

# INEL 4301 – COMMUNICATION THEORY ENGINEERING DESIGN PROJECT

**Due – 11:50 PM, Fri., Nov. 19, 2021**

Prof. Domingo Antonio Rodríguez – Fri., Oct. 01, 2021

## Analog and Digital Deep Underwater Acoustic Communications Using Double Sideband Suppressed Carrier Communication Systems

The objective of this [design project](#) is to use a double sideband suppressed carrier ([DSB-SC](#)) communications system for the transmission & reception of [dtmf signals](#) using analog (**Part 1**) and digital (**Part 2**) communications in an [underwater medium](#). In this engineering project, a [uniformly time-sampled](#) signal is considered to be an analog signal if  $20 \log_{10} R_a < -90$  dB, where  $R_a$  is defined as its [amplitude resolution](#).

### Part 1.- ANALOG COMMUNICATIONS:

The [maximum frequency content](#) of an analog continuous-time [dtmf](#) signal is assumed to be  $F_V = 2000\text{Hz}$  and the “one-sided” [channel bandwidth](#) is said to be  $B = 12000\text{Hz}$ . A receiver must be designed to recover the signal  $x_r(t) \approx s(t)$  (see [Fig. 3](#)).

The channel itself is modeled as a composition of two basic systems, an **ideal, linear phase, low-pass filter**  $T_C$ , with [cut-off frequency](#)  $f = F_L$ , and a signal [summing system](#),  $T_N$ , where the channel [underwater noise signal](#),  $n(t)$ , is added to the output of the linear phase filter  $T_C$ . This DSB-SC communications channel is given the name  $T_{CN} = T_{AM}$  (see [Fig. 2](#)).

The overall sampling frequency of the DSB-SC communications system must be set to a value greater than **twice the maximum frequency** ([Nyquist-Shannon sampling theorem](#)) content of the output of the demodulator at the receiver side. That is,  $F_S > 2(2f_c + F_V)$ , where  $f_c$  is the carrier frequency of the modulator (demodulator) and must be  $6000 < f_c < 10000$ .

The input signal  $x_m(t) = s(t) + g(t)$  to the modulator is the sum of a “**wanted**” [dtmf](#) signal  $s(t)$  and an “**unwanted**” [interference signal](#)  $g(t)$ . After the demodulator, an ideal, linear phase, low-pass filter,  $T_L$  is used, with cut-off frequency  $F_M = 2000\text{Hz}$ , to recover the “**wanted**” [dtmf](#)  $s(t)$  (see [Fig. 1](#)).

## Part 1.- PROJECT TASKS:

1. **Design** an ideal, linear phase, [band-pass filter](#) to eliminate the input interference signal  $g(t)$ . Important [figures of merit](#) to rate this task will be center frequency, filter's order, and filter's bandwidth.
2. **Design** an ideal, linear phase, [low-pass filter](#) to model the channel filter  $T_C$ . Important [figures of merit](#) to rate this task will be filter's bandwidth and filter's order.
3. **Modify** the power of the noise signal  $n(t)$  and describe the computed channel's output [signal/noise ratio](#) (SNR) characteristics. For this task, assume the SNR at the channel's input is equal to 80 dB. Important [figures of merit](#) to rate this task will be the lowest SNR obtained at the channel's output, allowing [intelligibility](#) of the wanted output signal, as well as the average and variance values of the [AWGN](#).
4. **Design** an ideal, linear phase, [band-pass filter](#)  $T_R$  to reduce the [receiver's noise](#) and improve the [signal/noise ratio](#) at the input of the demodulator's subsystem when compared to the [signal/noise ratio](#) at the output of the channel; that is, by comparing the [spectral densities](#) between the channel output signal  $y_{co}(t)$  and the demodulator input signal  $y_{di}(t)$ . Important [figures of merit](#) to rate this task will be center frequency, filter's order, filter's bandwidth, as well as the highest SRN obtained at the filter's output.
5. **Design** a linear phase, [low-pass filter](#), with cut-off frequency  $F_V = 2000\text{Hz}$  for the receiver's filter  $T_L$ . The most important figure of merit for this task will be the lowest time-delay,  $D_r = \left(\frac{M_L-1}{2}\right)T_s$ , obtained for this filter, where  $M_L$  is the order of the filter and  $T_s = \frac{1}{F_s}$  is the overall [sampling time](#) of the system.
6. **Design** an ideal, linear phase, [band-pass filter](#) ([upper sideband](#)) to eliminate the input interference signal  $g(t)$ . Proceed to leave all the designed subsystems without modifications, except for the **band pass filter** at the **transmitter** which will be modified and substituted by this new **upper sideband** band pass filter. Important [figures of merit](#) to rate this task will be the filter's order.

