3- effect Evaporator

For 13-4 KPa (1.44 psia), trout = 51-67°C

(0.013, 51.034) (0.014, 52.547) (0.0134, x)

\$ 52-547-51-034 . 52-547-2 0-014-0-0134 0. 014 - 0.013

x = 51-6392°C (from steam table)

clains the ext for BPR for evaporator no. 3 with x = 0.5

BPR 3 = 1.78 x + 6.22 x2

= 2.45 °C

T3 - 51-64 + 2-45 = 54-09 °C

F = 8000 kg/h = L3 + (V1+V1+V3)

FXF = 8000 (0.1) = L3 (0.5) + (V1+V2+V3) 10

L3 = 1600 kg/hr

Total vaporised = V1+V2+V3 = 6400 kg | hr

 $V_1 = V_2 = V_3 = 2133.33$  kg/ha

Total Material balance on 1,2 E 3

F= V, + 4

8000 = 2133-33 + 4

Li = 5866,67 kg/hr

2

.... show Steam table DTavailable = TS, - TS (sat) - (BPR, + BPR2 + BPR2) + 121.1 - 51.64 - (0.36 + 0.66 + 2.41)

rEK L1 - V2 + L2

58 86 . 67 = 2133.33 + L2 L2 = 3733.34 kg/h

L2 = V3 + L3 3733.34 = 2133.33 + L3 L3 = 1600.01 kg/hr

## Solids balance on 1,2 & 3

FXF = Lixi 0 8000 X 0.1 = 5866-67 X X1 = 0.136

L1 x1 = L2 x2 2 5866.67 × 0-136 = 3733.34 ×2 ×2 = 0.213

> L2 X2 = L3 X3 3733.34 (0.213) = 1600.01 23 713 = D. 496

BPR1 = 1.78 x1 + 6.22 x12 = 0.36°C BPR2 = 1.78 x2 + 6.22 x22 = 0.66 °C BPR3 - 2.41 °C

values from Sceam table D'Invailable . To, - To (ear) - (BPR, + BPR2 + BPR2) 3 + 121-1 - 51-64 - (0:36 + 0:66 + 2:41) ( from interpolation; steam table ) . CG.03°C AT1 = 66.03 ( 3123) = 12.40°C 1 + 1 + L 3123 + 1987 + L AT1 = 19.50°C AT3 - 34.11°C ① T1 = T31 - ΔT, = 121.1 - 15.8°C = 105.54°C T2 = T1 - BPR1 - AT2 = 105.54 - 0.36 - 18.34 = 86.84°C

Ts2 = T1 - BPR1 = 105.54 - 0.36 = 105.18 °C

 $T_3 = T_2 - BPR_2 - \Delta T_3$ = 86.84 - 0.66 - 32.11 = 53.87 °C waters from Steam table

Tos Ta - BPR2 \* 86.84 - D.66 € 85.98 °C

Effect 1 Effect 2 Effect 3 Condense

(0)

Ts1 = 121.1°C Ts2 = 105.18°C Ts3 = 85.98°C

Tgy = 51.6°C

Ti= 105.54°C T1 = 86.84°C T3 = 53.87°C

tcp 4: F: Cp = 3726 J/kgk (copy)

4: Cp = (10, 3726) (20, 3559) (13.4, x)

3559-3726 = 3559-X 20 - 13.4 20-10

n = 3669.22

Cp = 3669.22 I/kg K

£2 : Cp 0.213

(20,3559) (30,3349) (21.3,x)

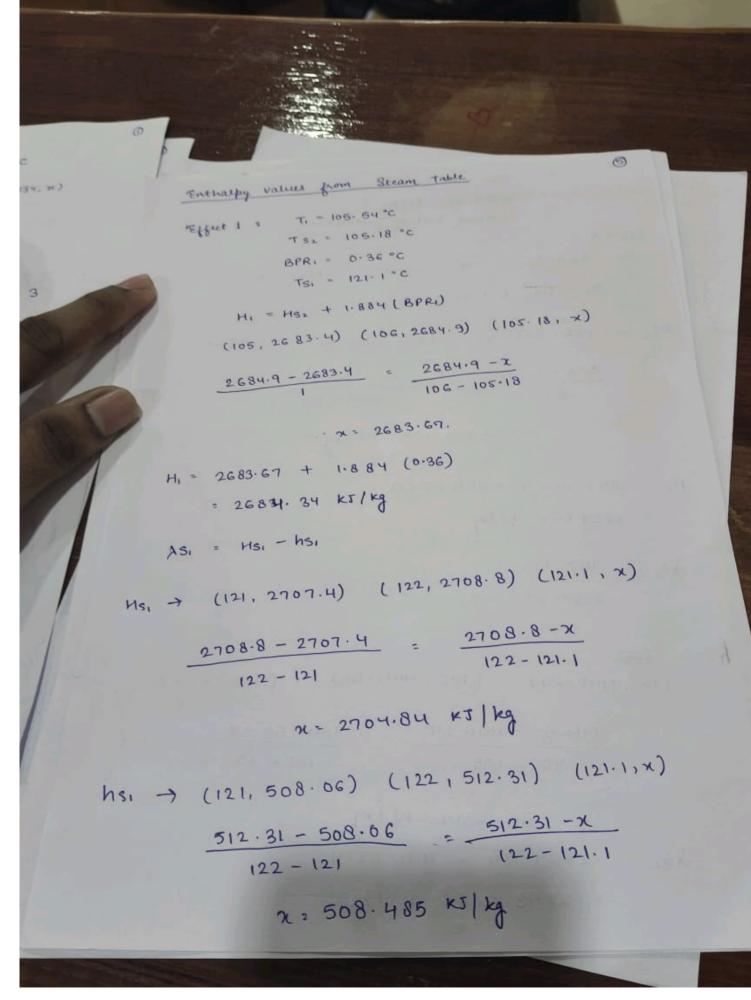
3559 - 3349 = 3349 - 2 30 - 21.3 20 - 30

