ME 280a: HW 1

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September 27, 2016

# 1 Introduction and Objectives

The purpose of this study is to solve a simple finite element (FE) problem and perform a convergence study to determine the number of elements needed to reach a particular error relative to an analytical solution. The Galerkin FE method is used, which for certain classes of problems possesses the "best approximation property," a characteristic that signifies that the FE solution obtained is the best possible solution for a given mesh refinement and choice of shape functions. The mathematical procedure and numerical implementation is described in Section 2.

# 2 Procedure

This section details the problem statement and mathematical method used for solving the problem.

#### 2.1 Problem Statement

This section describes the mathematical process used to solve the following problem:

$$\frac{d}{dx}\left(E(x)\frac{du}{dx}\right) = k^2 \sin\left(\frac{2\pi kx}{L}\right) \tag{1}$$

where E is the modulus of elasticity, u is the solution, k is a known constant, L is the problem domain length, and x is the spatial variable. In order to verify that the program functions correctly, the FE solution to Eq. (1) will be compared with the analytical solution to Eq. (1). To determine the analytical solution, integrate Eq. (1) once to obtain:

$$\frac{du}{dx} = -\frac{1}{E}k^2 \cos\left(\frac{2\pi kx}{L}\right) \frac{L}{2\pi k} + C_1 \tag{2}$$

It has been assumed that E is not a function of x, and hence can be treated as constant in the integration. Integrating once more:

$$u(x) = -\frac{1}{E}k^2 \sin\left(\frac{2\pi kx}{L}\right) \left(\frac{L}{2\pi k}\right)^2 + C_1 x + C_2 \tag{3}$$

The boundary conditions for this problem are Dirichlet at both endpoints, such that:

$$u(0) = 0$$

$$u(L) = 1$$
(4)

By the first BC,  $C_2 = 0$ , and  $C_1$  based on the second condition equals:

$$C_1 = \frac{u(L) + k^2 \sin(2\pi k) \left(\frac{L}{2\pi kE}\right)^2}{L} \tag{5}$$

The purpose of this assignment is to solve Eq. (1) with the finite element method (FEM) and then to determine how many elements are needed to obtain a specified error as a function of the frequency k. The solutions for various numbers of elements will also be compared to illustrate how increasing the number of elements "hones in" on the analytical solution.

## 2.2 Finite Element Implementation

The Galerkin FEM achieves the best approximation property by approximating the true solution u(x) as  $u^N(x)$ , where both  $u^N(x)$  and the test function  $\psi$  are expanded in the same set of N basis functions  $\phi$ :

$$u \approx u^{N} = \sum_{j=1}^{N} a_{j} \phi_{j}$$

$$\psi = \sum_{j=1}^{N} b_{j} \phi_{j}$$
(6)

Galerkin's method is stated as:

$$r^N \cdot u^N = 0 \tag{7}$$

where  $r^N$  is the residual. Hence, to formulate the weak form to Eq. (1), multiply Eq. (1) through by  $\psi$  and integrate over all space,  $d\Omega$ .

$$\int_{\Omega} \frac{d}{dx} \left( E(x) \frac{du}{dx} \right) \psi d\Omega - \int_{\Omega} k^2 \sin\left(\frac{2\pi kx}{L}\right) \psi d\Omega = 0$$
 (8)

Applying integration by parts to the first term:

$$-\int_{\Omega} E(x) \frac{du}{dx} \frac{d\psi}{dx} d\Omega + \int_{\partial \Omega} E(x) \frac{du}{dx} \psi d(\partial \Omega) - \int_{\Omega} k^2 \sin\left(\frac{2\pi kx}{L}\right) \psi d\Omega = 0$$
 (9)

where  $\partial\Omega$  refers to one dimension lower than  $\Omega$ , which for this case refers to evaluation at the endpoints of the domain. Hence, for this particular 1-D problem, the above reduces to:

$$-\int_{0}^{L} E(x) \frac{du}{dx} \frac{d\psi}{dx} dx + E(x) \frac{du}{dx} \psi \Big|_{0}^{L} - \int_{0}^{L} k^{2} \sin\left(\frac{2\pi kx}{L}\right) \psi dx = 0$$

$$\int_{0}^{L} E(x) \frac{du}{dx} \frac{d\psi}{dx} dx = -\int_{0}^{L} k^{2} \sin\left(\frac{2\pi kx}{L}\right) \psi dx + E(x) \frac{du}{dx} \psi \Big|_{0}^{L}$$
(10)

