

FUEL CYCLE PERFORMANCE OF FAST SPECTRUM MOLTEN SALT REACTOR DESIGNS

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INTRODUCTION

A liquid-fueled Molten Salt Reactor (MSR) concepts promise one of the most desirable and competitive, sustainable energy among of many advanced reactor systems [1]. In MSR fissile and/or fertile materials are dissolved in carrier molten salt (e.g., LiF, NaCl) which leads to immediate advantages over traditional, solid-fueled, reactors. These include near-atmospheric pressure in the primary loop, relatively high coolant temperature, outstanding neutron economy, a high level of inherent safety, reduced fuel preprocessing, and the ability to continuously remove fission products and add fissile and/or fertile elements without shutdown [2].

Historically, researchers focused on thermal spectrum MSR concepts with solid graphite moderator. Oak Ridge National Laboratory (ORNL) operated ≈ 8 MW_{th} Molten Salt Reactor Experiment (MSRE) pilot reactor from 1965 to 1969 to test approaches/materials, demonstrate fissile recycle (both ²³³U and ²³⁵U), and determine generic MSR operational characteristics [3]. Obtained experience plus promising breakthrough in reprocessing technology [4] chained ORNL attention to the simply configured, also graphite-moderated (i.e., thermal or epithermal), single-fluid Molten Salt Breeder Reactor (MSBR) by the end of the 1960's. The primary weakness of all one-fluid thermal MSR concepts is the fact that the hundreds tons (≈ 300 t for MSBR [5]) of expensive, radiologically contaminated, neutron-damaged graphite would have to be replaced every 4-10 years, which raises significant waste and economical issues.

In contrast, consistent with Generation IV International Forum (GIF) sustainability and safety goals [6], unmoderated (no graphite), one- or two-fluid (blanket equipped) fast spectrum MSR concept eventually became the EUROATOM Consortium's "reference" MSR [7]. Other identified advantages of fast MSR systems comparing with conventional reactors include: (1) they can operate in breeding ($CR^1 > 1$) [7, 8, 9], fertile-free Trans-Uranium (TRU) burning, or U/Th-supported TRU burning [10] regime; (2) they can potentially work in both ²³²Th/²³³U and ²³⁸U/²³⁹Pu fuel cycles (i.e., thermal MSR supports only Th/U); (3) they can be operated in ways that would generate very little long-lived TRU waste, and (4) they would use less natural resources (e.g., natural uranium, natural thorium) per unit energy generated. To quantitatively estimate benefits of these capabilities fuel cycle performance analysis for various fast spectrum MSR concepts is necessary.

Much of the analysis herein uses unit cell representations of four different fast MSR designs: (1) European Molten

Salt Fast Reactor (MSFR) [7]; (2) Molten Chloride Salt Fast Reactor (MCSFR) [8]; (3) REBUS-3700 [9]; (4) Molten Salt Actinide Recycler and Transmuter (MOSART) [10]. Some of these designs are two-fluid (1, 2), operate in thorium fuel cycle (1,4), or use TRU as start-up fissile material. The concepts (2) and (3) use chloride salts² while (1) and (2) employ fluorides. This paper discusses the depletion simulation of different fast MSRs to identify fuel cycle performance for deployment of this reactor technology.

METHODS

To determine Fuel Cycle Performance parameters full-core and simplified unit cell models of four different fast spectrum MSRs designs are created (Fig. 1). Table I contains summary of principal data of these designs. Fuel cycle performance analysis required depletion simulation for each reactor concept over the system whole lifetime which in this work assumed 60 years³. Full-core 60-year depletion computation of MSR required massive computing power. Computation time can be significantly reduced by performing depletion simulation for simplified unit cell representation instead of full-core one with sophisticated geometry.

All salt treatments and separation in this work are performed as truly continuous (online) processes using SCALE/TRITON version 6.2.4 Alpha with 238 group ENDF VII.1 cross-section library [11]. Earlier researchers usually used batch-wise approach because most of the reactor physics burnup calculation codes designed to model batch-fueled reactors with solid fuel [12, 13, 14, 15, 16]. This approach requires short depletion time steps to minimize the impact of no feed or removal during the time step which leads to a large number of depletion time steps to simulate longer periods of time. It makes lifetime-long depletion calculations computationally expensive. ORIGEN [17] supports continuous feed and removal but does not track the feed and discharge materials that are important to fuel cycle performance analysis. Thus, alpha version of SCALE/TRITON currently developing in ORNL allows simulate lifetime-long truly continuous depletion for MSR with reasonable time steps and computation cost.

Models description

In contrast with thermal MSR, fast spectrum concepts do not have channel or assembly structure but contain ho-

¹Conversion ratio (CR) \equiv fissile generated/fissile consumed: if $CR < 1$ the reactor is a "converter"; $CR = 1$, an "isobreeder"; $CR > 1$, a "breeder".

²The chlorine in the MCSFR is fully enriched in ³⁷Cl because ³⁵Cl (76% abundance) is a very strong neutron poison in fast neutron energy range.

³Lifetime for fast MSR limited by neutron damage on the reactor vessel. Further R&D activities should be performed to evaluate maximum fast neutron fluence and assess structural materials choice.

TABLE I. Principal data of selected fast spectrum MSRs designs.

