

TP2: Poisson's equation

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TC5 : TP sur les méthodes numériques et simulations
Séances du 18 et 22 novembre 2019 à Jussieu



- For which plasma studies do we need to solve Poisson's equation and not Maxwell equations?
- Work to be done

For which plasma studies do we need to solve Poisson's equation?

For low-temperature plasmas:

- Electrostatic Particle-In-Cell (PIC) simulations for low-pressure plasmas
 - Fluid simulations of low-temperature plasmas at atmospheric pressure
- back-up slides for details

- For which plasma studies do we need to solve Poisson's equation?
- Work to be done : Solve Poisson's equation in 1D and then in 2D

Poisson's equation

$$\varepsilon_0 \nabla \cdot (\varepsilon_r \nabla V) = -q_e(n_p - n_n - n_e)$$

In this work, the source term will be defined as ρ

$$\varepsilon_0 \nabla \cdot (\varepsilon_r \nabla V) = -\rho$$

We propose the following exercices:

- Exercice 1 : 1D poisson solver for a plasma between metallic walls ($\varepsilon_r = 1$)
- Exercice 2 : 1D poisson solver: performances
- Exercice 3 : 2D poisson solver for a plasma between metallic walls
- Exercice 4 (optional) : 1D poisson solver for a plasma between metallic walls covered by dielectric walls

In 1D:

$$\varepsilon_0 \nabla_x \cdot (\varepsilon_r \nabla_x V(x)) = -\rho(x)$$

For the numerical integration : we propose to use a finite volume approach. This approach is conservative

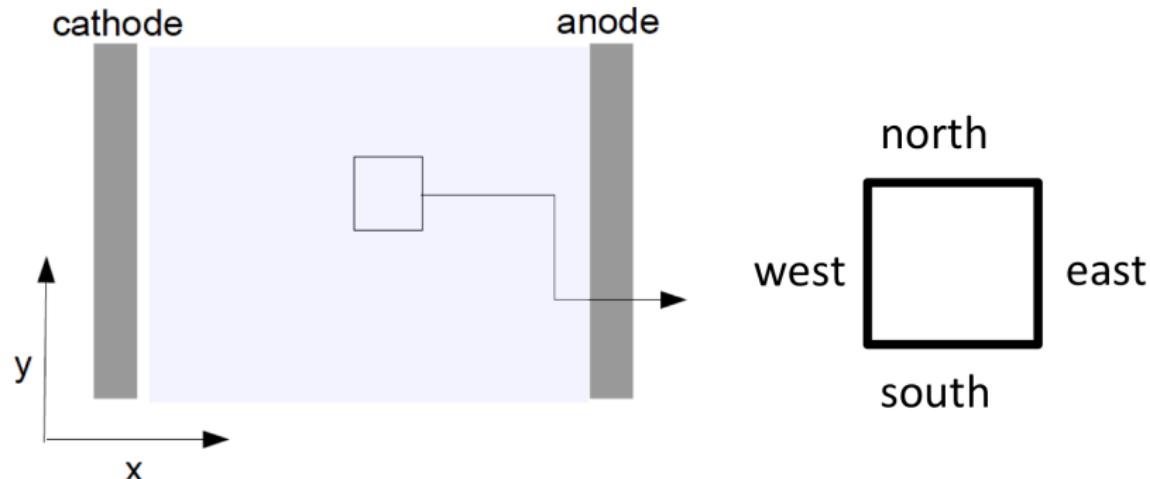
In 1D for a uniform mesh finite volume, and finite difference approaches give the same discretized form.

