectively. In order to improve the compressive property of the optical fiber and enhance the measurement range of compression force, the optical fiber has been configured with the pre-stress, which caused the center wavelength of #1FBG to shift 506 pm. The schematic structure design and fabricated prototypes of the sensor are shown in Figure 3. Substituting these parameters into Equations (8) and (13), the resonant frequency and peak-valley sensitivity are, respectively, determined as 967.7 Hz and 36.56 pm/g.

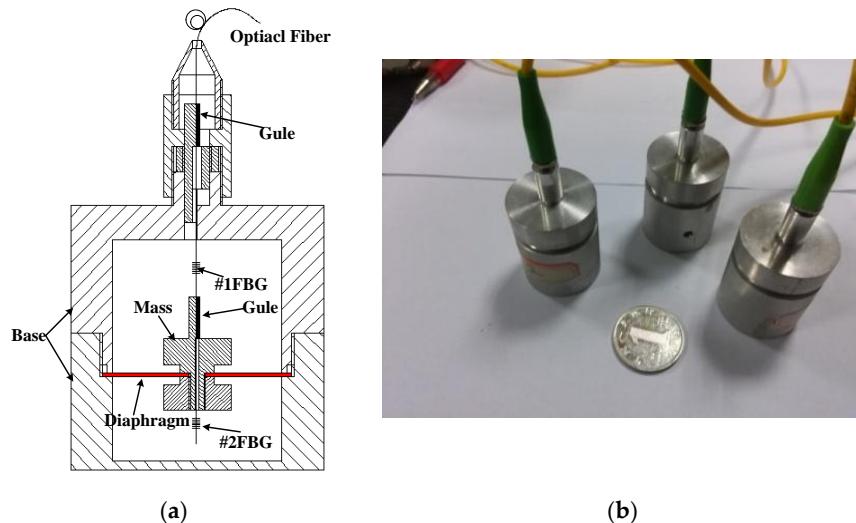


Figure 3. Assembly diagram and prototype of the proposed sensor: (a) 2D mechanical assembly drawing of the proposed sensor; and (b) physical prototypes of the proposed sensors.

4. Experiments and Discussion

4.1. Characterization of Temperature Effect

In order to characterize the temperature effect of this sensor, the experimental setup has been built as shown in Figure 4. The commercial WS-type GWD50 temperature sensor was employed as a standard reference. The signals of the FBG-based vibration sensor and the commercial WS-type temperature sensor (range: 0~100 °C; fitted equation: voltage = 0.04001 × T + 1.00262) were collected using an FBG interrogator (high-speed FBG interrogator, Wuhan Wutos Co., Ltd., Wuhan, China) and a NI acquisition card (USB-6351, National Instrument, Austin, TX, USA), respectively. The experiments have been repeated three times with the temperature changing in the range of 30~90 °C.

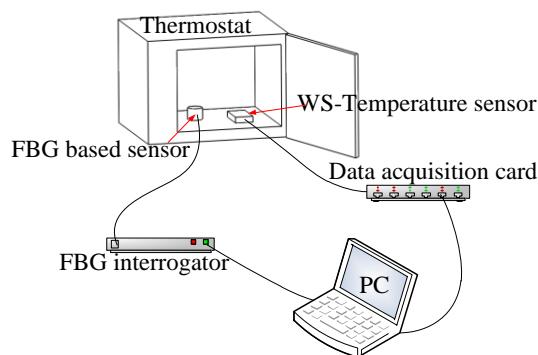


Figure 4. Schematic diagram for characterization of temperature effect.

