

18/01/2023

# Dynamics of linear 1<sup>st</sup> order autonomous systems in State space domain

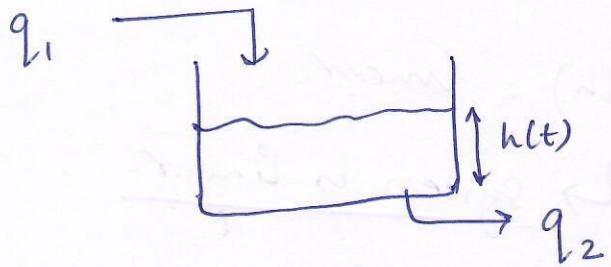
Q. State space domain = ??

Dynamical system = ??

State of system.

Example :- linear autonomous 1<sup>st</sup> order

$$\frac{dh}{dt} = \frac{1}{A} (q_1 - q_2)$$



order = 1 ;  $h(t)$  = dynamical variable

$q_1$  =  $\frac{V}{P}$  vol. flow rate ;  $A$  = cross-sectional area of tank

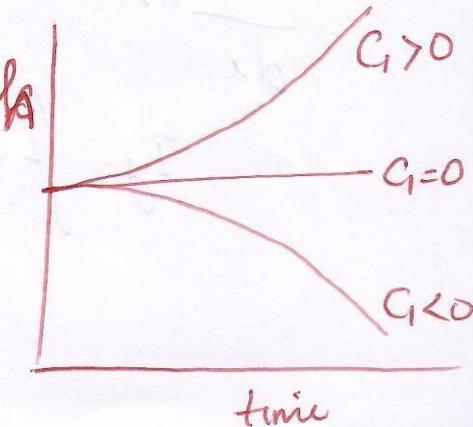
$q_2$  =  $\frac{O}{P}$  vol. flow rate

✓ time rate of change =  $\frac{V}{P} - \frac{O}{P} + \text{generation rate} - \text{consumption rate}$   
 (mass / momentum / energy)

Case I :-  $q_1 = q_2 = \text{constant}$

$$\frac{dh}{dt} = \frac{1}{A} (C_1 - C_2) \Rightarrow \frac{dh}{dt} = C$$

Linear system



$$\text{Case 2: } q_1 = \text{const.} = C_1$$

$$q_2 = f(h)$$

$$\frac{dh(t)}{dt} = \frac{1}{A} (C_1 - f(h))$$

$$\frac{dh}{dt} + \frac{1}{A} f(h) = \frac{C_1}{A}$$

if  $f(h) = \text{linear}$

$\hookrightarrow$  system is linear

Solve by integrating factor method

$$\frac{dy}{dx} + P y = Q$$

$$I = e^{\int P dx}$$

$$I \frac{dy}{dx} + I P y = IQ$$

$$\int (I \frac{dy}{dx} + I P y) dx = \int IQ dx$$

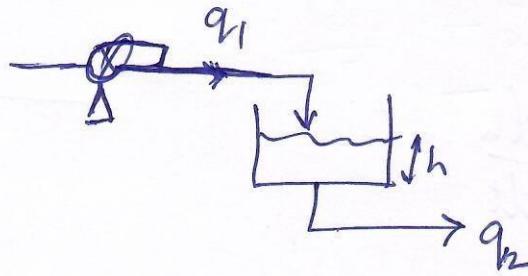
$$\frac{d(Iy)}{dx} \cdot dx = \int IQ dx$$

$$Iy = \int IQ dx$$

Case 3:-

$$q_1 = f(t)$$

$$q_2 = g(h)$$



$$\frac{dh}{dt} = \frac{1}{A} f(t) - \frac{1}{A} g(h)$$

$$\frac{dh}{dt} + \frac{1}{A} g(h) = \frac{1}{A} f(t)$$

If  $g(h) = \text{linear}$  then  
system is linear

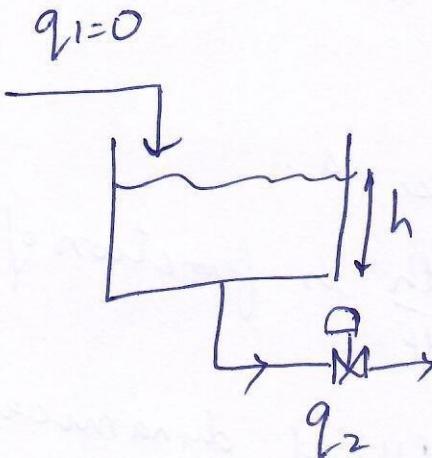
Solve by If method

Case 4 -

$$q_1 = 0$$

$$q_2 = ah$$

$$\frac{dh}{dt} = \frac{1}{A} (-ah) \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{let } -\frac{a}{A} = b$$



$$\boxed{\frac{dh}{dt} = bh}$$

specific case

case 1:

$$\frac{dh}{dt} = C \longrightarrow \frac{dx}{dt} = C$$

case 2:

$$\frac{dh}{dt} + \frac{1}{A} f(h) = \frac{C_1}{A} \longrightarrow \frac{dx}{dt} + \alpha f(x) = \beta$$
$$\frac{dx}{dt} = -\alpha f(x) + \beta$$

case 3:  $\frac{dh}{dt} + \frac{1}{A} g(h) = \frac{1}{A} f(t) \rightarrow \frac{dx}{dt} + \alpha g(x) = \beta f(t)$

$$\frac{dx}{dt} = -\alpha g(x) + \beta f(t)$$

case 4:  $\frac{dh}{dt} = bh \rightarrow \frac{dx}{dt} = bx$

In case 4.

$\frac{dh}{dt}$  is function of  $x$  only

⇒ RHS of dynamical eq<sup>n</sup> is a function of dynamical variable only = autonomous system.

## Phase portraits

linear 1<sup>st</sup> order autonomous system

$$\frac{dx}{dt} = ax \quad \left\{ \begin{array}{l} \text{(rate of change of} \\ \text{dynamical variable)} \end{array} \right. \text{is} \left\{ \begin{array}{l} \text{(function of} \\ \text{dynamical} \\ \text{variable)} \end{array} \right.$$

understand dynamical behaviour  $\equiv$  value of  $a$  is important

$$\text{if } a=1 \Rightarrow \frac{dx}{dt} = x$$

$$a=-1 \Rightarrow \frac{dx}{dt} = -x$$

$$a \in \mathbb{R} \quad (\text{infinitely no. of eqns})$$



process dynamics depends on this value

exponential function

$$x(t) = x_0 e^{at}$$

consti.

$x_0$  = initial condition

let  $x_0 = 1$

$a > 0$

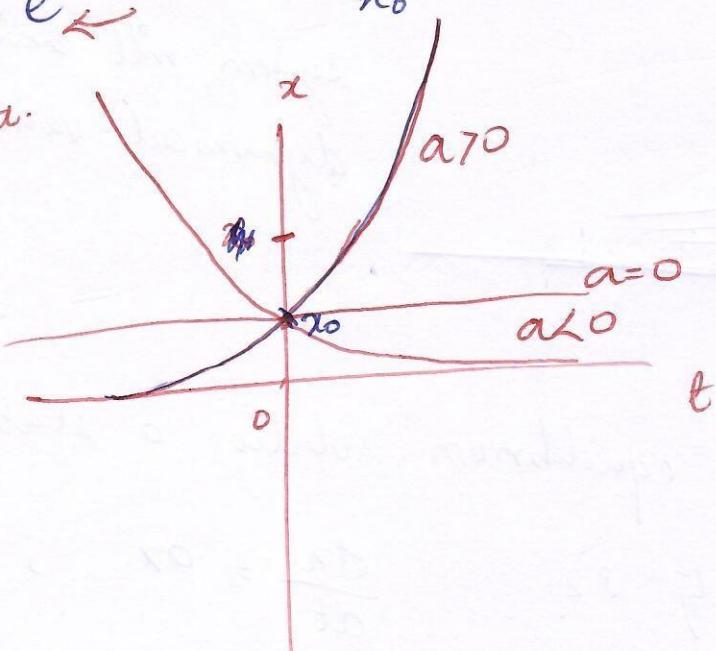
$x(t) \rightarrow \infty$

$a < 0$

$x(t) \rightarrow 0$

$a=0$

$x(t) = x_0$



phase portrait

↳ helps to predict system performance with time.

