

## Lecture 4

# The Gradient of a Scalar Field

### 4.1 The vector operator 'Del'

You have met the *vector operator*, 'del', in Part IA. We represent 'del' by the 'upside down triangle'  $\nabla$  (which has nothing to do with big delta,  $\Delta$ ). In Cartesian coordinates,  $\nabla$  is defined by,

$$\nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z} \quad (4.1)$$

We call  $\nabla$  an operator because it acts on, or *operates* on, whatever comes immediately after it. For example, if  $\phi$  is a scalar function  $\phi = \phi(x, y, z)$  then,

$$\nabla \phi = \left( \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z} \right) \phi = \mathbf{i} \frac{\partial \phi}{\partial x} + \mathbf{j} \frac{\partial \phi}{\partial y} + \mathbf{k} \frac{\partial \phi}{\partial z}$$

$\nabla \phi$  is called the gradient of  $\phi$  (or 'grad  $\phi$ ') and is a *vector*.  $\nabla$  can only operate directly on a scalar function, and the result is a vector.

### Example

Find the gradient of the scalar field  $\phi = x^2 y \sin z$ .

$$\frac{\partial \phi}{\partial x} = 2x y \sin z$$

$$\frac{\partial \phi}{\partial y} = x^2 \sin z$$

$$\frac{\partial \phi}{\partial z} = x^2 y \cos z$$

$$\nabla \phi = (2xy \sin z) \mathbf{i} + (x^2 \sin z) \mathbf{j} + (x^2 y \cos z) \mathbf{k}$$

Two ‘vector’ identities involving the gradient that are useful are,

$$\nabla(f+g) = \nabla f + \nabla g \quad (4.2)$$

$$\nabla(fg) = f\nabla g + g\nabla f \quad (4.3)$$

where  $f$  and  $g$  are both scalar fields. The easiest way to prove these is by expanding terms in Cartesian coordinates.

### Example

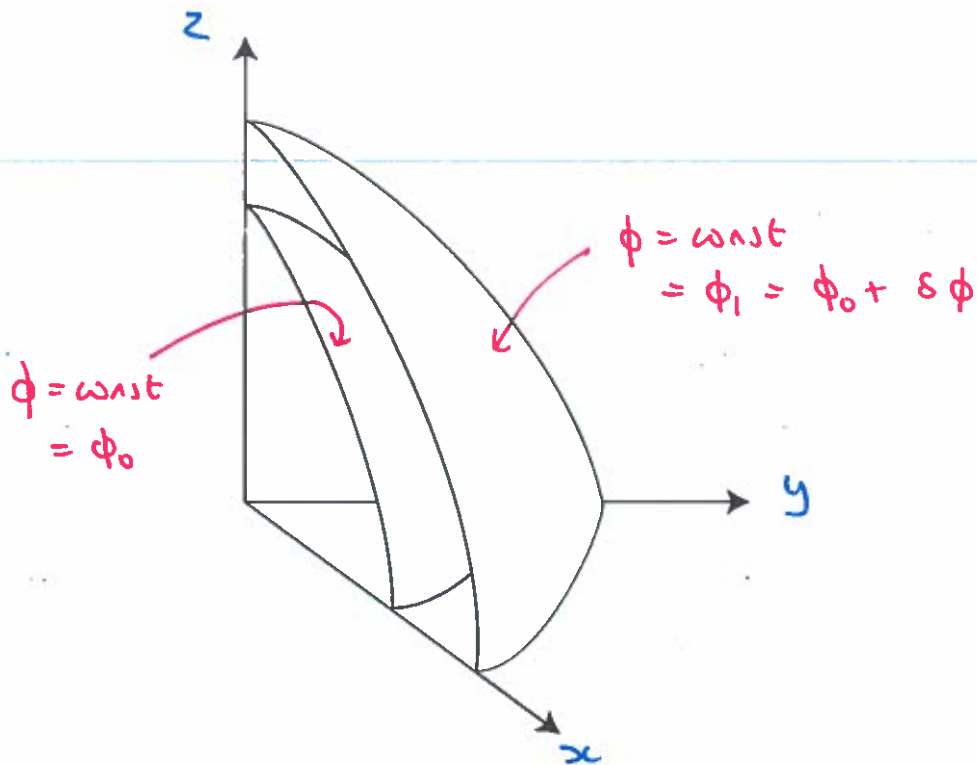
Prove,  $\nabla(fg) = f\nabla g + g\nabla f$ .

