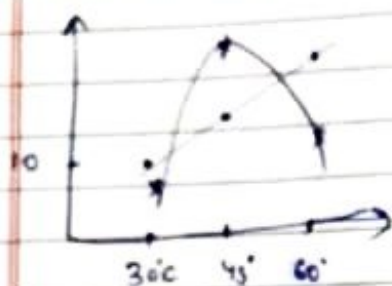


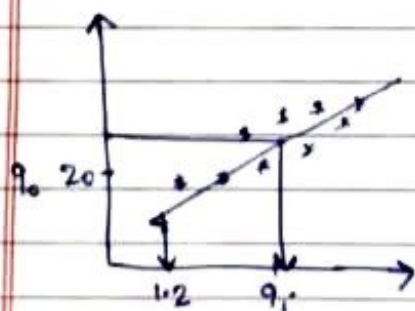
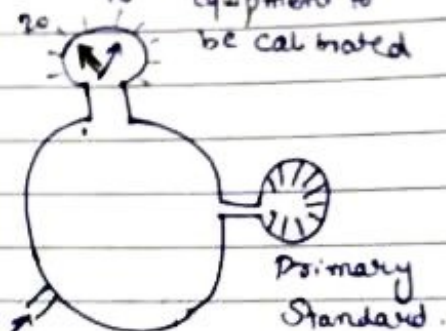
1/1/23.



What's wrong?
not taking into a/c errors

Random Variable \rightarrow Whatever we're measuring.

Equipment to be calibrated



q_0 = random variable

$\hat{q}_0 = m q_i + b$
Value on the fit-line

$$L = \sum (q_0 - \hat{q}_0)^2$$

$$\frac{dL}{dm} = 0 \quad \frac{dL}{db} = 0$$

$$m = \frac{N \sum q_i q_0 - \sum q_i \sum q_0}{[N \sum q_i^2 - (\sum q_i)^2]}$$

$$b = \frac{\sum q_0 \sum q_i^2 - (\sum q_i q_0) (\sum q_i)}{N \sum q_i^2 - (\sum q_i)^2}$$

N = Total no. of data points.

m & b are fⁿ of R.V. So, they are R.V. itself.
For R.V. we have to specify prob. distribution.

$$m = 12.3$$

$$s = 0.05$$

⇒ If we follow normal distribution, $\pm 3s$ (99%)

$$m = 12.3 \pm 0.15$$

$$Y = X + C$$

$$E(Y) = E(X) + E(C)$$

Expected value

$$V(Y) = V(X) + V(C) \rightarrow 0$$

$$S_m^2 = \frac{N(Sq_0)^2}{N \sum q_i^2 - (\sum q_i)^2}$$

$$S_b^2 = \frac{(Sq_0)^2 \sum q_i^2}{N \sum q_i^2 - (\sum q_i)^2}$$

$$S_{q_0}^2 = \frac{1}{N-2} \sum [(mq_i + b) - q_0]^2$$

Obs	q_i	q_0	q_i^2	$m, b = ?$	$q_i q_0$	Res.
1	0.19	3.8	0.0361		0.722	-0.90
2	0.40	10.4	0.16		4.16	1.85
3	0.63	15.1	0.3969		9.513	2.34
4	0.60	9.3	0.36		5.58	-2.91
5	0.78	14.6	0.60		11.388	-0.90
6	1.05	20.9	1.10		21.945	0.47
7	1.74	31.3	3.02		54.462	-1.75
8	1.62	32.7	2.62		52.974	1.24
	7.01	138.1	8.293		160.739	

$$m = \frac{8 \times 160.739 - 7.01 \times 138.1}{8 \times 8.293 - (7.01)^2} = 18.474$$

$$b = \frac{138.1 \times 8.293 - 160.739 \times 7.01}{8 \times 8.293 - (7.01)^2} = 18.482$$

a) 11/23.

$$\hat{q}_0 = ma + b$$

$$m = 18.28, S_m = 1.4 \text{ } 1.4034.$$

$$b = 1.24 \quad S_b = 1.3137.$$

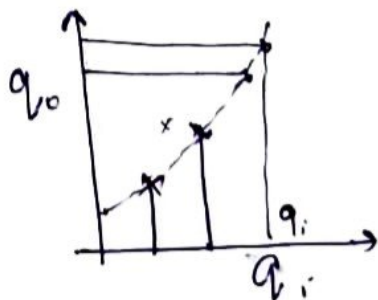
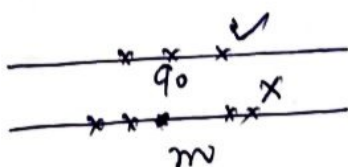
$$m = 18.28 \pm 4.2$$

$$b = 1.24 \pm 3.9$$

$$q_0 = 24.61 \quad q_i = 1.2781 \pm 3.99$$

$$Sq_i^2 = \frac{Sq_0^2}{m^2}$$

measure of spread is Std. Deviation.