The system has opposite behaviour at  $t=0$  at both ends

Thus system has bifurcation

$$\therefore \frac{dx}{dt} = ax \quad \left\{ \begin{array}{ll} a > 0 & \lim_{t \rightarrow \infty} x(t) \rightarrow \infty \\ a < 0 & \lim_{t \rightarrow \infty} x(t) \rightarrow 0 \end{array} \right.$$

Thus system has bifurcation at  $a=0$

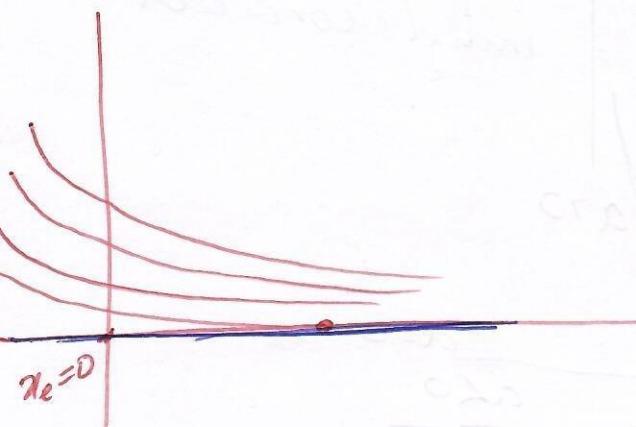
Equilibrium solution  $\Leftrightarrow$  gradient of system = 0

$$\frac{dx}{dt} = ax$$

$$\frac{dx}{dt} \Big|_{x_e} = 0 \Rightarrow ax = 0$$

$$x_e = 0$$

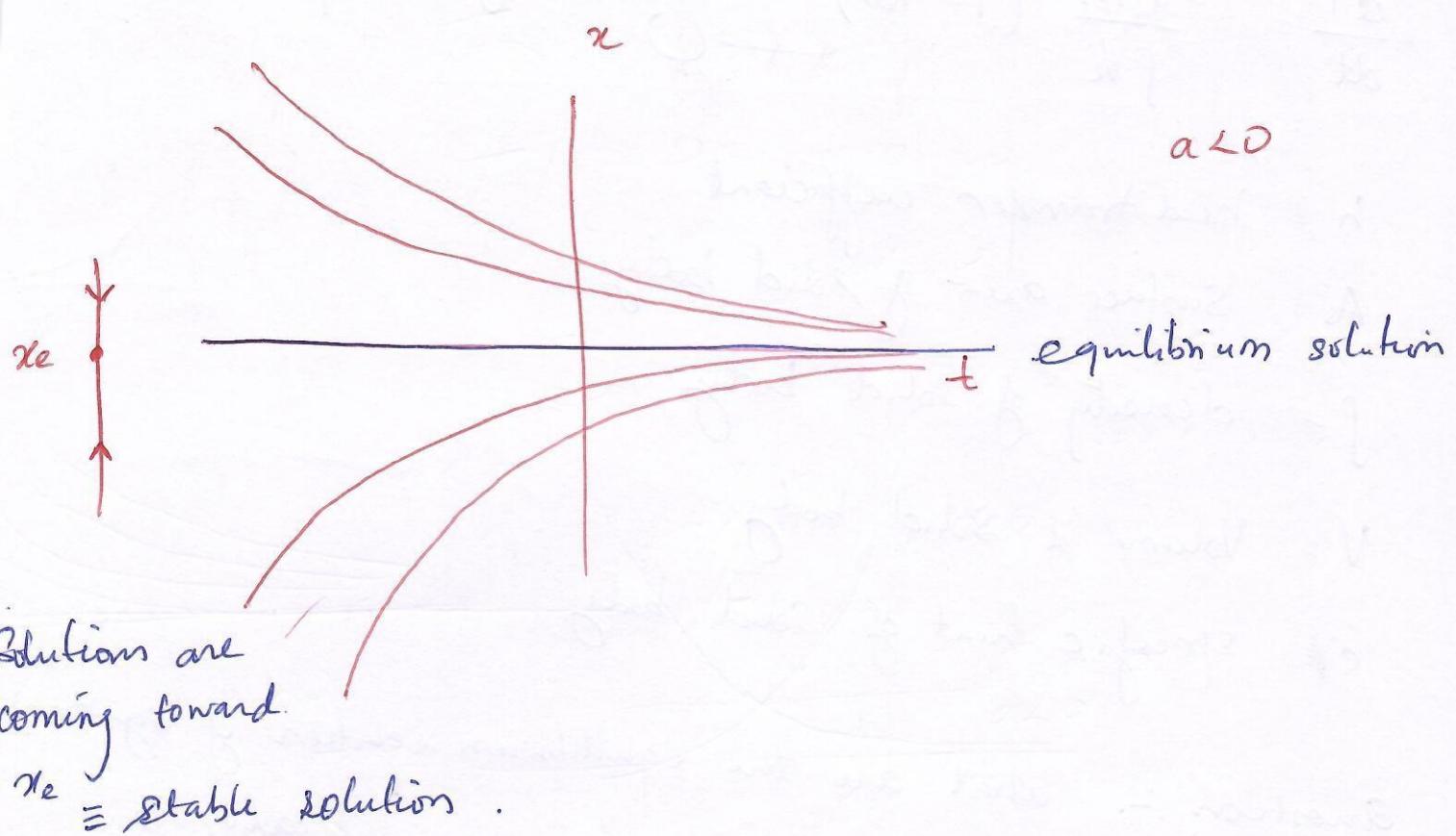
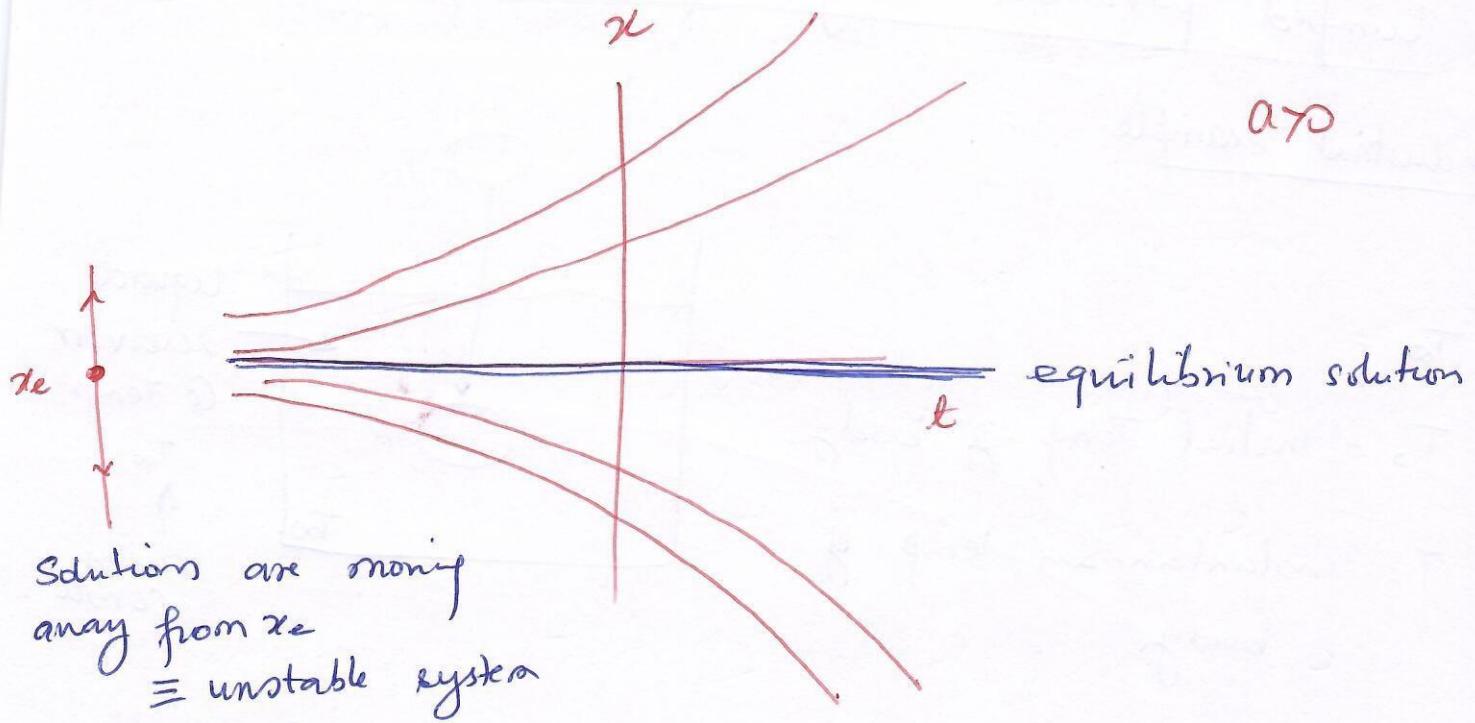
This means at point  $x_e$  the system will have same value of dynamical variable in future.



