

EE16B Course Notes

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1 Discrete Time Models

Although circuits and other systems function in continuous time, computers can only act in discrete time. This means the signals they send out to try and control the system are piecewise-continuous, and they can only sense the system at specified intervals δ . At a discrete time-step i , the computer will measure $\vec{x}_d[i]$ and applies the control $\vec{u}[i]$ over the time-interval $[i, i + 1]$. Keep in mind that $i = \delta t$ where t is the continuous time.

Definition 1 *The discrete time model is $\vec{x}_d[i + 1] = A_d \vec{x}_d[i] + B_d \vec{u}[i] + \vec{w}[i]$ where $\vec{w}[i]$ is some disturbance.*

1.1 Converting between continuous time and discrete time

To see how to convert between a continuous time model to a discrete time model, consider the following system.

$$\begin{aligned} \frac{dx}{dt} &= \lambda x + u, u = e^{st} \\ \left(\frac{d}{dt} - \lambda\right) x &= u \end{aligned}$$

Solving will give $x = \alpha e^{\lambda t} + \beta e^{st}$. Plugging this into the original equation

$$\begin{aligned} \alpha \lambda e^{st} + \beta s e^{st} &= \lambda(\alpha e^{\lambda t} + \beta e^{st}) + e^{st} \\ \text{if } \lambda &\neq s \\ \beta s &= \beta \lambda + 1 \implies \beta = \frac{1}{s - \lambda} \end{aligned}$$

Since the computer only outputs constant signals, $s = 0$, so $x = \alpha e^{\lambda t} - \frac{u}{\lambda}$. If $x(0) = x_0$

$$\begin{aligned} x(0) &= \alpha - \frac{u}{\lambda} = x_0 \\ x &= \left(x_0 + \frac{u}{\lambda} e^{\lambda t}\right) - \frac{u}{\lambda} \\ x &= x_0 e^{\lambda t} + u \left(\frac{e^{\lambda t} - 1}{\lambda}\right) \end{aligned}$$

Thus the discrete time model is

$$x[i + 1] = e^{\lambda \delta} x[i] + \left(\frac{e^{\lambda \delta} - 1}{\lambda}\right) u[i]$$

since the initial condition for the next time-step is simple the value at the previous time-step

1.2 Finding A and B

What would happen if we didn't know what A and B were though? It turns out that we can find it by gathering data about the system and then using least squares. In the scalar case:

$$\begin{aligned} x[i+1] &= ax[i] + bu[t] + w[i] \\ x[1] &= ax[0] + bu[0] \\ x[2] &= ax[1] + bu[1] \\ &\vdots \\ x[m] &= ax[m-1] + bu[m-1] \end{aligned}$$

This means with m observations, we can construct a matrix D and a vector \vec{s} such that we have the least squares problem

$$D\vec{p} = \vec{s}, \vec{p} = \begin{bmatrix} a \\ b \end{bmatrix}$$

The same thing can be done in the vector case. We just create multiple parallel systems by multiplying out the rows.

2 Control Theory

2.1 Controllability

Definition 2 A system is controllable if $\forall x^*, \forall x[0] \exists u[0], u[1], \dots, u[k-1]$ such that $x[k] = x^*$ given that the system starts at $x[0]$

In words, this means that there exists a sequence of control actions that can eventually get the system anywhere we want it to be from any given initial state.

Theorem 1 If a state is n -dimensional, then a system $\vec{x}_d[i+1] = A\vec{x}[i] + B\vec{u}[i] + \vec{w}[i]$ is controllable in k time-steps if $\text{span}(B, AB, \dots, A^{k-1}B) = \mathbb{R}^n$

