

Group-S

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8.5/10

## INDIAN INSTITUTE OF TECHNOLOGY

DATE 8/08/23

SHEET NO. 1

Design of double pipe heat exchanger:  
(Hot) Engine oil

$$T_{H,in} = 120^\circ\text{C}$$

$$T_{H,out} = 65^\circ\text{C}$$

$$\dot{x} = 5 \text{ kg/s}, \Delta P_{\text{allowable}} = 80 \text{ kPa}$$

$$T_{H,avg} = \frac{120+65}{2} = 92.5^\circ\text{C}$$

$$R_o, \text{ fouling resistance} = 0.00018 \text{ m}^2\text{K/W}$$

SAE 15W-40.

Physical properties:

Heat capacity of oil,  $C_o =$ 

$$1.958 \text{ kJ/kg}$$

viscosity,  $\mu_o =$ 

$$13.77 \times 10^{-3} \text{ Pa.s}$$

thermal conductivity,  $k_o =$ 

$$0.145 \text{ W/m.K}$$

density,  $\rho_o =$ 

$$0.8336 \text{ g/cm}^3$$

Reference: Figshare.

(Cold) Seawater

$$T_{c,in} = 30^\circ\text{C}, T_{c,out} = 45^\circ\text{C}, T_{c,avg} = 37.5^\circ\text{C}$$

$$\Delta P_{\text{allowable}} = 65 \text{ kPa}$$

$$R_w = 0.0001 \text{ m}^2\text{K/W}$$

Physical properties,

 $C_w =$ 

$$4.18 \text{ — } 4.177 \text{ — } 4.179 \text{ kJ/kg}$$

 $\mu_w =$ 

$$0.000685 \text{ Pa.s}$$

 $k_w =$ 

$$0.63$$

 $\rho_w =$ 

$$993.18 \text{ kg/m}^3$$

Given, thermal conductivity for exchanger material =  $52 \text{ W/mK}$



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SHEET NO. 2.

$$LMTD = \frac{\Delta T_2 - \Delta T_1}{\ln \left( \frac{\Delta T_2}{\Delta T_1} \right)}$$

$\xrightarrow{T_{H,in}} 1$   
 $\xleftarrow{T_{C,out}}$

$\xrightarrow{2} T_{H,out}$   
 $\xleftarrow{T_{C,in}}$

$$= \frac{(120-45) - (65-30)}{\ln \left( \frac{75}{35} \right)} = \underline{\underline{52.48^\circ C}}$$

Let, mass flow rate of seawater be  $x$  kg/s.

$$Q_H = Q_C$$

$$5 \times C_p \Delta T_H = x C_w \Delta T_C$$

$$x = \frac{5 \times 55 \times C_p}{4.18 \times 15}$$

$$= \underline{\underline{8.59 \text{ kg/s}}}$$

$\therefore$  mass flow rate of water is greater than oil, so seawater should be kept inside and oil should be outside. Also cooling water should be inside because cooling water fouls severely. It is easier to clean/replace inner pipe because it can be removed easily, as compared to cleaning the annulus region which has a very small thickness.



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SHEET NO. 3

Standard dimensions of the pipe,

$$L = 6 \text{ m} = 1.83 \text{ m} \quad 6 \text{ m.}$$

$$D_i = 22.63 \text{ mm.}$$

$$D_o = 28.17 \text{ mm.}$$

$$D_{io} = 52.48 \text{ mm.}$$

For the inner pipe. (seawater is inside).

$$a_i = \frac{\pi D_i^2}{4} = 402.2156 \times 10^{-6} \text{ m}^2.$$

$$G_i = \dot{m}_i / a_i = 21,556.705 \text{ kg/m}^2\text{s}$$

$$Re_i = \frac{G_i D_i}{\mu_w} = 7.05 \times 10^5$$

we observed that the flow is turbulent

$$h_i = \frac{k \cdot 0.027}{D_e} Re^{0.8} Pr^{0.33} \left( \frac{\mu}{\mu_w} \right)^{0.14}, \quad Pr = \frac{C_p \mu}{k} = 4.54$$