Is equilibrium solution a stable solution ??

stability ??  $\frac{dx}{dt} = ax ; x_e = 0$

with increase in time, system diverges from  $x_e = ??$



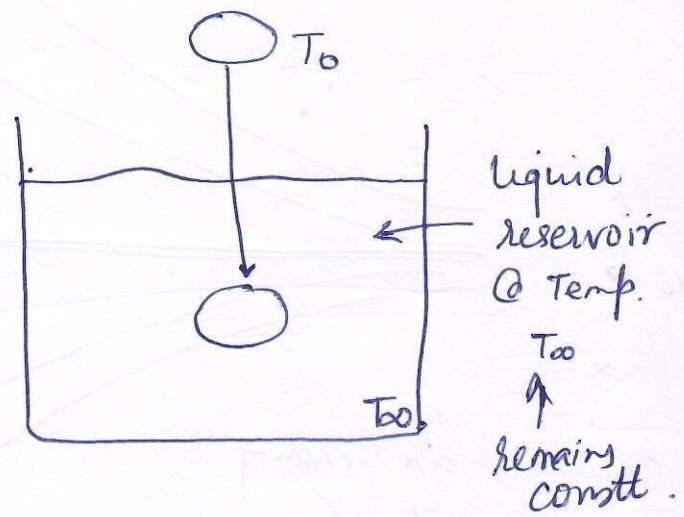
# Lumped parameters analysis of cooling of body

## Industrial example

$$T_{\infty} =$$

$T_{\infty}$  = initial Temp. of body

$T$  = instantaneous temp. of body



$$\frac{dT}{dt} = -\frac{hA_s}{\rho V c} (T - T_{\infty}) \quad \text{--- (1) governing eq^n}$$

$h$  = heat transfer coefficient.

$A_s$  = surface area of solid body

$\rho$  = density of solid body

$V$  = Volume of solid body

$c$  = specific heat of solid body

Question :- what are the equilibrium solution of system??

- solve model equation analytically to determine the time evolution of the system.
- Develop phase portrait for the system.

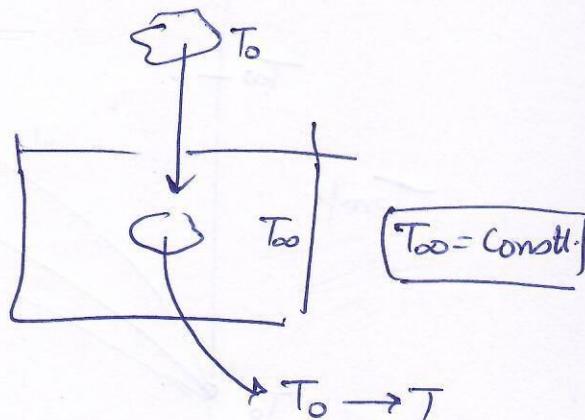
Consider  $\frac{hA_s}{PVc} = \alpha$  (constt.) — ②

$$\frac{dT}{dt} = -\alpha(T - T_{\infty}) \quad \text{— } ③$$

@  $x_e \frac{dx}{dt} = 0$

$$-\alpha(T - T_{\infty})/T_e = 0$$

$$T_e = T_{\infty} \Rightarrow ??$$



with time

$$\begin{aligned} T_0 &\rightarrow T_{\infty} \\ \& \text{ &} \\ T_e &= T_{\infty} \end{aligned}$$

$$\frac{dT}{dt} = -\alpha(T - T_{\infty})$$

$$T(0) = T_0$$

$$T^* = T - T_{\infty} \quad (\text{say}) \quad \text{— } ②$$

$T_{\infty}$  is constt

$$dT^* = dT \quad \text{— } ③$$

$$\frac{dT^*}{dt} = -\alpha T^* \Rightarrow T^* = C e^{-\alpha t}$$

$$T - T_{\infty} = C e^{-\alpha t} \quad \text{— }$$

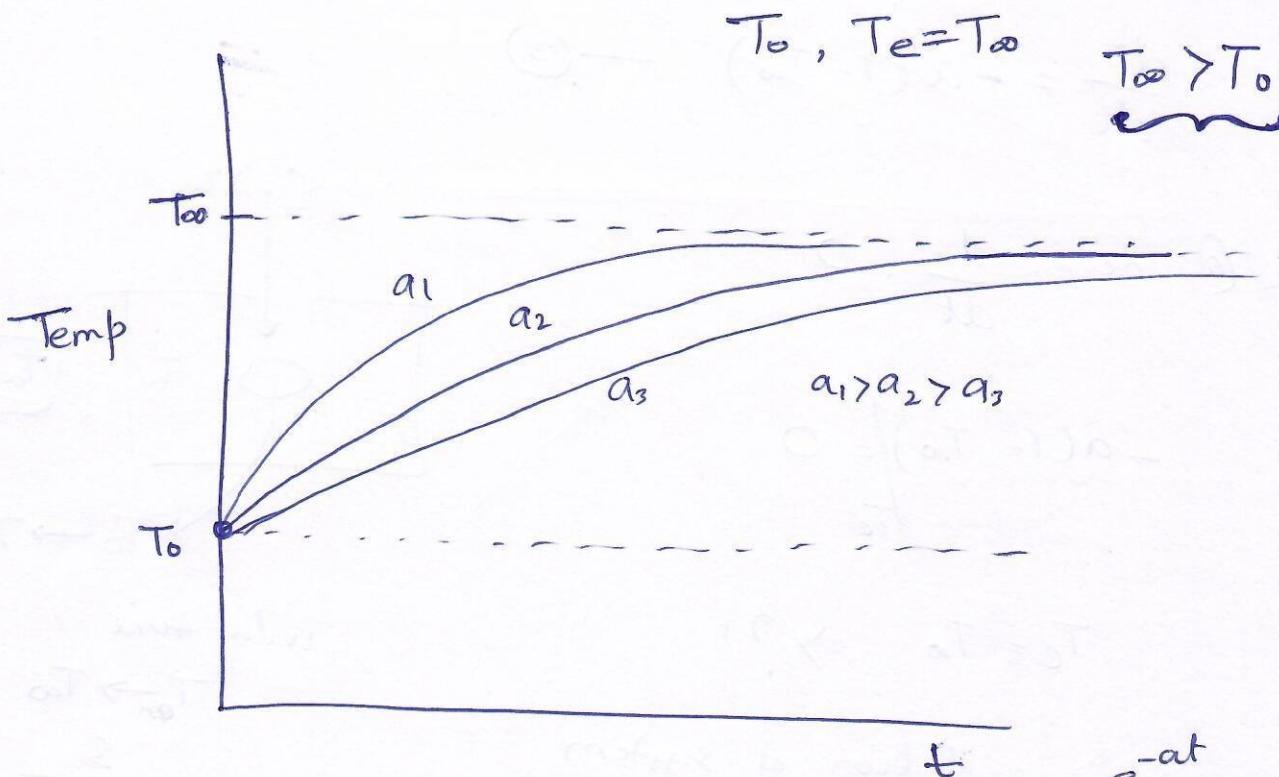
$$\left( \frac{dx}{dt} = -\alpha x \right)$$

