


$$W = 1500 \text{ lb}$$

$$b = 35 \text{ ft}$$

$$c = 6 \text{ ft}$$

$$v_{st} = 45 \text{ mph} = 39 \text{ knots}$$

$$v_A = 95 \text{ mph} = 83 \text{ kts} \rightarrow \text{manoeuvre speed } (= 42.12 \text{ m/s})$$

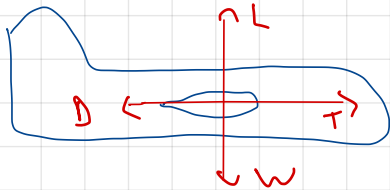
$$v_c = 170 \text{ mph} = 96 \text{ kts} \rightarrow \text{cruising speed}$$

$$v_D = 120 \text{ kts} \rightarrow \text{diving speed}$$

$\rightarrow 132 \text{ kts! (see later calculations)}$

$$C_{L, \max} = 15$$

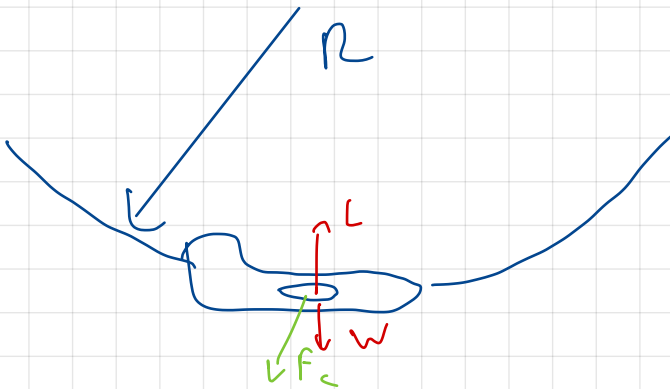
Cruise



$$L = W$$

$$D = T$$

Manoeuvre:



$$L = W + F_c = W + \frac{mv^2}{R}$$

$$n = \frac{L}{W} = 1 + \frac{v^2}{Rg} > 1$$

\hookrightarrow load factor

$$W = L + F_c$$

$$L = W = \frac{mv^2}{R}$$

$$n = 1 - \frac{v^2}{Rg}$$

Stall

$$\left. \begin{aligned} L &= W = \frac{1}{2} \rho V_{st,1}^2 S C_{L,max} \\ L &= nW = \frac{1}{2} \rho V_{st,2}^2 S \cdot C_{L,max} \end{aligned} \right\} \frac{n}{2} \cancel{\rho} \cancel{V_{st,1}^2} \cdot \cancel{S} \cdot \cancel{C_{L,max}} = \frac{1}{2} \rho V_{st,2}^2 \cdot \cancel{S} \cdot \cancel{C_{L,max}}$$

$n V_{st,1}^2 = V_{st,2}^2$

Our design

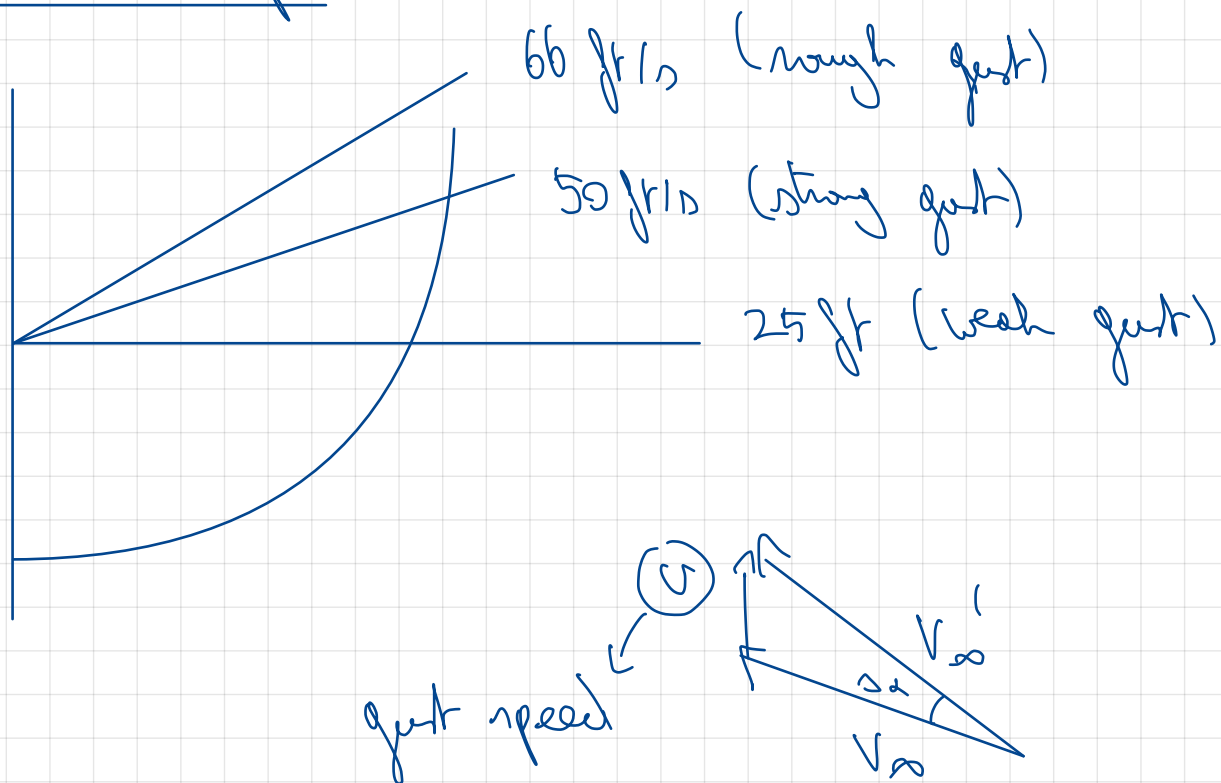
$V_c > 88 \rightarrow V_c = 95$ is good choice (or 96)