Inserting the approximation described in Eq. (6):

$$\int_{0}^{L} E(x) \frac{d\left(\sum_{j=1}^{N} a_{j} \phi_{j}\right)}{dx} \frac{d\left(\sum_{i=1}^{N} b_{i} \phi_{i}\right)}{dx} dx = -\int_{0}^{L} k^{2} \sin\left(\frac{2\pi kx}{L}\right) \sum_{i=1}^{N} b_{i} \phi_{i} dx + E(x) \frac{du}{dx} \sum_{i=1}^{N} b_{i} \phi_{i} \bigg|_{0}^{L}$$
(11)

Recognizing that  $b_i$  appears in each term, the sum of the remaining terms must also equal zero (i.e. basically cancel  $b_i$  from each term).

$$\int_0^L E(x) \frac{d\left(\sum_{j=1}^N a_j \phi_j\right)}{dx} \frac{d\phi_i}{dx} dx = -\int_0^L k^2 \sin\left(\frac{2\pi kx}{L}\right) \phi_i dx + E(x) \frac{du}{dx} \phi_i \bigg|_0^L$$
(12)

This equation can be satisfied for each choice of j, and hence can be reduced to:

$$\int_0^L E(x) \frac{d(a_j \phi_j)}{dx} \frac{d\phi_i}{dx} dx = -\int_0^L k^2 \sin\left(\frac{2\pi kx}{L}\right) \phi_i dx + E(x) \frac{du}{dx} \phi_i \bigg|_0^L$$
(13)

This produces a system of matrix equations of the form:

$$\mathbf{K}\vec{a} = \vec{F} \tag{14}$$

where:

$$K_{ij} = \int_0^L E(x) \frac{d\phi_i}{dx} \frac{d\phi_j}{dx} dx$$

$$a_j = a_j$$

$$F_i = -\int_0^L k^2 \sin\left(\frac{2\pi kx}{L}\right) \phi_i dx + E(x) \frac{du}{dx} \phi_i \Big|_0^L$$
(15)

where the second term in  $F_i$  is only applied at nodes that have Neumann boundary conditions (since  $\psi$  satisfies the homogeneous form of the essential boundary conditions). The above equation governs the entire domain. **K** is an  $n \times n$  matrix, where n is the number of global nodes. The solution is contained within  $\vec{a}$ . This matrix system is solved in this assignment by simple Gaussian elimination, such that  $\vec{a} = \mathbf{K}^{-1} \vec{F}$ .

Quadrature is used to perform the numerical integration because it is much faster, and more general, than symbolic integration of the terms appearing in Eq. (15). In order for these equations to be useful with Gaussian quadrature, they must be transformed to the master element which exists over  $-1 \le \xi \le 1$ :

$$K_{ij} = \int_{0}^{L} E(x) \frac{d\phi_{i}}{dx} \frac{d\phi_{j}}{dx} dx \rightarrow \int_{-1}^{1} E(x(\xi)) \frac{d\phi_{i}}{dx} \frac{d\phi_{j}}{dx} dx \left(\frac{dx}{d\xi} \frac{dx}{d\xi} \frac{d\xi}{dx}\right) \rightarrow \int_{-1}^{1} E(x(\xi)) \frac{d\phi_{i}}{d\xi} \frac{d\phi_{j}}{d\xi} dx \left(\frac{d\xi}{dx}\right)$$

$$a_{j} = a_{j} \quad (16)$$

$$F_{i} = -\int_{0}^{L} k^{2} \sin\left(\frac{2\pi kx}{L}\right) \phi_{i} dx \rightarrow -\int_{-1}^{1} k^{2} \sin\left(\frac{2\pi kx(\xi)}{L}\right) \phi_{i} \frac{dx}{d\xi} d\xi$$

where the second term in  $F_i$  has been dropped because there are no Neumann boundary conditions in this assignment. For linear elements, the shape functions have the following form over the master element:

$$\phi_1(\xi) = \frac{1 - \xi}{2} \phi_2(\xi) = \frac{1 + \xi}{2}$$
 (17)

And the derivative of these functions with respect to the isoparametric coordinate are:

$$\frac{d\phi_1(\xi)}{d\xi} = -1/2$$

$$\frac{d\phi_2(\xi)}{d\xi} = 1/2$$
(18)

The transformation from the physical domain (x) to the parent domain  $(\xi)$  is done with an isoparametric mapping:

$$x(\xi) = \sum_{i=1}^{N} X_i \phi_i(\xi) \tag{19}$$

where  $X_i$  are the coordinates in each element. This mapping is performed for each element individually. The Jacobian  $dx/d\xi$  is obtain from Eq. (19) by differentiation:

$$\frac{dx(\xi)}{d\xi} = \sum_{i=1}^{N} X_i \frac{d\phi_i(\xi)}{d\xi} \tag{20}$$

With all these transformations from the physical domain to the isoparametric domain, Gaussian quadrature can be used. For simplicity, a two-point quadrature rule is used, with the following weights w and sampling points x:

$$w = [1.0, 1.0]$$

$$x = [-\sqrt{1/3}, \sqrt{1/3}]$$
(21)