$$\text{At } t=0 \Rightarrow T = T_0$$

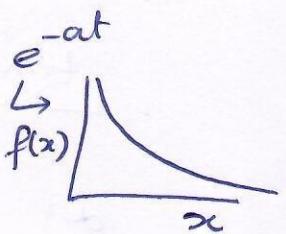
$$T_0 - T_{\infty} = C$$

$$T - T_{\infty} = (T_0 - T_{\infty}) e^{-\alpha t}$$

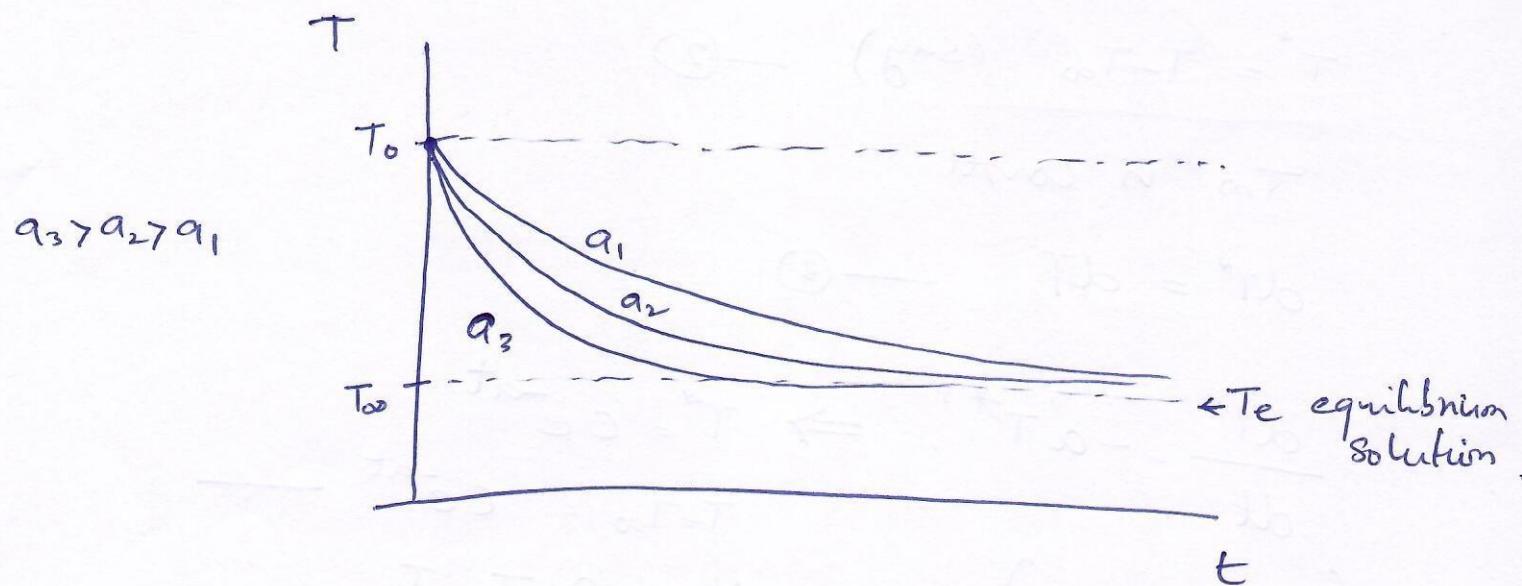
$$T(t) = T_\infty + (T_0 - T_\infty)e^{-at} \quad \leftarrow \text{model eqn solution}$$