$$V_D > 1,25 V_c = 1,25 \times 95 = 119 \text{ kt}$$

$$> 1,50 V_{c,min} = 1,5 \times 88 = 132 \text{ kt}$$

$$V_{st} = \sqrt{\frac{2W}{\rho S C_{L,max}}} = 37,5 \text{ kt} \quad (\text{given } V_D = 39 \text{ kt} > 37,5 \checkmark)$$

Gust envelope



$$L = W = \frac{1}{2} \rho V_{\infty}^2 S C_L \rightarrow a(\alpha + \beta)$$

$$L' = \frac{1}{2} \rho V_{\infty}^2 S C_L' \rightarrow \underbrace{\frac{1}{2} \rho V_{\infty}^2 S a(\alpha + \beta) + \frac{1}{2} \rho V_{\infty}^2 S a D \alpha}_{a(\alpha + D \alpha + \beta)}$$

$$\Delta \alpha = \Delta \alpha = \frac{5}{V_{\infty}'} \\ \Downarrow$$

$$\frac{1}{2} \rho V_{\infty}^2 S a(\alpha + \beta) + \left(\frac{1}{2} \rho V_{\infty}^2 S a \right) V_{\infty}'$$

Wing lift data

$$C_L = a(\alpha + \beta)$$

$$C_L = a_0(\alpha + \beta)$$

$$a = \frac{a_0}{1 + \frac{a_0}{\pi AR}}$$

(fact in slides: $C_L = 0,1 \alpha + 0,1$)

$$AR = \frac{b^2}{S} = \frac{(35 \text{ ft})^2}{270} = 5,8$$

$$\Rightarrow a = \frac{5,729}{1 + \frac{5,729}{\pi \cdot 5,8}} = 4,36 / \text{rad}$$

$$C_L = 0,0762 \alpha + 0,1 \Rightarrow \alpha = \frac{1,4}{0,0762} = 18,47^\circ$$

Lift?

$$n_A^+ = 44 = \frac{L}{W} \Rightarrow L = 44 W = 6600 \text{ lb}$$

Moment?

$$M = \frac{1}{2} \rho v^2 S c_l C_m$$

$$= \frac{1}{2} \cdot 1,225 \cdot 42,2^2 \cdot 19,5 \cdot 7,8 \cdot (-0,007)$$

$$= -277 \text{ Nm} = -2400 \text{ lb} \cdot \text{in}$$

Drag?

$$D = \frac{1}{2} \rho v^2 S C_D$$

$$\hookrightarrow C_D = C_{D0} + C_{Di} = 0,748$$

$$\downarrow$$
$$0,078$$

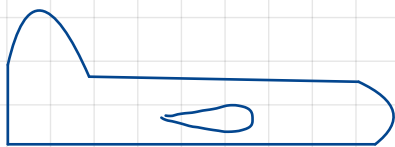
$$\downarrow h C_L^2 = 0,064 \cdot 7,5^2 = 0,73$$

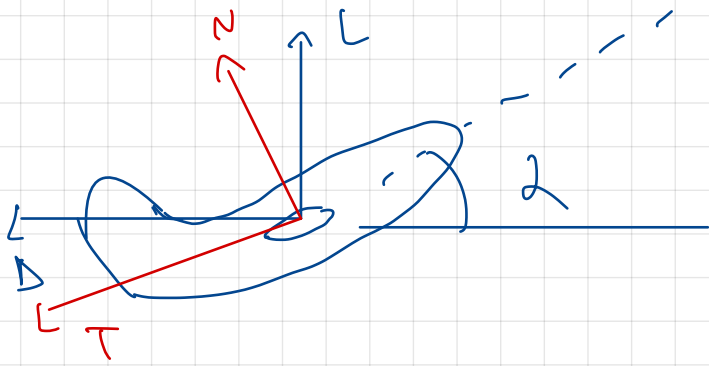
\uparrow

$$h = \frac{1}{\pi A R e} = \frac{1}{\pi 5,8 \cdot 0,845} = 0,064$$

$$= \frac{1}{2} \cdot 1,225 \cdot 42,2^2 \cdot 19,5 \cdot 0,748 \approx 3000 \text{ N}$$