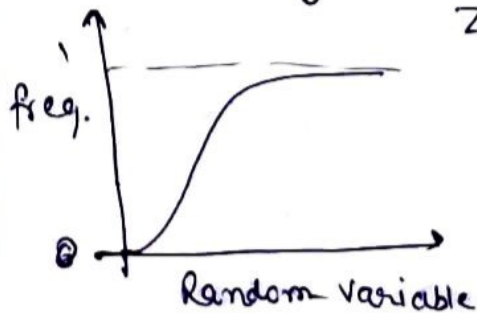


Spread of q_i
 $m = \text{slope}$.

$$\# Sq_i^2 = \frac{Sq_0^2}{m^2} = 0.113$$

Probability curve (plot)

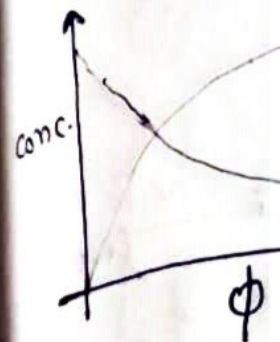
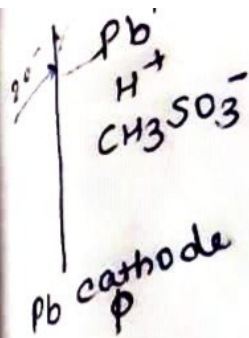
$Z = \text{normalised, cumulative freq}$



Norms inv \Rightarrow stretch y-axis so that plot look linear.

Differential Algebraic Eqⁿ

$$\text{Flux} = \text{Velocity} \times \text{density}.$$



11/23.

Drag force
 \rightarrow viscosity.

on giving
towards e

After

ions beco

chemical

Movement

2 Potenti

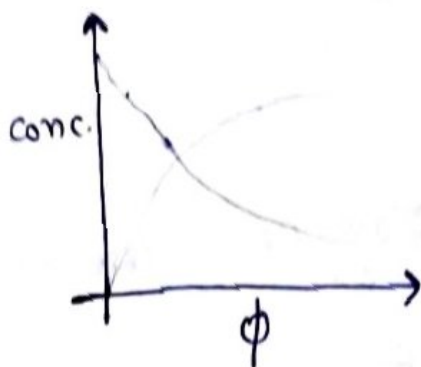
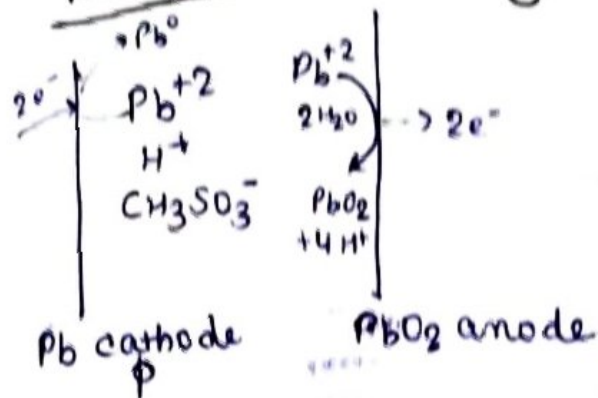
2 fluxes

\rightarrow diffusive

\rightarrow Migrati

- zE
Valence
of ion

Lead - acid Battery



$\phi \rightarrow$ potential

(e-)

10/11/23:

Develop model eqⁿ.

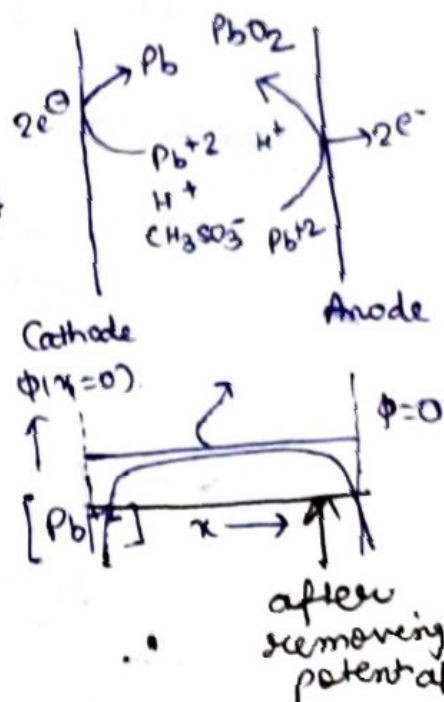
Drag force affected by.

\rightarrow viscosity.

On giving potential, ions move towards electrode because of ∇ gradient of potential

\Rightarrow Under After removing potential, ions become uniform coz of chemical potential.

Movement of ions governed by 2 potential i.e. chemical & electric.