Proof 1 Without any noise, $\vec{x}_d[i+1] = A\vec{x}[i] + B\vec{u}[i]$

$$\begin{aligned} \vec{x}[1] &= A\vec{x}[0] + B\vec{u}[0] \\ \vec{x}[2] &= A\vec{x}[1] + B\vec{u}[1] = A^2\vec{x}[0] + AB\vec{u}[0] + B\vec{u}[1] \\ \vec{x}[3] &= A\vec{x}[2] + B\vec{u}[2] = A^3\vec{x}[0] + A^2B\vec{u}[0] + AB\vec{u}[1] + B\vec{u}[2] \\ &\vdots \\ \vec{x}[k] &= A^k\vec{x}[0] + \sum_{i=0}^{k-1} A^{k-i-1}B\vec{u}[i] \end{aligned}$$

Thus the current state is merely a linear combination of vectors in the column spaces of A^k and $B \dots A^{k-1}$, so if this span is equal to \mathbb{R}^n , we can reach every state.

Definition 3 *The controllability matrix is a the matrix whose column space is all the reachable states.*

$$[B \mid AB \mid A^2B \mid \dots \mid A^{k-1}B]$$

However, if we want to check if a system is controllable in 100 time-steps for a 900 state system, it will be painful to calculate the column space of the controllability matrix. It turns out that we can stop checking when $\dim(\text{col}(B, AB, \dots, A^{p-1})) = \dim(\text{col}(B, AB, \dots, A^p))$, ($p \leq k$) (i.e the dimension of the column space stops growing) This means we can build the controllability matrix up piece-by-piece and stop early rather than computing the full column space only to fail. Consider the following proof for why this works.

Proof 2 *If \vec{b} is column vector of the matrix B , then $A^p \vec{b} = \sum_{i=0}^{p-1} \alpha_i A^i \vec{b}$ since we assume the dimension of the column space has stopped growing, so $A^p \vec{b}$ is a linear combination of the vectors preceding it. We want to show $\exists \beta_i$ such that $A^{p+1} = \sum_{i=0}^{p-1} \beta_i A^i \vec{b}$*

$$\begin{aligned} A^{p+1} \vec{b} &= A(A^p \vec{b}) = \\ A \sum_{i=0}^{p-1} \alpha_i A^i \vec{b} &= \sum_{i=0}^{p-1} \alpha_i A^{i+1} \vec{b} = \\ \alpha_{p-1} A^p \vec{b} + \sum_{i=0}^{p-2} \alpha_i A^{i+1} \vec{b} &= \\ \alpha_{p-1} \sum_{i=0}^{p-1} \alpha_i A^i \vec{b} + \sum_{i=0}^{p-2} \alpha_i A^{i+1} \vec{b} \end{aligned}$$

By writing A^{p+1} as a linear combination of B, AB, \dots, A^{p-1} , we have shown β_i exists, so by induction, all future vectors $p + m \leq k$ will be linear combinations of these same vectors, so the dimension will never grow again and we can be justified in stopping early.

2.2 Stability

The question of stability is whether or not disturbances will over time control a system if left alone. Specifically, it is asking if the disturbances are bounded, will the states be bounded too?

Definition 4 *Bounded Input, Bounded Output (BIBO) stability means if $|\vec{w}[i]| < \epsilon$, then $\exists \delta > 0$ such that $|\vec{x}[i]| < \delta$*

To see where this definition comes into play, consider the following scalar systems:

1. $x[i+1] = u[i] + w[i]$
2. $x[i+1] = \frac{1}{2}x[i] + u[i] + w[i]$ ("Weak" dependence on previous state)
3. $x[i+1] = 2x[i] + u[i] + w[i]$ ("Strong" dependence on previous state)

System 1: In this system, there is no dependence on the previous state. Thus any disturbances are limited to affecting only the next state and no others.