\Rightarrow





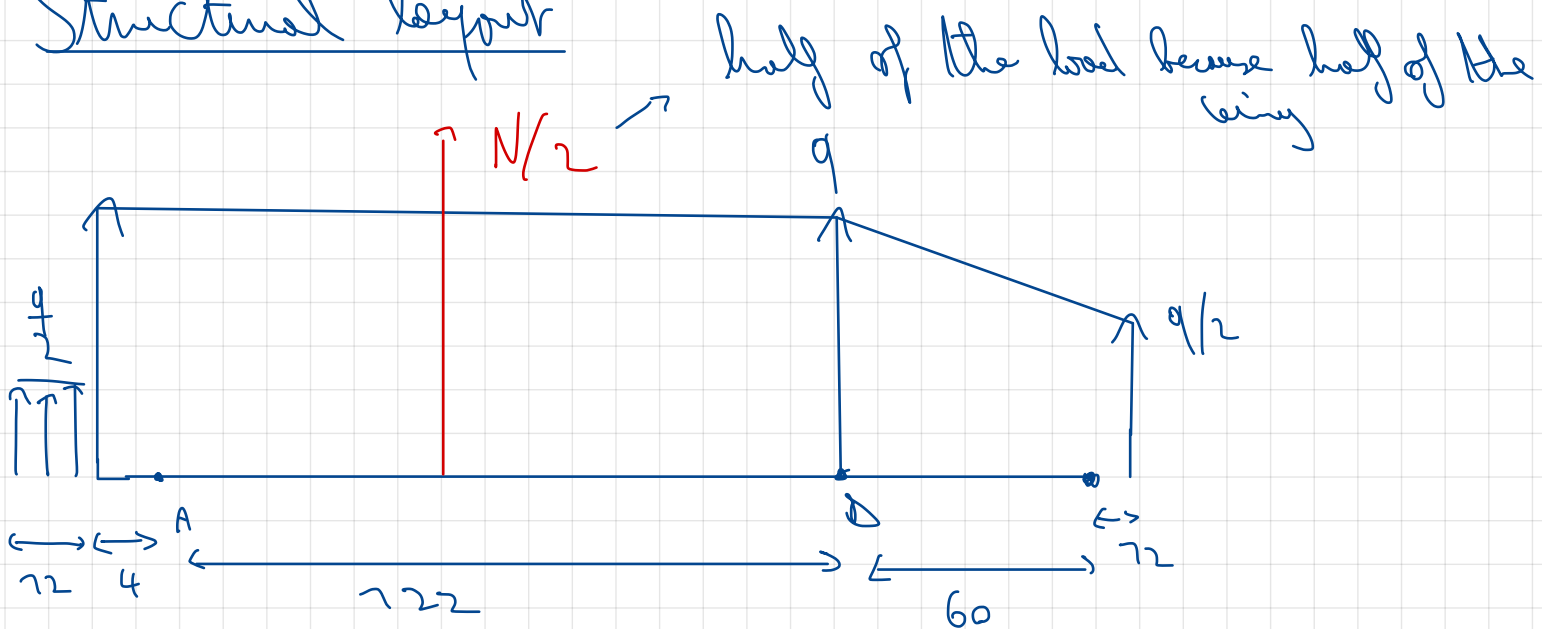
$$N = L \cos \alpha + D \sin \alpha$$

$$T = D \cos \alpha - L \sin \alpha \quad \alpha = 77^\circ$$

$$N = 6500 \text{ lb} \quad (\text{normal})$$

$$T = -7328 \text{ lb} \quad (\text{tangential})$$

Structural layout



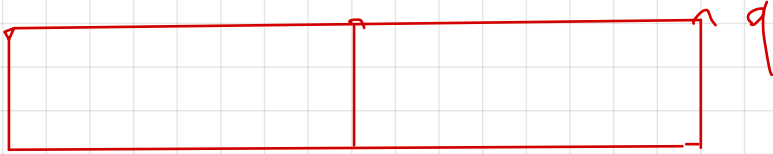
$$q \cdot 726 + \frac{q}{2} \cdot 72 + \frac{q}{2} \cdot \frac{72}{2} + 72 \cdot \frac{q}{2} = N = 6500 \text{ lb}$$