The relationship between the center wavelength λ_1 of #1FBG and the environmental temperature has been determined as shown in Figure 5. The results suggest that there is a linear relationship between them. The relationship between the center wavelength λ_2 of #2FBG and the temperature can be obtained using the same method, which is shown in Figure 6. Temperature effect characteristics of the two FBGs are shown in Table 1. The results suggest that the temperature sensitivity of the #1FBG is 9.97 pm/ $^{\circ}$ C, greater than 8.66 pm/ $^{\circ}$ C of #2FBG. This conclusion matches the theoretical analysis that the response sensitivity of #1FBG is greater than that of #2FBG according to Equations (1) and (3). It also indicates that the temperature influence coupling on #1FBG cannot be completely eliminated by two different FBGs.

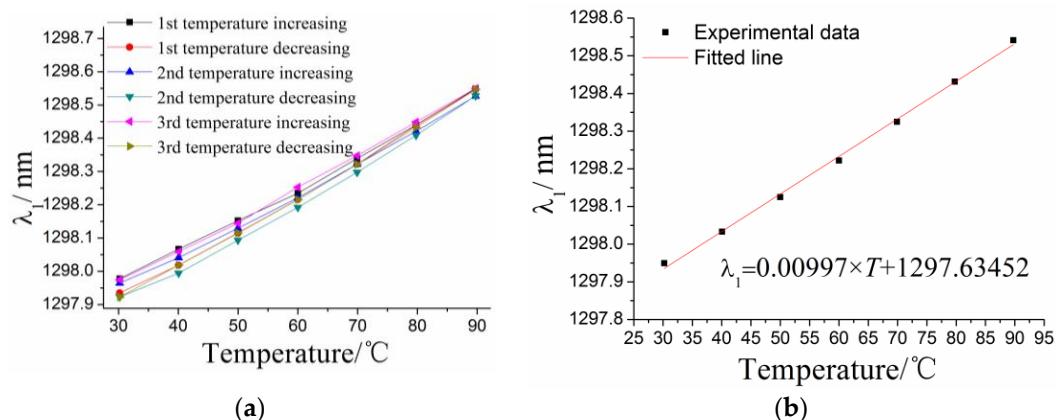


Figure 5. Relationship between the center wavelength of #1FBG λ_1 and the temperature: (a) the experimental data for the the center wavelength of #1FBG λ_1 and the temperature; and (b) the linearly fitted curve for the experimental data.

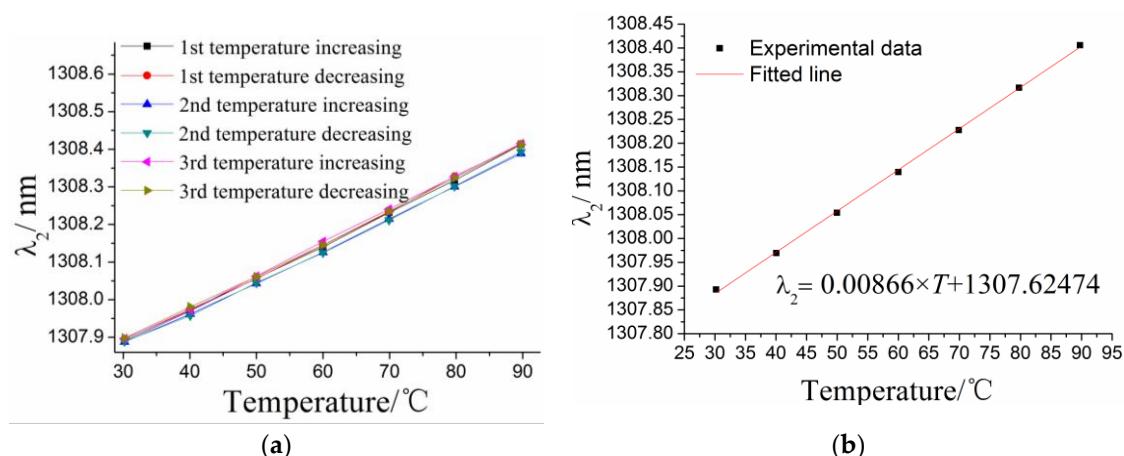


Figure 6. Relationship between the center wavelength λ_2 of #2FBG and the temperature: (a) the experimental data for the the center wavelength of #2FBG λ_2 and the temperature; and (b) the linearly fitted curve for the experimental data.

