

Heat Exchanger

⑦

$$A \propto \frac{1}{\Delta T_{\text{LMTD}}}$$

$$80 \rightarrow 50$$

$$30 \rightarrow 45$$

$$\frac{A_{\text{counter}}}{A_{\text{cocurrent}}} \propto \frac{(\Delta T_{\text{LMTD}})_{\text{cocurrent}}}{(\Delta T_{\text{LMTD}})_{\text{counter}}}$$

$$= \frac{19.54}{26.8}$$

$$\therefore 1 - \frac{A_{\text{counter}}}{A_{\text{cocurrent}}} = \left[1 - \frac{(\Delta T_{\text{LMTD}})_{\text{cocurrent}}}{(\Delta T_{\text{LMTD}})_{\text{counter}}} \right] \times 100$$

$$= 0.271 \times 100$$

$$= 27.1\%$$

②

$$A = \frac{Q}{U_0 (\Delta T)_{\text{LMTD}}}$$

$$70 \rightarrow 40$$

$$40 \leftarrow 25$$

$$\Delta T_{\text{LMTD}} = \frac{30 - 15}{\ln(30/15)}$$

$$= 21.64$$

$$Q = \dot{m} c_p \Delta T$$

$$= \frac{1000}{3600} \times 2 \times 10^3 \times (70 - 40)$$

$$= 16.6 \text{ kW}$$

$$\therefore A = \frac{16.6 \times 10^3}{0.2 \times 10^3 \times 21.64}$$

$$\underline{\underline{A = 3.85 \text{ m}^2}}$$

③ $(\dot{m}c_p)_{\text{hot fluid}} = (\dot{m}c_p)_{\text{cold fluid}}$

$\Rightarrow T_1 - T_2 = t_2 - t_1$

$90 - 40 = t_2 - 10$

$t_2 = 60^\circ\text{C}$

$90 \longrightarrow 40$
 $t_2 \longrightarrow 10$

$\Delta T_{\text{LMTD}} = \frac{30 + 30}{2} = 30$

$U_i = \frac{Q}{A_i (\Delta T)_{\text{LMTD}}}$

$Q = (\dot{m} c_p)_{\text{water}} \Delta T = 1 \times 4.2 \times 10^3 \times 50 = 210 \text{ kW}$

$\therefore U_i = \frac{210 \times 10^3}{30 \times 3.14 \times 0.06 \times 5} = 7.427 \text{ kW/m}^2\text{K}$

1.

$$k = 43; \quad r_1 = 0.015; \quad r_2 = 0.04; \quad T_0 = 250^\circ\text{C}; \quad T_\infty = 35^\circ\text{C}; \quad h = 43$$

$$L = 0.025$$

$$L_c = 0.0255$$

$$r_{2c} = 0.0405$$

$$r_{2c}/r_1 = 2.7$$

$$L_c^{3/2}(h/kA_m)^{1/2} = 0.825$$

$$\eta_f = 0.59$$

$$q = (43)(2)\pi(0.0405^2 - 0.015^2)(250 - 35)(0.59) = 5.08 \text{ W}$$

2.

The general solution of eq. 2-19 (b) is:

$$\theta = T - T_{\infty} = c_1 e^{-mx} + c_2 e^{mx} \quad (1)$$

boundary conditions:

$$(1) \quad \text{at } x = 0 \quad \theta = \theta_1 = T_1 - T_{\infty}$$

$$(2) \quad \text{at } x = L \quad \theta = \theta_2 = T_2 - T_{\infty}$$

from:

$$(1) \quad \theta_1 = c_1 + c_2 \quad c_1 = \theta_1 - c_2$$

$$(2) \quad \theta_2 = c_1 e^{-mL} + c_2 e^{mL}$$

$$\theta_2 = (\theta_1 - c_2) e^{-mL} + c_2 e^{mL} = \theta_1 e^{-mL} - c_2 (e^{-mL} - e^{mL})$$

$$c_2 = \frac{\theta_2 - \theta_1 e^{-mL}}{e^{mL} - e^{-mL}} \quad (2)$$

$$c_1 = \theta_1 - c_2 = \theta_1 - \frac{\theta_2 - \theta_1 e^{-mL}}{e^{mL} - e^{-mL}}$$

$$c_1 = \frac{\theta_2 - \theta_1 e^{mL}}{e^{-mL} - e^{mL}} \quad (3)$$

Then eq. (1) becomes

$$\theta = \frac{\theta_2 - \theta_1 e^{mL}}{e^{-mL} - e^{mL}} e^{-mx} + \frac{\theta_2 - \theta_1 e^{-mL}}{e^{mL} - e^{-mL}} e^{mx}$$

$$\theta = \frac{e^{-mx}(\theta_2 - \theta_1 e^{mL}) + e^{mx}(\theta_1 e^{-mL} - \theta_2)}{e^{-mL} - e^{mL}}$$

