

Effect of Graphene coating on Hypervelocity Impact Resistance of Aluminium: A Molecular Dynamics approach

Final Project Report: Molecular Dynamics and Multiscale Modeling of Materials

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1. Introduction:

Hypervelocity is very high velocity, approximately over 3,000 meters per second. This is especially relevant in the field of space exploration and military in anything from minor component degradation to the complete destruction of a spacecraft or missile. Graphene, an allotrope of carbon has a special set of properties which sets it apart from the other allotropes. In relation to its thickness, it is about 100 times stronger than the strongest steel. Yet its density is dramatically lower than any steel. Hypervelocity impact simulations were conducted on Aluminium, one of the most popular and lightweight metals, to study its resistance to these impacts. The resistance to the impacts was measured in terms of the reduction in kinetic energy of the indenter, upon impact with the block. The block was further coated with graphene, and the reduction in energy was monitored.

2. System Construction:

System Modeling and simulations were performed using LAMMPS and OVITO was used for post processing of the data.

An aluminium block of volume $135 \times 135 \times$

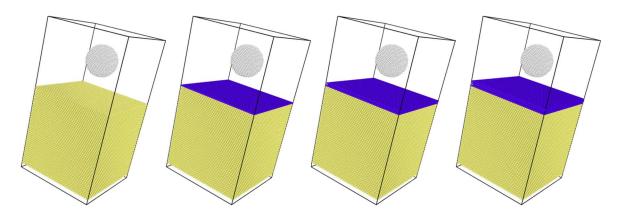


Figure 1. (a) Aluminium Block without graphene sheets. **(b)** Aluminium Block with 1 graphene sheet. **(c)** Aluminium Block with 2 graphene sheets. **(d)** Aluminium Block with 3 graphene sheets.



3. Simulation Setup:

Periodic boundary conditions were defined in the x and z direction, with non-periodic boundary condition in the y direction.

The system consisted of three groups of atoms:

- Group 1: Graphene (Carbon).
- Group 2: Diamond Indenter (Carbon).
- Group 3: Aluminium Block (Aluminium).

The following atomic interactions were defined:

- C-C (Graphene): The adaptive intermolecular reactive bond order (AIREBO) potential was used to consider both the short- and long-range interactions between the atoms.
- Al-Al (Aluminium Block): EAM potential.
- C-Al (Graphene Aluminium Block): Morse potential.
- C-Al (Diamond indenter Aluminium Block): Morse potential.
- C-C (Graphene Diamond Indenter): Lennard Jones potential.
- C-C (Diamond Indenter): None. Since it was considered as a rigid body.

For minimization, the Conjugate Gradient (CG) method was used. Equilibration of the system was carried out using the NVE (constant volume, constant energy) ensemble. Since, the NVE ensemble does not control the temperature, velocity scaling was used to maintain a system temperature of 300K.

The aluminium block was divided into three different zones: fixed atoms zone, heat sink atoms zone and Newtonian atoms zone. The fixed atoms were kept fixed to provide a support to the block for the impact. The heatsink atoms were used to absorb the excessive heat after the impacts. The motion of the Newtonian atoms was determined by the forces produced by Newton's equation of motion.

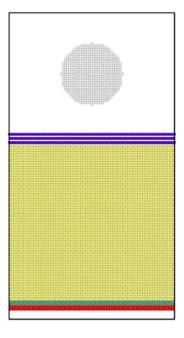


Figure 2. Fixed atoms (red). Heatsink atoms (green). Newtonian atoms (yellow).



After the system was equilibrated, impact simulations were carried out at different velocities with different layers of graphene coating on the aluminium block. The diamond indenter was specified as rigid during the impact simulations as the deformation of the indenter was not in the scope of the project.

4. Results and discussions:

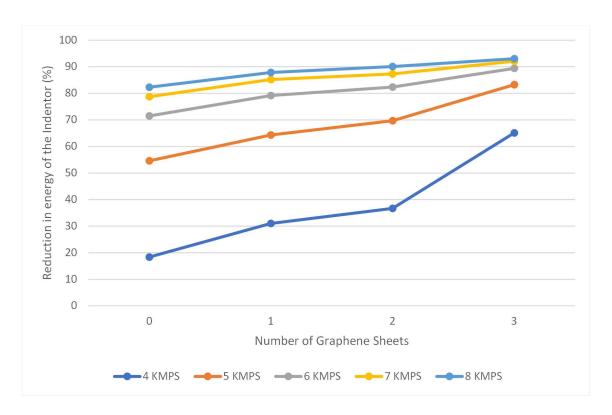


Figure 3. Reduction in energy of the Indenter (%) vs Number of Graphene sheets for different impact velocities.