Table 1. Characterization of the temperature effects on the two FBGs.

Type	Linearity %	Hysteresis Error/%	Fitted Equation
#1FBG	2.36	8.76	$\Delta\lambda_1 = 0.00997 \times T + 1297.63452$ ($\Delta\lambda_{10}:\text{nm}$)
#2FBG	1.30	2.04	$\Delta\lambda_2 = 0.00866 \times T + 1307.62474$ ($\Delta\lambda_2:\text{nm}$)

4.2. Characterization of Static Properties

The schematic diagram and hardware configuration for static experiments are shown in Figure 7. The exciting signals with different frequencies and amplitudes were generated by an AFG-2005 signal generator, and then were amplified by a power amplifier to drive the exciter to produce stimulations. The 4507B-piezoelectric sensor with a sensitivity of $9.91 \text{ mV/m}\cdot\text{s}^{-2}$ was employed as a reference to calibrate the proposed FBG-based vibration sensor. Both of the piezoelectric sensor and the designed sensor were mounted on the vibration exciter.

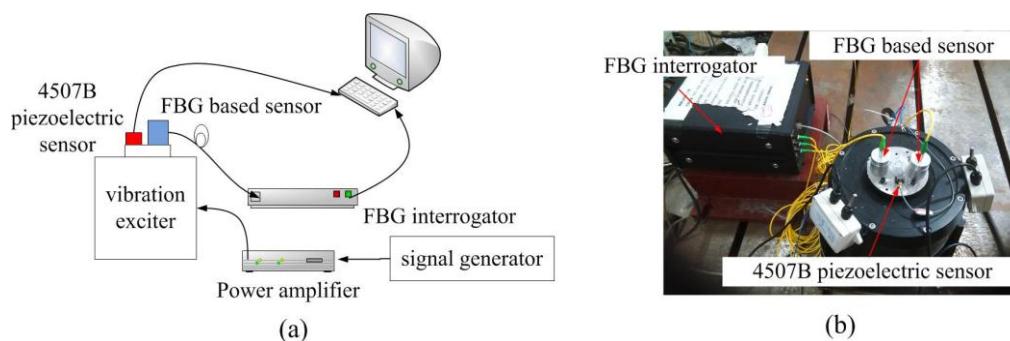


Figure 7. Schematic diagram and experimental setup for static experiments: (a) the schematic diagram for the static experiments; and (b) the experimental setup for static characterization.

The amplitude of stimulation acceleration changed from 5 m/s^2 to 65 m/s^2 , and the corresponding frequency was always kept at 30 Hz. The experiment has been repeated four times. The temperature of the whole process in the static experiments fluctuated around 27.4°C , which can be regarded as a constant temperature. Combining the two fitted equations of temperature effects on the two FBGs, the center wavelength shift $\Delta\lambda_{10}$ of #1FBG can be determined as: $\Delta\lambda_{10} = 1.15 \times \lambda_2 - 1505.7026$. Figure 8 shows the response of #1FBG and #2FBG under the stimulation amplitude of 60 m/s^2 . The response of #1FBG is a clearly sinusoid signal. However, there is almost no reflective wavelength response from #2FBG, because #2FBG was suspended and only affected by temperature variation.

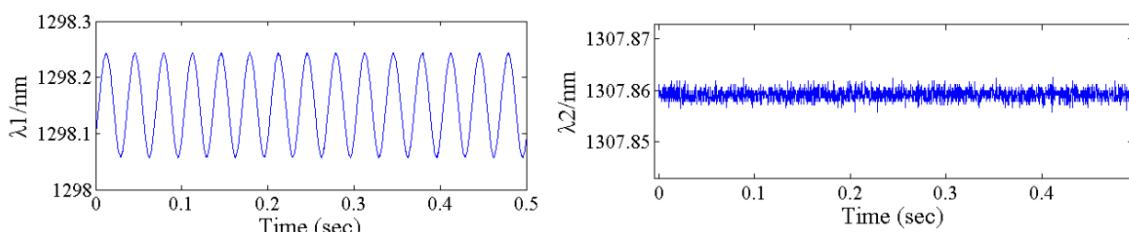


Figure 8. Reflective wavelength response of the #1FBG and #2FBG under a stimulation amplitude of 60 m/s^2 .

