# Validation of Spent Nuclear Fuel Output by Cyclus, a Fuel Cycle Simulator Code

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## INTRODUCTION

Cyclus [1], a nuclear fuel cycle simulator, was used to simulate the United States' nuclear fuel cycle from 1967 through 2013. The spent nuclear spent nuclear fuel (SNF) inventory from the Cyclus simulation was compared to the SNF inventory from the Department of Energy (DOE) sponsored Used Nuclear Fuel Storage, Transportation & Disposal Analysis Resource and Data System (UNFST&DARDS) Unified Database (UDB) [2]. The UDB provides comprehensive and consistent technical data on reactor sites and SNF from the beginning of nuclear reactor operation in the United States (US) until 2013. This comparison between Cyclus and UDB establishes a realistic validation of Cyclus' capability to produce total spent fuel mass and accurate isotopic compositions that closely match reality.

## BACKGROUND

Cyclus is an agent-based nuclear fuel cycle simulation framework [3], which means that each entity (i.e. Region, Institution, or Facility) in the fuel cycle is modeled as an agent. Cycamore [4] provides agents to represent process physics of various components of the nuclear fuel cycle (e.g. mine, fuel enrichment facility, reactor) [5]. The nuclear fuel assemblies tracked within the simulation are recipe-based. Recipes specify mass fractions for each isotope for fresh and spent fuel. They are calculated ahead of time using neutronics depletion analysis tools such as ORIGEN [6], then entered directly into the fuel cycle simulation [7].

## MOTIVATION

The US is currently considering various and geologic disposal options [8]. Decisions such as waste package spacing, waste repository size, and geometry will be influenced by key criteria such as thermal load of waste packages and the thermal capacity of the selected geologic host media. Waste package thermal evolution depends on the decay heat contribution from each isotope in the spent fuel. Therefore, to correctly simulate loading of a waste repository based on thermal constraints in Cyclus, the simulation must first give isotopic compositions and spent fuel masses that closely replicate reality.

## METHODOLOGY

A Cyclus simulation of the US nuclear fuel cycle was created using published data of the 112 commerical nuclear reactors that have operated since 1967 in the US. The reactor deployment data was obtained from Power Reactor Information System (PRIS) reactor database [9]. Relevant data includes country, reactor unit, reactor type, net capacity (MWe), first

grid date, and shutdown date. US' reactor data was extracted and used to populate the Cyclus simulation. The recipes used in the Cyclus simulations are taken from a reference depletion calculation done using ORIGEN [6] for burnup of 51 and 33 GWD/MTU. They were also used in [10, 11].

Jinja2 [12], a Python templating language, was then used in Python to render the data into an input file that is accepted by Cyclus. The output file produced by Cyclus was also analyzed using Python.

The assumptions made for this Cyclus simulation include:

1. Cycle time is assumed to be 18 months.
2. Refueling time is assumed to be 1 month.
3. There is isotopic decay.

The UDB database contains commercial SNF information from 1967 through 2013. Data such as initial enrichment, burnup, mass of spent fuel and discharged dates were collected from multiple sources [7]. Meanwhile, data such as isotopic compositions, heat and activity were determined by performing irradiation and decay calculations on every fuel assembly based on the collected data.

The UDB dataset used for this work included discharged fuel assembly data per reactor, specific isotopic concentrations and decay heat for each assembly along with its discharge date [2]. The UDB dataset was imported into Python, processed and compared with Cyclus simulation output. All scripts and data used are available in [13].

## RESULTS AND ANALYSIS

The primary outcome of this validation is to provide comparisons between Cyclus data and UDB data for spent fuel mass and isotopic contributions to the spent fuel mass.

### Cumulative Total Spent Fuel Mass Comparison

Figure 1 shows the cumulative spent fuel mass for both Cyclus and UDB data from 1967 to 2013. The spent fuel mass estimated by Cyclus is larger than the UDB calculation before the year 2000. After 2000, the UDB calculation reports a larger spent fuel mass. The discrepancies can be attributed to rigidity of Cyclus simulation input with respect to cycle and refueling duration. In Cyclus, the user specifies refueling and cycle times for each reactor as constant integer months. In reality, the cycle and refueling durations vary throughout each reactor's lifetime and are not exact integer multiples of one month.