The reduction in the kinetic energy of the indenter was monitored after 1 picosecond of the impact.

Figure 3 predicts a trend between the reduction in energy of the indenter upon impact vs the number of graphene sheets coated on the block, for different impact velocities. It can be clearly observed that as the number of graphene sheets are increased, the reduction in energy of the indenter increases, basically it slows down faster.

It can also be observed that as the impact velocity increases, the difference in reduction in energy, with increase in graphene sheets decreases. This can be attributed to the fact that the graphene sheets start to fracture as the velocity increases and their ability to absorb the energy reduces.



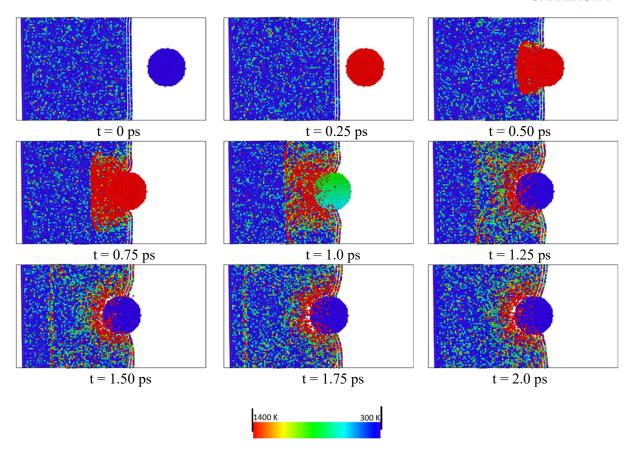


Figure 4. Temperature distribution at different timesteps for impact velocity of 8KMPS with 3 graphene sheets. A slice of 10 angstrom has been used to view the geometry.

From figure 4, the temperature distribution of the system can be observed. It can be clearly seen that the temperature near the heat sink atoms is the lowest and is higher near the impact area.

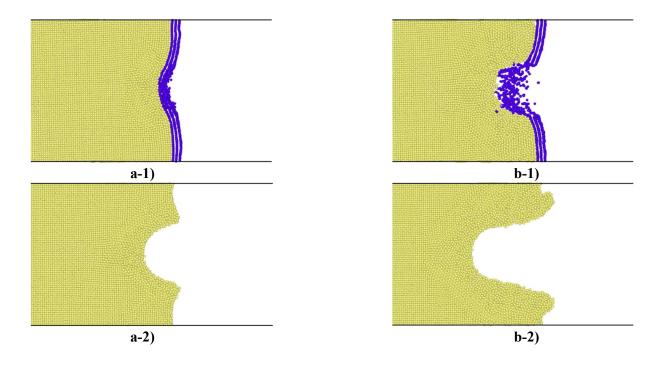




Figure 5. a-1) Penetration depth with 3 graphene sheets at 4KMPS. **a-2)** Penetration depth without graphene sheets at 4KMPS. **b-1)** Penetration depth with 3 graphene sheets at 8KMPS. **b-2)** Penetration depth without graphene sheets at 8KMPS. A slice of 10 angstrom has been used to view the geometry.

From figure 5 it can be observed that the penetration depth reduces with addition of 3 graphene sheets. The penetration depth can also be related to the damage caused to the block. Thus, the penetration depth must be as less as possible. The results are in conformance with the desired physical behaviour.

5. Conclusion:

The results obtained in the project clearly imply that coating a metal with graphene can improve its resistance to Hypervelocity impacts. The above study can be extended to other metals to establish confidence in the observed trends.