 $\phi = \text{viscosity correction factor} = 1.$ 

$$h_i = 0.751 \times 47,703.61 \times (4.54)^{0.33}$$

$$= 0.751 \times 47,703.61 \times 1.647.$$



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SHEET NO 4

$$\begin{aligned}
 h_i &= 5.9 \times 10^4 \\
 \text{For oil in outside region,} \\
 D_e &= D_{i0} - D_o = 24.31 \text{ mm} \\
 a_o &= \frac{\pi (D_{i0}^2 - D_o^2)}{4} = 1539.8 \times 10^{-6} \text{ m}^2 \\
 G_o &= \dot{m} / a_o = 3247.17 \\
 Re_o &= \frac{G_o D_e}{\mu_o} = 5782.658
 \end{aligned}$$

$\therefore$  We can observe that the flow is ~~turbulent~~ <sup>transition</sup>.

Assuming  $\phi_o = 1$

$$\begin{aligned}
 h_o &= \frac{k}{D_e} 0.116 \left[ (Re)^{2/3} - 125 \right] (Pr)^{0.33} \left[ 1 + (D_i/L)^{2/3} \right] \\
 &= 0.6918 \times [195.31] \cdot \underbrace{(185.94)}_{5.707}^{0.33} [1.024] \\
 &= \underline{\underline{811.9724}} \quad \underline{\underline{753.031}}
 \end{aligned}$$

Now, the wall temperature,  $T_w$ ,



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SHEET NO. 5

$$T_w = \frac{h_i T_{i,avg} + h_o (D_o/D_i) T_{o,avg}}{h_i + h_o (D_o/D_i)}$$

$$= \frac{5.9 \times 10^4 \times 310.5 + \frac{753.03}{811.9724} (1.245) (365.5)}{5.9 \times 10^4 + \frac{753.03}{811.9724} (1.245)}$$

$$= \frac{38.4264 \times 310.5}{38.4264} K = 38.35^\circ C$$

→ for oil,

$$\mu_w \text{ at } T_w = 108.583 \times 10^{-3}$$

viscosity at wall temp.  $T_w$

$$\phi_i = \left( \mu / \mu_w \right)^{0.14} = 2.0134$$

$$h_i (\text{actual}) = h_i \phi_i = \frac{1.186 \times 10^5}{1}$$

→ for seawater:

$$\left( \frac{\mu}{\mu_w} \right)^{0.14} \approx 1$$

$$\frac{1}{U_o} = \frac{1}{h_o} + \frac{D_o}{h_i D_i} + \frac{D_o \ln(D_o/D_i)}{2K} + 0.00018 \times \frac{D_o}{D_i} + 0.0001$$

$$U_o = \frac{1}{\frac{1}{1.186 \times 10^5} + \frac{D_o}{h_i D_i} + \frac{D_o \ln(D_o/D_i)}{2K} + 0.00018 \times \frac{D_o}{D_i} + 0.0001}$$

$$U_o = \frac{1}{0.0012 + 0.0019 + 0.0001 + 0.0001} = 657.82$$



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SHEET NO. 6

So,

$$Q = U_o A_o \text{LMTD}$$

$$5 C_H \Delta T_H = U_o \pi D_o l \times 52.48$$

$$l = \frac{5 C_H \Delta T_H}{U_o \pi D_o \times 52.48}$$

$$= 154.23 \text{ m}$$

$$\therefore \text{No. of hair pins} = \frac{l}{12.12} = \frac{12.85}{25.7} \approx 13.$$

for the inner pipe,

$$\Delta P_i = H_{fi} \times f_i g$$

friction factor,  $f_i = 0.0043$

$$H_{fi} = \frac{4 f_i G_i^2 L}{2 \times g \times \rho_w^2 \times \phi_i} \approx 2.429 \text{ m}$$

$$\Delta P_i = \rho_w g H_{fi}$$

$$= 23.665 \text{ KPa}$$

for the outer pipe,

$$f_o =$$

$$= 0.0099$$



$$H_{fo} = \frac{4f_o G_o^2 L}{2 \times g f_o^2 \phi_o} = \underline{\underline{0.91 \text{ m}}}$$

oil velocity,  $v_o = G_o / f_o$   
 $= 3.89 \text{ m/s}$

$$H_{fo, \text{ bend}} = \frac{(2N_{\text{Hairpins}} - 1)}{2g} v_o^2 = (19.28) \text{ m}$$

$$\begin{aligned} \Delta P_o &= (H_{fo} + H_{fo, \text{ bend}}) f_o g \\ &= (0.91 + 19.28) f_o g \\ &= \underline{\underline{165.106 \text{ kPa}}} \quad \Delta P_{\text{765 kPa}} \end{aligned}$$

Result:

After taking different combinations,  
 of inner and outer pipe dimensions.