$$\Rightarrow q \cdot 786 = \frac{N}{2} \Rightarrow q_N = \frac{3250}{786}$$

$$= 77.5 \approx 78 \text{ lb/in}$$

Dray distribution

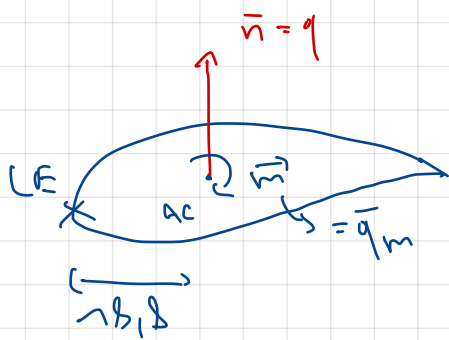
12 198 270



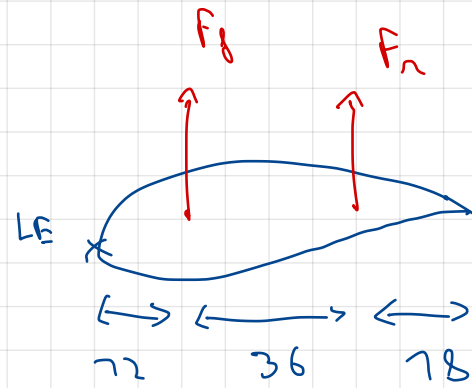
$$q = -\frac{1326}{2 \cdot 198} = -3,35 \text{ lb/in}$$

Moment

$$q_m = -\frac{2400}{2 \cdot 198} = 6 \cdot \text{lb} \cdot \text{in/in}$$



\leftrightarrow



$$F_f = ?$$

$$F_n = ?$$

$$\begin{cases} q_n = F_f + F_n \\ 18,8 q_n - q_m = 12 F_f + 48 F_n \end{cases}$$

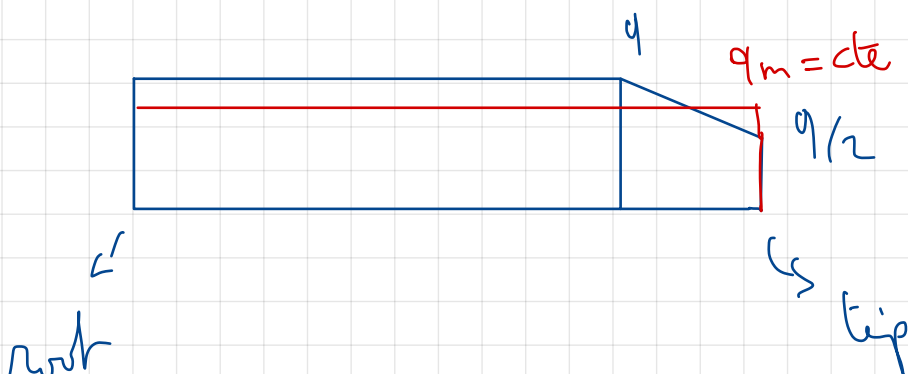
$$\downarrow$$

$$F_n = q_n - F_f$$

$$\begin{aligned} 12 F_f - 48 F_f + 48 q_n &= 18,8 q_n - q_m \\ -36 F_f &= (-18,8 - 48) q_n - q_m \\ F_f &= \frac{(-18,8 - 48) 18 + 6}{-36} \end{aligned}$$

$$= 74,43 \text{ lb/in}$$

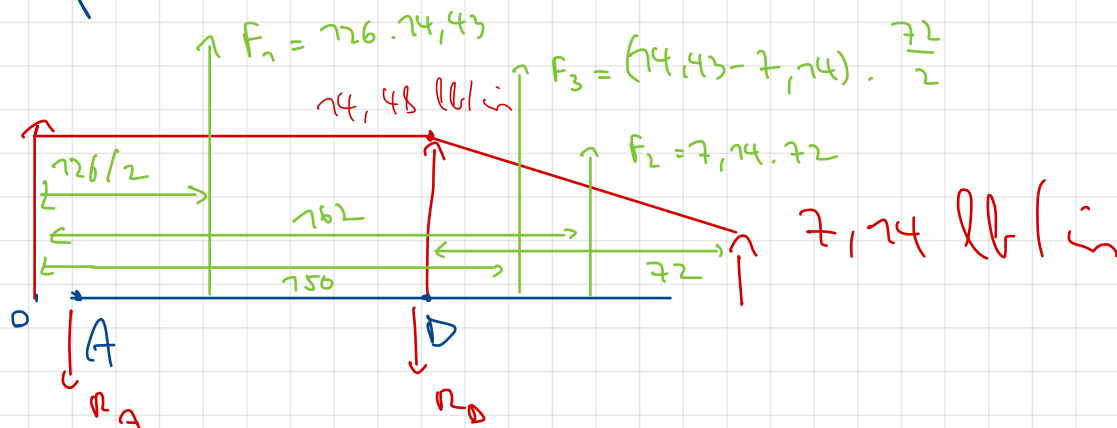
$$\Rightarrow F_n = q_n - F_f = 3,6 \text{ lb/in}$$