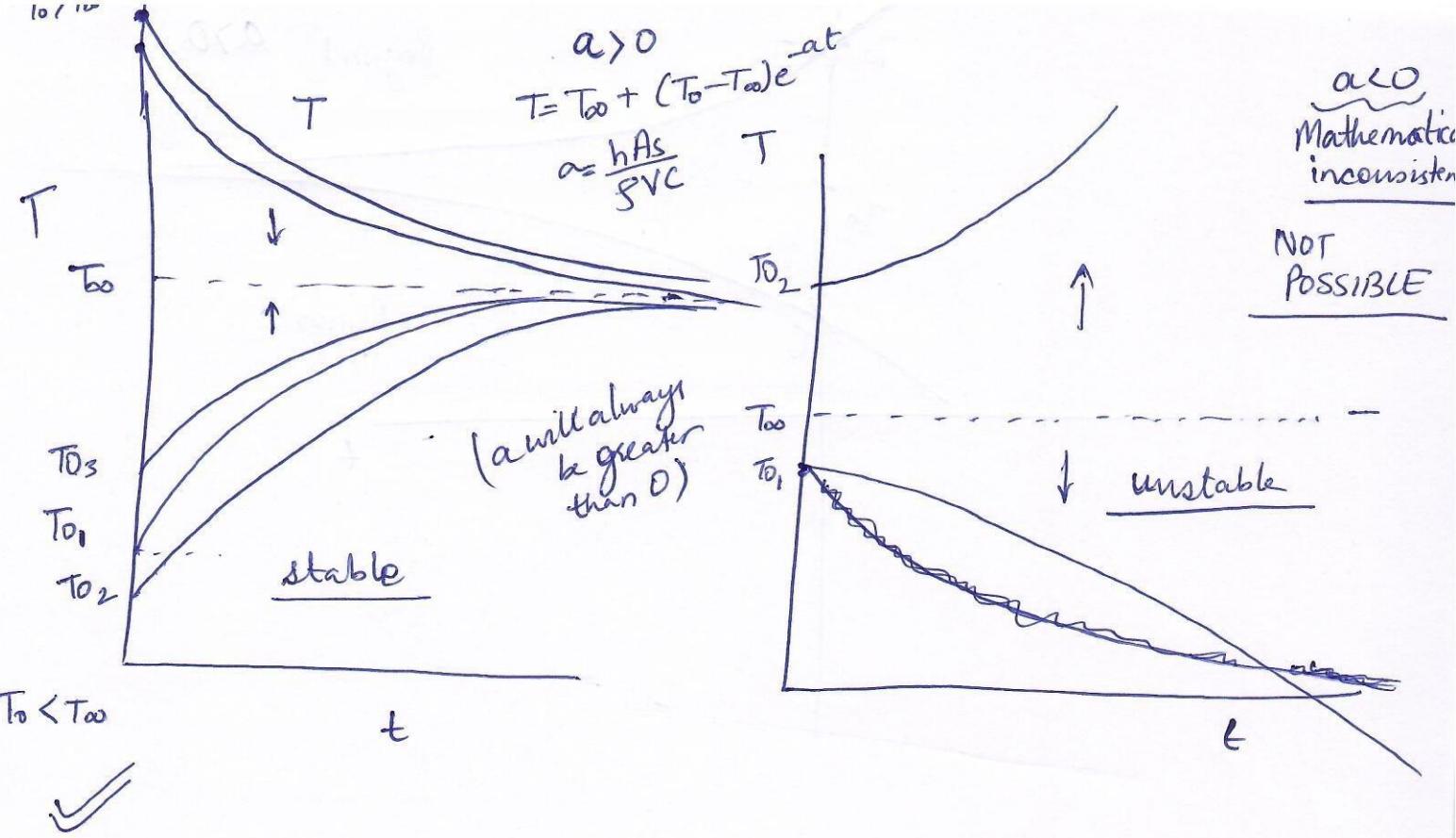
If  $a$  is large . . faster response



$$T(t) = T_\infty + (T_0 - T_\infty)e^{-at} \quad \leftarrow T_0 > T_\infty$$



Example :- hot plate quenched in oil bath

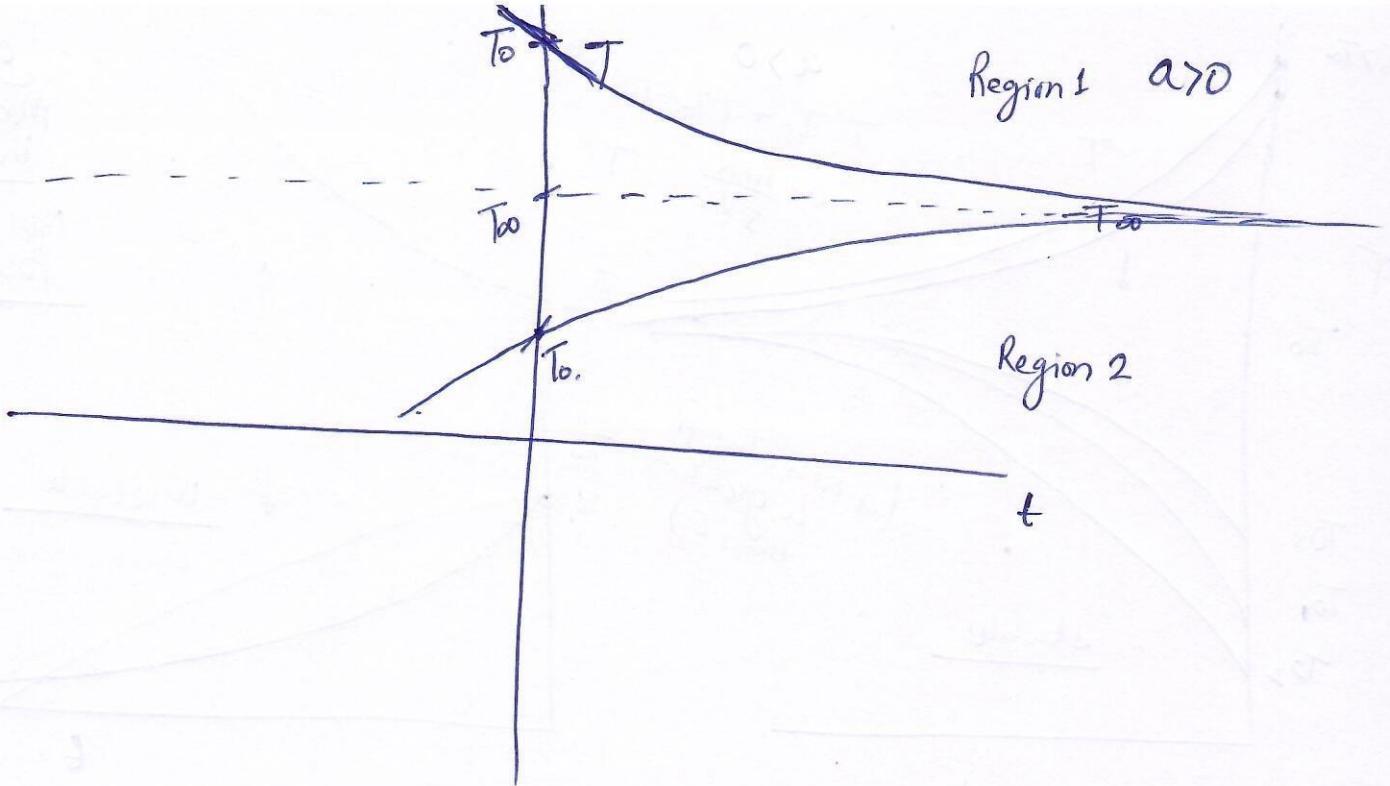


Q. How to develop phase portraits w/o solving governing eq' ??

- Analyse the solution & phase ~~portraits~~ portraits for  $T_0 < T_\infty$   
 $T_0 = T_\infty \leftarrow T_0 > T_\infty$
- Study the effect of different system & material property on system dynamics
- Comment on bifurcation in the system

$$\frac{dT}{dt} = -a(T - T_\infty) \quad \text{--- (1)}$$

If  $a > 0$



identify equilibrium solution

$$T_e = T_\infty \quad (\text{in this case})$$

$$\frac{dT}{dt} = -\alpha(T - T_\infty)$$

In Region 1

$$T > T_\infty$$

we know  $\alpha > 0$

$$T - T_\infty > 0$$

$$\frac{dT}{dt} = (-\alpha) \cdot (+ve)$$

- gradient is going to be  
-ve.

- But you need to reach  $T_\infty$   
as it is equilibrium  
solution

In Region 2

$$T_\infty > T$$

$\alpha > 0$  we know

$$\frac{dT}{dt} = (-\alpha)(-ve) = +ve (x)$$

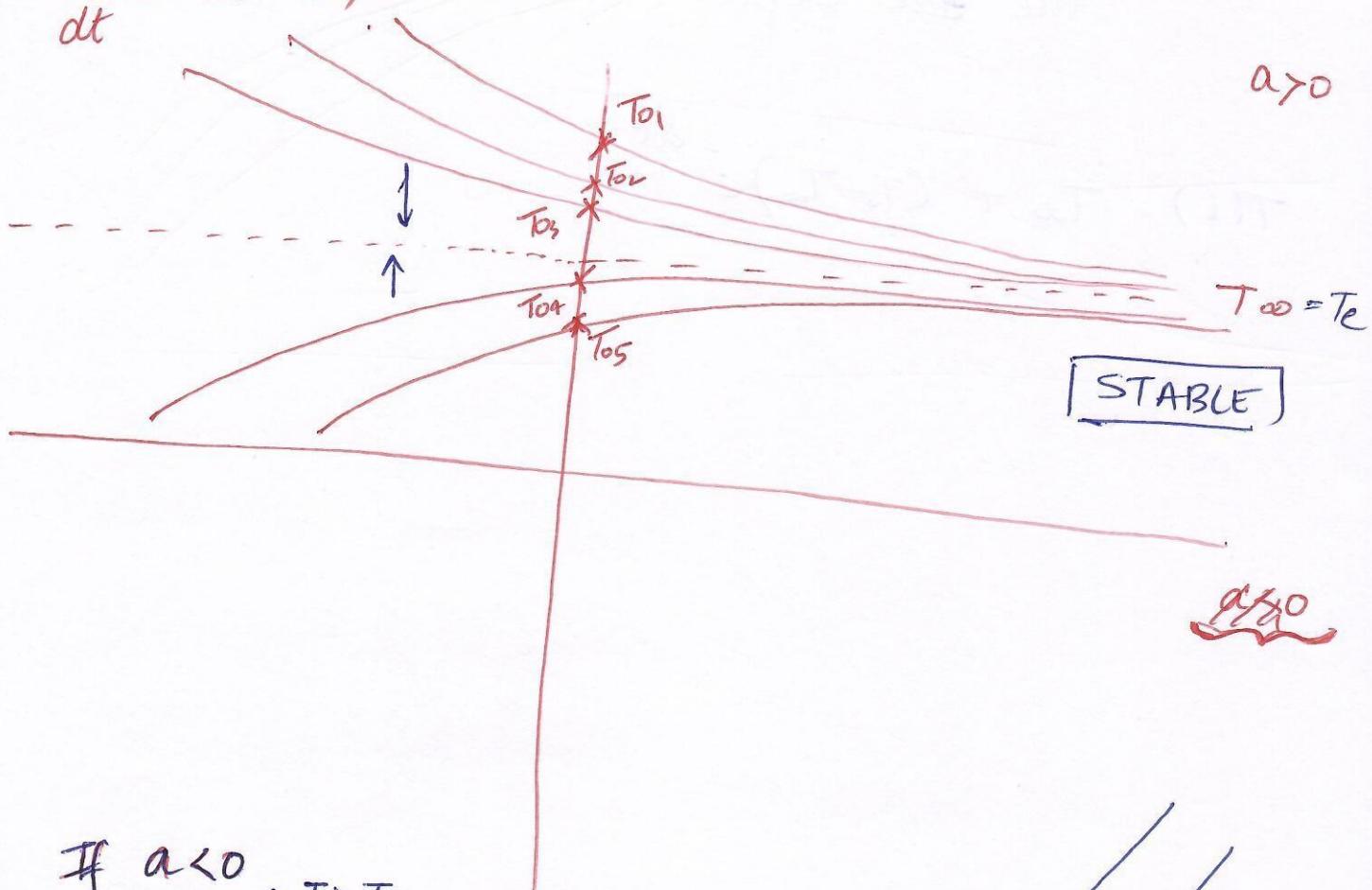
- gradient is always  
+ve

- reach  $T_\infty$  asymptotically

Although -ve time ~~is~~ does not exist in ~~our~~ real  
but mathematically it does.