$$\begin{aligned} \nabla(fg) &= \mathbf{i} \frac{\partial}{\partial x} (fg) + \mathbf{j} \frac{\partial}{\partial y} (fg) + \mathbf{k} \frac{\partial}{\partial z} (fg) \\ &= f \left( \mathbf{i} \frac{\partial g}{\partial x} + \mathbf{j} \frac{\partial g}{\partial y} + \mathbf{k} \frac{\partial g}{\partial z} \right) \\ &\quad + g \left( \mathbf{i} \frac{\partial f}{\partial x} + \mathbf{j} \frac{\partial f}{\partial y} + \mathbf{k} \frac{\partial f}{\partial z} \right) \\ &= f \nabla g + g \nabla f \end{aligned}$$

## 4.2 Physical interpretation of the gradient

The vector gradient is the 3-D equivalent of the slope of a curve in 1-D.

$\phi = \phi(x, y, z)$  is a scalar field in Cartesian space (for example, the temperature at every point in space of a 3-D object). We can draw surfaces of constant  $\phi$ :



The sketch shows two surfaces, one at  $\phi_0$  and one at  $\phi_1 = \phi_0 + \delta\phi$ . If we move from a point  $(x, y, z)$  on the  $\phi_0$  surface to a point  $(x + \delta x, y + \delta y, z + \delta z)$  on the  $\phi_1$  surface, we can write,

$$\delta\phi = \frac{\partial\phi}{\partial x} \delta x + \frac{\partial\phi}{\partial y} \delta y + \frac{\partial\phi}{\partial z} \delta z$$

Now, using  $\nabla\phi$ , we can write this, more compactly, as,

$$\delta\phi = \left( \underline{i} \frac{\partial\phi}{\partial x} + \underline{j} \frac{\partial\phi}{\partial y} + \underline{k} \frac{\partial\phi}{\partial z} \right) \cdot (\delta x \underline{i} + \delta y \underline{j} + \delta z \underline{k})$$

so that

$$\delta\phi = \nabla\phi \cdot \delta\mathbf{r} \quad , \quad (4.4)$$

and this holds for any coordinate system.

If we write  $\delta\mathbf{r}$  as  $\delta s \hat{\mathbf{n}}$  where  $\hat{\mathbf{n}}$  is the unit vector in the direction of  $\delta\mathbf{r}$ ,

$$\delta\phi = \nabla\phi \cdot (\delta s \hat{\mathbf{n}})$$

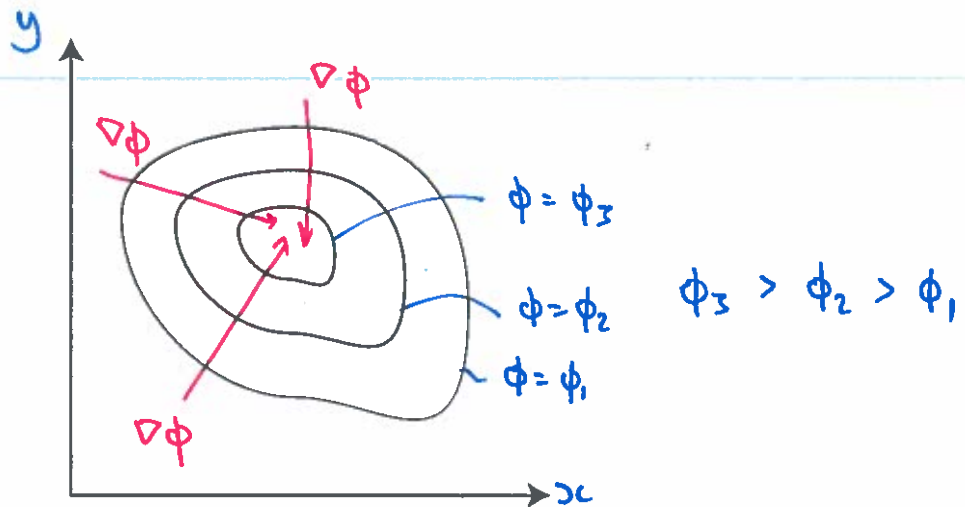
so that, as  $\delta s \rightarrow 0$

$$\frac{d\phi}{ds} = \nabla\phi \cdot \hat{\mathbf{n}} \quad . \quad (4.5)$$

This is known as the 'directional derivative' and  $d\phi/ds = \nabla\phi \cdot \hat{\mathbf{n}}$  is valid for any coordinate system. Notice that:

