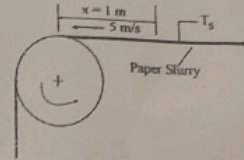


1. In a paper mill drying process, a sheet of paper slurry (water-fibre mixture) has a linear velocity of 5 m/s as it is rolled. Radiant heaters maintain a sheet temperature of $T_s = 330$ K, as evaporation occurs to dry, ambient air at 300 K, above and below the sheet. What is the evaporative flux at a distance of $x = 1$ m from the leading edge of the roll? What is the corresponding value of radiation flux (irradiation, G) that must be supplied to the sheet to maintain the temperature at 330 K? The sheet has an absorptivity of 1. Properties: Air ($T_f = 315$ K, 1 atm): $\gamma = 17.4 \times 10^{-6}$ m²/s, $k = 0.0274$ W/m.K, $Pr = 0.705$, Water vapor - Air ($T_f = 315$ K): $D_{AB} = 0.28 \times 10^{-4}$ m²/s, $Sc = 0.616$, Sat. water vapor ($T_s = 330$ K): $\rho_{A, sat} = 0.1134$ kg/m³, $h_{fg} = 2366$ kJ/kg



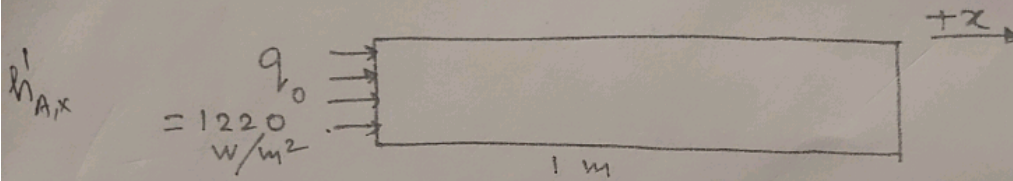
$$Sh_x = 0.332 Re_x^{1/2} Sc^{1/3} \quad \bar{Sh} = 0.664 Re_x^{1/2} Sc^{1/3}$$

Reynold's Analogy $St = \frac{C_{fx}}{2}$, $St = Nu/(Re.Pr)$; Chilton Coulburn Analogy $\frac{C_f}{2} = St.Pr^{1/3} = St_m.Sc^{1/3}$

Marks 10

2. Consider a wooden block (initial temperature = 25°C) of length 1m (as shown in figure below), whose one surface is exposed to constant solar flux of 1220 W/m². Determine the temperature of exposed surface after 20min. Consider only 1D heat transfer in +x direction. Properties of wood: thermal conductivity = 0.16 W/(m.K), thermal diffusivity = 1.8×10^{-7} m²/s. (You can skip the derivation, partial marking will be provided only for right approach).

Marks 10



Relations/Equations:

$$Sc = \frac{\mu}{\rho D_{AB}} \quad Sh = \frac{h_m l}{D_{AB}} \quad St = \frac{Nu}{Re.Pr} \quad Fo = \frac{\alpha t}{l^2} \quad Bi = \frac{hl}{k_s} \quad Le = \frac{\alpha}{D_{AB}} \quad C_f = \frac{\tau_w}{\frac{1}{2} \rho v^2} \quad C_D = \frac{F_D/A_p}{\frac{1}{2} \rho v^2}$$

Flow over flat plate

Laminar flow ($0.6 \leq Pr \leq 60$, $Re \leq 5 \times 10^5$) $\delta = \frac{5x}{\sqrt{Re_x}}$ $C_{fx} = \frac{0.664}{\sqrt{Re_x}}$ $C_{fL} = \frac{1.328}{\sqrt{Re_x}}$ $Nu_x = 0.332 Re_x^{1/2} Pr^{1/3}$ $\bar{Nu} = 0.664 Re_x^{1/2} Pr^{1/3}$

Turbulent flow $\delta = \frac{0.37x}{Re_x^{1/5}}$ $\frac{\bar{v}_z}{U} = \left(\frac{y}{R}\right)^{1/7}$ $C_{fx} = \frac{0.0577}{Re_x^{1/5}}$ ($Re \geq 5 \times 10^5$)

$Nu_x = 0.0296 Re_x^{4/5} Pr^{1/3}$ $\bar{Nu}_L = 0.037 Re_L^{4/5} Pr^{1/3}$

Mixed flow

$C_f = \frac{0.072}{Re_L^{1/5}} - \frac{1740}{Re_L}$ $Re \leq 10^7$ $C_D = \frac{0.455}{\log(Re_L)^{2.88}} - \frac{1610}{Re_L}$ $Re \geq 10^7$ $\bar{Nu}_L = \left(0.037 Re_L^{4/5} - 871\right) Pr^{1/3}$ $5 \times 10^5 \leq Re \leq 10^7$

Reynold's Analogy $St = \frac{C_{fx}}{2}$, $St = Nu/(Re.Pr)$; Chilton Coulburn Analogy

$$St \times Pr^{2/3} = \frac{C_{fx}}{2} \quad 0.5 \leq Pr \leq 50$$

error function: $erf(z) = \left(\frac{2}{\sqrt{\pi}}\right) \int_0^z \exp(-t^2) dt$, gamma function: $\Gamma(z) = \int_0^\infty t^{z-1} e^{-t} dt$, and $\Gamma(1/2) = \sqrt{\pi}$

complementary error function, $erfc(y) = 1 - erf(y)$, $erf(0) = 0$, $erf(\infty) = 1$.

$$\int erf_c(ay) dy = y(erfc(ay)) - \left(1/a\sqrt{\pi}\right) \exp(-a^2 y^2), \quad \frac{d(erf(y))}{dy} = \frac{2}{\sqrt{\pi}} \exp(-y^2)$$