This makes the system stable because disturbances will not add up. To see this mathematically, pretend $u[i] = 0$ since we want to see how the system evolves without doing anything.

$$|x[i+1]| = |w[i]| < \epsilon, \quad \therefore |x[i]| < \epsilon$$

Thus we have BIBO stability

System 2: Unlike the previous system, this system has a "weak" dependence on previous states. We consider it "weak" because only half of the previous state influences the next state. Intuitively, this system must be BIBO stability then because although disturbances will accumulate, they will be attenuated through an infinite geometric sum. Once again, we will pretend $\bar{u}[i] = 0$ to check this mathematically.

$$|x[i+1]| = \frac{1}{2}x[i] + w[i] < \frac{1}{2}x[i] + \epsilon$$

Unrolling the recursive relationship, we see

$$|x[i+1]| < \epsilon + \frac{1}{2}\epsilon + \frac{1}{4}\epsilon + \dots + \left(\frac{1}{2}\right)^i \epsilon$$

$$\lim_{i \rightarrow \infty} |x[i+1]| < \frac{\epsilon}{1 - \frac{1}{2}} = 2\epsilon$$

Thus the system is BIBO stability since $|x[i]| < 2\epsilon$

System 3: This system has a "strong" dependence on previous states since the contribution of previous states is doubled each times. Intuitively, this means the system must be unstable because small disturbances will be explode over time. To see this mathematically, once again consider what happens if we apply no inputs.

$$|x[i+1]| = 2x[i] + w[i] < 2x[i] + \epsilon$$

Unrolling the recursion,

$$|x[i+1]| < \epsilon + 2\epsilon + 4\epsilon + \dots + 2^i \epsilon$$

$$\lim_{i \rightarrow \infty} |x[i+1]| < \infty$$

Thus $|x[i]|$ has no bound, so the system is not stable.

Note that in the scalar case, as long as $|\lambda| < 1$ for the system $x[i+1] = \lambda x[i] + bu[i] + w[i]$, the system will be stable. Note that this is $\lambda < 1$, not $\lambda \leq 1$. That is because when $\lambda = 1$, we can see the errors will add up. It turns out that in the vector case, for the system $\vec{x}[t+1] = A\vec{x}[t] + B\vec{u}[t] + \vec{w}[t]$, the system will be stable if the eigenvalues of A are less than 1.

Proof 3 If $\exists n \vec{v}_i$ such that $A\vec{v}_i = \lambda_i \vec{v}_i$, then changing coordinates to the eigenbasis gives

$$\tilde{A} = \begin{bmatrix} \lambda_1 & & 0 \\ & \ddots & \\ 0 & & \lambda_n \end{bmatrix}$$

This means $\tilde{x}[t+1] = \tilde{A}\tilde{x}[t] + V^{-1}B\vec{u}[t] + V^{-1}\vec{w}[t]$ where V is the matrix whose columns are A 's eigenvectors. This is merely n different scalar cases, but we still have to make sure that $|\vec{w}[t]| < \epsilon \implies |V^{-1}\vec{w}[t]| < \kappa$ where κ is some bound. Lets say $m = V_{ij}^{-1}$ is the largest entry in V^{-1} . In the worst case all $\vec{w}_i[t]$ and all $V_{ij} = m$. Then $\forall i, [V^{-1}\vec{w}[t]]_i \leq nm\epsilon$ where n is the dimension of V , which means $|V^{-1}\vec{w}[t]| < \kappa$. Thus we can say that $\tilde{x}[t]$ is BIBO implies that $\tilde{x}[t]$ is BIBO.

2.3 Closed Loop Control

Lets say we have a system which is modeled by $\vec{x}[t+1] = A\vec{x}[t] + B\vec{u}[t] + \vec{w}[t]$. We must choose our inputs $\vec{u}[t]$ based on only $\vec{x}[t]$ since we can't observe the disturbances. How should we choose our inputs to control the system? If we try $\vec{u}[t] = k\vec{x}[t]$, then

$$\begin{aligned} \vec{x}[t+1] &= A\vec{x}[t] + Bk\vec{x}[t] + \vec{w}[t] \\ \vec{x}[t+1] &= (A + Bk)\vec{x}[t] + \vec{w}[t] \end{aligned}$$