at root: $F_f = 74,43 \text{ lb/in}$
 $F_n = 3,6 \text{ lb/in}$

at tip: $F_f = \frac{(18,8 - 48) \cdot 9 + 6}{-36} = 7,74 \text{ lb/in}$
 $F_n = 1,85 \text{ lb/in}$

tip



force & moment eqs to find R_A & R_D

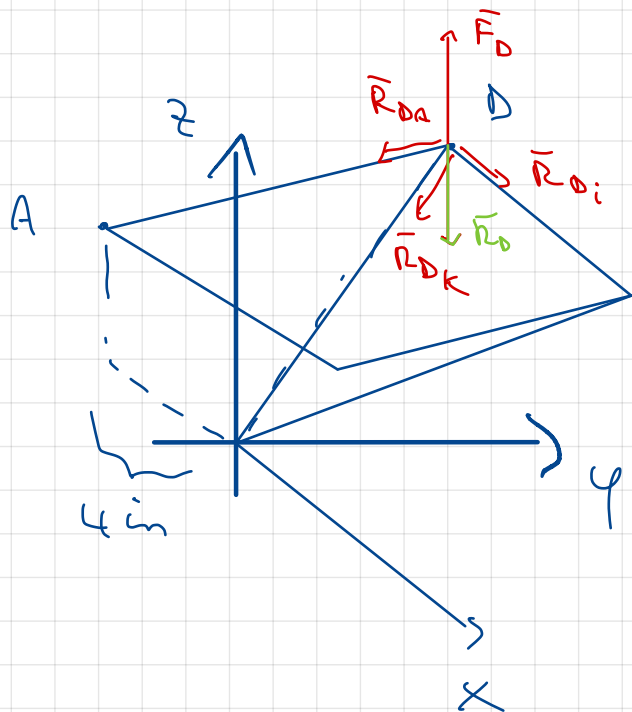
$$\begin{cases} F_1 + F_2 + F_3 = R_A + R_D & (1) \\ -4R_A - 126R_D + F_1 \cdot 63 + F_2 \cdot 162 + F_3 \cdot 150 = 0 & (2) \end{cases}$$

(2) - 4 · (1)

$$122R_D = 59F_1 + 158F_2 + 146F_3$$

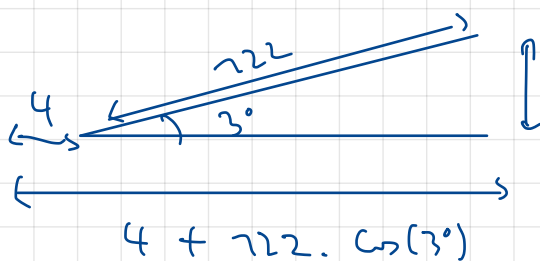
$$R_D = \frac{59F_1 + 158F_2 + 146F_3}{122} = 1847 \text{ lb}$$

$$\begin{aligned} (1): R_A &= F_1 + F_2 + F_3 - R_D \\ &= (726 \cdot 74,43) + (7,74 \cdot 72) + (74,43 - 7,74) \cdot 36 \\ &\quad - 1847 = 776 \text{ lb} \end{aligned}$$



$$\vec{F}_D + \vec{R}_{DA} + \vec{R}_{DK} + \vec{R}_D = \vec{0}$$

	x	y	z
A	-10	4	52
D	-10	125.8	58.4
I	26	125.8	57.9
F	26	4	57.5
K	0	0	0



$$D_z = 52 + \sin(3^\circ) \cdot 122 = 58.4$$

$$\begin{aligned} \vec{D}_A &= (-10 + 10; 4 - 125.8; 52 - 58.4) \\ &= (0; -121.8; -6.4) \end{aligned}$$

$$\begin{aligned} \|\vec{D}_A\| &= \sqrt{(-121.8)^2 + (-6.4)^2} \\ &= 121.97 \end{aligned}$$

$$\vec{e}_{DA} = (0; -0.9986; -0.0523)$$

	$\hookrightarrow t_x$	$\hookrightarrow t_y$	$\hookrightarrow t_z$
\vec{e}_{DA}	0	-0,9986	-0,0523
\vec{e}_{DI}	0,9999	0	-0,0739
\vec{e}_{DK}	0,0779	-0,9048	-0,4298
$\vec{F}_D \rightarrow \vec{e}_\perp$	0,0739	-0,0523	0,9885