1. if  $\hat{\mathbf{n}}$  lies on the surface of constant  $\phi$ ,  $\nabla\phi \cdot \hat{\mathbf{n}} = d\phi/ds = 0$
2. the magnitude of  $d\phi/ds$  is greatest when  $\hat{\mathbf{n}}$  is parallel to  $\nabla\phi$

3. the direction of  $\nabla\phi$  is always in the direction of increasing  $\phi$  (“ $\nabla\phi$  always points up hill”)



### 4.3 Flux-gradient empirical “laws”

For any scalar field  $\phi$  it is always possible to obtain a vector field  $\mathbf{V}$  using the relationship  $\mathbf{V} = \nabla\phi$ . However, if we have a particular vector field  $\mathbf{V}_0$ , it is not always possible to find a scalar field  $\phi_0$  such that  $\mathbf{V}_0 = \nabla\phi_0$ . For cases when we can find the required  $\phi_0$  field,  $\phi_0$  is known as the *scalar potential* and  $\mathbf{V}_0$  is the *flux vector*. Considerable mathematical simplifications then follow: once we have obtained the scalar potential, we also know all three components of the vector field.

There are several engineering applications where the flux-gradient approach is used to model a physical process. Here, we will consider Fourier’s law of heat conduction, Fick’s law of diffusion and Ohm’s law of current flow. Each of these is not actually a law, but rather a model that has been found to fit empirical data.

#### Heat conduction

Fourier’s law of heat conduction tells us that heat flows down a temperature gradient. For example, in a straight metal bar aligned with the  $x$ -axis, the heat flow is given by  $Q_x = -\lambda A \partial T / \partial x$  where  $T$  is the temperature,  $A$  is the cross-sectional area of the bar and  $\lambda$  is the thermal conductivity of the metal. The *heat flux* is the heat flow per unit area,

$$q_x = -\lambda \frac{\partial T}{\partial x}$$

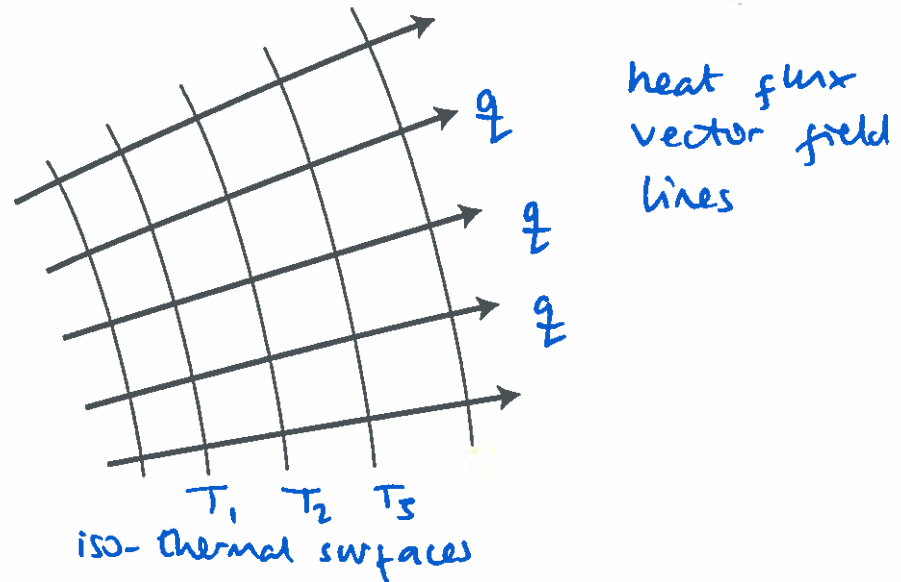
Similarly, in a three-dimensional problem, we would also have,

$$q_y = -\lambda \frac{\partial T}{\partial y} \quad q_z = -\lambda \frac{\partial T}{\partial z}$$

We can express Fourier’s law, concisely, as,

$$\mathbf{q} = -\lambda \nabla T$$

where  $\mathbf{q}$  is the heat flux vector. We have derived this expression in Cartesian coordinates (where  $\mathbf{q}$  has components  $q_x$ ,  $q_y$  and  $q_z$ ), but  $\mathbf{q} = -\lambda \nabla T$  applies in any coordinate system. A common assumption is that  $\lambda$  is constant and so we may write  $\mathbf{q} = \nabla(-\lambda T)$  and we see that  $(-\lambda T)$  is the scalar potential.