x = 3531.7

£3 € Cp

0.496 \$ 0.5

Cp = 2923. 608 J/ kgk



0 0 151 - HS1 - HS. = 219 6.355 KJ/Kg (latent heat of condensation) T2 = 86.84°C T53 = 86.19°C BPR2 = 0.66 Effect 2: H2 = H33 + 1.884 (0.66) Hs, -> (86, 2653.6) (87, 2654.6) (80.19, x) 2654-6-2653 = 2653.0 87-86 2653. 304 KS/kg H2 = 2653.304 + 1.884 (0.66) = 2654.547 KJ/kg 152 = H1 - h52 = 2684.34 - hs2 Teat (105, 440.27) (106, 444.50) (105.18, x) \$S<sub>2</sub> → (35) 444.50 - 440.27 ; 444.50 - 2 106 - 105,18 106 - 105

 $\lambda = 441.0314 \text{ kJ/kg}$   $\lambda = 2684.34 - 441.0314$  = 2243.3086 kJ/kg

745200 + 2196.355 × P - --

Effect 3 :

0

T2 - 53 87 C T54 - 51-6 C BPR3 - 2-45

0

H3 : HS4 + 1.884 (2.45) = 2598 - 4158

As3 = H2 - hs3 = 2654.547 - hs3

 $S_3 \rightarrow (86, 360.22)$  (87, 364-42) (86.19, x)

7 = 361. 618

25/5/ 26/5/4/547 - 13/6/1918

As3 = 2654.547 - 361.018 = 2293.529 k5/kg

→ V1 = 8000 - L1 V2 = L1-L2

V3 , L2 - L3

Heat balance :

FCP(TF) + SASI = LICP(Ti-0) + VIMI

1 8000 x 3. 726 x 25 + 8 (2196.355) =

LI X 3.669 (105.54-0) + (8000 - LI) (2684.34)

0

②  $L_1C_p(T_1-0) + V_1A_{S_2} = L_2C_p(T_2-0) + V_4H_2$   $+ (3.669) (105.54-0) + (8000 - L_1) (2243.3086)$   $= L_2 (3.531) (86.84-0) + (L_1-L_2) (2454.547)$   $L_2 C_p(T_2-0) + V_2 A_{S_3} = L_3 C_p (T_3-0) + V_3 H_3$   $L_2 (3.631) (86.84-0) + (L_1-L_2) (2293.529)$ 

= 1600.01 (2.923) (54.09-0) + (12-1600.01) (2598-61)

 $\Rightarrow$  387. 22 L1 + 179 46468. 8 - 2243. 31 L1 = 306. 63 L2 + 2654.547 L1 - 2654. 547 L2  $\Rightarrow$  -4510. 637 L1 + 17946468. 8 = -2347. 917 L2  $\Rightarrow$  4510. 637 L1 - 2347. 917 L2 = 17946468. 8 — ①

 $A_1 = 3 \, \epsilon 9^n \Rightarrow 306.63 \, L_2 + 2293.529 \, L_1 - 2293.529 \, L_2$   $= 252969.69 + 2598.61 \, L_2 - 4157801.98$ 

 $-4585.509 L_2 + 2293.529 L_1 = -3904832.3$  $2293.529 L_1 - 4585.509 L_2 = -3904832.29$ 

L1 = 5978. 469 kg 1 hr

L2 = 3841.0036 kglhr

L3 = 1600.01 kg/hr

745200 + 2196.355 × 8 = 2315020 · 191 + 5426476.525

S = 3185 + 412

Vi= 2021.531 kg/hr

112: 2136.66 kg/hr

V3 = 2241.79 kg/hr

 $\frac{3185.412}{3600} \times \frac{2196.355}{3600} \times \frac{1.943}{3600} \times \frac{1000}{3600}$ 

 $92 = V_1 \lambda S_2 = \frac{2021.531}{3600} \times 82243.3086 \times 10^3$ 

= 1-26 × 108 W

 $93 = V_2 \lambda S_3 = \frac{2136.66}{3600} \times 2293.529 \times 10^3$ 

= 1.36 × 106 W

 $A_1 = \frac{91}{U_1 \Delta T_1} = \frac{1.943 \times 10^6}{3123 (15.56)} = 39.98 \text{ m}^2$ 

 $A_2 = \frac{1.26 \times 10^6}{1987 (18.34)} = 34.57 \text{ m}^2$ 

A3 = 1.36 × 106 1136 (32.11) = 37.28 m2