\rightarrow 2 fluxes

\rightarrow diffusive

\rightarrow Migratory

(conc. diff)

(potential diff)

electric potential

$$-ze \frac{\partial \phi}{\partial x} = 6\pi R_s u \mu \rightarrow \text{drag force}$$

Valence of ion

$$\frac{\partial \bar{c}_i}{\partial t} = - \frac{\partial N_i}{\partial x} \rightarrow \text{Net flux}$$

conc. of ion

$$N_i = -D_i \frac{\partial C_i}{\partial x} + (\quad)$$

Diffusive flux

$$m \frac{1}{m^5} \cdot \frac{1}{m^2}$$

$$D_i^0 = \frac{RT \cdot \text{temp.}}{6\pi\eta R_s}$$

$$-z_i e \frac{\partial \phi}{\partial x} = \frac{RT}{D_i} u_i$$

$$u_i = - \frac{z_i D_i e}{RT} \frac{\partial \phi}{\partial x}$$

$$\begin{aligned} \text{Migration flux} &= - \frac{z_i D_i}{RT} \frac{\partial \phi}{\partial x} C_i \quad (N_e = F) \\ &= - \frac{z_i D_i F}{RT} \frac{\partial \phi}{\partial x} \end{aligned}$$

$$\frac{\partial C_i}{\partial t} = - \frac{\partial}{\partial x} \left[\frac{D_i}{RT} \frac{\partial \phi}{\partial x} C_i - \frac{z_i C_i D_i F}{RT} \frac{\partial \phi}{\partial x} \right]$$

$i=1,2,3$

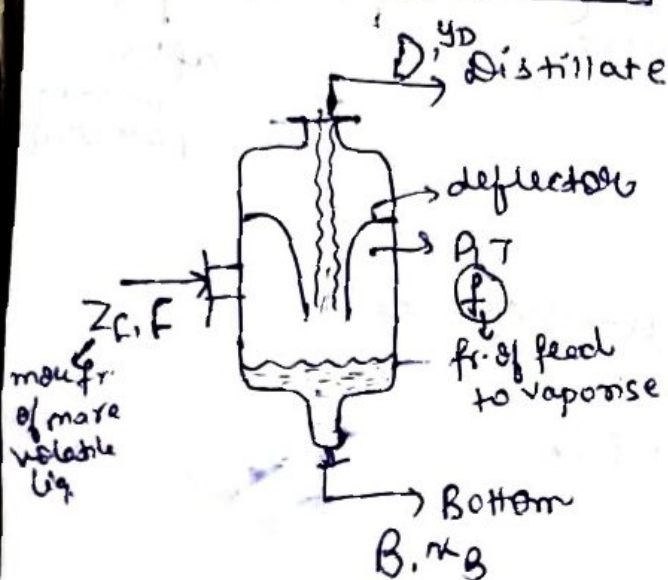
Condition of ElectroNeutrality:

Poisson's Eqⁿ

$$\nabla^2 \phi = - \frac{F}{\epsilon} \sum z_i C_i$$

very large ($\sim 10^{14}$)

$$\Rightarrow \boxed{\sum z_i C_i \approx 0}$$



$$F = D + B$$

$$F Z_F = D Y_D + B X_B \quad [\text{comp. balance}]$$

$$Z_F = f Y_D + (1-f) X_B$$

Assumption:-

- ① F is given (z, f) also.
- ② Relative volatility is constant.

$$y_D, x_B = ?$$

$$f = \frac{D}{F}$$

$$\alpha_{ij} = \frac{y_i x_j}{x_i y_j}$$

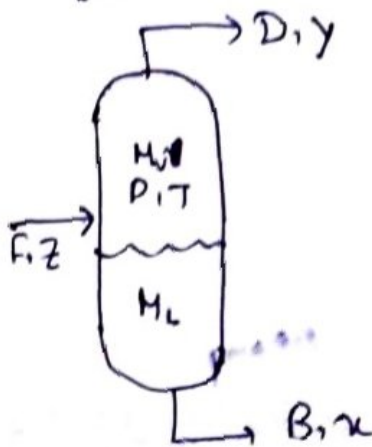
$$y_D = K_i x_B$$

$$y_{D,B} = \frac{\alpha x_B}{1 + (\alpha - 1) x_B}$$

change conc.

Transient state model

$$\frac{d}{dt} () = F z_f - (D y_D + B x_B) \cdot X$$



$$\frac{d}{dt} (M_v + M_l) = F - D - B$$

$$\frac{d}{dt} (M_i) = F z_i - D y_i - B x_i$$

Transient mass balance for this flash vessel & formulate close set of DAE.

At Steady state, $\frac{\partial C_i}{\partial t} = 0$. in et flux = constant.

~~$$D \frac{dC_1}{dx} + \frac{z_1 C_1 D f}{RT} \frac{d\phi}{dx} = k_1$$~~

$$D \frac{dC_1}{dx} + \frac{z_1 C_1 D f}{RT} \frac{d\phi}{dx} = k_1$$

$$D \frac{dC_2}{dx} + \frac{z_2 C_2 D f}{RT} \frac{d\phi}{dx} = k_2$$

$$D \frac{dC_3}{dx} + \frac{z_3 C_3 D f}{RT} \frac{d\phi}{dx} = k_3$$

$$z_1 C_1 + z_2 C_2 + z_3 C_3 = 0$$