Part heat lost by rod:

$$q = -kA \left. \frac{d\theta}{dx} \right|_{x=0} + kA \left. \frac{d\theta}{dx} \right|_{x=L}$$

$$\frac{d\theta}{dx} = m \left[\frac{-e^{-mx}(\theta_2 - \theta_1 e^{mL}) + e^{mx}(\theta_1 e^{-mL} - \theta_2)}{e^{-mL} - e^{mL}} \right]$$

$$q = \frac{kAm[-e^{-mL}(\theta_2 - \theta_1 e^{mL}) + e^{mL}(\theta_1 e^{-mL} - \theta_2)]}{e^{-mL} - e^{mL}}$$

$$+ \frac{kAm[-(\theta_2 - \theta_1 e^{mL}) + (\theta_1 e^{-mL} - \theta_2)]}{e^{-mL} - e^{mL}}$$

$$q = \frac{kAm[(\theta_2 - \theta_1 e^{mL})(1 - e^{-mL}) + (\theta_2 - \theta_1 e^{-mL})(1 - e^{mL})]}{e^{-mL} - e^{mL}}$$

$$\frac{d^2\theta}{dx^2} - \frac{hP}{kA}\theta = 0 \text{ let } m = \sqrt{\frac{hP}{kA}}$$

$$T_\infty = 38 \quad d = 12.5 \text{ mm} \quad L = 30 \text{ cm} \quad h = 17$$

$$\theta = c_1 e^{mx} + c_2 e^{-mx} \text{ at } x = 0 \quad \theta = 200 - 38 = 162 \quad k = 386$$

$$P = \pi d \quad A = \frac{\pi d^2}{4} \quad x = 0.3 \quad \theta = 93 - 38 = 55$$

$$m = \left[\frac{(17)\pi(0.0125)(4)}{(386)\pi(0.0125)^2} \right]^{1/2} = 3.754 \quad 162 = c_1 + c_2$$

$$55 = 3.084c_1 + 0.324c_2 \quad c_1 = 0.91 \quad c_2 = 161.09$$

$$\theta = 0.91e^{mx} + 161.09e^{-mx}$$

$$q \int_0^L hP\theta dx = hP \frac{1}{m} [0.91e^{mx} - 161.09e^{-mx}]_0^L = \sqrt{hPkA} [0.91e^{mx} - 161.09e^{-mx}]_0^{0.3}$$

$$= [(17)\pi(0.0125)(386)\pi(0.0125)^2]^{1/2} \times [0.91e^{mx} - 161.09e^{-mx}]_0^{0.3}$$

$$= 122.7 \text{ W}$$

4.

$$k = 204 \frac{\text{W}}{\text{m} \cdot ^\circ\text{C}} \quad L_c = L + \frac{d}{4} = 12 + \frac{2}{4} = 12.5 \quad T_0 = 250^\circ\text{C} \quad T_\infty = 15^\circ\text{C}$$

$$h = 12 \frac{\text{W}}{\text{m}^2 \cdot ^\circ\text{C}} \quad A = \frac{\pi d^2}{4} \quad P = \pi d$$

$$m = \sqrt{\frac{hP}{kA}} = \left[\frac{(12)\pi(0.02)(4)}{(204)\pi(0.02)^2} \right]^{1/2} = 3.43$$

$$mL_c = (3.43)(0.125) = 0.429 \quad q = \sqrt{hPkA}\theta_0 \tanh(mL_c)$$

$$q = \left[(12)\pi(0.02)(204)\pi \frac{(0.02)^2}{4} \right]^{1/2} (250 - 15) \tanh(0.429) = 20.89 \text{ W}$$

5.

$$q = \sqrt{hPkA}\theta_0 = \left[\frac{(20)\pi(0.0005)(372)\pi(0.0005)^2}{4} \right]^{1/2} (120 - 20) = 0.152 \text{ W}$$

6.