- We discretize the domain $x = [0, L_x]$ in $N - 2$ cells of size dx and 2 half-cells
- The center of each cell is defined by the index i
- The unknown potential $V(x)$ becomes V_i and the source term $\rho(x)$ becomes ρ_i
- The unknowns are **mean values at the center** of cells
- The center of the cell $i = 1$ corresponds to $x = 0$, and $i = N$ corresponds to $x = L_x$

→ exercices 1 and 2

Exercice 3 : Finite volume method in 2D

Volume of the discharge = \sum elementary cells



Exercice 3 : Integration of Poisson's equation in 2D

$$\varepsilon_0 \nabla \cdot (\varepsilon_r \nabla V) = -\rho \quad (1)$$

Poisson's equation can be written as :

$$\nabla \cdot D = -\rho \quad (2)$$

with

$$D = -\varepsilon_0 \varepsilon_r \nabla V = \varepsilon_0 \varepsilon_r E \quad (3)$$

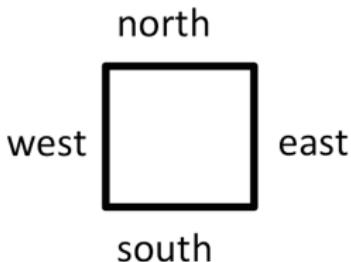
Exercice 3 : Integration of Poisson's equation in 2D

$$\nabla \cdot \mathbf{D} = -\rho \quad (4)$$

$$\iiint_{V_c} \nabla \cdot \mathbf{D} dV = - \iiint_{V_c} \rho dV \quad (5)$$

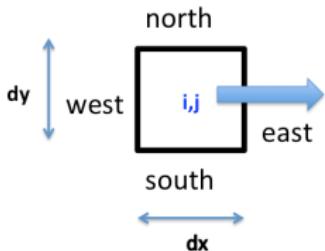
$$\oint_S \mathbf{D} \cdot d\mathbf{s} = -\bar{\rho} V_c \quad (6)$$

$$\frac{1}{V_c} \sum_f D_{Nf} \cdot S_f = -\bar{\rho} \quad (7)$$



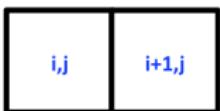
Exercice 3 : Integration of Poisson's equation in 2D

As an example: the EAST interface



$$\frac{D_{Ne} S_{fe}}{V_c} = \frac{1}{dx \cdot dy} \epsilon_0 \epsilon_r E_{Ne} dy$$

As $\epsilon_r = 1$ and the mesh is uniform:



$$E_{Ne} = -\frac{V_{i+1} - V_i}{dx}$$

Exercice 3 : Integration of Poisson's equation in 2D on a control volume

In doing the same on all interfaces, we obtain:

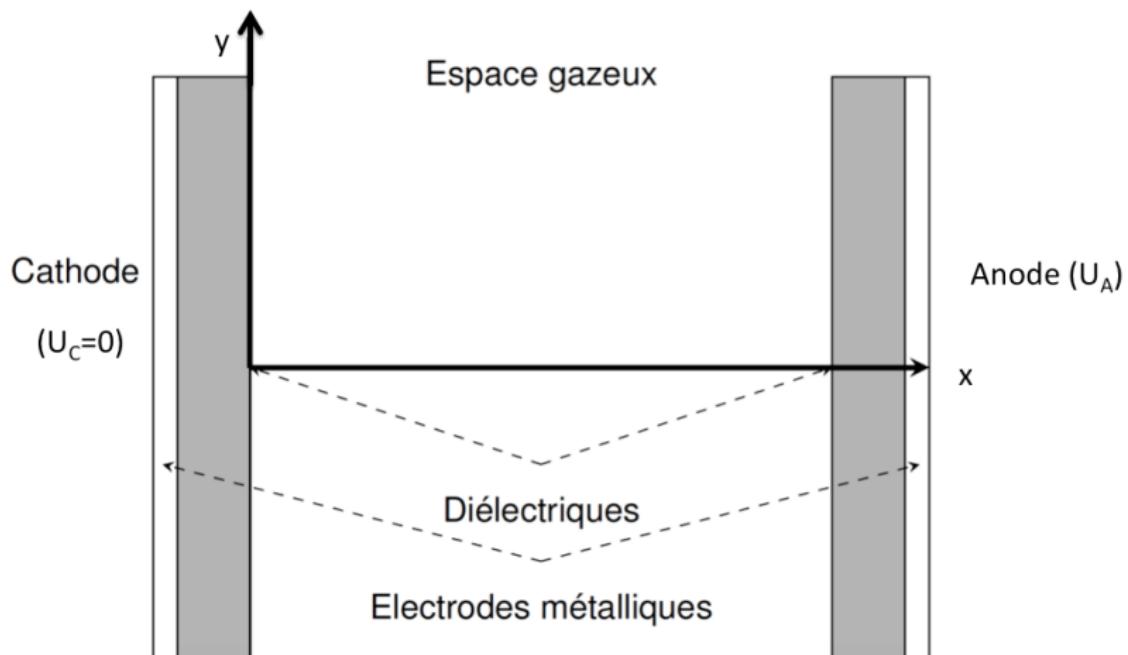
$$V_{e,i,j} \cdot V_{i+1,j} + V_{w,i,j} \cdot V_{i-1,j} + V_{n,i,j} \cdot V_{i,j+1} + V_{s,i,j} \cdot V_{i,j-1} - V_{c,i,j} \cdot V_{i,j} = -\rho_{i,j} \quad (8)$$