Transformation to the isoparametric domain therefore easily allows construction of the local stiffness matrix and local force matrix. The actual numerical algorithm computes the elemental k(i,j) and b(i) by looping over i,j, and the quadrature points. Because each calculation is computed over a single element, a connectivity matrix is used to populate the global stiffness matrix and the global forcing vector with the elemental matrices and vectors. See the Appendix for the full code used in this assignment. After the global matrix and vector are formed, the global matrix has a banded-diagonal structure.

In order to apply the boundary conditions within the numerical context of the finite element method, the matrix equation in Eq. (14) must be rewritten to reflect that some of the nodal values are actually already specified through the Dirichlet boundary conditions.

$$\begin{bmatrix} K_{kk} & K_{ku} \\ K_{uk} & K_{uu} \end{bmatrix} \begin{bmatrix} x_k \\ x_u \end{bmatrix} = \begin{bmatrix} F_k \\ F_u \end{bmatrix}$$
 (22)

where k indicates a known quantity (specified through a boundary condition) and u indicates an unknown quantity. Explicitly expanding this equation gives:

$$K_{kk}x_k + K_{ku}x_u = F_k$$

$$K_{uk}x_k + K_{uu}x_u = F_u$$
(23)

Solving this matrix system is sometimes referred to as "static condensation," since the original matrix system in Eq. (14) must be separated into its components. The nodes at which Dirichlet conditions are specified are "known," while all other nodes, including Neumann condition nodes, are "unknown," since it is the value of u that we are looking to find at each node. The second of these equations is the one that is solved in this assignment, since there are no natural boundary conditions.

Once the solution is obtained by simple Gaussian elimination, the solution is transformed back to the physical domain (from the isoparametric domain) by solving a linear matrix system to determine the coefficients on the basis functions over each element (in the physical domain). For example, for a quadratic shape function, over one element with coordinates  $x_1, x_2$ , and  $x_3$ , with solution values  $a_1, a_2$ , and  $a_3$ , the following linear system solves for the coordinates on the shape function in the physical domain, in that element:

$$\begin{bmatrix} 1 & x_1 & x_1^2 \\ 1 & x_2 & x_2^2 \\ 1 & x_3 & x_3^2 \end{bmatrix} \begin{bmatrix} A \\ B \\ C \end{bmatrix} = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$
 (24)

Each element is looped over to obtain the coefficients on the shape functions in the physical domain. This then transforms the solution back to the physical domain, and completes the FE solution.

#### 2.3 Error Estimates and Convergence Criteria

The accuracy of the FE solution is estimated using the energy norm  $e^N$ , defined as:

$$e^{N} = \frac{\|u - u^{N}\|}{\|u\|} \tag{25}$$

where:

$$||u|| = \sqrt{\int_{\Omega} \frac{du}{dx} E \frac{du}{dx}}$$
 (26)

$$||u - u^N|| = \sqrt{\int_{\Omega} \frac{d(u - u^N)}{dx} E \frac{d(u - u^N)}{dx}} = \sqrt{\int_{\Omega} \left(\frac{du}{dx} - \frac{du^N}{dx}\right) E \left(\frac{du}{dx} - \frac{du^N}{dx}\right)}$$
(27)

The derivatives of the FE solution are determined according to:

$$\frac{du^{N}}{dx} = \frac{d}{dx} \sum_{j=1}^{N} a_{j} \phi_{j}(x) = \sum_{j=1}^{N} a_{j} \frac{d\phi_{j}(x)}{dx} = \sum_{j=1}^{N} a_{j} \frac{d\phi_{j}(x)}{d\xi} \frac{d\xi}{dx}$$
(28)

while the derivative of the analytical solution is obtained from Eq. (3). Convergence is defined to have been achieved for a given k and number of elements N once:

$$e^N = \frac{\|u - u^N\|}{\|u\|} \le 0.05 \tag{29}$$

## 2.4 Solution Results and Discussion

Table 1 shows the number of elements needed to satisfy Eq. (29) for each k.