In order to investigate the vibration characteristics of this sensor, the relationship between the average values of the experimental data and the applied acceleration a is determined as shown in Figure 9. The results show that: (i) the sensitivity of this sensor is $3.01 \text{ pm/m}\cdot\text{s}^{-2}$ with a linearity of 0.764%, which is basically consistent with the numerical analysis value of $3.656 \text{ pm/m}\cdot\text{s}^{-2}$; (ii) the fitted equation is $\Delta\lambda_1 = 3.01893 \times a + 5.47227$.

Combining $\Delta\lambda_1$ with $\Delta\lambda_{10}$, a new equation for determination of the center wavelength shift of the FBGs and acceleration without temperature effects can be expressed as $\Delta\lambda_1 - (1150 \times \lambda_2 - 1,505,702.6) = 3.01893 \times a + 5.47227$.

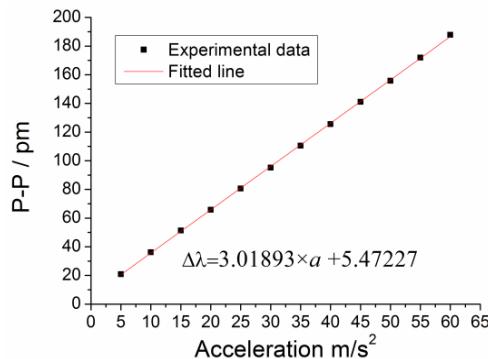


Figure 9. Relationship between the center wavelength shift $\Delta\lambda_1$ of #1FBG and acceleration.

4.3. Characterization of Dynamic Properties

The amplitude of vibration exciting acceleration was set at 10 m/s² with the frequency increasing from 10 to 1500 Hz to investigate the dynamic properties of this sensor. The experiment was repeated four times. The corresponding frequency-amplitude response curves are shown in Figure 10. These results indicate that (i) when frequency is within the range of 10~200 Hz, the curve is almost parallel to horizontal axis, suggesting this sensor works in a linear working bandwidth; (ii) The peak-to-peak value reaches its maximum at approximately 600 Hz, which represents the resonant frequency of this sensor according to Equation (8).

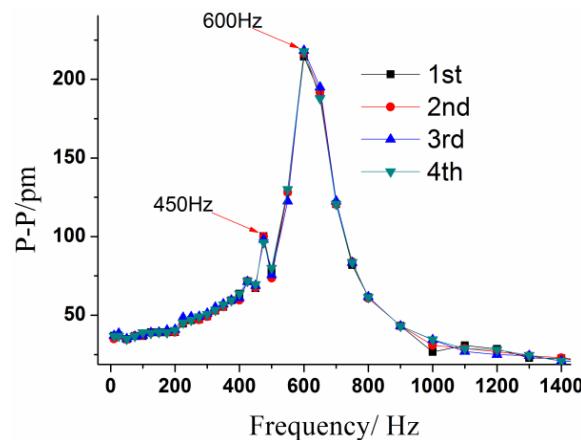


Figure 10. Frequency-amplitude response curves of this sensor.

The errors of the measured frequencies between the proposed FBG vibration sensor and the commercial piezoelectric sensor have been displayed in Figure 11. The results indicate that when the frequency is within 10~100 Hz (zone-I), the maximum relative error is about 2.34%. This error decreases with the increase of the frequency. When the frequency varies within the range of 100~1500 Hz (zone-II), the relative error is less than 0.2%. These small errors have demonstrated the close performance agreement between the proposed sensor and the commercial sensor, validating the effectiveness of the presented design.