Which means that if we choose K appropriately, we can potentially change the behavior of the system. Consider the following simple scalar case example

$$\begin{aligned} x[t+1] &= 3x[t] + u[t] + w[t] \\ u[t] &= kx[t] \\ x[t+1] &= (3+k)x[t] + w[t] \end{aligned} \quad c$$

Notice that even if the system is initially unstable, we can set our k to make it stable since the domain of $\lambda = 3+k$ is ∞ . What if we have a system $\vec{x}[t+1] = A\vec{x}[t] + \vec{b}u[t] + \vec{w}[t]$ where A, \vec{b} are controllable, but we only get a scalar input $u[t]$. Can we find a set of feedback gains $\vec{f}^T = [f_0, f_1, \dots, f_{k-1}]$ such that $u[t] = -\vec{f}^T \vec{x}[t]$ makes $A - \vec{b}\vec{f}^T$ have the eigenvalues we want?

We know how to easily solve scalar cases like $z[t+1] = az[t] + u[t]$, but it is hard to get this from a vector case because we only have a simple input, so we will be limited in how we can set our eigenvalues this way. Since this won't work, consider the following recursive system.

$$z[t+1] = a_{k-1}z[t] + a_{k-2}z[t-1] + \dots + a_0z[t-(k-1)] + u[t]$$

This is definitely controllable since our input $u[t]$ could potentially be any value in \mathbb{R} . Moreover, if we choose $u[t] = -\sum_{i=0}^{k-1} f_i z[t-(k-1)+i]$, we can create any recurrence relation we want. For example, if we wanted $z[t+1] = d_{k-1}z[t] +$

$d_{k-2}z[t-1] + \dots + d_0z[t-(k-1)]$, then $f_i = a_i - d_i$. Writing this in vector form, we get

$$\vec{z}[t+1] = A_z z[t] + \vec{b}u[t]$$

$$\vec{z}[t] = \begin{bmatrix} z[t-(k-1)] \\ \vdots \\ z[t-2] \\ z[t-1] \\ z[t] \end{bmatrix}$$

Notice that the vector $\vec{z}[t]$ here is different from the scalar $z[t]$ which it is made up of. Each "state" here is a scalar quantity, but to represent the recursive relationship properly, we collect all of the previous states in a vector to define the next state.

Given our definition of $\vec{z}[t]$ (which are the scalar values of previous states), we can fill in values for A_z and \vec{b}

$$A_z = \begin{bmatrix} 0 & 1 & 0 & 0 & \dots & 0 \\ 0 & 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 0 & 1 & \dots & 0 \\ \vdots & & & & \ddots & \vdots \\ a_0 & a_1 & a_2 & \dots & & a_{k-1} \end{bmatrix}, \vec{b} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 1 \end{bmatrix}$$

To understand where these come from, think of the A_z matrix "scrolling down" the state vector $\vec{z}[t]$ to get how it influences $\vec{z}[t+1]$. All the rows except the last are 0's and 1's since the previous states can't change, but the last row determines the next state. Notice that all entries in the b-vector are 0 except the last since we can't affect the past with present control. We can assume $a_0 \neq 0$ since we defined the recurrence to have length k . Breaking A_z into its block components gives us some more insight to its structure.

$$A_z = \begin{bmatrix} 0 & | & I_{k-1} \\ \hline \vec{a}^T \end{bmatrix}$$

We can check through multiplication that this system will be controllable. When the A matrix of a system is in this form, we say it is in **Controllable Canonical Form**.