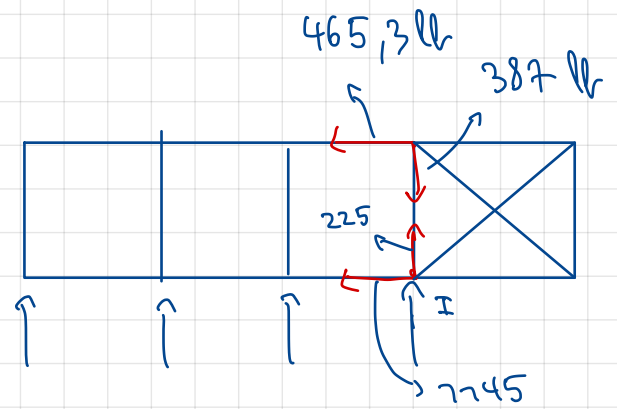
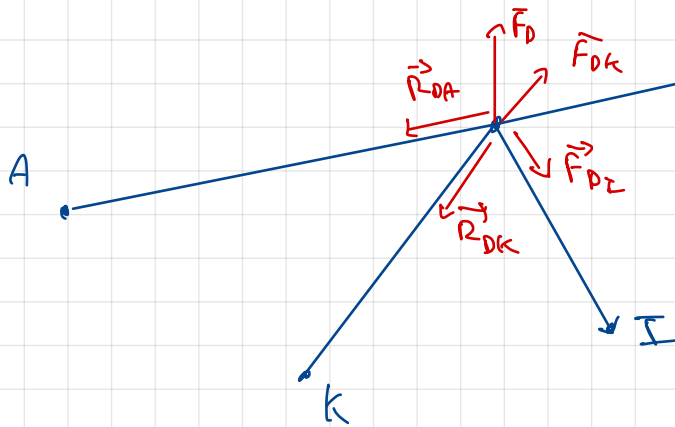
$$\vec{e}_\perp = \vec{e}_{DI} \times \vec{e}_{DK}$$

$$\begin{aligned} / \vec{e}_x \quad & 0 \cdot R_{DA} + 0,9999 R_{DI} + 0,0779 R_{DK} \\ & + 0,0739 F_D = 0 \end{aligned}$$

$$\Rightarrow R_{DA} = -4653 \text{ N}$$

$$R_{DK} = 5028 \text{ N}$$

$$R_{DI} = -387 \text{ N}$$



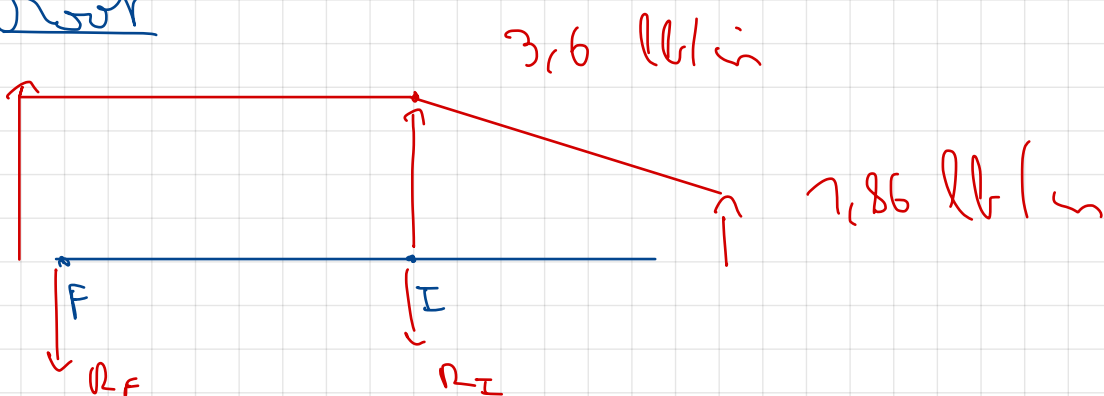
↓
By knowing the reaction
forces you can dimension
the trusses