The Nuclear Energy Institute (NEI) reported significant variance in the refueling period for US reactors. While average refuelling time in 1990 was 104 days, it decreased to average refuelling time of 35 days in 2017 [14].

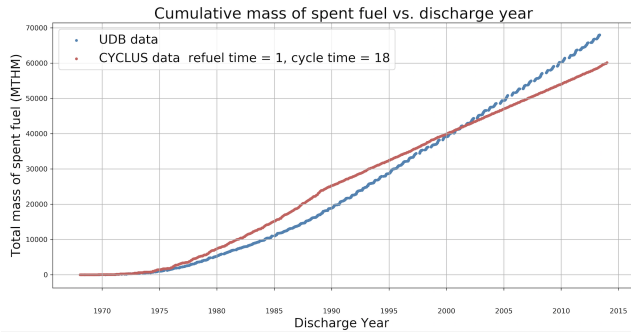Figure 2 includes plots of total spent fuel mass from Cy-

Fig. 1: The total cumulative spent fuel mass against discharge time for CYCLUS and UDB data from 1967 through 2013.
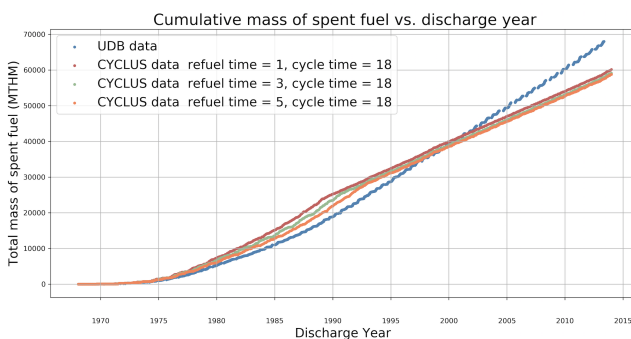


Fig. 2: The total cumulative spent fuel mass against discharge time for CYCLUS and UDB data from 1967 through 2013 for various refueling durations.

CLUS simulations where refueling duration is increased. A longer refueling duration brings the total spent fuel mass from CYCLUS simulations closer to the UDB data before 2000.

The larger cumulative UDB spent fuel mass compared to the CYCLUS simulation after 2000 can be attributed to the real world cycle lengths being shorter on average than the 18 month cycle time assumed in the CYCLUS simulations. The US DOE reported that there was a downward trend of forced outage rates of nuclear reactors from 2000 to 2014. The forced outage rate was 4.24% in 2000 and 2.98% in 2013 [15]. As the rate of forced outages decreased from 2000 to 2013, the
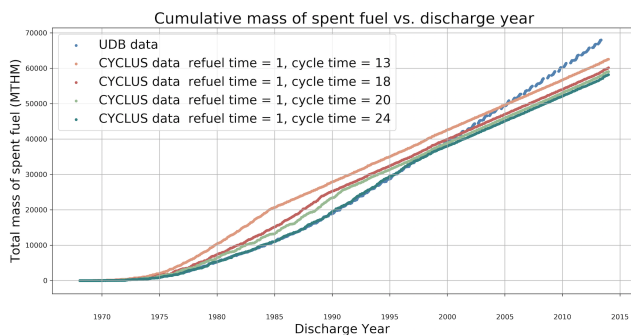


Fig. 3: The total cumulative spent fuel mass against discharge time for CYCLUS and UDB data from 1967 to 2013 for various cycle times.
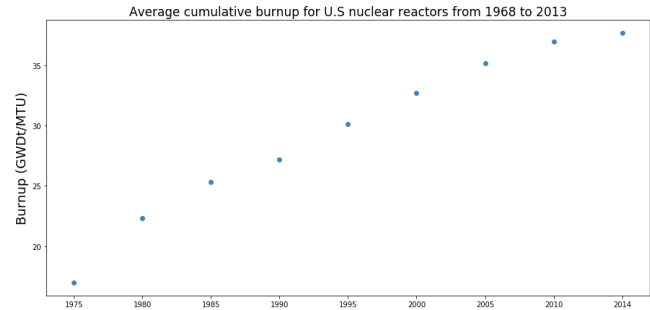