Let's try finding the eigenvalues of A_z . If A_z is large, it'll be hard to calculate the characteristic polynomial, so instead let's guess their form and figure them out that way.

$$\vec{v}_\lambda = \begin{bmatrix} 1 \\ * \\ * \\ \vdots \end{bmatrix}$$

Where $*$ is any element. We know $A_z \vec{v}_\lambda = \lambda v_\lambda$, and since A_z scrolls the vector down, we can see that the second $*$ must be λ . Applying this same logic to the second $*$, it must be λ^2 . Continuing this, we get

$$\vec{v}_\lambda = \begin{bmatrix} 1 \\ \lambda \\ \lambda^2 \\ \vdots \\ \lambda^{k-1} \end{bmatrix}$$

If we wanted to find the characteristic polynomial, we could look at the last entry in $A_z \vec{v}_\lambda$

$$\begin{aligned} \sum_{i=0}^{k-1} a_i \lambda_i &= \lambda * \lambda^{k-1} = \lambda_k \\ \lambda_k - \sum_{i=0}^{k-1} a_i \lambda_i &= \lambda * \lambda^{k-1} = 0 \end{aligned}$$

Now that we know about this matrix form, the question becomes: can we transform any controllable system with matrix A into controllable canonical form? (i.e can we make $\vec{x}[t+1] = A\vec{x}[t] + \vec{b}u[t]$ into $\vec{z}[t+1] = A_z\vec{z}[t] + \vec{b}_z u[t]$) We know that $A\vec{b}, A^2\vec{b}, \dots, A^{k-1}\vec{b}$ are linearly independent since our system is controllable. Let this define basis \mathbb{G} . If we write the matrix A in the basis of \mathbb{G} , we get $\tilde{A} = G^{-1}AG$. The naming choice is very appropriate here because this matrix multiplication will be painful by hand, so lets look for another way to get \tilde{A} .

Remember that any linear transformation is defined by what it does to the basis vectors. We know

$$\tilde{\vec{b}} = G^{-1}\vec{b} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \end{bmatrix}$$

since \vec{b} is the first basis vector of \mathbb{G} . Thus,

$$\tilde{A}\tilde{\vec{b}} = G^{-1}A\vec{b} = \begin{bmatrix} 0 \\ 1 \\ 0 \\ \vdots \end{bmatrix}, \quad \tilde{A}^2\tilde{\vec{b}} = G^{-1}A^2\vec{b} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ \vdots \end{bmatrix} \dots$$

This gives us k columns of \tilde{A} . For the last column must be a linear combination of all the basis vectors, so $\tilde{A}^k\tilde{\vec{b}} = \sum_{i=0}^{k-1} \alpha_i \tilde{A}^i\tilde{\vec{b}}$. This means

$$\tilde{A} = \begin{bmatrix} 0 & 0 & \dots & \alpha_0 \\ 1 & 0 & \dots & \alpha_1 \\ 0 & 1 & \dots & \alpha_2 \\ \vdots & & \ddots & \vdots \\ 0 & \dots & 1 & \alpha_{k-1} \end{bmatrix}$$

which is A_z^T . Now we have a basis \mathbb{G} with (\tilde{A}, \tilde{b}) , but we want a basis \mathbb{H} with $(\tilde{A}^T, \tilde{b}_z)$. We want \tilde{A}^T, \tilde{b}_z to be controllable, which means $\tilde{b}_z, \tilde{A}^T \tilde{b}_z, \dots, (\tilde{A}^T)^{k-1} \tilde{b}_z$ are linearly independent.

Let's construct a matrix H which will take us from a coordinates in basis \mathbb{H} to coordinates in the basis \mathbb{G} . **Important:** the matrix

$$\left[\begin{array}{c|c|c|c} \tilde{b}_z & \tilde{A}^T \tilde{b}_z & \dots & (\tilde{A}^T)^{k-1} \tilde{b}_z \end{array} \right]$$

is **not** the matrix H . To compute H , we have to see how it transforms the \mathbb{G} basis vectors.

Once we have the matrix H , to get $(\tilde{A}^T, \tilde{b}_z)$ from (A, \vec{b}) , we can apply the change of coordinates $G^{-1}H$ so $\vec{x}_z[t] = HG^{-1}\vec{x}[t]$ and put our entire system into controllable canonical form.

The reason we can't find HG^{-1} in a single-step and must go through an intermediary basis is because we might not know what our system will look like in canonical form.

2.4 Linearization

Up until now, we have been assuming our systems are linear. To understand what this means, we must first understand what linearity means.