$$r_1 = 1.0 \text{ cm} \quad L = 5 \text{ mm} \quad t = 2.5 \text{ mm} \quad h = 25 \quad T_0 = 260^\circ\text{C}$$

$$T_\infty = 93^\circ\text{C} \quad k = 43 \quad L_c = 5 + 1.25 = 6.25 \text{ mm} \quad r_{2c} = 1.625 \text{ cm}$$

$$\frac{r_{2c}}{r_1} = 1.625 \quad A_m = (0.0025)(0.00625) = 1.56 \times 10^{-5} \text{ m}^2$$

$$L_c^{3/2} \left(\frac{h}{kA_m} \right)^{1/2} = 0.00625^{3/2} \left[\frac{25}{(43)(1.56 \times 10^{-5})} \right]^{1/2} = 0.095 \quad \eta_f = 97\%$$

$$q = (0.97)(25)(2)\pi(0.01625^2 - 0.01^2)(260 - 93) = 4.17 \text{ W}$$

7.

$$d = 1.5 \text{ mm} \quad k = 19 \quad L = 12 \text{ mm} \quad T_0 = 45^\circ\text{C} \quad T_\infty = 20^\circ\text{C}$$

$$h = 500$$

Use insulated tip solution

$$L_c = L + \frac{d}{4} = 12 + 0.375 = 12.375 \text{ mm}$$

$$m = \left(\frac{hP}{kA} \right)^{1/2} = \left[\frac{(500)\pi(0.0015)}{(19)\pi(0.0015)^2(4)} \right]^{1/2} = 264.9$$

$$mL_c = (0.012375)(264.9) = 3.278$$

$$q = \sqrt{hPkA}\theta_0 \tanh(mL)$$

$$= \left[(500)\pi(0.0015)(19)\pi(0.0015) \left(\frac{2}{4} \right) \right]^{1/2} (45 - 20) \tanh(3.278) = 0.177 \text{ W}$$

ID heat transfer through fins

⑧

$$D = 1 \text{ m}$$

$$K = 4 \text{ W/mK}$$

$$h = 10 \text{ W/m}^2\text{K}$$

effectiveness = ?

$$\varepsilon = \sqrt{\frac{KP}{hAc}}$$

$$= \sqrt{\frac{4 \times 3.14 \times 1 \times 4}{10 \times 3.14 \times 1 \times 1}}$$

$$P = \pi D$$

$$Ac = \frac{\pi D^2}{4}$$

$$\varepsilon = 1.265$$

effectiveness of fin = 1.265

⑨

$$D = 10 \text{ mm}$$

$$L = 300 \text{ mm}$$

$$K = 500 \text{ W/mK}$$

$$h = 250 \text{ W/m}^2\text{K}$$

effectiveness = ?

$$\epsilon = \sqrt{\frac{KP}{hAc}} \tanh mL$$

$$m = \sqrt{\frac{hP}{KA_c}} = \sqrt{\frac{h\pi D^4}{K\pi D^2}} = \sqrt{\frac{4h}{KD}} = \sqrt{\frac{4 \times 250}{500 \times 10 \times 10^{-3}}} = 14.14$$

$$\therefore \tanh mL = \tanh (14.14 \times 300 \times 10^{-3}) = \tanh (4.242) = 0.999$$

$$\epsilon = \sqrt{\frac{K\pi D^4}{h\pi D^2}} \tanh mL = \sqrt{\frac{4K}{hD}} \tanh mL = \sqrt{\frac{4 \times 500}{250 \times 10 \times 10^{-3}}} \times 0.999$$

$$\epsilon = 28.255$$

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$$\text{effectiveness } (\varepsilon) = \frac{Q \text{ with fin}}{Q \text{ w/o fin}}$$

$$\begin{aligned} \text{efficiency } (\eta) &= \frac{\text{Actual heat transfer through fin}}{\text{max possible heat transfer through fin}} \\ &= \frac{Q_{\text{actual}}}{Q_{\text{max}}} \end{aligned}$$

$$\therefore \varepsilon (Q \text{ w/o fin}) = Q \text{ with fin}$$

$$\therefore \eta (Q \text{ w/o fin}) = Q_{\text{max}} (\eta)$$

$$\varepsilon = \eta \frac{Q_{\text{max}}}{Q_{\text{fin}}}$$

$$\varepsilon = \eta \frac{h A_s \theta_b}{h A_c \theta_b}$$

$$\boxed{\varepsilon = \eta \frac{A_{\text{surface}}}{A_{\text{crosssectional}}}}$$

$$= 0.5 \frac{\pi D L}{\pi D^2 / 4}$$

$$= 0.5 \frac{4L}{D}$$

$$= \frac{0.5 \times 4 \times 5}{1}$$

$$\varepsilon = \underline{\underline{10}}$$