Fig. 4: The average cumulative burnup for U.S. nuclear reactors from 1968 to 2013 [16].
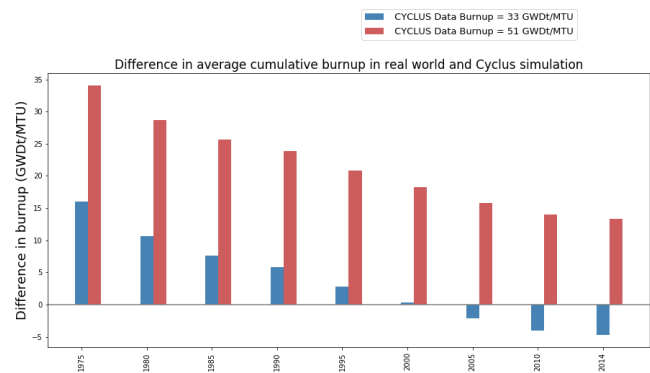


Fig. 5: The difference between average cumulative burnup for U.S. nuclear reactors and burnup used in CYCLUS simulations.

cycle length also decreased.

Figure 3 plots total spent fuel mass from CYCLUS simulations where th varying cycle. A shorter cycle time brings the total spent fuel mass from CYCLUS simulations closer to the UDB data after 2000.

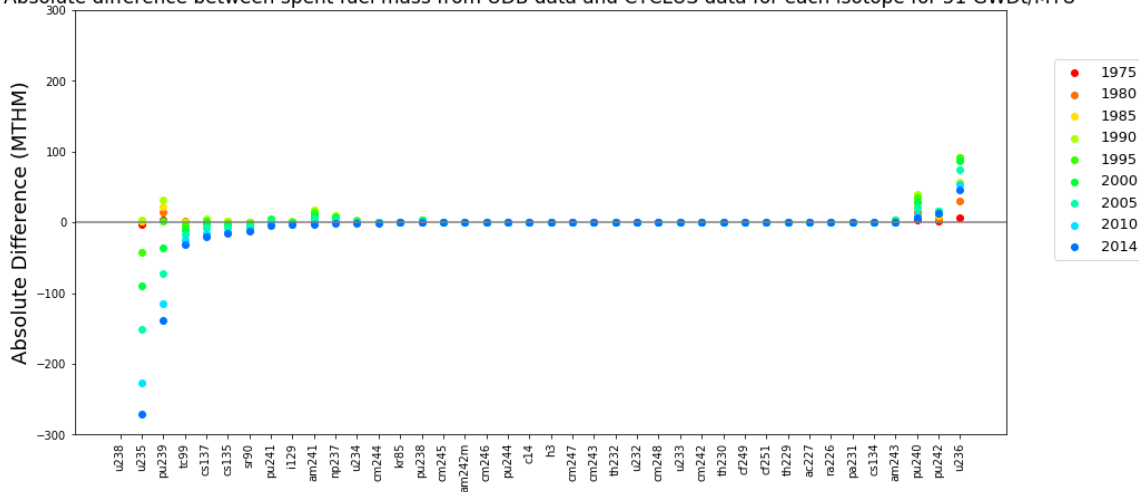*Major Isotopic Composition of Spent Fuel Mass Comparison*

To accurately simulate the U.S. nuclear fuel cycle from 1968 through the present, it important to use spent fuel recipes that have similar burnup in relation to the U.S. nuclear reactor burnup.

Figure 4 shows the average cumulative burnup for U.S. nuclear reactors from 1968 to 2013 [16]. Figure 5 shows the difference between burnup of the spent fuel recipes used in the CYCLUS simulations and cumulative burnup of U.S. nuclear reactors as seen in figure 4. On average, spent fuel burnup of 33 GWD/MTU is closer to the cumulative burnup of U.S. nuclear reactors than 51 GWD/MTU.