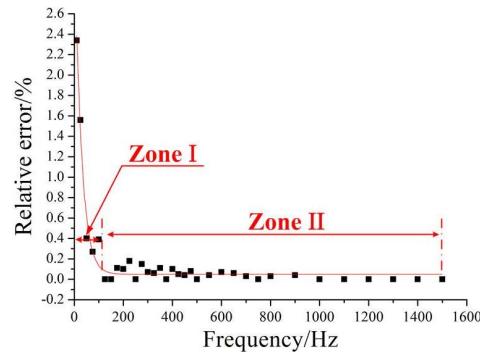


Figure 11. The measured frequency errors between the proposed sensor and the commercial piezoelectric sensor.

4.4. Characterization of Cross-Sensitivity

Cross-sensitivity is another important indicator to evaluate the vibration sensors. In order to demonstrate the cross-sensitivity for the cross direction, the acceleration amplitude was remained at 10 m/s^2 with frequency increasing from 10 to 1500 Hz. The frequency-amplitude response curves of the #1FBG along the cross direction are shown in Figure 12. The response curve of the cross-interference is a small constant. Except when the frequency is around 450 Hz. This value is the resonant frequency along the cross direction. The average values from the experimental data were used to calculate the amplitude-frequency response curves along the cross and vertical directions, as shown in Figure 13. The resonant response of the cross direction has been stimulated under the excitation along the main direction. These results suggest that the cross sensitivity is about 3.31% ($1/30.1893$) compared to the vertical direction, and it is mainly caused by sensor fabrication and assembly errors.

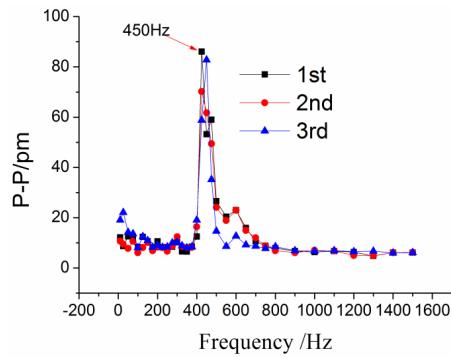


Figure 12. Amplitude-frequency response curves of the #1FBG along the cross direction.

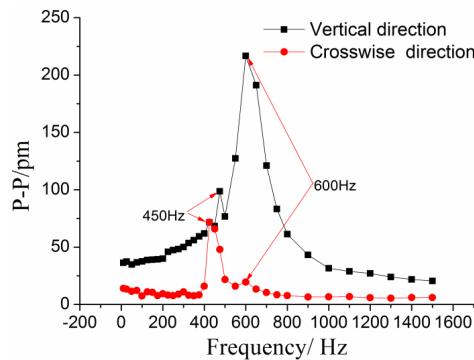


Figure 13. Amplitude-frequency response curves of the cross direction and vertical direction.

5. Conclusions

A novel and practical FBG acceleration sensor that is designed based on the combined configuration of a diaphragm and the axial property of a tightly suspended optical fiber has been proposed and implemented in this work. The proposed decoupling method has also been implemented to realize the separate detection of temperature and acceleration with considering the thermal expansion of the sensor structure. The tightly suspended optical fiber configuration with two fixed ends enables the improvement of the sensor's sensitivity and repeatability, and avoids the drawbacks associated with the FBG-pasting process. The proposed design has achieved a medium-high working bandwidth with a low cross-sensitivity. Both static and dynamic experiments have been performed to validate the effectiveness of the derived theoretical models and the simulation results, which have effectively supported the parameter determination of the sensor design. The sensor performance can be adjusted by changing the sensor's mechanical parameters to target different measurements, and its implementation can also be extended to realize multi-point distributed measurements in real-time.

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Conflicts of Interest: The authors declare no conflict of interest.

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