**Table 1.** Number of elements N needed to reach convergence according to Eq. (29).

k	N to reach convergence
1	28
2	67
4	142
8	289
16	580
32	1160

Fig. ?? shows the FE solutions for N=2,4,8,16,32,64, and 128 for k=1,2,4,8,16,32. The exact solution is also plotted for comparison. As can be seen, in general, increasing N improves the finite element solution with respect to better-approximating the analytical solution. It is interesting to note that, for choices of the number of elements N that are twice the value of k (i.e. for N=2k), the finite element solution is a straight line between the two endpoints. This likely occurs because of the highly oscillatory nature of the analytical solution, and the fact that too-few elements fails to place nodes at locations that represent the peaks and valleys of the analytical solution.

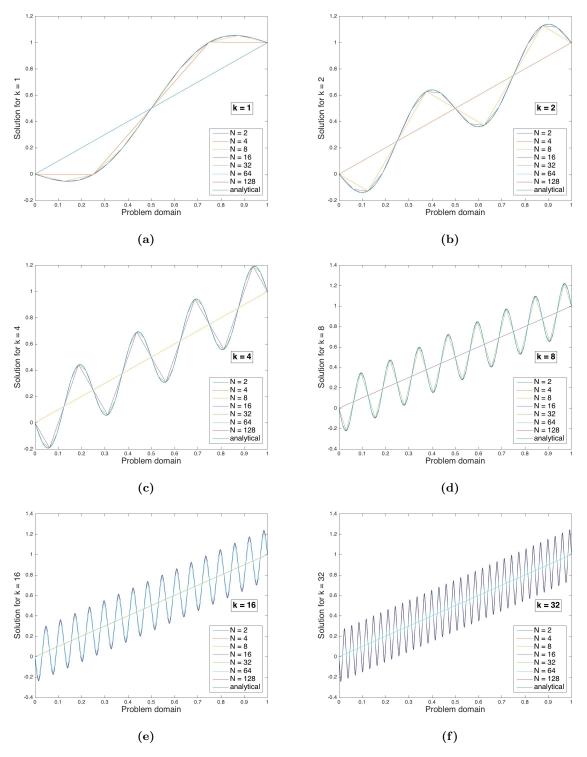
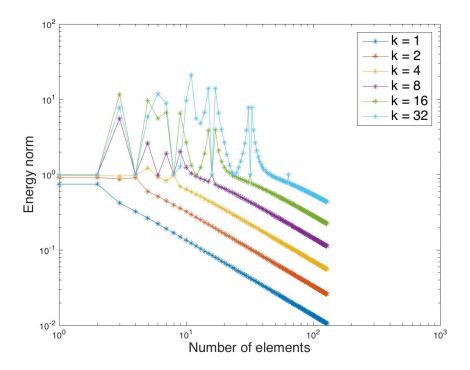


Figure 1. Finite element and exact (analytical) solutions for N = 2, 4, 8, 16, 32, 64, and 128 for (a) k = 1, (b) k = 2, (c) k = 4, (d) k = 8, (e) k = 16, and (f) k = 32.

Fig. 2 shows  $e^N$  as a function of N for each value of k represented in the previous figure. N is allowed to vary from 1 to 128 to obtain a fine-enough plot to observe the convergence behavior. As can be seen, the higher the k, the more elements that are needed to obtain a desired global energy norm. For very oscillatory solutions, for coarser meshes, nodes may happen to consistently not "fall" in the peaks and valleys of the

solution, completely missing the oscillatory behavior. Hence, increasing the mesh resolution for oscillatory solutions with high frequency does not always reduce the energy norm simply due to where the nodes may happen to lie. However, with a fine-enough mesh, by increasing the number of elements, the energy norm will monotonically decrease.



**Figure 2.** Energy norm  $e^N$  as a function of N for k = 1, 2, 4, 8, 16, and 32.

# 3 Appendix

This section contains the code used for this modeling. The main program is FEProgram.m, and functions perform specialized tasks for a high degree of modularity.