where

$$V_{c,i,j} = V_{e,i,j} + V_{w,i,j} + V_{n,i,j} + V_{s,i,j} \quad (9)$$

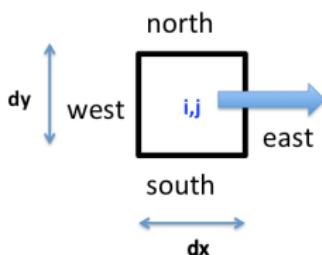
In 2D : The coefficients V_e, V_w, V_n and V_s are known : how to calculate $V_{i,j}$?
→ exercice 3

Exercice 4 : Studied configuration:



Exercice 4 : Integration of Poisson's equation with a permittivity that may vary from one cell to another

As an example: the EAST interface



$$\frac{D_{Ne} S_{fe}}{V_c} = \frac{1}{dx \cdot dy} \epsilon_{i,j} E_{Ne} dy \quad (10)$$



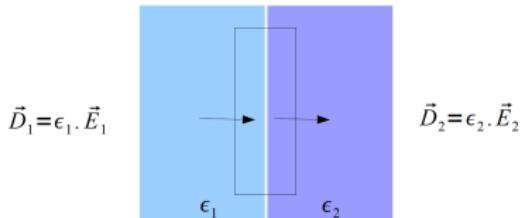
with $\epsilon = \epsilon_0 \epsilon_r(x, y)$

$$E_{Ne} = -\frac{V_{i+1/2} - V_i}{dx/2} \quad (11)$$

Exercice 4 : Integration of Poisson's equation on a control volume

Case of the interface of two materials with different dielectric properties:

The mesh is done such that the interface between materials corresponds to an interface between cells



$$\iiint_V \nabla \cdot \mathbf{D} dV = - \iiint_V \rho dV \quad (12)$$

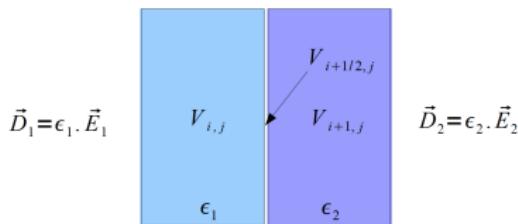
$$\iint_S \mathbf{D} \cdot d\mathbf{S} = -\bar{\rho}V \quad (13)$$

with no surface charges on the dielectric surface

$$D_{N1} = D_{N2} \quad (14)$$

Exercice 4 : Integration of Poisson's equation on a control volume

Case of the interface of two materials with different dielectric properties:



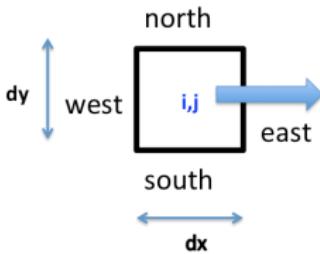
$$D_{N1} = D_{N2} \quad (15)$$

$$\epsilon_i \frac{V_{i+1/2} - V_i}{dx/2} = \epsilon_{i+1} \frac{V_{i+1} - V_{i+1/2}}{dx/2} \quad (16)$$

$$V_{i+1/2} = \frac{\epsilon_{i+1}}{\epsilon_i + \epsilon_{i+1}} V_{i+1} + \frac{\epsilon_i}{\epsilon_i + \epsilon_{i+1}} V_i \quad (17)$$