## Diffusion

Fick's law governs the diffusion in solids, liquids and gases. In one dimension, the mass transfer rate of the diffusing species across a plane of area  $A$  is given by  $M_x = -DA \partial c / \partial x$  where  $c$  is the concentration of the species (mass per unit volume) and  $D$  is the diffusion coefficient. The diffusive mass flux is  $m_x = M_x / A$  and,

$$m_x = -D \frac{\partial c}{\partial x}$$

governs our 1-D diffusion. In 3-D, Fick's law is captured by the vector equation,

$$\mathbf{m} = -D \nabla c$$

where  $\mathbf{m}$  is the diffusive mass flux vector. Just as  $\mathbf{q}$  is perpendicular to lines of constant  $T$ , we see that  $\mathbf{m}$  must be perpendicular to lines of constant  $c$ .

## Current flow

The current flowing in a conductor aligned with the  $x$ -axis obeys Ohm's Law,  $I_x = \sigma A \partial V / \partial x$  where  $\sigma$  is the electrical conductivity,  $A$  is the cross-sectional area and  $V$  is the electric potential. The current per unit cross-sectional area is  $j_x = I_x / A$  and this is called the current density (the terminology would be more consistent if  $j_x$  was known as the current flux). In 1-D, we have

$$j_x = -\sigma \frac{\partial V}{\partial x}$$

and the general, 3-D, expression is,

$$\mathbf{j} = -\sigma \nabla V$$

If  $\sigma$  is constant, we see that the scalar potential in this case is  $(-\sigma V)$  and the current density vector is everywhere normal to surfaces of constant electric potential.

### Example

The concentration of a species is axi-symmetric,  $c = c(r)$ , and is given by  $c = c_0 - a \ln(r/r_0)$ . Given that the diffusion coefficient is  $D$  (constant), find an expression for the diffusive mass flux in the radial direction and for the total diffusive mass flow rate crossing radius  $r = R$ .

$$\underline{m} = -D \nabla c$$

$$m_r = -D \frac{\partial c}{\partial r} = a D \frac{1}{r}$$

$$\text{At } r = R \quad M_r = 2\pi R a D \frac{1}{R} = 2\pi a D \quad (\text{per unit in } z \text{ dir}^n)$$

## 4.4 A return to the substantive derivative

In Lecture 1 we found the rate of change of temperature, as measured by a probe moving through a time-varying temperature field  $T = T(x, y, z, t)$ , was given by the total derivative,

$$\frac{dT}{dt} = \left( V_x \frac{\partial T}{\partial x} + V_y \frac{\partial T}{\partial y} + V_z \frac{\partial T}{\partial z} \right) + \frac{\partial T}{\partial t} \quad (4.6)$$

where  $V_x$ ,  $V_y$  and  $V_z$  are the components of the velocity of the probe. We can use vector notation to write the first term on the right hand side as a scalar product,

$$\frac{dT}{dt} = (V_x \underline{i} + V_y \underline{j} + V_z \underline{k}) \cdot \left( \underline{i} \frac{\partial T}{\partial x} + \underline{j} \frac{\partial T}{\partial y} + \underline{k} \frac{\partial T}{\partial z} \right) + \frac{\partial T}{\partial t}$$

which we now recognise as,

$$\frac{dT}{dt} = \underline{V} \cdot \nabla T + \frac{\partial T}{\partial t}$$

where  $\underline{V} = V_x \underline{i} + V_y \underline{j} + V_z \underline{k}$  is the velocity of the probe. We can see that the combination  $(\underline{V} \cdot \nabla)$  acts on the temperature field,  $T$ ,

$$\underline{V} \cdot \nabla = V_x \frac{\partial}{\partial x} + V_y \frac{\partial}{\partial y} + V_z \frac{\partial}{\partial z} \quad , \quad (4.7)$$

and is a 'scalar operator' (due to the dot product) that can act on either a scalar field (as in the above example) or a vector field (as in  $(\underline{V} \cdot \nabla) \underline{V}$  used in IB Paper 4).