## Part 2.- DIGITAL COMMUNICATIONS:

In this part of the design project, an analog modulating signal is [quantized](#) in order to produce a digital signal which serves as input to the modulator of the designed system in **Part 1**.

## Part 2.- PROJECT TASKS:

- 2.1 Proceed** to quantize the modulating signal  $x_m(t)$  used in **Part 1** of the project. **Record** the output signal  $x_{mq}(t)$  of the quantizer. A figure of merit for this task will be the lowest number of quantization levels used. Record intelligible  $x_r(t)$ .
- 2.2 Proceed** to quantize the desired or wanted signal  $s(t)$  and the interference or unwanted signal  $g(t)$ , separately. Use this added quantized signal  $\overline{x_{mq}}(t)$  as a new modulating signal for the system, repeating **Task 2.1**, above.

Hand in a formal design report in **.pdf** format and name the script for **Part 1** "s086gpzz115" and the script for **Part 1, Task 6**, "s086gpzz166." Name the script for **Part 2.1** "s086gpzz201". Name script for **Part 2.2** "s086gpzz202." These script files must plot, in the time domain, segments of the input signals and output signals of every subsystem of the designed DSB-SC system. It must also plot the entire frequency axis of the magnitude of the spectrum of every input signal and output signal of every subsystem of the designed DSB-SC system. Please, follow these [report format guidelines](#).

Hand in the following [.WAV](#) files:

**S086GPZZ\_EDP\_INP1s** (input **Part 1**:  $s(t) = \text{"dtmfzz.wav"}$ )  
**S086GPZZ\_EDP\_INP1g** (input **Part 1**:  $g(t) = \text{"uwtdzz.wav"}$ )  
**S086GPZZ\_EDP\_INP1n** (input **Part 1**:  $n(t) = \text{"noiszz.wav"}$ )  
**S086GPZZ\_EDP\_INP1x** (input **Part 1**:  $x_m(t) = s(t) + g(t) = \text{"dtmfzz.wav"} + \text{"uwtdzz.wav"}$ )  
**S086GPZZ\_EDP\_INP2s** (input **Part 2**:  $Q\{s(t)\} = \text{"qdtmfzz.wav"}$ )  
**S086GPZZ\_EDP\_INP2g** (input **Part 2**:  $Q\{g(t)\} = \text{"quwtdzz.wav"}$ )  
**S086GPZZ\_EDP\_INP2qa** (input **Part 2, Task 1**:  $x_{mq}(t) = Q\{s(t) + g(t)\} = Q\{x_m(t)\}$ )  
**S086GPZZ\_EDP\_INP2aq** (input **Part 2, Task 2**:  $\overline{x_{mq}}(t) = Q\{s(t)\} + Q\{g(t)\}$ )

**S086GPZZ\_EDP\_OUP115** (output **Part 1, Tasks 1-5**:  $x_r(t) \approx \text{"dtmfzz.wav"}$ )  
**S086GPZZ\_EDP\_OUP166** (output **Part 1, Task 6**:  $x_r(t) \approx \text{"dtmfzz.wav"}$ )  
**S086GPZZ\_EDP\_OUP201** (output **Part 2, Task 1**:  $x_r(t) \approx Q\{s(t) + g(t)\}$ )  
**S086GPZZ\_EDP\_OUP202** (output **Part 2, Task 2**:  $x_r(t) \approx Q\{s(t)\} + Q\{g(t)\}$ )

### Remarks:

- 1.- Here,  $Q$  is a Uniform Quantizer System.
- 2.- You must design your own  $s(t)$  signal to test your system.
- 3.- You must design your own  $g(t)$  signal to test your system.
- 4.- You must design your own  $n(t)$  signal to test your system.
- 5.- For **Part 1, Task 6** you need to submit the requested m-script file. This script file is going to be the same as the script for **Part 1, Tasks 1 to 5**. The only difference will be the designed upper single sideband, band-pass filter.

Name of **.zip** folder and the name of the **e-mail subject**:

**Inel4301\_MCWDP\_SXXX\_GPZZ**

**REMEMBER TO INCLUDE TAT INFORMATION**