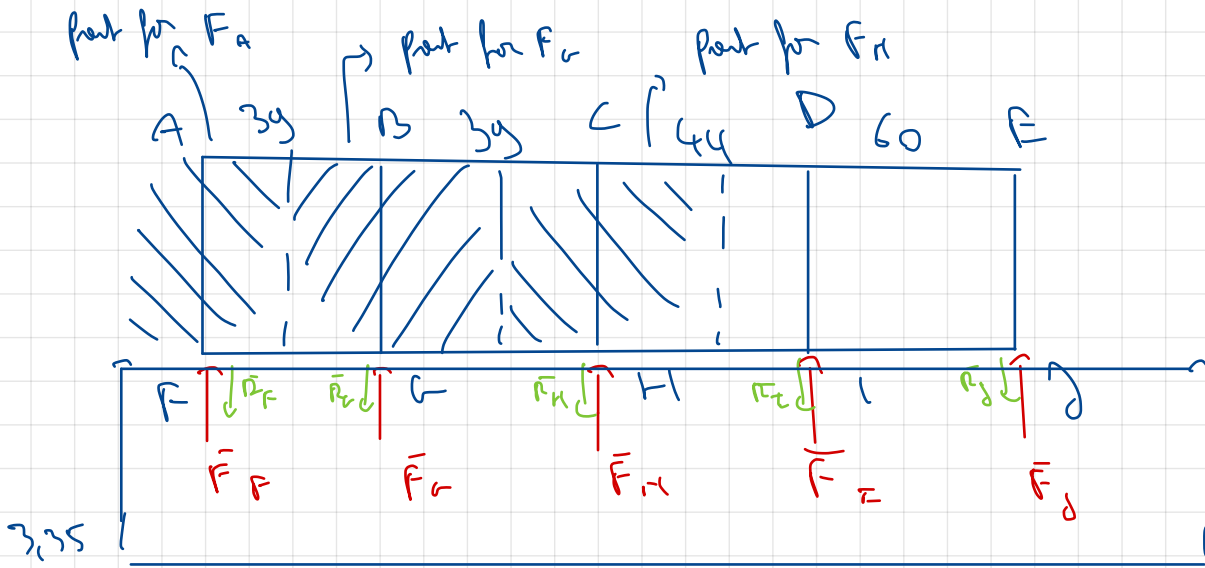
$$R_{IF} = -7745 \text{ lb}$$

$$R_{ID} = -225 \text{ lb}$$

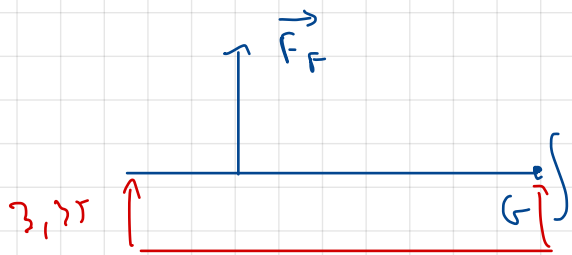
$$R_{Ik} = 7254 \text{ lb}$$

roof



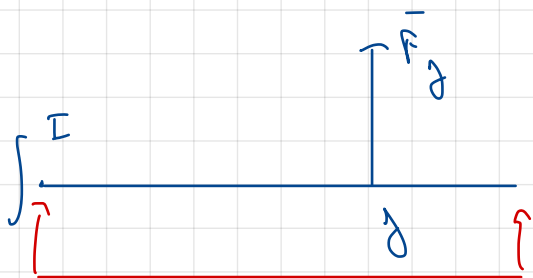


$$F_C = 39 \cdot 3,35 = 130 \text{ kN}$$



$$39 \bar{F}_F = 43 \cdot 3,35 \cdot \frac{43}{2}$$

$$\begin{aligned} \bar{F}_F &= \frac{43}{39} \cdot 3,35 \cdot 27,5 \\ &= 79,4 \text{ kN} \end{aligned}$$