Figures 6a and 6b show the cumulative spent fuel isotopic mass difference between UDB and CYCLUS data in 5 year intervals for burnup of 51 GWD/MTU and 33 GWD/MTU correspondingly. The CYCLUS data that had 33 GWD/MTU burnup deviated less compared to the CYCLUS data that had 51 GWD/MTU burnup. This is apparent for $^{236}$U, $^{242}$Pu and $^{240}$Pu. They are similar for the isotopes on the left side of both figures. With an exception of $^{239}$Pu having a substantial larger difference for 33 GWD/MTU than 51 GWD/MTU.
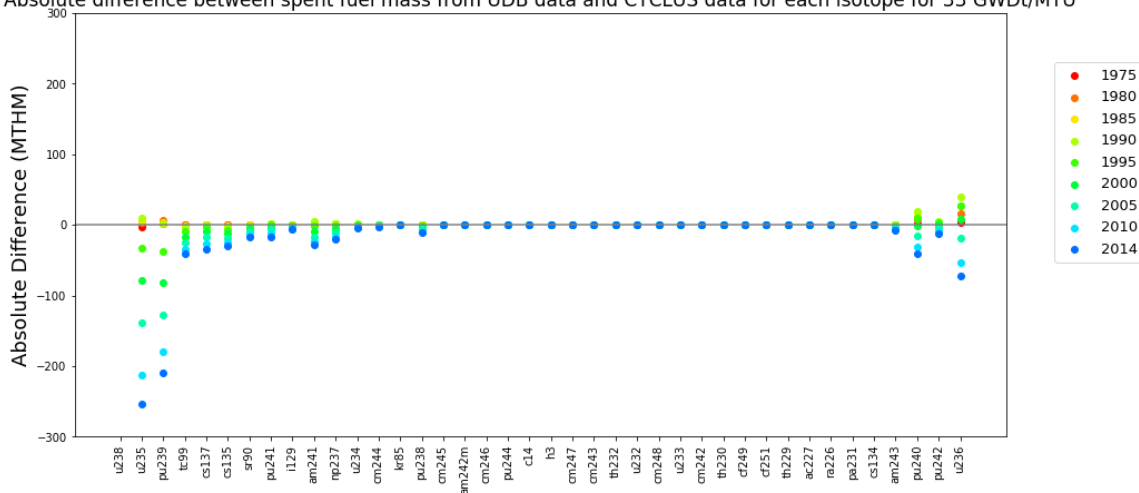
(a) 51 GWD/MTU burnup.



(b) 33 GWD/MTU burnup.



(c) Both burnup states, year 2000 data.

Fig. 6: The absolute difference between spent fuel mass calculated by UDB and CYCLUS for each isotope. Positive difference indicates CYCLUS mass estimate is larger.

The cumulative spent fuel isotopic mass difference between UDB and Cyclus data for the year 2000 (figure 6c) demonstrates the impact of burnup on isotopic composition. In figure 4, at year 2000, the cumulative average U.S. nuclear reactor burnup was very close to 33 GWD/MTU. Therefore, the difference in burnup between the U.S. nuclear reactor burnup and Cyclus data burnup was around 20 GWD/MTU for 51 GWD/MTU burnup and 0 GWD/MTU for 33 GWD/MTU burnup (as seen in figure 5).

As discussed by Wigeland et al [17], $^{240}$Pu, $^{239}$Pu and $^{241}$Am are the most significant long-term decay heat contributors to each waste package. While, $^{238}$Pu, $^{244}$Cm, $^{90}$Sr and $^{137}$Cs are the most significant short term decay heat contributors [17] to each waste package.

In figure 6c, the Cyclus simulation that uses the 33 GWD/MTU burnup recipe has a small mass difference between UDB and Cyclus data for $^{240}$Pu and $^{241}$Am compared to 51 GWD/MTU burnup. However, it has a substantial difference for $^{239}$Pu. Figure 4 also shows small differences between UDB and Cyclus data for $^{238}$Pu, $^{244}$Cm, $^{90}$Sr and $^{137}$Cs.

The large mass difference between UDB and Cyclus data (where UDB $^{239}$Pu mass is larger than Cyclus $^{239}$Pu mass) for $^{239}$Pu in figures 6c, 6a and 6b can be attributed to conservative depletion parameters used in the calculations for isotopic compositions in the UDB database [7]. These assumptions result in the hardening of the neutron spectrum that results in increased $^{239}$Pu production in the UDB data [7].