Exercice 4 : Integration of Poisson's equation on a control volume

As an example: the EAST interface



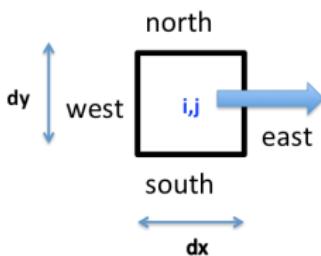
$$\frac{D_{Ne} S_{fe}}{V_c} = \frac{1}{dx \cdot dy} \epsilon_{i,j} E_{Ne} dy \quad (18)$$

$$E_{Ne} = -\frac{V_{i+1/2,j} - V_{i,j}}{dx/2} = -\frac{2\epsilon_{i+1,j}(V_{i+1,j} - V_{i,j})}{dx(\epsilon_{i,j} + \epsilon_{i+1,j})} \quad (19)$$

$$\frac{D_{Ne} S_{fe}}{V_c} = -\frac{2\epsilon_{i,j}\epsilon_{i+1,j}}{dx^2(\epsilon_{i,j} + \epsilon_{i+1,j})} (V_{i+1,j} - V_{i,j}) \quad (20)$$

Exercice 4 : Integration of Poisson's equation on a control volume

As an example: the EAST interface



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$$\downarrow \\ Ve_{i,j}$$

back-up slides

For which plasma studies do we need to solve Poisson's equation?

For low-temperature plasmas:

- Electrostatic Particle-In-Cell (PIC) simulations for low-pressure plasmas with static magnetic fields
- Non magnetized plasmas : Fluid simulations of low-temperature plasmas at atmospheric pressure

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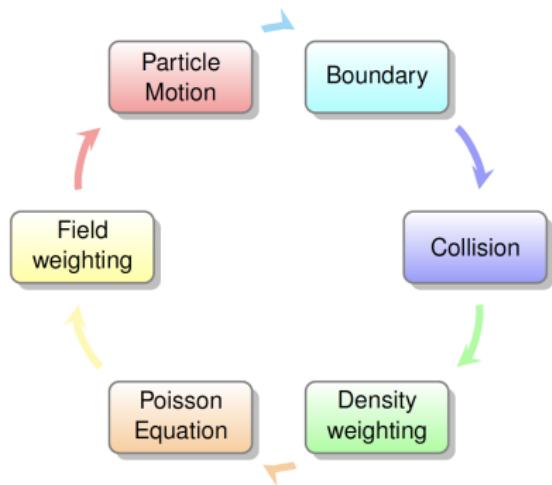
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Electrostatic PIC simulations for low-temperature plasmas at low pressure

Standard Particle in Cell simulation:

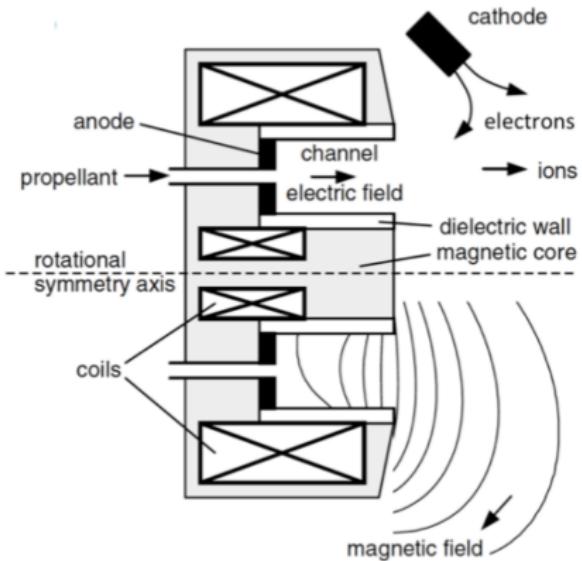
- ▶ Explicit
- ▶ Electrostatic
- ▶ Numerous gases
 - Helium
 - Argon
 - Krypton
 - Xenon