So complete phase portrait is

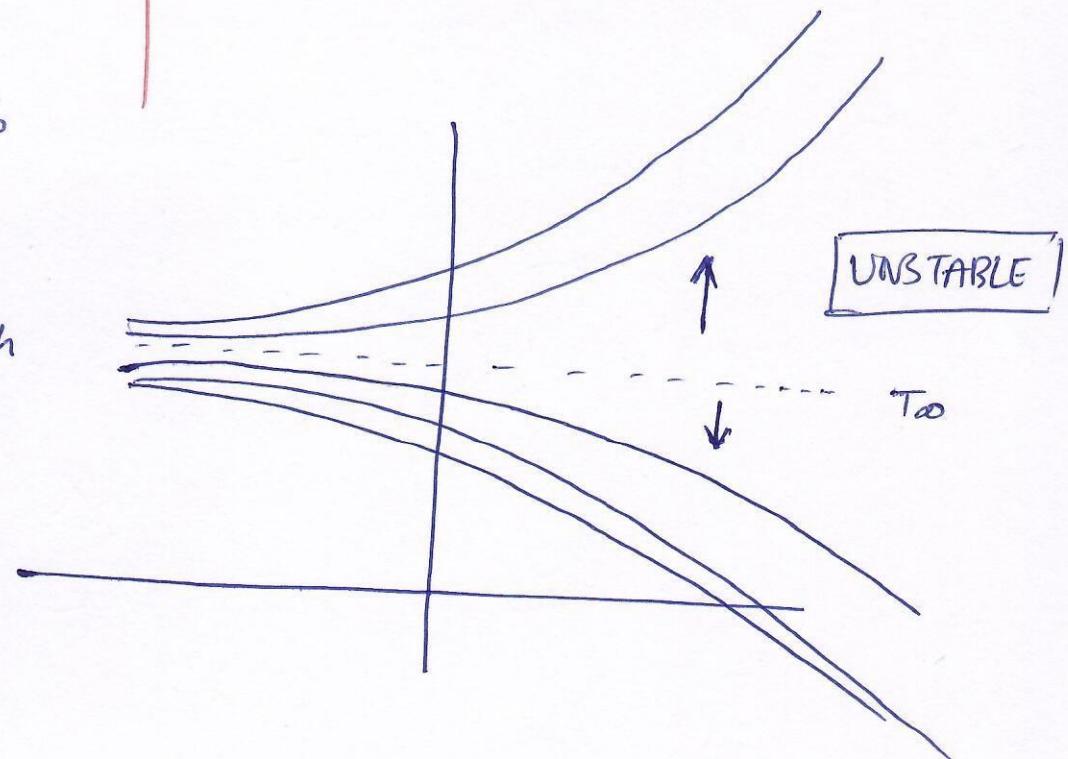
$$\frac{dT}{dt} = -\alpha(T-T_{\infty})$$



If  $\alpha < 0$ ,  $T > T_{\infty}$

$$\frac{dT}{dt} = +ve$$

gradient  $\uparrow$  with  
time

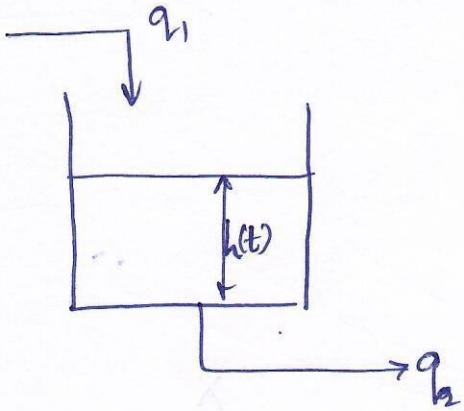


SYSTEM HAS BIFURCATION AT  
 $\alpha = 0$

Question :- if we draw phase portrait w/o solving the model equations , how do we ensure that the <sup>curve</sup> ~~line~~ depict actual solution ?

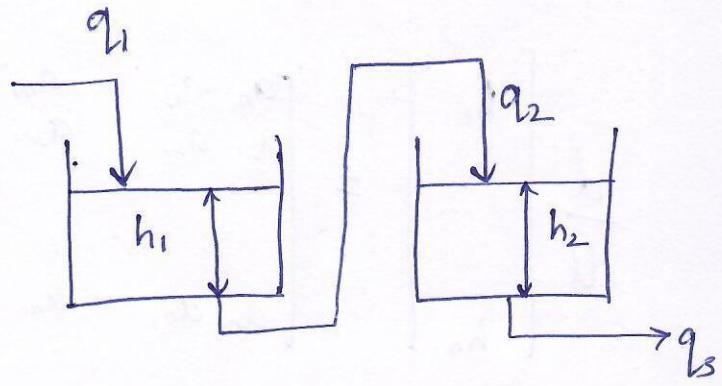
$$T(t) = T_{\infty} + (T_0 - T_{\infty}) e^{-at}$$

## Higher order systems



1<sup>st</sup> order

$$\frac{dh}{dt} = \frac{1}{A} (q_1 - q_2) \quad \text{--- (1)}$$



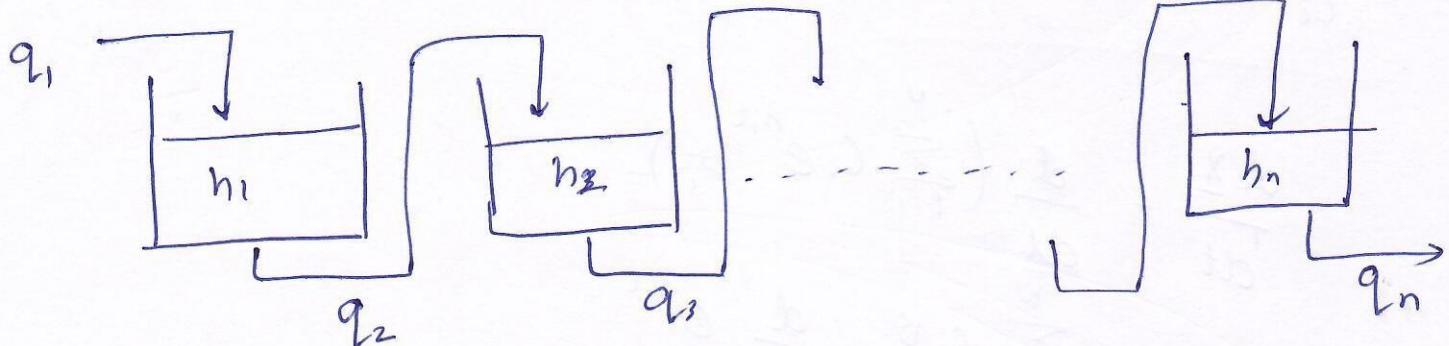
$$\frac{dh_1}{dt} = \frac{1}{A_1} (q_1 - q_2) \quad \text{--- (2)}$$

$$\frac{dh_2}{dt} = \frac{1}{A_2} (q_2 - q_3) \quad \text{--- (3)}$$

2<sup>nd</sup> order

Dynamical Variable =  $\begin{bmatrix} h_1(t) \\ h_2(t) \end{bmatrix}$

for  $n^{\text{th}}$  order



$$\frac{dh_1}{dt} = \frac{1}{A_1} (q_1 - q_2)$$

$$\text{let } q_1 = 0; \quad q_2 = ah_1, \\ q_3 = bh_2$$

$$\frac{dh_2}{dt} = \frac{1}{A_2} (q_2 - q_3)$$

$$\Rightarrow \frac{dh_1}{dt} = -\frac{a}{A_1} h_1 \quad ; \quad \frac{dh_2}{dt} = \frac{1}{A} (ah_1 - bh_2)$$

