INDIAN INSTITUTE OF TECHNOLOGY KHARAGPUR

End-Spring Semester 2023-2024 (Closed Book)

Course No.: CH 61016 Duration: 3 hrs
Course Title: Process Dynamics and Control Total Marks: 50

Department: Chemical Engineering

Instructions: 1. No need of graph paper, logbook 2. Assume any missing data

Answer all questions

- Q1. (a) Configure the override controller with a boiler system for steam pressure control showing all relevant elements.
 - (b) Find the action (direct/reverse) of the involved controllers when the control valve is in air-to-open mode.
 - (c) Perform the RGA analysis (with finding relative gain and relative gain array) for a chemical process example that involves one-way interaction. Does the RGA analysis truly show one-way/both-way/no interaction?
 - (d) The transfer function of a deethanizer is given as:

$$G_{p}(s) = \begin{bmatrix} \frac{1.318 e^{-2.4s}}{(18s+1)} & -\frac{e^{-4.2s}}{3s} \\ \frac{0.038(180s+1)}{(25s+1)(12s+1)(7s+1)} & \frac{0.36}{s} \end{bmatrix} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix}$$

Obtain the RGA for this system and use it to recommend loop pairing.

[2+1+(3+1)+3=10]

Q2. (3) Considering both measured disturbance d_1 and unmeasured disturbance d_2 , one can have $d(s) = g_d(s)d_1(s) + d_2(s)$

Derive the IMC control action in terms of u(s).

(b) Consider the following gain plus dead time process:

$$\overline{g} = \overline{k} e^{-\theta s}$$

- Design the IMC controller, using Pade approximation and simple factorization.
- Onnected with a first-order filter in series (g_c) that is equivalent to PID connected with a first-order filter in series
- (iii) Find the simplified expressions for PID parameters (k_c, τ_l, τ_D) and filter time constant (τ_F)
- (c) Derive the DMC control scheme for a CSTR (2×2 system) highlighting the computer-assisted sequential steps in details. Discuss the tuning heuristics of the multivariable DMC controller.

[2+(2+3+2)+(4+2)=15]

[Please Turn Over]

$$\frac{dC_b}{dt} = (\mu - F_d)C_b$$

$$\frac{dC_s}{dt} = F_d(C_{sf} - C_s) - \frac{\mu C_b}{P}$$

$$\mu = \frac{\mu_m C_s}{k_m + C_s + k_1 C_s^2}$$

Where, C_b and C_s are the biomass and substrate concentration respectively.

Derive linear state space model for the system to control C_b by manipulating

 F_d Show that this reactor is not fully state controllable irrespective of parameter and steady state values.

[2+4=6]

Consider the following system
$$\frac{dx_1}{dt} = a_{11}x_1 + a_{12}x_2$$

$$\frac{dx_2}{dt} = a_{21}x_1 + a_{22}x_2 + bu$$

$$v = x_2$$

- a) Derive reduced order state observer equation and corresponding error dynamics equation for the following system
- ★ b) Show that the reduced order observer controller system obeys separation principle
- x c) Derive the transfer function of reduced order observer controller system. [5+2+3=10]

Q5/ Consider the design of regulator system for the following process

$$\frac{dx_1}{dt} = x_2$$

$$\frac{dx_2}{dt} = 20.6 x_1 + 2u$$

$$y = x_1$$

- a) Find the state feedback controller gain in terms of desired pole location at μ_1 and μ_2 using Bass-Gura method.
- b) Determine optimal state feedback controller gain by minimizing the following performance index $J = \int_0^\infty (X^T X + u^2) dt$
- C) Determine the μ_1 and μ_2 based on the results obtained from a) and b) [Algebraic Riccati Eqn is $A^TP + PA - PBR^{-1}B^TP + Q = 0$]

[3+5+1=9]