Example : Electrostatic PIC simulations for electric propulsion applications



Figure: Example of HET - PPS[©] 1350 Safran



Hall effect thruster (HET) :

A low-temperature low-pressure plasma with a fixed magnetic field
Plasma interaction with dielectric walls

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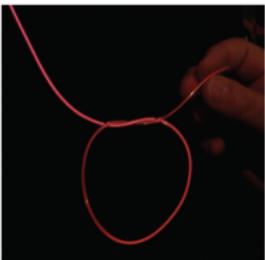
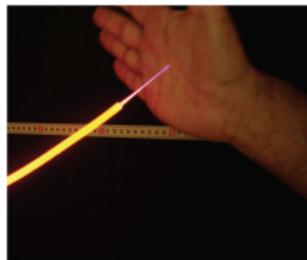
What is a low-temperature plasma at P_{atm} ?

- ▶ Electron density \ll neutral density : ionization degree of about 10^{-4} - 10^{-5}
- ▶ T_e (10 000 to 50 000 K) $\gg T_N=300$ K
- ▶ Interest of low-temperature plasmas at P_{atm} : nonequilibrium chemistry at room temperature

Non-thermal discharges at atmospheric pressure

Applications of non-thermal discharges at P_{atm} ?

- ▶ Since a few years, many studies on non-thermal discharges at atmospheric ground pressure
- ▶ Wide range of applications at low pressure → possible at ground pressure to reduce costs (no need for pumping systems) ?
- ▶ New applications as biomedical applications, plasma assisted combustion



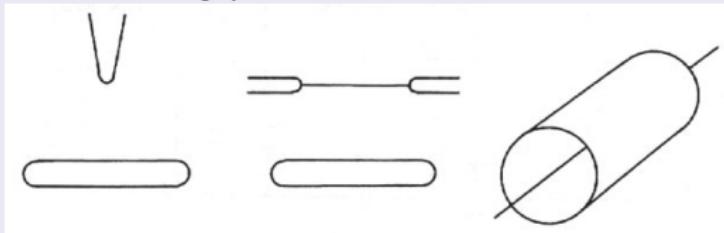
Robert et al., Plasma Process. Polym. 2009, 6, 795-802

G. Pilla, PhD thesis (2008)

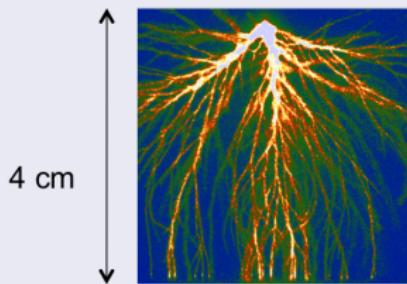
How to generate non-thermal discharges at atmospheric pressure ?

Between two metallic electrodes

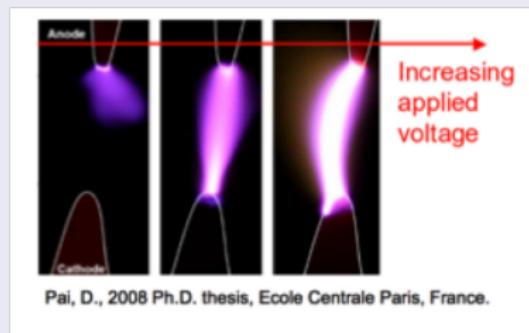
- ▶ Interelectrode gaps of a few mm to a few cm at P_{atm}



- ▶ If the gap distance > 1cm → complex discharge structure



Briels, PhD (2007)



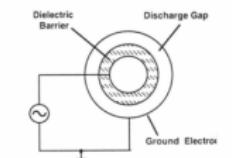
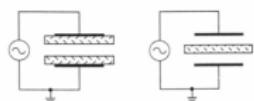
- ▶ Risk: If the voltage pulse is too long → transition to **spark** (thermal plasma!)