# 3.1 FEProgram.m

```
clear all
% select which type of plot you want to make - at least one flag must equal 1
                                 \% 1 - plot the error as a function of N
k_{plot_flag} = 1;
N_{plot_flag} = 0;
                                 \% 1 - plot the solutions for various N
L = 1.0;
                                 % problem domain
k_f req = 2;
                                 % forcing frequency
num_elem = 5;
                                 % number of finite elements (initial guess)
shape\_order = 2;
                                 % number of nodes per element
E = 0.1;
                                 % elastic modulus
left = 'Dirichlet';
                                 % left boundary condition
                                 % left Dirichlet boundary condition value
left_value = 0.0;
right = 'Dirichlet';
                                 % right boundary condition type
right_value = 1.0;
                                 % right Dirichlet boundary condition value
```

```
tolerance = 0.05;
                                  % convergence tolerance
energy\_norm = tolerance + 1;
                                  % arbitrary initialization value
                                  % fontsize for plots
fontsize = 16;
% form the permutation matrix for assembling the global matrices
[permutation] = permutation(shape_order);
if (N_plot_flag)
     N_{elem} = [2, 4, 8, 16, 32, 64, 128];
elseif (k_plot_flag)
     N_{elem} = 1:128;
else
    disp('Either_N_plot_flag_or_k_plot_flag_has_to_equal_1.');
end
for k_{\text{freq}} = [1, 2, 4, 8, 16, 32]
% index for collecting error
e = 1;
for num_elem = N_elem
% uncomment to find how many elements are required to reach the error
\% \ while \ energy\_norm > tolerance
      num_{-}elem = num_{-}elem + 1;
    % ---- ANALYTICAL SOLUTION ---- %
    parent_domain = -1:0.01:1;
    physical_domain = linspace(0, L, num_elem * length(parent_domain) - (
        \hookrightarrow num_elem -1);
    C_{-1} = (right\_value + (k\_freq^2 * sin(2 * pi * k\_freq) * (L / (2 * pi * left)))
        \hookrightarrow k_freq))^2 / E)) / L;
    solution\_analytical = (1 ./ E) .* -k\_freq.^2 .* sin(2 .* pi .* k\_freq .*
        \hookrightarrow physical_domain ./ L) .* (L ./ (2 .* pi .* k_freq)).^2 + C_1 .*
        → physical_domain + left_value;
    solution_analytical_derivative = -(1 ./ E) * k_freq * k_freq * cos(2 * pi
        \rightarrow * k_freq * physical_domain ./ L) * L ./ (2 * pi * k_freq) + C_1;
    % perform the meshing
    [num_nodes, num_nodes_per_element, LM, coordinates] = mesh(L, num_elem,

    shape_order);
    % specify the boundary conditions
    [dirichlet_nodes, neumann_nodes, a_k] = BCnodes(left, right, left_value,

→ right_value, num_nodes);
    % define the quadrature rule
    [wt, qp] = quadrature(shape_order);
    \% assemble the elemental k and elemental f
    K = zeros(num\_nodes);
    F = zeros(num\_nodes, 1);
```

```
for elem = 1:num_elem
        k = zeros(num_nodes_per_element);
        f = zeros (num_nodes_per_element, 1);
         for 1 = 1:length(qp)
             for i = 1:num_nodes_per_element
                  [N, dN, x_xe, dx_dxe] = shapefunctions(qp(1), shape_order,
                     \hookrightarrow coordinates, LM, elem);
                  % assemble the (elemental) forcing vector
                  f(i) = f(i) - wt(1) * k_freq * k_freq * sin(2 * pi * k_freq *
                     \rightarrow x_xe / L) * N(i) * dx_dxe;
                  for j = 1:num_nodes_per_element
                      \% assemble the (elemental) stiffness matrix
                      k(i,j) = k(i,j) + wt(l) * E * dN(i) * dN(j) / dx_dxe;
                  end
             end
         end
         \% place the elemental k matrix into the global K matrix
         for m = 1: length(permutation(:,1))
            i = permutation(m, 1);
            j = permutation(m, 2);
            K(LM(elem, i), LM(elem, j)) = K(LM(elem, i), LM(elem, j)) + k(i, j)
                \hookrightarrow ;
         end
         \% place the elemental f matrix into the global F matrix
         for i = 1:length(f)
            F(LM(elem, i)) = F((LM(elem, i))) + f(i);
         end
    end
% perform static condensation to remove known Dirichlet nodes from solve
[K_uu, K_uk, F_u, F_k] = condensation(K, F, num_nodes, dirichlet_nodes);
% perform the solve
a_u-condensed = K_u \ (F_u - K_u * dirichlet_nodes (2,:)');
% expand a_condensed to include the Dirichlet nodes
a = zeros(num\_nodes, 1);
a_row = 1;
            \% index for dirichlet_nodes
i = 1;
j = 1;
            % index for expanded row
for a_row = 1:num_nodes
    if (find(dirichlet_nodes(1, :) == a_row))
        a(a_row) = dirichlet_nodes(2,i);
        i = i + 1;
    else
        a(a_row) = a_u\_condensed(j);
        j = j + 1;
```

```
end
end
% assemble the solution in the physical domain
[solution_FE, solution_derivative_FE] = postprocess(num_elem, parent_domain, a

→ , LM, num_nodes_per_element , shape_order , coordinates , physical_domain);

% compute the energy norm
energy_norm_bottom = sqrt(trapz(physical_domain,

→ solution_analytical_derivative .* E .* solution_analytical_derivative));

energy_norm_top = sqrt(trapz(physical_domain, (solution_derivative_FE -
   → solution_analytical_derivative) .* E .* (solution_derivative_FE -
   → solution_analytical_derivative)));
energy_norm = energy_norm_top ./ energy_norm_bottom;
sprintf('energy_norm: \_%f', energy_norm)
if (N_plot_flag)
    plot(physical_domain, solution_FE)
    hold on
end
% uncomment to find out how many elements are needed to reach the error
% tolerance
\%end
e_N(e) = energy_norm;
e = e + 1;
end
if (N_plot_flag)
    plot(physical_domain, solution_analytical)
    \mathbf{set}(h, 'FontSize', fontsize - 2);
    xlabel('Problem_domain', 'FontSize', fontsize)
    ylabel(sprintf('Solution_for_k_=_%i', k_freq), 'FontSize', fontsize)
    text(0.85, 0.5, sprintf('k_=_%i', k_freq), 'FontSize', fontsize, '
       → FontWeight', 'bold', 'EdgeColor', [0 0 0])
    saveas(gcf, sprintf('Nplot_for_k_%i', k_freq), 'jpeg')
    close all
end
if (k_plot_flag)
    loglog(N_elem, e_N, *-')
    xlabel('Number_of_elements', 'FontSize', fontsize)
    ylabel('Energy_norm', 'FontSize', fontsize)
end
end
if (k_plot_flag)
    h2 \, = \, \mathbf{legend} \, ( \, \, `k\_=\_1 \, \, `, \quad `k\_=\_2 \, \, `, \quad `k\_=\_4 \, \, `, \quad `k\_=\_8 \, \, `, \quad `k\_=\_16 \, \, `, \quad `k\_=\_32 \, \, `) \, ;
    set(h2, 'FontSize', fontsize);
```

```
saveas(gcf, 'eN_vs_N', 'jpeg')
end

% uncomment to find out how many elements are needed to reach the error
% tolerance
%sprintf('For k = %i, number elements: %i', k_freq, num_elem)
```