## CONCLUSIONS

This work demonstrates that the spent fuel mass and isotopic composition calculated by the Cyclus simulation of the US nuclear fuel cycle closely follow the results from real world metrics. This provides confidence that Cyclus can be used to produce accurate isotopic decay heat contributions and simulate loading of a waste repository based on thermal constraints. To more closely replicate reality, future work will give the reactor agent the capability to accept varying cycle lengths, refueling durations and spent fuel recipes.

## ACKNOWLEDGMENTS

## REFERENCES

1. R. W. CARLSEN, M. GIDDEN, K. HUFF, A. C. OPOTOWSKY, O. RAKHIMOV, A. M. SCOPATZ, Z. WELCH, and P. WILSON, "Cyclus v1.0.0," *Figshare* (Jun. 2014), http://dx.doi.org/10.6084/m9.figshare.1041745.

2. J. PETERSON, B. VAN DEN AKKER, R. CUMBERLAND, P. MILLER, and K. BANERJEE, "UNF-ST&DARDS Unified Database and the Automatic Document Generator," *Nuclear Technology*, **199**, 3, 310–319 (2017).

3. K. D. HUFF, M. J. GIDDEN, R. W. CARLSEN, R. R. FLANAGAN, M. B. MCGARRY, A. C. OPOTOWSKY, E. A. SCHNEIDER, A. M. SCOPATZ, and P. P. H. WILSON, "Fundamental concepts in the Cyclus nuclear fuel cycle simulation framework," *Advances in Engineering Software*, **94**, 46–59 (Apr. 2016), arXiv: 1509.03604.

4. R. W. CARLSEN, M. GIDDEN, K. HUFF, A. C. OPOTOWSKY, O. RAKHIMOV, A. M. SCOPATZ, and P. WILSON, "Cycamore v1.0.0," *Figshare* (Jun. 2014), http://figshare.com/articles/Cycamore_v1_0_0/1041829.

5. K. D. HUFF, M. FRATONI, and H. R. GREENBERG, "Extensions to the cyclus ecosystem in support of market-driven transition capability," Tech. rep., Lawrence Livermore National Laboratory (LLNL), Livermore, CA (2014).

6. M. BELL, "ORIGEN - The ORNL Isotope Generation and Depletion Code," Tech. Rep. ORNL-4628, Oak Ridge National Laboratory (May 1973), software, Codes & Tools.

7. J. PETERSON, C. OLSON, J. ST. AUBIN, and B. CRAIG, "Additional Capability Being Developed from UNF-ST&DARDS Unified Database: System Analysis and Fuel Cycle Option Analysis," *Nuclear Technology*, **199**, 3, 320–329 (Sep. 2017).

8. DOE, "Strategy for the Management and Disposal of Used Nuclear Fuel and High-Level Radioactive Waste," Tech. rep., United States Department of Energy, Washington D.C., United States (Jan. 2013).

9. IAEA, "PRIS - Home," (2017).

10. P. WILSON, "The Adoption of Advanced Fuel Cycle Technology Under a Single Repository Policy," Tech. rep., University of Wisconsin – Madison (2009).

11. J. W. BAE, K. HUFF, and C. SINGER, "Synergistic Spent Nuclear Fuel Dynamics Within the European Union," in "Transactions of the American Nuclear Society Winter Conference," American Nuclear Society, Washington, D.C. (Oct. 2017).

12. RONACHER, "Welcome to Jinja2 - Jinja2 Documentation (2.10)," (2018).

13. G. CHEE, G. T. PARK, and K. HUFF, "arfc/transition-scenarios : Validation of Spent Nuclear Fuel Output by Cyclus, a Fuel Cycle Simulator Code," (Jun. 2018).

14. IAEA, "Current Trends in Nuclear Fuel for Power Reactors," p. 11.

15. J. GEHIN, "Nuclear Power Reactors - An Example of Improvements in Reliability and Potential for Improvement," (Apr. 2016).

16. EIA, "Spent Nuclear Fuel," (Dec. 2015).

17. R. A. WIGELAND, T. H. BAUER, T. H. FANNING, and E. E. MORRIS, "Separations and Transmutation Criteria to Improve Utilization of a Geologic Repository," *Nuclear Technology*, **154**, 95–106 (Apr. 2006).