First, let's define what we know as a function.

Definition 5 *A function is a simple mapping from a domain to a range (i.e. $y(t)=L(u(t))$). To evaluate $y(t)$, we only need to know $u(t)$, making the function "memory-less"*

Definition 6 *A function $f(x)$ is linear iff*

- $\forall \alpha, \forall x \in \mathbb{R}, f(\alpha x) = \alpha f(x)$ (Scaling)
- $\forall u, \forall v \in \mathbb{R}, f(u + v) = f(u) + f(v)$ (Superposition)

Notice that by this definition, any linear function must necessarily have $f(0) = 0$ since otherwise with $\alpha = 1, x = 0, f(1 * 0) = f(0) = 1 * f(0) \neq 0$. These conditions can be simplified down into a single expression $f(\alpha u + v) = \alpha f(u) + f(v), \forall u, \forall v, \forall \alpha \in \mathbb{R}$. If we can find a single setting of (u, v, α) for which this equation does not hold, then our function is not linear.

If we have a scalar nonlinear function we can linearize it in a simple way. Remember that the Taylor series expansion of a function around a certain point is

$$f(x) = \frac{f(c)}{0!} + \frac{f'(c)}{1!}(x - c) + \frac{f''(c)}{2!}(x - c)^2 + \dots = \sum_{i=0}^{\infty} \frac{f^{(i)}(c)}{i!}(x - c)^i$$

where c is some expansion point we choose. Let's say we choose some point x^* and decide to linearize around that point. The tangent line to the function is

$$f_L(x) = f'(x^*)(x - x^*) + f(x^*)$$

However, $f(0) \neq 0$, so this tangent line is still not linear. To linearize it, we can change coordinates.

$$\begin{aligned} m &= \left. \frac{df}{dx} \right|_x \\ f(x^* + \delta x) &= f(x^*) + m\delta x \\ \delta y &= f(x^* + \delta x) - f(x^*) \\ f(x^* + \delta x) &= f(x^*) + \delta y = f(x^*) + m\delta x \\ \delta y &= m\delta x \end{aligned}$$

Thus the linearized expression is in terms of the "error" δy , a.k.a how far it deviates from what it was at the point of linearization. While this makes sense for functions, how does it apply to systems. Systems are more than simple functions, they are functionals.

Definition 7 A functional $y(t) = L\{u(t)\}$ is a function which requires knowing the entire u in order to evaluate it.

A good example of a functional is

$$L\{u(t)\} = \int_{\tau-1}^{\tau} u(t) d\tau$$

The definition of linearity for functionals is virtually the same as for a normal function.

Definition 8 A system $L\{\}$ is linear iff

- $\forall \alpha \in \mathbb{R}, \forall u(t), L\{\alpha u(t)\} = \alpha L\{u(t)\}$ (Scaling)
- $\forall u(t), \forall v(t), L\{u(t) + v(t)\} = L\{u(t)\} + L\{v(t)\}$ (Superposition)

With this definition, we can now formally define how to linearize a non-linear system. Take the system $\frac{d}{dt}x(t) = f(x(t)) + bu(t)$ where f is a nonlinear function and b is a scalar multiplier

To linearize the system

1. Choose a constant with time input $u(t) = u^*$
2. Find a solution $x(t) = x^*$ to the system

$$\frac{dx^*}{dt} = f(x^*) + bu^* \implies f(x^*) = -bu^*$$

3. Linearize $f(x)$ around x^*

$$f(x) \approx f(x^*) + \left. \frac{df}{dx} \right|_{x^*} (x - x^*)$$

4. Use the linearization of f to make the differential equation linear

$$\frac{dx}{dt} = f(x^*) + \frac{df}{dx}|_{x^*}(x(t) - x^*) + bu(t)$$

$$\text{Let } \delta x = x(t) - x^*, \delta u = u(t) - u^*$$

$$\frac{d}{dt}(\delta x + x^*) = f(x^*) + \frac{df}{dx}|_{x^*}\delta x + b(u^* + \delta u)$$