How to generate non-thermal discharges at atmospheric pressure ?

Dielectric Barrier Discharge (DBD)

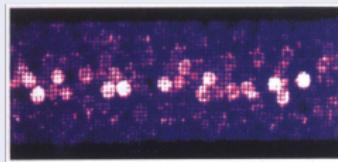
- ▶ Interelectrode gaps of a few mm to a few cm at P_{atm}



Plane-plane reactor (LPGP Orsay)



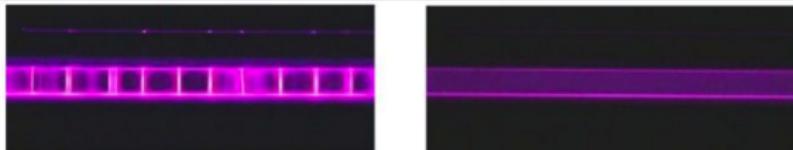
Wire-cylinder (GREMI Orléans)



H.Russ et al , IEEE Trans. Plasma Sci. 27 (1999) 38

Structure of P_{atm} discharges

- ▶ At P_{atm} , non-thermal atmospheric pressure discharges may have filamentary or diffuse structures



Filamentary discharges: most frequent

- ▶ High electron density (10^{14} cm^{-3}) in a filament with a radius of the order of $100 \mu\text{m}$ → high density of active species (radicals, excited species). In some cases, local heating may occur

Diffuse discharges

- ▶ Low density of electrons, large volume of the discharge and negligible heating

- Continuity equation is solved for electrons, positive and negative ions

$$\frac{\partial n_i}{\partial t} + \operatorname{div} \mathbf{j}_i = S_i \quad (21)$$

- Drift-diffusion approximation

$$\mathbf{j}_i = \mu_i n_i \mathbf{E} - D_i \operatorname{grad} n_i \quad (22)$$

- Poisson's equation:

$$\varepsilon_0 \nabla \cdot (\varepsilon_r \nabla V) = -q_e(n_p - n_n - n_e) \quad (23)$$

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- Strong non-linear coupling between drift-diffusion and Poisson's equations
- The species densities have to be calculated accurately as their difference is used to compute the potential and then the electric field → crucial to simulate the propagation of ionization fronts

- Continuity equation is solved for electrons, positive and negative ions

$$\frac{\partial n_i}{\partial t} + \operatorname{div} \mathbf{j}_i = S_i \quad (24)$$

- Drift-diffusion approximation

$$\mathbf{j}_i = \mu_i n_i \mathbf{E} - D_i \operatorname{grad} n_i \quad (25)$$

- Source terms for air:

$$\begin{cases} S_e = (\partial_t n_e)_{\text{chem}} &= (\nu_\alpha - \nu_\eta - \beta_{ep} n_p) n_e + \nu_{\text{det}} n_n + S_{ph}, \\ S_n = (\partial_t n_n)_{\text{chem}} &= -(\nu_{\text{det}} + \beta_{np} n_p) n_n + \nu_\eta n_e, \\ S_p = (\partial_t n_p)_{\text{chem}} &= -(\beta_{ep} n_e + \beta_{np} n_n) n_p + \nu_\alpha n_e + S_{ph}. \end{cases} \quad (26)$$

- Local field approximation: $\nu_\alpha(|\vec{E}|/N)$, $\nu_\eta(|\vec{E}|/N)$, $\mu_i(|\vec{E}|/N)$, $D_i(|\vec{E}|/N)$
Morrow et al., *J.Phys. D:Appl. Phys.* **30**,(1997)
- Transport parameters and source terms are pre-calculated (Bolsig+ solver - <http://www.bolsig.laplace.univ-tlse.fr/>)

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- Poisson's equation

$$\varepsilon_0 \nabla \cdot (\varepsilon_r \nabla V) = -q_e(n_p - n_n - n_e) \quad (27)$$