## 4.5 $\nabla$ in non-Cartesian coordinate systems

So far, we have made use of the definition of the  $\nabla$  operator in Cartesian coordinates,

$$\nabla = \mathbf{i} \frac{\partial}{\partial x} + \mathbf{j} \frac{\partial}{\partial y} + \mathbf{k} \frac{\partial}{\partial z} \quad . \quad (4.8)$$

But we can use the result,

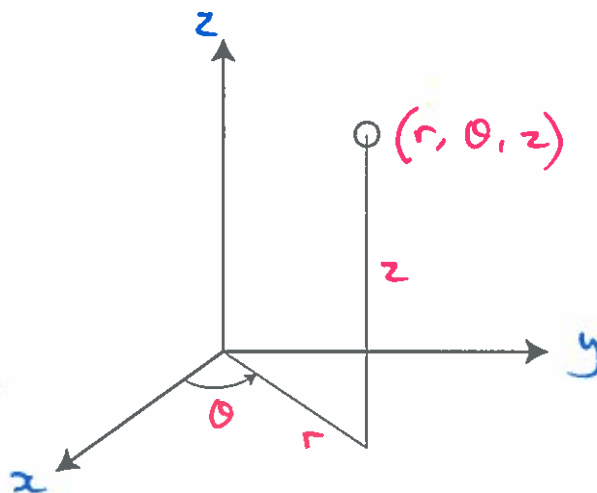
$$\delta f = \nabla f \cdot \delta \mathbf{r} \quad , \quad (4.9)$$

to define  $\nabla$  in other coordinate systems.

### Cylindrical polar coordinates $(r, \theta, z)$

A cylindrical polar coordinate system  $(r, \theta, z)$  has base vectors  $(\mathbf{e}_r, \mathbf{e}_\theta, \mathbf{e}_z)$ . The small change in position vector as we move from  $(r, \theta, z)$  to  $(r + \delta r, \theta + \delta \theta, z + \delta z)$  is given by,

$$\delta \underline{r} = \delta r \underline{e}_r + r \delta \theta \underline{e}_\theta + \delta z \underline{e}_z$$



In order to satisfy  $\delta f = \nabla f \cdot \delta \mathbf{r}$ , we can see that,

$$\nabla = \mathbf{e}_r \frac{\partial}{\partial r} + \mathbf{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \mathbf{e}_z \frac{\partial}{\partial z} \quad . \quad (4.10)$$

As a check,

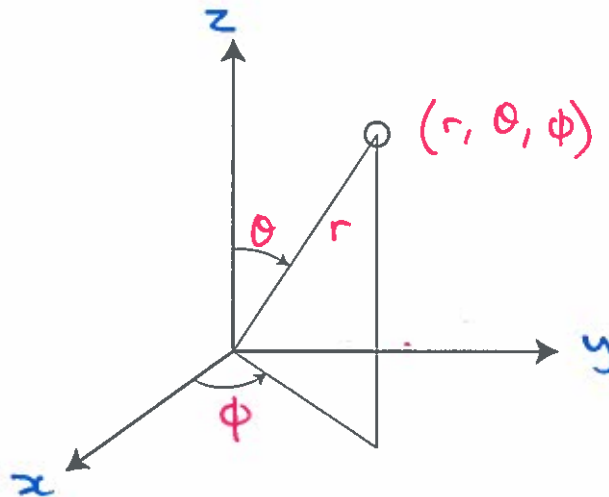
$$\nabla f \cdot \delta \mathbf{r} = \left( \mathbf{e}_r \frac{\partial f}{\partial r} + \mathbf{e}_\theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \mathbf{e}_z \frac{\partial f}{\partial z} \right) \cdot (\delta r \mathbf{e}_r + r \delta \theta \mathbf{e}_\theta + \delta z \mathbf{e}_z) \quad (4.11)$$

$$= \frac{\partial f}{\partial r} \delta r + \frac{\partial f}{\partial \theta} \delta \theta + \frac{\partial f}{\partial z} \delta z = \delta f \quad (4.12)$$

## Spherical polar coordinates $(r, \theta, \phi)$

We can follow the same procedure in spherical polar coordinates  $(r, \theta, \phi)$ . The base vectors are now  $(\mathbf{e}_r, \mathbf{e}_\theta, \mathbf{e}_\phi)$  and the small change in position vector as we move from  $(r, \theta, \phi)$  to  $(r + \delta r, \theta + \delta \theta, \phi + \delta \phi)$  is given by,

$$\delta \mathbf{r} = \delta r \mathbf{e}_r + r \delta \theta \mathbf{e}_\theta + r \sin \theta \delta \phi \mathbf{e}_\phi \quad (4.13)$$



In order to satisfy  $\delta f = \nabla f \cdot \delta \mathbf{r}$ , we must have,

$$\nabla = \mathbf{e}_r \frac{\partial}{\partial r} + \mathbf{e}_\theta \frac{1}{r} \frac{\partial}{\partial \theta} + \mathbf{e}_\phi \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \quad (4.14)$$

**You can now do Examples Paper 1: Q8, 9, 10, 11 and 12**