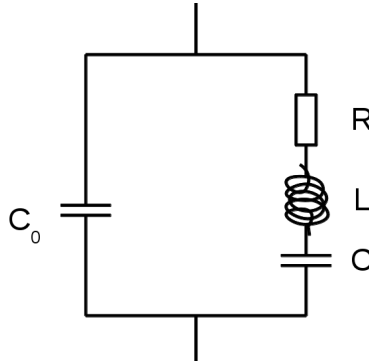


# Chapter 1

## Formulae for analysing $Y$ - and $Z$ -circles

Here is the formula collection I have put together from [1–3, 5] while writing the code.



**Fig. 1.1** Often viable equivalent circuit of a piezoelectric transducer.

Taking measured admittance and impedance circles as a starting point and the equivalent circuit of figure 1.1 as the model basis, a set of quantities can be calculated to characterise a given piezoelectric transducer. Table 1.2 lists several useful formulae for this sort of analysis. They have been taken from [2, 3, 5] and [1]<sup>1</sup>. Adopting the nomenclature of [3],  $f_1$  is the collective term for the resonance splitting up into  $(f_m, f_s, f_r)$  and  $f_2$  denotes the antiresonance  $(f_a, f_p, f_n)$ . DeAngelis & Schulze use the terms  $f_1$  and  $f_2$  for the top and the bottom of the admittance circle. These frequencies are labeled here as  $f_{mB}$ , the frequency of maximum susceptance  $B$  and  $f_{nB}$  the frequency of minimum  $B$ .

---

<sup>1</sup>who compiled formulae from [4, 5]

label	description
$f_1 \rightarrow (f_m, f_s, f_r)$	resonance (with $f_m \leq f_s \leq f_r$ )
$f_2 \rightarrow (f_n, f_p, f_a)$	antiresonance (with $f_a \leq f_p \leq f_n$ )
$f_m$	maximum $ Y $
$f_s$	maximum $\text{Re}(Y)$ , <i>motional resonance, series resonance</i>
$f_r$	$\text{Im}(Y) = 0$ , <i>electrical resonance</i>
$f_n$	maximum $ Z $
$f_p$	maximum $\text{Re}(Z)$ , <i>parallel resonance</i>
$f_a$	$\text{Im}(X) = 0$ , <i>electrical antiresonance</i>
order:	$f_m \leq f_s \leq f_r < f_a \leq f_p \leq f_n$
$f_{mB}, f_{nB}, f_{mX}, f_{nX}$	corresponds to $\max B$ , $\min B$ , $\max X$ , $\min X$
order:	$f_{mB} < f_s < f_{nB}$ and $f_{mX} < f_p < f_{nX}$

---

**Table 1.1** The characteristic frequencies of electromechanical transducers

---

formula	description
$k = \sqrt{1 - \frac{f_s^2}{f_p^2}} = \sqrt{\frac{C}{C_0 + C}}$	electromechanical coupling coefficient (Paraphrasing Wilson, $k^2$ is, in a sense, like a transduction efficiency, but more precisely, it is a characteristic of the mechanism with all dissipative processes ignored.)
$Q = Q_m = \frac{f_s}{\frac{f_{nB} - f_{mB}}{\frac{\text{sqr}t{L/C}}{R}}} =$	quality factor $Q$ or mechanical $Q$ (higher means less losses)
$Q_e = \frac{B_s}{G_{\max}}$	electrical $Q$ (lower means less dielectric losses, as it is a measure of the admittance circle vertical offset)
$Q_e Q_m = \frac{C_0}{C} = \frac{1 - k^2}{k^2} = r$	$Q$ -product is the same as the capacitance ratio
$R = \frac{1}{G_{\max}}$	motional resistance, represents the mechanical dissipation
$L = \frac{Q_m R}{\omega_s}$	motional inductance
$C = \frac{1}{Q_m R \omega_s}$	motional capacitance
$C_0 = \frac{f_r^2}{f_a^2 - f_r^2} C \approx \frac{B_s}{\omega_s}$	parallel capacitance, also called parasitic capacitance, it is a result of the electrode surface geometry (and sometimes cables as well), and it affects the ability of the electrical driver unit to deliver energy to the transducer
$\Gamma = C d / A$	motional capacitance constant ( $d$ : linear dimension $\ \vec{E}$ , $A$ : electrode area)
$B_s = \omega_s C_0$	susceptance of admittance circle centre (susceptance at the series resonance $f_s$ )
$r = \frac{C_0}{C}$	capacitance ratio
$M = \frac{Q_m}{r} = \frac{1}{\omega_s C_0 R} = \frac{k^2 Q_m}{1 - k^2}$	figure of merit
$\delta = \omega C_0 R$	normalised damping factor
$\Omega = \frac{f_p^2 - f_s^2}{f_p^2 - f_s^2}$	normalised frequency factor
$Z = \frac{1}{Y} = \frac{i}{\omega C_0} \frac{\Omega - i\delta}{1 - \Omega + i\delta}$	equation for impedance $Z(\omega)$ or admittance $Y(\omega)$
$Q = \frac{f_{\text{peak}}}{f_{\text{hdp2}} - f_{\text{hdp1}}}$	generic $Q$ -factor of a resonant system where $f_{\text{hdp2}} - f_{\text{hdp1}}$ gives the peak width at half dissipation power which corresponds to a reduction by a factor $1/\sqrt{2}$ for many signal amplitudes

---

**Table 1.2** Useful formulae for transducer analysis



# Bibliography

- [1] D.A. DeAngelis and G.W. Schulze. “Optimizing piezoelectric ceramic thickness in ultrasonic transducers”. In: *Ultrasonic Industry Association Symposium (UIA), 2010 39th Annual*. 2010, pp. 1–9.
- [2] “IEEE Standard Definitions and Methods of Measurement for Piezoelectric Vibrators”. In: *IEEE Std No.177* (1966), pp. 1–19.
- [3] “IEEE Standard on Piezoelectricity”. In: *ANSI/IEEE Std 176-1987* (1988), 0\_1–.
- [4] D. Stansfield. *Underwater electroacoustic transducers a handbook for users and designers*. English. Bath; St. Albans: Bath University Press ; Institute of Acoustics, 1991.
- [5] Oscar Bryan Wilson. *Introduction to theory and design of sonar transducers*. en. Los Altos, CA: Peninsula, 1988.