(8)

$$\frac{d}{dt} \begin{bmatrix} h_1 \\ h_2 \\ \vdots \\ h_n \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} & \dots & a_{1N} \\ a_{21} & a_{22} & \dots & a_{2N} \\ \vdots & \vdots & & \vdots \\ a_{n1} & a_{n2} & \dots & a_{nn} \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ \vdots \\ h_n \end{bmatrix}$$

(n × n)

$$\frac{d\underline{X}}{dt} = \underline{\underline{A}} \underline{X}$$

Vector =  $\underline{\underline{X}}$   
 Matrix =  $\underline{\underline{A}}$

Solution

$$\underline{X} = \sum_{i=1}^N c_i e^{\lambda_i t} \underline{v}_i \quad -\textcircled{2}$$

$\lambda_i$  = eigen values of  $\underline{\underline{A}}$

$\underline{v}_i$  = eigen vectors

$c_i$  = constant multipliers.

$$\begin{aligned} \frac{d\underline{X}}{dt} &= \frac{d}{dt} \left( \sum_{i=1}^N c_i e^{\lambda_i t} \underline{v}_i \right) \\ &= \sum_{i=1}^N c_i \underline{v}_i \frac{d}{dt} e^{\lambda_i t} \\ &= \sum_{i=1}^N c_i \underline{v}_i \lambda_i e^{\lambda_i t} \\ &= \cancel{\sum c_i \underline{v}_i} = \sum_{i=1}^N c_i e^{\lambda_i t} (\lambda_i \underline{v}_i) \quad -\textcircled{3} \end{aligned}$$

$\uparrow$   
eigen values      eigen vector

$$\underline{A} \underline{v}_i = \lambda_i \underline{v}_i \longrightarrow (4)$$

$$\frac{d \underline{x}}{dt} = \sum_{i=1}^N c_i e^{\lambda_i t} (\underline{A} \underline{v}_i)$$

$$= \sum_{i=1}^N \underline{A} [c_i e^{\lambda_i t} \underline{v}_i]$$

$$= \underline{A} \sum_{i=1}^N c_i e^{\lambda_i t} \underline{v}_i$$

$$\frac{d \underline{x}}{dt} = \underline{A} \underline{x} \quad (5)$$

$$\text{Example} \quad = \frac{d x_1}{dt} = -2x_1 - 4x_2 + 2x_3$$

$$\frac{d x_2}{dt} = -2x_1 + x_2 + 2x_3$$

$$\frac{d x_3}{dt} = 4x_1 + 2x_2 + 5x_3$$

} 1st order  
autonomous  
coupled

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} -2 & -4 & 2 \\ -2 & 1 & 2 \\ 4 & 2 & 5 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

$$\frac{d \underline{x}}{dt} = \underline{A} \underline{x}$$

$$\begin{aligned} \lambda_1 &= 3 & v_1 &= [2 \ -3 \ -1]' \\ \lambda_2 &= -5 & v_2 &= [2 \ -1 \ 1]' \\ \lambda_3 &= 6 & v_3 &= [1 \ 6 \ 16]' \end{aligned}$$

(9)

$$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = C_1 e^{3t} \begin{bmatrix} 2 \\ -3 \\ -1 \end{bmatrix} + C_2 e^{-5t} \begin{bmatrix} 2 \\ -1 \\ 1 \end{bmatrix} + C_3 e^{6t} \begin{bmatrix} 1 \\ 6 \\ 16 \end{bmatrix}$$

If we know initial conditions  
then  $C_1, C_2, C_3$  can be determined.

Assume at  $t=0$ ,  $x_1(0) = x_2(0) = x_3(0) = 0$

$$C_1 =$$

$$C_2 =$$

$$C_3 =$$

Do it Yourself.

### Phase plane analysis

$$\frac{dx}{dt} = Ax$$

eigen value of

$\frac{dx}{dt}$   $\rightarrow$  bifurcation at 'a'

Case 2 If  $a > 0 ; b < 0 \rightarrow \text{DIY}$

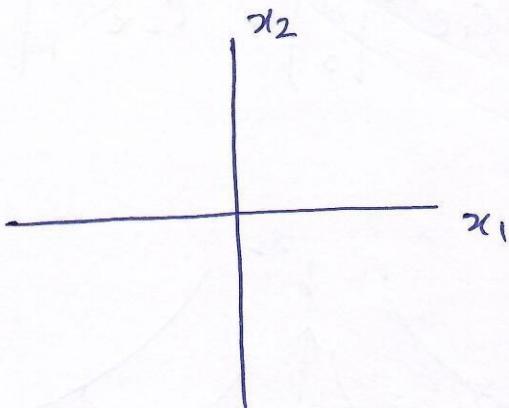
Saddle solution

One direction is stable other unstable

Case 3

$a > 0 \quad b > 0 \rightarrow \text{DIY}$

$$a > b > 0$$



Both axes  
unstable

Case 4

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = c_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix} +$$

$$c_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$a > b > 0$$

$$\lim_{t \rightarrow \infty} e^{at} \rightarrow \infty$$

$$\lim_{t \rightarrow \infty} e^{bt} \rightarrow \infty$$

$$x_1 = c_1 e^{at} \Rightarrow dx_1 = c_1 a e^{at}$$

$$x_2 = c_2 e^{bt} \Rightarrow dx_2 = c_2 b e^{bt}$$

$$\frac{dx_2}{dx_1} = \frac{c_2 b}{c_1 a} e^{(b-a)t}$$

$$\frac{dx_2}{dx_1} = \left( \frac{c_2 b}{c_1 a} \right) e^{(b-a)t}$$

slope

now we have idea about how  
slope varies with time

$$b - a < 0$$

In case of ~~A~~ 2<sup>nd</sup> order system  $\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$   
 let  $\underline{A} = \begin{bmatrix} a & 0 \\ 0 & b \end{bmatrix}$   $\frac{dx}{dt} = \underline{A} \underline{x}$   
 diag. matrix

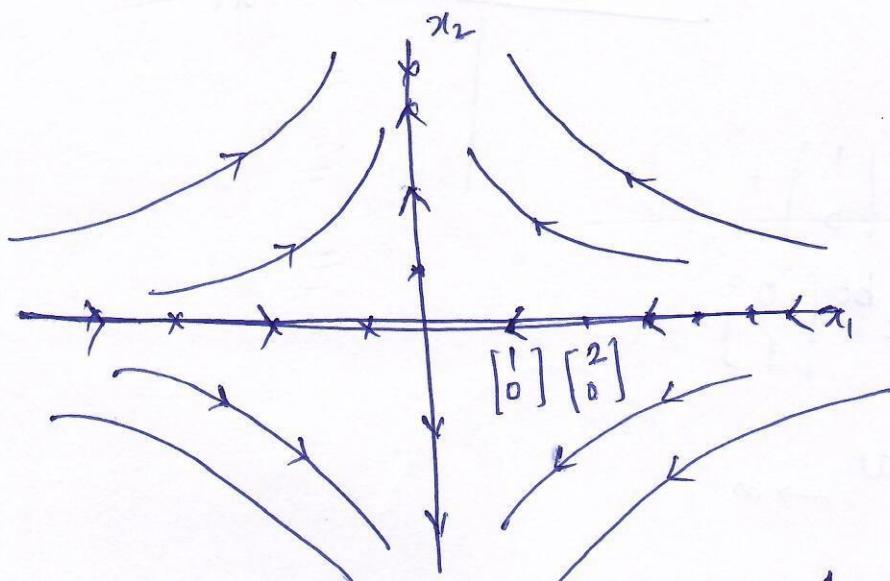
(diag. matrix)

$$\lambda_1 = a \quad v_1 = [1 \ 0]'$$

$$\lambda_2 = b \quad v_2 = [0 \ 1]'$$

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = C_1 e^{at} \begin{bmatrix} 1 \\ 0 \end{bmatrix} + C_2 e^{bt} \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

2



direction of arrow  
gives time  
evolution.