### 3.2 permutation.m

This function determines the permutation matrix for use with the connectivity matrix.

```
function [permutation] = permutation(num_nodes_per_element)

permutation = zeros(num_nodes_per_element ^ 2, 2);

r = 1;
c = 1;
for i = 1:num_nodes_per_element^2
    permutation(i,:) = [r, c];
    if c == num_nodes_per_element
        c = 1;
        r = r + 1;
    else
        c = c + 1;
    end
end
```

#### 3.3 mesh.m

This function performs the meshing.

```
function [num\_nodes, num\_nodes\_per\_element, LM, coordinates] = mesh(L,
   → num_elem, shape_order)
num\_nodes = (shape\_order - 1) * num\_elem + 1;
% for evenly-spaced nodes, on a 3-D mesh. Each row corresponds to a node.
coordinates = zeros(num_nodes, 3);
\% in 1-D, the first node starts at (0,0), and the rest are evenly-spaced
for i = 2:num\_nodes
   coordinates(i,:) = [coordinates(i-1, 1) + L/(num\_nodes - 1), 0, 0];
end
% Which nodes correspond to which elements depends on the shape function
% used. Each row in the LM corresponds to one element.
num_nodes_per_element = shape_order;
LM = zeros (num_elem, num_nodes_per_element);
for i = 1:num_elem
    for j = 1:num_nodes_per_element
        LM(i,j) = num\_nodes\_per\_element * (i - 1) + j - (i - 1);
```

```
end
end
end
```

#### 3.4 BCnodes.m

This function applies boundary conditions.

```
% Script to return the node numbers associated with different types of
\%\ boundary\ conditions
function [dirichlet_nodes, neumann_nodes, a_k] = BCnodes(left, right,
   → left_value, right_value, num_nodes)
% arrays that hold the nodes in the first row and the values in each column
dirichlet_nodes = [];
neumann\_nodes = [];
% assign the nodes to either dirichlet or neumann BCs
i = 1;
switch left
    case 'Dirichlet'
        dirichlet_nodes(1, i) = 1;
        dirichlet_nodes(2, i) = left_value;
    case 'Neumann'
        neumann\_nodes(1, i) = 1;
    otherwise
        disp ('You_entered_an_incorrect_field_for_the_type_of_BC_on_the_left_
           → boundary.');
end
i = i + 1;
switch right
    case 'Dirichlet'
        dirichlet_nodes(1, i) = num_nodes;
        dirichlet_nodes (2, i) = right_value;
    case 'Neumann'
        neumann_nodes(1, i) = num_nodes;
    otherwise
        disp ('You_entered_an_incorrect_field_for_the_type_of_BC_on_the_right_
           → boundary.');
end
a_k = [];
if isempty(dirichlet_nodes)
    disp('no_dirichlet_nodes')
else
    a_k = dirichlet_nodes(2,:);
end
```

