

FLUID FLOW AND DESIGN LAB

ASSIGNMENT

Given information :-

$$\text{Design Pressure} = 2.5 \text{ MPa}$$

$$\text{Design Temperature} = 200^\circ\text{C}$$

$$\text{Shell ID} = 1.5 \text{ m}$$

$$\text{Gasket material} = \text{Asbestos}$$

$$\text{Gasket width} = 1.6 \text{ mm}$$

$$\text{Allowable stress for Shell and Flange} = 100 \text{ MPa}$$

$$\text{Allowable stress for Bolting} = 138 \text{ MPa}$$

$$\text{Hub Thickness} = 12 \text{ mm}$$

$$\text{Distance b/w outer shell and Gasket} = 6 \text{ mm}$$

$$\text{Weld Joint efficiency} = 0.85$$

$$m = 2.75, \quad y = 25.5 \text{ MPa}$$

We have,

$$\frac{d_o}{d_i} = \sqrt{\frac{y - P(m)}{y - P(m+1)}}$$

$$\frac{d_o}{d_i} = \sqrt{\frac{25.5 - (2.75)(2.5)}{25.5 - (3.75)(2.5)}}$$

$$\frac{d_o}{d_i} = 1.0747$$

Now, we have

$$(\text{Shell Thickness})_{\text{ess}} g_o = \frac{p D_o}{2 f J + p} = \frac{2.5 (1.5 + 0.002 + g_o)}{2 \times 100 \times 0.85 + 2.5}$$

$$172.5 g_0 = 3.755 + 2.5 g_0$$

$$g_0 = 0.022 \text{ m}$$

Considering corrosion allowance = 0.002 m ( $t_c$ )

$$\begin{aligned} g &= g_0 + t_c \\ &= 0.022 + 0.002 \\ &= 0.024 \text{ m} \end{aligned}$$

Next Standard Thickness available = 0.025 m (25 mm)

$$\begin{aligned} \text{Shell Outer Diameter} &= \text{Shell Inner Diameter} + 2(\text{shell Thickness}) \\ &= 1.5 + (2 \times 0.025) \\ &= 1.55 \text{ m} \end{aligned}$$

Now we have

$$\begin{aligned} \text{Gasket Inner Diameter, } d_i &= 1.55 + 2(0.006) \\ &= 1.562 \text{ m} \end{aligned}$$

As Gasket is placed 6mm from outer shell.

$$\frac{d_o}{d_i} = 1.0747 \Rightarrow d_o = 1.0747 \times 1.562 \Rightarrow d_o = 1.6787 \text{ m}$$

$$\text{Minimum Gasket width} = \frac{d_o - d_i}{2} = \frac{1.6787 - 1.562}{2} = 0.0583 \text{ m}$$

$$\Rightarrow b_0 = \frac{0.0583}{2} = 0.02917 \text{ m} \quad (29.17 \text{ mm}).$$

Since  $b_0 (29.17 \text{ mm}) > 6.3 \text{ mm}$

$$b = 2.5 \sqrt{b_0} = 2.5 \sqrt{29.17} = 13.5 \text{ mm}$$

We also have

$$\begin{aligned} G &= d_o - 2b \\ &= 1.6787 - (2 \times 0.0135) \\ &= 1.6517 \text{ m} \end{aligned}$$

$$\begin{aligned} \text{Bolt Load because of Design Pressure} &= \frac{\pi G^2 \times P}{4} \\ &= \frac{\pi \times (1.6517)^2 \times 2.5}{4} \\ &= 5.353 \text{ MN} \\ &= \underline{\underline{\quad}} \end{aligned}$$

$$\begin{aligned} \text{Bolt Load due to Adequate Compression} &= 2\pi G b m p \\ &= 2 \times \pi \times 1.6517 \times 0.0135 \times 2.75 \times 2.5 \\ &= 0.963 \text{ MN} \\ &= \underline{\underline{\quad}} \end{aligned}$$