References:

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- 2. https://lammps.sandia.gov/mail.html
- 3. https://en.wikipedia.org/wiki/Hypervelocity
- 4. https://en.wikipedia.org/wiki/Graphene
- 5. https://www.researchgate.net/publication/324477174_A_novel_nonlinear_nano-scale_wear_law_for_metallic_brake_pads
- 6. https://www.researchgate.net/publication/332217214_Nanoindentation_of_Graphene-Reinforced Silica Aerogel A Molecular Dynamics Study

```
1
     # Equilibration script
2
3
     # Atom Definition
4
5
    units metal
6
     dimension 3
7
    boundary p f p
     atom style full # to consider molecular effects into account
8
9
10
     # Simulation box and geometry modeling
11
12
     read data geoinput.data # read geometry data file
13
     group graphene type 1 # specify atom number
14
15
     group projectile type 2
     group alblock type 3
16
17
     region fixedatoms block INF INF 64 68 INF INF units box # select atoms to create
18
     fixedatoms for support
19
     group fixedatoms region fixedatoms
20
21
     region thermoatoms block INF INF 59 63 INF INF units box # select atoms to create
    heat sink
22
     group thermoatoms region thermoatoms
23
24
     # ForceFields
25
26
    pair style hybrid airebo 3.0 eam/alloy morse 2.5 lj/cut 2.5
27
     pair coeff * * airebo CH.airebo C NULL NULL
28
     pair coeff * * eam/alloy Al99.eam.alloy NULL NULL Al
     pair coeff 1*2 3 morse 0.4691 1.738 2.246
29
     pair coeff 1 2 lj/cut 1 1 2.5
30
    pair coeff 2 2 none # since projectile is rigid
31
32
3.3
     # Minimization
34
35
    min style cg
    minimize 1.0e-10 1.0e-10 1000 10000
36
37
38
     # Equilibration
39
40
     velocity all create 300 1234567 mom yes rot yes sum no dist gaussian
41
     reset timestep 0
42
     timestep 0.0005 # smaller timestep for better accuracy
43
     fix 1 all nve
44
45
     fix 2 all momentum 1 linear 1 1 1
46
     fix 3 projectile move linear 0 0 0
     fix 4 all temp/rescale 25 300.0 300 0.02 0.5 # to maintain a temp of 300K
47
48
     fix 5 projectile rigid single
49
     fix 6 fixedatoms move linear 0 0 0
50
51
52
    thermo style custom step lx ly lz press pxx pyy pzz pe temp
53
54
    run 50000
55
56
    unfix 1
57
    unfix 2
    unfix 3
58
59
    unfix 4
60
    unfix 5
    unfix 6
61
62
63
64
    write restart restart equilibratedg system.equil # input file for impact simuations
65
66
     write data equilibrated.data # to view equilibrated system
```

```
1
    # Impact Simulation script
2
3
    read restart restart equilibratedg system.equil #read equilibrated system
4
5
    #-----Force Fields-----
6
7
    pair style hybrid airebo 3.0 eam/alloy morse 2.5 lj/cut 2.5
    pair coeff * * airebo CH.airebo C NULL NULL
8
   pair coeff * * eam/alloy Al99.eam.alloy NULL NULL Al
9
10 pair coeff 1*2 3 morse 0.4691 1.738 2.246
11
   pair coeff 1 2 lj/cut 1 1 2.5
    pair coeff 2 2 none
12
13
14
15
   compute keproj projectile ke #compute kinetic energy of projectile
16 compute keatom all ke/atom
17 compute peatom all pe/atom
18 variable kb equal 8.671333262145e-5
19 variable alltemp atom (2*c_keatom)/(3*v_kb) #compute temperature of atoms
20
21
    reset timestep 0
22
    timestep 0.0005 # smaller timestep due to high velocities
23
24
    thermo 100
25
    thermo style custom step cpu temp pe vol etotal ke c keproj
    dump RESULTS all custom 100 RESULTS *.cfg id type x y z vx vy vz fx fy fz c keatom
26
    v alltemp v blocktemp
27
    thermo modify lost ignore flush yes
28
    run 200
29
30
    velocity projectile set 0.0 80.0 0.0 units box # specify linear velocity
31
    fix 1 all nve
32
    fix 2 all momentum 1 angular
33
34
    fix 3 projectile rigid/nve single # specify projectile as rigid
    fix 4 fixedatoms move linear 0 0 0 # fix atoms for support
35
36
    fix 5 thermoatoms temp/rescale 25 300.0 300 0.02 0.5 # maintain a temperature of
    300K to create a heat sink
37
    run 5000
38
```