## 3.5 shapefunctions.m

This function contains the library of shape functions.

```
: shape functions in the master domain
% dN
            : derivative of the shape functions with respect to xe
% x_{-}xe
           : x as a function of xe
% dx_{-}dxe
          : derivative of x with respect to xe
\hookrightarrow LM, elem)
% shape functions and their derivatives
N = \mathbf{zeros}(\operatorname{shape\_order}, 1);
dN = zeros (shape_order, 1);
switch shape_order
    case 2
       N(1) = (1 - xe) . / 2;
       N(2) = (1 + xe) ./ 2;
       dN(1) = -1/2;
       dN(2) = 1/2;
    case 3
       N(1) = xe .* (xe - 1) ./ 2;
       N(2) = - (xe - 1) \cdot * (1 + xe);
       N(3) = xe .* (1 + xe) ./ 2;
       dN(1) = xe - 1/2;
       dN(2) = -2 .* xe;
       dN(3) = 1/2 + xe;
    otherwise
        disp('You_entered_an_unsupported_shape_function_order.');
end
\% x(xe) transformation to the parametric domain
x_x = 0.0:
dx_dxe = 0.0;
for i = 1: shape\_order
   x_x = x_x + coordinates(LM(elem, i)) * N(i);
    dx_dxe = dx_dxe + coordinates(LM(elem, i)) * dN(i);
end
```

### 3.6 quadrature.m

This function selects the quadrature rule.

```
function [wt, qp] = quadrature(shape_order)

switch shape_order
    case 2
    wt = [1.0, 1.0];
    qp = [-sqrt(1/3), sqrt(1/3)];
    case 3
    wt = [5/9, 8/9, 5/9];
    qp = [-sqrt(3/5), 0, sqrt(3/5)];
    otherwise
```

#### 3.7 condensation.m

This function separates out the matrix equation as in Eq. (22).

```
% Performs static condensation and removes Dirichlet nodes from the global
\% \ matrix \ solve \ K * a = F
% To illustrate the process here, assume that the values at the first and
% last nodes (1 and 5) are specified. The other nodes (2, 3, and 4) are
\% unknown. For a 5x5 node system, the following matrices are defined:
\% K =
                 K(1,1)
                         K(1,2)
                                  K(1,3)
                                          K(1,4)
                                                   K(1,5)
%
                         K(2,2)
                                  K(2,3)
                                          K(2,4)
                 K(2,1)
                                                   K(2,5)
%
                 K(3,1)
                         K(3,2)
                                  K(3,3)
                                          K(3,4)
                                                   K(3,5)
%
                                  K(4,3)
                                          K(4,4)
                 K(4,1)
                         K(4,2)
                                                   K(4,5)
%
                 K(5,1)
                        K(5,2)
                                  K(5,3)
                                          K(5,4)
                                                   K(5,5)
\% K_-uu_-rows =
                 K(2,1)
                         K(2,2)
                                  K(2,3)
                                          K(2,4)
                                                   K(2,5)
                 K(3,1) \quad K(3,2)
                                 K(3,3)
                                          K(3,4)
                                                   K(3,5)
%
                 K(4,1) \quad K(4,2)
                                 K(4,3)
                                          K(4,4) K(4,5)
\% K_-uu =
                         K(2,2) \quad K(2,3)
                                          K(2,4)
%
                         K(3,2) \quad K(3,3) \quad K(3,4)
%
                         K(4,2) \quad K(4,3) \quad K(4,4)
% K_{-}uk =
                 K(2,1)
                                                   K(2,5)
%
                 K(3,1)
                                                   K(3,5)
%
                 K(4,1)
                                                   K(4,5)
% K_{-}ku =
                         K(1,2) K(1,3) K(1,4)
%
%
%
%
                         K(5,2) K(5,3) K(5,4)
% K_{-}kk =
                K(1,1)
                                                   K(1,5)
%
%
%
%
                K(5,1)
                                                   K(5,5)
```

```
function [K_uu, K_uk, F_u, F_k] = condensation(K, F, num_nodes,

    dirichlet_nodes)
K_uu_rows = zeros(num_nodes - length(dirichlet_nodes(1, :)), num_nodes);
K_uk = zeros(num_nodes - length(dirichlet_nodes(1,:)), length(dirichlet_nodes
   \hookrightarrow (1,:));
F_u = zeros(num\_nodes - length(dirichlet\_nodes(1, :)), 1);
F_{-k} = zeros(length(dirichlet_nodes(1,:)), 1);
K_{row} = 1;
i = 1;
            % index for dirichlet_nodes
j = 1;
            % index for condensed row
            % index for unknown condensed row
1 = 1;
            % index for known condensed row
m = 1;
for K_{row} = 1:num_{nodes}
    if (find(dirichlet_nodes(1, :) == K_row))
        F_{-k}(m) = F(K_{-row});
        m = m + 1;
        i = i + 1;
    else
        K_uu_rows(j,:) = K(K_row,:);
        F_u(1) = F(K_row);
        j = j + 1;
        1 = 1 + 1;
    end
end
% perform static condensation to remove Dirichlet node columns from solve
K_uu = zeros(num_nodes - length(dirichlet_nodes(1, :)), num_nodes - length(
   \hookrightarrow dirichlet_nodes (1, :));
K_{\text{-}}column = 1;
                 % index for dirichlet nodes
i = 1;
                 % index for condensed column
i = 1;
m = 1;
                 % index for K_{-}uk column
for K_column = 1:num_nodes
    if (find(dirichlet_nodes(1, :) = K_column))
        K_uk(:,m) = K_uu_rows(:, K_column);
        m = m + 1;
        i = i + 1;
    else
        K_uu(:,j) = K_uu_rows(:, K_column);
        j = j + 1;
    end
end
```