$$\begin{aligned} \text{Total operating Load} &= (5.353 \text{ MN} + 0.963 \text{ MN}) \\ (\text{No.}) &= 6.315 \text{ MN} \\ &= \underline{\underline{\quad}} \end{aligned}$$

$$\begin{aligned} \text{Bolt Load under bolting up condition} &= \pi G b y \\ (W_g) &= \pi \times 1.6517 \times 0.0135 \times 25.5 \\ &= 1.785 \text{ MN} \\ &= \underline{\underline{\quad}} \end{aligned}$$



$$\text{Minimum bolting} = \frac{W_0}{S_0} \quad (S_0 = 138 \text{ MPa})$$

↳ Given

$$= \frac{6.315}{138} = 0.0457 \text{ m}^2$$

Selection of Bolt: We know that if dimension of bolt is  $M(a \times b)$  .... dimensions

$$\text{Root Area} = \frac{\pi (a-b)^2}{4} \times 10^{-6} \text{ m}^2$$

$$n (\text{no. of bolts}) = \frac{\text{Bolting Area}}{\text{Root Area}} \quad \left( \begin{array}{l} \text{Next suitable} \\ \text{multiple of 4} \end{array} \right)$$

Also,

$$\textcircled{1} \leftarrow c_1 = B + 2(g_1 + R)$$

$$\textcircled{2} \leftarrow c_2 = \frac{n B_s}{\pi}$$

$c_1, c_2$  should be as close as possible.

$$\textcircled{i} \quad M(18 \times 2) \Rightarrow \text{Root Area} = \frac{\pi (18-2)^2}{4} \times 10^{-6}$$

↓  
M 18 × 2

$$= 1.5399 \times 10^{-4} \text{ m}^2$$

$$n = \frac{4.57 \times 10^{-2}}{1.5399 \times 10^{-4}} \approx 297$$

Therefore actual  $n = 300$

From  $\textcircled{1}$  and  $\textcircled{2}$  we get

$$c_1 = 1.55 + 2(0.012 + 0.027) = 1.628 \text{ m}$$

$$c_2 = \frac{300 \times 0.075}{\pi} = 7.16 \text{ m}$$

$$(ii) \quad \text{M } 20 \times 2 \quad \nrightarrow \quad \text{Root Area} = \frac{\pi (20-4)^2}{4} \times 10^{-6}$$

$$\text{M } 20 \times 2 \quad \quad \quad = 0.201 \times 10^{-3} \text{ m}^2$$

$$n = 227.66$$

$$\approx 228$$

From ① and ②

$$C_1 = 1.55 + 2(0.012 + 0.03) = 1.634 \text{ m}$$

$$C_2 = \frac{228 \times 0.075}{\pi} = 5.44 \text{ m}$$

Similarly

$C_1$

$C_2$

M 22x2

1.64 m

4.297 m

M 24x2

1.644 m

3.53 m

M 27x2

1.65 m

2.67 m

M 30x2

1.662 m

2.1 m

→

M 33x2

1.668 m

1.666 m

→ Best choice

M 36x3

1.674 m

1.62 m

M 39x3

1.678 m

1.53 m

M 42x3

1.684 m

1.27 m

Therefore we select M 33x2, bolt circle diameter = 1.668 m

$$C_1 = 1.668$$

$$n = \frac{0.0457 \times 10^6}{\frac{\pi (33-2^2)^2}{4}} \approx 69 \text{ bolts}$$

n is 64 bolts

⇒ we have to consider next multiple of 4

$$\therefore \boxed{n = 72 \text{ bolts}}$$

$$\text{Flange Outer Diameter} = 1.668 + 0.033 + 0.002$$

$$= 1.703$$

Finally we have ⇒

$$\text{Gasket Inner Diameter} = 1.562 \text{ m}$$

$$\text{Gasket Outer Diameter} = 1.6787 \text{ m}$$

$$\text{Gasket width} = 0.0583 \text{ m}$$

$$\text{Bolt Circle Diameter} = 1.668 \text{ m}$$

$$\text{No. of Bolts} = 72 \text{ bolts}$$

$$\text{Flange Outer Diameter} = 1.703 \text{ m}$$