at  $t=0$ ; for  $C_2=0$

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = C_1 \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

at  $t=0$  for  $C_1=0$

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = C_2 \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

case 1a

at  $t=t$

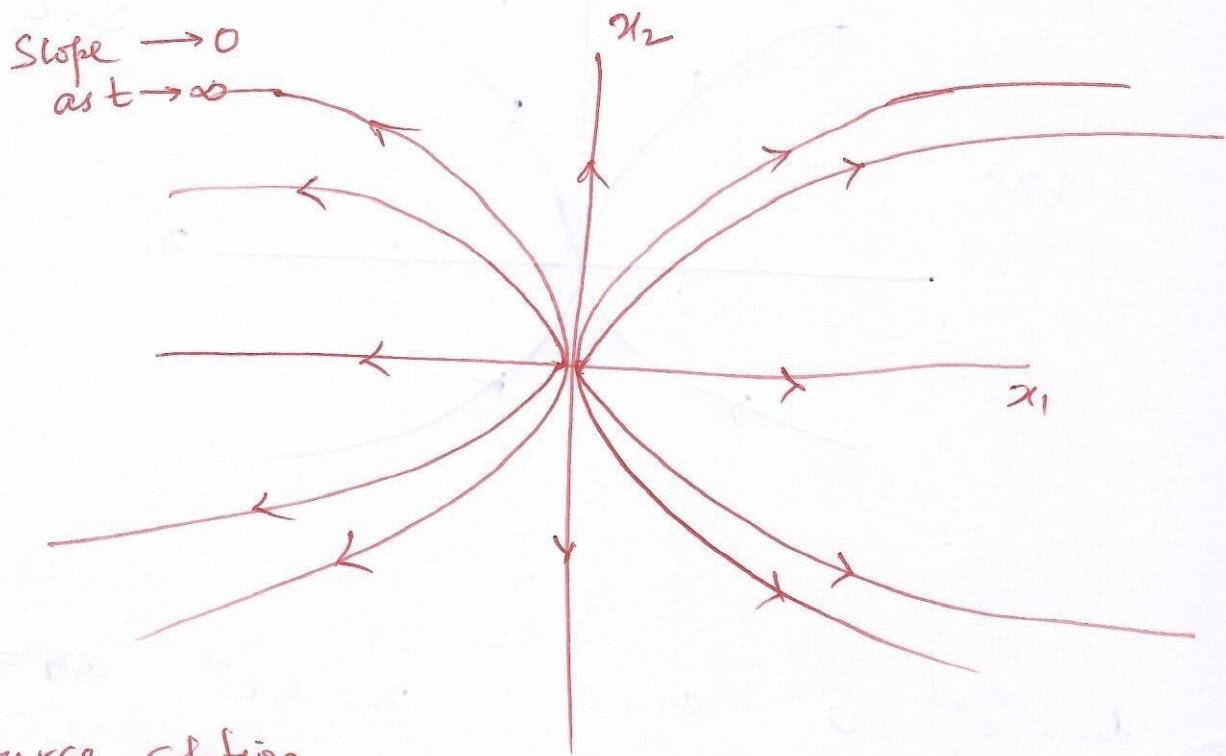
$$\boxed{[a < 0; b > 0]}$$

$\dim e^{at} = 0$  (stable)  
 $t \rightarrow \infty$

$\dim e^{bt} \rightarrow \infty$  (unstable)  
 $t \rightarrow \infty$

at equilibrium

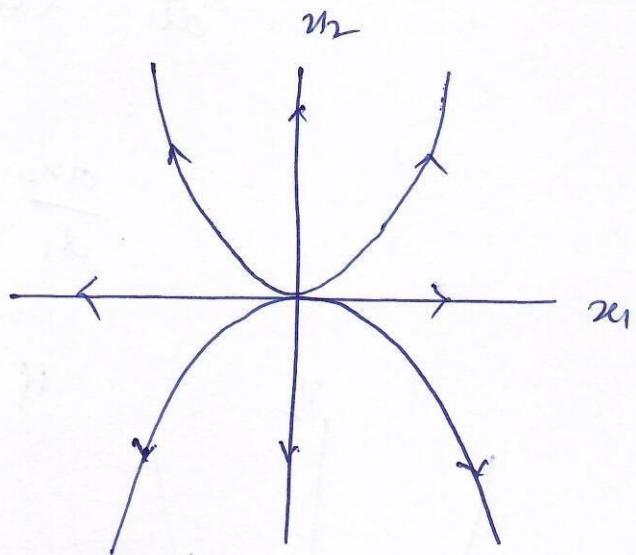
$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} a & 0 \\ 0 & b \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = 0$$



Source solution.

Case 5

$$b > a > 0$$

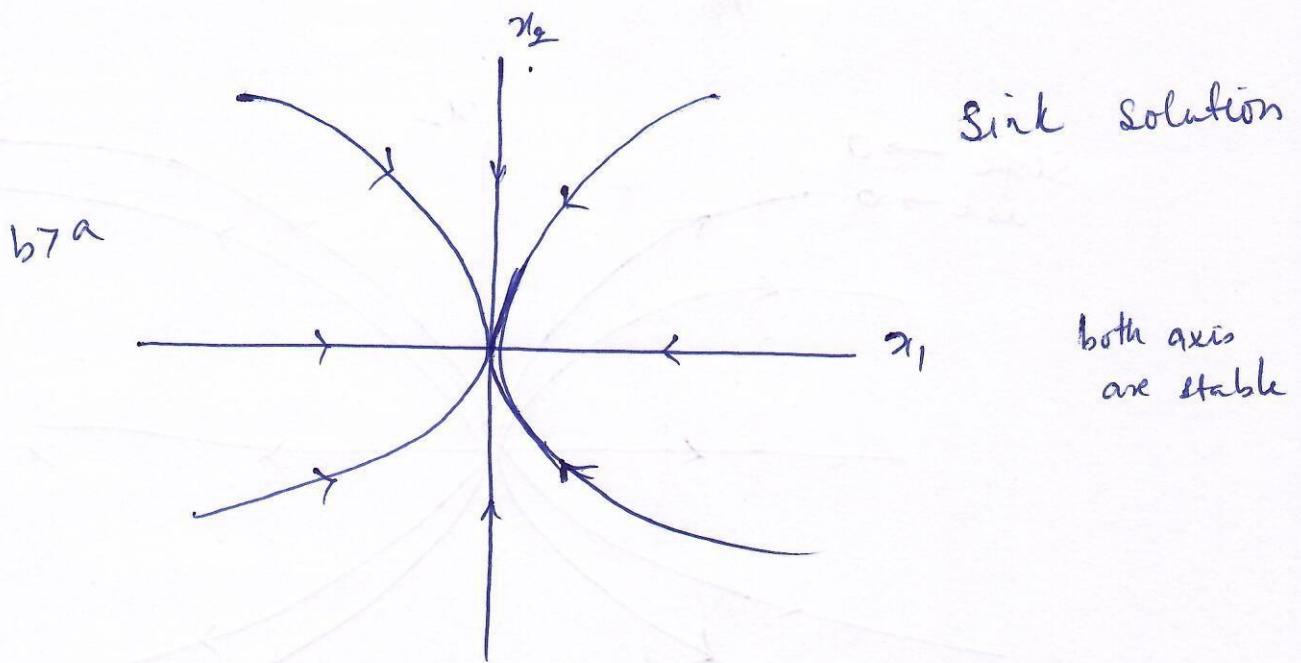


Case 6

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} a & 0 \\ 0 & b \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$a < 0 \quad b < 0$$

(ii)



$$\lim_{t \rightarrow \infty} e^{at} = 0 \quad a < 0$$

$$\lim_{t \rightarrow \infty} e^{bt} = 0 \quad b < 0$$

$$x_1 = c_1 e^{at} \quad dx_1 = c_1 a e^{at}$$

$$x_2 = c_2 e^{bt} \quad dx_2 = c_2 b e^{bt}$$

$$\frac{dx_2}{dx_1} = \left( \frac{c_2 b}{c_1 a} \right) e^{(b-a)t}$$

if  $b > a$

$$\frac{dx_2}{dx_1} \rightarrow \infty$$