#### 3.8 postprocess.m

This function postprocesses the FE solution and transforms it back to the physical domain using a linear system solve as described in Eq. (24).

```
function [solution_FE, solution_derivative_FE] = postprocess(num_elem,
   → parent_domain, a, LM, num_nodes_per_element, shape_order, coordinates,
   → physical_domain)
b = zeros(1, shape\_order);
A = zeros(shape\_order);
m = length(parent\_domain) + 1;
p = 1;
u_sampled_solution_matrix = zeros(num_elem, length(parent_domain));
u_sampled_solution_derivative_matrix = zeros(num_elem, length(parent_domain));
for elem = 1:num_elem
    % over each element, figure out the polynomial by solving a linear
    \% system, Ax = b, where A depends on the order of the shape functions
    for i = 1:num_nodes_per_element
        b(i) = a(LM(elem, i));
    end
    for j = 1: shape-order % loop over the rows of A
        coordinate = coordinates (LM(elem, j));
        for l = 1: shape_order % loop over the columns of A
            A(j,l) = coordinate . (l - 1);
        end
    end
    % solve for the coefficients on the actual polynomial
    coefficients = A \setminus (b');
    % determine the solution over the element
    solution_over_element = zeros(1, length(parent_domain));
    element_domain = linspace (coordinates (LM(elem, 1)), coordinates (LM(elem,
       → num_nodes_per_element)), length(parent_domain));
    for i = 1:num_nodes_per_element
        solution_over_element = solution_over_element + coefficients(i) .* (
           \hookrightarrow element_domain . (i - 1);
    end
    % determine the derivative over the element
    derivative_over_element = zeros(1, length(parent_domain));
    for i = 2:num_nodes_per_element % the derivative of the constant is zero
        derivative_over_element = derivative_over_element + coefficients(i) .*
           \hookrightarrow (i - 1) .* (element_domain .^ (i - 2));
    end
    % put into a matrix
    u_sampled_solution_matrix(p,:) = solution_over_element;
    u_sampled_solution_derivative_matrix(p,:) = derivative_over_element;
    p = p + 1;
end
% assemble solution and derivative into a single vector
solution_FE = zeros(1, length(physical_domain));
```

```
solution_derivative_FE = zeros(1, length(physical_domain));
for i = 1:length(u_sampled_solution_matrix(:,1))
    if i == 1
       solution_FE(1:length(u_sampled_solution_matrix(i,:))) =

    u_sampled_solution_matrix(i,:);
       solution_derivative_FE(1:length(u_sampled_solution_derivative_matrix(i
          else
       solution_FE(m:(m + length(u_sampled_solution_matrix(1,:)) - 2)) =

    u_sampled_solution_matrix(i,2:end);
       solution_derivative_FE (m: (m + length (
          \hookrightarrow u_sampled_solution_derivative_matrix (1,:) - 2) =

    u_sampled_solution_derivative_matrix(i,2:end);
       m = m + length(u\_sampled\_solution\_matrix(1,:)) - 1;
   end
end
```