- Surface charges on the dielectric surface are obtained by time integrating charged particle fluxes to the surface.
- At the dielectric surface, secondary emission of electrons by ion bombardment

Specificities of the simulation of low-temperature plasmas at atmospheric pressure

- ▶ Simulation of ionization front propagation is known to be computationally **expensive**
- ▶ Temporal multiscale nature of **explicit** simulation: $\Delta t = 10^{-12} - 10^{-14}$ s

Convection: $\Delta t_C = \min \left[\frac{\Delta x_j}{v_{X(i,j)}}, \frac{\Delta r_j}{v_{r(i,j)}} \right]$

Diffusion: $\Delta t_d = \min \left[\frac{(\Delta x_j)^2}{D_{X(i,j)}}, \frac{(\Delta r_j)^2}{D_{r(i,j)}} \right]$

Chemistry: $\Delta t_l = \min \left[\frac{n_{K(i,j)}}{S_{K(i,j)}} \right]$

Diel. relaxation: $\Delta t_{Diel} = \min \left[\frac{\epsilon_0}{q_e \mu e_{(i,j)} n_e(i,j)} \right]$

- ▶ Time scale of discharge propagation in centimeter gaps is ~ 10 ns, $\rightarrow \sim 10^4$ time steps
- ▶ For a gap of 1 cm, $\Delta x, r = 10 - 1 \mu\text{m} \rightarrow$ nbre of points $> 1 \times 10^6$

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Specificities of the simulation of low-temperature plasmas at atmospheric pressure

- ▶ One time-step Δt : more than 50 % of the time for solving Poisson's equation
- ▶ Need for an accurate and efficient method to solve Poisson's equation at each time-step

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Numerical solution of Poisson's equation

$$V_{e,i,j} \cdot V_{i+1,j} + V_{w,i,j} \cdot V_{i-1,j} + V_{n,i,j} \cdot V_{i,j+1} + V_{s,i,j} \cdot V_{i,j-1} - V_{c,i,j} \cdot V_{i,j} = -\rho_{i,j} \quad (28)$$

where

$$V_{c,i,j} = V_{e,i,j} + V_{w,i,j} + V_{n,i,j} + V_{s,i,j} \quad (29)$$

The coefficients V_e, V_w, V_n and V_s are known, the source term is also known.

We want to calculate $V_{i,j}$

→ The system to be solved can be written as $Ax=B$.

Different methods can be used (iterative or direct methods).

In this work, we propose to use 2 iterative methods:

- Gauss-Seidel
- SOR (successive over-relaxation)

$$Ve_{i,j} \cdot V_{i+1,j} + Vw_{i,j} \cdot V_{i-1,j} + Vn_{i,j} \cdot V_{i,j+1} + Vs_{i,j} \cdot V_{i,j-1} - Vc_{i,j} \cdot V_{i,j} = -\rho_{i,j} \quad (30)$$

If we write the Gauss-Seidel algorithm, we have to calculate:

$$V_{i,j} = (-Ve_{i,j} \cdot V_{i+1,j} - Vw_{i,j} \cdot V_{i-1,j} - Vn_{i,j} \cdot V_{i,j+1} - Vs_{i,j} \cdot V_{i,j-1} + \rho_{i,j}) / Vc_{i,j} \quad (31)$$

and iterate until convergence.

Numerical solution - successive over-relaxation (SOR)

The SOR method is a slight modification of the Gauss-Seidel method.

In the SOR, we define $0 < \omega < 2$ and calculate iteratively:

$$V_{i,j} = (1 - \omega)V_{i,j}^{old} + (-Ve_{i,j} \cdot V_{i+1,j} - Vw_{i,j} \cdot V_{i-1,j} - Vn_{i,j} \cdot V_{i,j+1} - Vs_{i,j} \cdot V_{i,j-1} + \rho_{i,j})\omega / Vc_{i,j} \quad (32)$$

until convergence

$V_{i,j}^{old}$ is the solution obtained at the last iteration.

If $\omega = 1$ we have the Gauss-Seidel method.

A good compromise for the SOR method is to use $\omega = 1.5$