$$\frac{d}{dt}\delta x = \cancel{f(x^*) + bu^*}^0 + \frac{df}{dx}|_{x^*}\delta x + b\delta u(t)$$

$$\frac{d}{dt}\delta x = \frac{df}{dx}|_{x^*}\delta x + b\delta u(t)$$

Note that this only works assuming that δx is small, so when linearizing our systems, we must check that this property is true otherwise our linearization may be invalid. To see why, consider the system $\frac{d}{dt} = -\sin(x)$. Try linearizing about $x^* = 0$.

$$\frac{d}{dt}\delta x = -\delta x$$

$$\therefore \delta x = \delta x(0)e^{-t}$$

Since δx is the "error" of our approximation, we can see that because $\delta x = \delta x(0)e^{-t}$ will grow smaller over time, meaning the system is stable, and our approximation is legitimate. However, if we linearize about $x^* = \pi$

$$\frac{d}{dt}\delta x = \delta x$$

$$\therefore \delta x = \delta x(0)e^t$$

and this will grow very large as time goes on, so our approximate will be illegitimate.

These concepts of linearization extend beyond simple 1D functions. For example, the linearization of a 2D function is

$$f(x^* + \delta x, u^* + \delta u) \approx f(x^*, u^*) + \frac{\partial f}{\partial x}|_{x^*, u^*}\delta x + \frac{\partial f}{\partial u}|_{x^*, u^*}\delta u$$

We can further generalize the idea of linearization to vector functions.

$$f(\vec{x}) = \begin{bmatrix} f_1(x_1, x_2) \\ f_2(x_1, x_2) \end{bmatrix} \text{ where } \vec{x} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

If we linearize each of the functions inside the vector, we get

$$\begin{aligned}
f(\vec{x}^* + \delta \vec{x}^*) &= \begin{bmatrix} f_1(x_1^* + \delta x_1, x_2^* + \delta x_2) \\ f_2(x_1^* + \delta x_1, x_2^* + \delta x_2) \end{bmatrix} \\
f_1(x_1^* + \delta x_1, x_2^* + \delta x_2) &\approx f_1(x_1^*, x_2^*) + \frac{\partial f_1}{\partial x_1} \Big|_{x_1^*, x_2^*} \delta x_1 + \frac{\partial f_1}{\partial x_2} \Big|_{x_1^*, x_2^*} \delta x_2 \\
f_2(x_1^* + \delta x_1, x_2^* + \delta x_2) &\approx f_2(x_1^*, x_2^*) + \frac{\partial f_2}{\partial x_1} \Big|_{x_1^*, x_2^*} \delta x_1 + \frac{\partial f_2}{\partial x_2} \Big|_{x_1^*, x_2^*} \delta x_2 \\
\therefore f(\vec{x}^* + \delta \vec{x}^*) &= \begin{bmatrix} f_1(x_1^* + \delta x_1, x_2^* + \delta x_2) \\ f_2(x_1^* + \delta x_1, x_2^* + \delta x_2) \end{bmatrix} = \begin{bmatrix} f_1(x_1^*, x_2^*) \\ f_2(x_1^*, x_2^*) \end{bmatrix} + \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix} \Big|_{x_1^*, x_2^*} \begin{bmatrix} \delta x_1 \\ \delta x_2 \end{bmatrix}
\end{aligned}$$

The matrix with partial derivatives is known as the **Jacobian** and is denoted either ∇f or J . Thus a succinct form the linearization of a vector system is

$$f(\vec{x}^* + \delta \vec{x}) = f(\vec{x}^*) + J_x f(\delta \vec{x})$$

For multiargument functions,

$$f(\vec{x}^* + \delta \vec{x}, \vec{u}^* + \delta \vec{u}) = f(\vec{x}^*, \vec{u}^*) + J_x \delta \vec{x} + J_u \delta \vec{u}$$