$$60 \bar{F}_d = 72 \cdot 3,35 \cdot \frac{72}{2}$$

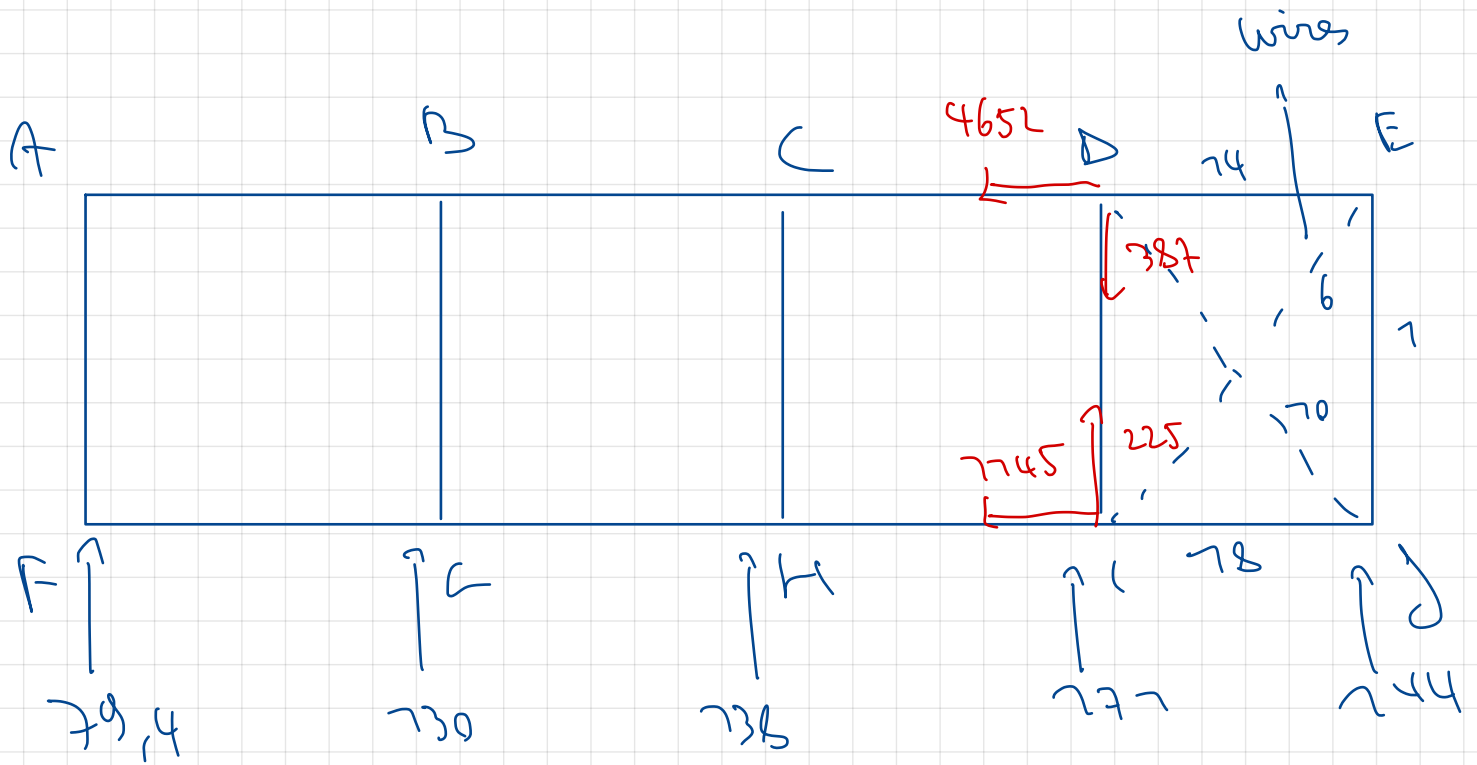
$$\bar{F}_d = 744 \text{ kN}$$

$$F_H = 738 \text{ kN}$$

$$F_Z = 777 \text{ kN}$$

$$F_F = \left(4 + \frac{39}{2}\right) \cdot q = 78,7 \quad (\text{alternative way to calculate})$$

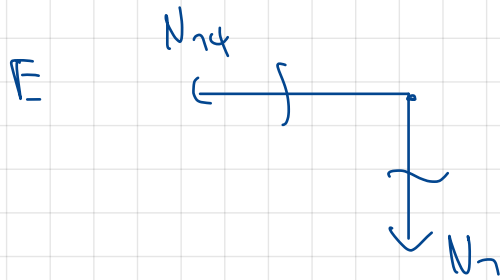
faster but less accurate



$N_{ed} = \text{force due to the normal force}$

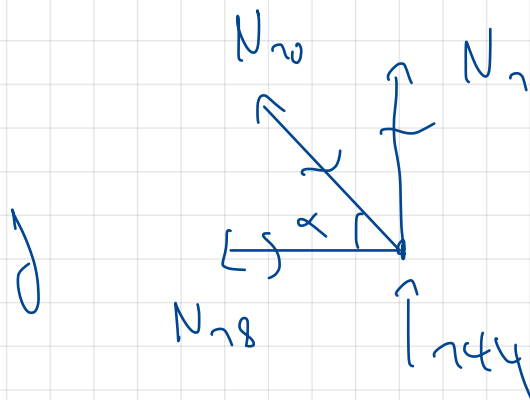
only one of 6 or 70 is in tension, so only one works at a time because compression doesn't exist in wires

Suppose 70 is in tension:



$$N_7 = 0$$

$$N_{74} = 0$$



$$N_7 = 0$$

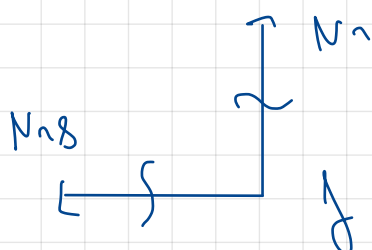
$$\sum F_x = -N_{78} - N_{70} \cos \alpha = 0 \Rightarrow N_{78} = -N_{70} \cos \alpha$$

$$\sum F_y = N_{70} \sin \alpha + 744 = 0 \quad N_{70} = -\frac{744}{\sin \alpha} < 0$$

↓

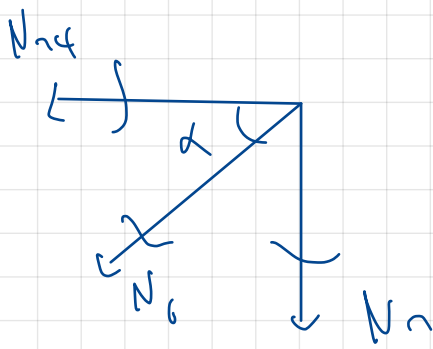
Compression so doesn't exist, we throw 70 and keep 6 ▽

⇒ 6 is in tension



$$N_7 = -744$$

$$N_{78} = 0$$



$$\sum \vec{F}_y = -N_7 - N_6 \sin \alpha = 0$$

$$N_6 = -\frac{N_7}{\sin \alpha} > 0$$

$$\sum \vec{F}_x = -N_4 - N_6 \cos \alpha = 0$$