Final dimension chosen are

outer pipe  $\rightarrow D_{io} = 154.051 \text{ mm}$  (Nominal pipe size = 6)

inner pipe  $\left\{ \begin{array}{l} D_o = 88.9 \text{ mm} \\ D_{io} = 77.9272 \text{ mm} \end{array} \right.$  [Nominal pipe size = 3]

No. of Hairpins = 9  
 $\Delta P_o = 40.84 \text{ kPa}$



# DOUBLE PIPE HEAT EXCHANGER DATA SHEET

Group-5

UNITS OF MEASUREMENT : (SI)																							
1	Service Of Unit:			No Of Units: 4		Item No:																	
2	Site: Chemical Engineering Department			Manufacturer:		Group 5																	
3	Type	Arrangement	Shell	Parallel	Series: Tube	Parallel:	Series:	Yes															
4	Surface/Unit (Eff.)	m <sup>2</sup>		Section/Unit		Surface/Section (Eff.)		m															
PERFORMANCE OF ONE UNIT																							
6	Fluid Allocation																						
7	Fluid Name																						
8	Fluid Quantity, Total																						
9	Vapor (In/Out)			Kg/hr	SHELL SIDE		TUBE SIDE																
10	Liquid			Kg/hr	Engine oil		Seawater																
11	Steam			Kg/hr	18000		30,294																
12	Water			Kg/hr	18000		30,294																
13	Non-Condensate (Mw)			Kg/hr																			
14	Temperature			°C	120		65																
15	Density (Vapor/Liquid)			Kg/m <sup>3</sup>	833.16		998.18																
16	Viscosity (Vapor/Liquid)			cP	0.137		0.000685																
17	Molecular Weight			Kg/Kmol	1.958		4.179																
18	Specific Heat (Vapor/Liquid)			KJ/Kg°C	0.145		0.63																
19	Thermal Conductivity (Vapor/Liquid)			W/m°C	3.89																		
20	Surface Tension			Dyn/cm																			
21	Boiling Point			°C																			
22	Latent Heat			KJ/Kg																			
23	Inlet Pressure			barg																			
24	Velocity			m/s																			
25	Pressure Drop, Allowable/Calculated			bar																			
26	Fouling Resistance (Min.)			m <sup>2</sup> °C/W	0.00018		0.0001																
27	Heat Exchanged			MW																			
28	Transfer Rate			W/m <sup>2</sup> °C	MTD (Corrected) (Weighted)		°C																
CONSTRUCTION OF ONE SHELL																							
30				SHELL SIDE	TUBE SIDE	Sketch																	
31	Design Pressure barg			120/65	45/30																		
32	Design Temperature Max/Min °C																						
33	Corrosion Allowance mm																						
34	Insulation THK. In/Out mm																						
35	Connections In																						
36	Size & Out																						
37	Rating																						
38	Tube No.	O.D.	(mm);	Thk.	mm (Ave/Min)	Length	mm;	Pitch	mm;	Flow Angle	Deg												
39	Tube Type			Material																			
40	Fins:	No.	Height	mm;	Thk.	mm	Type	Material															
41	Shell	O.D.	mm;	Thk.	mm	Material																	
42	Tube Sheet - Stationary			Impingement Protection																			
43	Baffles-Cross			Type	%Cut	Spacing/c/c	mm;	Inlet	mm														
44	Shell Return Bend - Housing Material			Cover Material																			
45	Tube Side Closure - Type			Material																			
46	External Return Bend: OD			mm;	Thk.	mm;	Material																
47	Gasket - Shell Side			Tube Side																			
48	Code Requirements			Stamp NO																			
49	Double Pipe Type?			Multi Tube Type?																			
50	Remarks:																						
51																							
52																							
53																							
<table border="1"> <thead> <tr> <th>Rev.</th> <th>Date</th> <th>Description</th> <th>App.1</th> <th>App.2</th> <th>App.3</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>												Rev.	Date	Description	App.1	App.2	App.3						
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