Parameter	MSFR	MCSFR	REBUS-3700	MOSART
Thermal power, MW	3,000	6,000	3,700	2,400
Fuel salt volume (in/out of the core), m ³	18 (9/9)	38 (16/22)	55.6 (36.9/18.7)	49.05 (32.7/16.35)
Fertile salt volume (in/out of the blanket), m ³	7.3 (7.3/0)	75 (55/22)	—	—
Fuel and fertile salt initial composition (mol%)	LiF-ThF ₄ - ²³³ UF ₄ (77.5-19.9-2.6) LiF-ThF ₄ (77.5-22.5)	NaCl-UCl ₃ - ²³⁹ PuCl ₃ (60-36-4) NaCl-UCl ₃ (60-40)	55mol%NaCl+ 45mol%(natU+ 16.7at.%TRU)Cl ₃	LiF-BaF ₂ -ThF ₄ - TRUF ₃ (69.72-27-1.28)
Fuel cycle	Th/ ²³³ U	U/Pu	U/TRU	Th/ ²³³ U
Initial fissile inventory, t	5.060	9.400	18.061	9.637

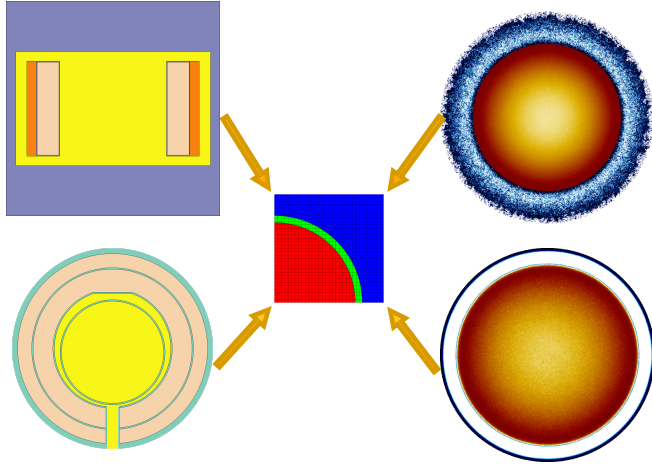


Fig. 1. Full-core 3D models of MSFR (upper left), MCSFR (lower left), REBUS-3700 (upper right), MOSART (lower right), and 2D unit cell model (center) showing fuel salt (red), fertile salt (green), structural material (blue).

mogenized fuel mixture into cylindrical or spherical vessel. Two-fluid systems also have cylindrical (MSFR) or spherical (MCSFR) blanket with fertile salt to reduce neutron leakage and enhance fissile material breeding (Fig. 1). Details about reactors' configuration can be found in Refs. [7, 8, 9, 18]. Two-fluid concepts' 2D unit cell model contains a cylindrical fuel salt channel with thin outer layer of fertile salt inside square block of structural material (Hastelloy N). The unit cell model for single-fluid REBUS-3700 has fuel salt and structural material only; MOSART simplified model consist of fuel salt square block with graphite cylinder in the center to represent 0.2 m graphite reflector which needed to increase ²³³U breeding from thorium.

To prove viability of unit cell models for depletion simulation high-fidelity full-core models were developed using Monte Carlo code SERPENT2 (16 millions neutron histories per run) with ENDF/B-VII.1 library [19, 20]. Single average unit cell model geometry and size are optimized to obtain sufficiently accurate multiplication factor and neutron energy spectrum in a reasonable time. Next metrics are used for

optimization:

1. eigenvalue discrepancy between full-core and unit cell models less than 300 pcm⁴;
2. correlation coefficient (r) for neutron spectrum normalized by lethargy more than 0.995;
3. approximation error (δ) in total neutron flux less than 3%.

The symmetry in a reactors is used to simplify the problem into one-quarter of the unit cell geometry. For this optimization the 16-by-16 spatial mesh for the NEWT neutron transport calculation is used in SCALE/TRITON.

Fuel Cycle Performance metrics

The main objective of the work is to analyze fast MSR systems and fuel cycles in support of the Fuel Cycle Options Campaign of the US Department of Energy, Office of Nuclear Energy (DOE-NE). The Evaluation and Screening Study (E&S) conducted by the DOE-NE gives information about the potential benefits and challenges of nuclear fuel cycle options (i.e., closed fuel cycle with continuous minor actinide (MA) reprocessing). This information needed to strengthen the basis and provide guidance for the activities started by the DOE-NE Fuel Cycle Research and Development program.

DOE established an Evaluation and Screening Team (EST) consisting of national laboratory and industry experts in nuclear fuel cycles to develop the Evaluation Metrics for 40 various nuclear fuel cycle options ("Evaluation Groups"). Based on continuous reprocessing depletion simulations, conducted for 4 selected fast MSR designs, following Evaluation Metrics are determined:

1. Natural Uranium per energy generated (for MCSFR, REBUS-3700);
2. Natural Thorium per energy generated (for MSFR, MOSART);
3. Mass of SNF+HLW⁵ disposed per energy generated;
4. Mass of DU+Ru+RTh⁶ disposed per energy generated;

⁴ 1 pcm = $10^{-5} \Delta k_{eff} / k_{eff}$

⁵ spent nuclear fuel (SNF)+high level waste (HLW)

⁶ depleted uranium (DU)+recovered uranium (RU)+recovered thorium (RTh)

Obtained results are compared with Metric Data for respective Evaluation Groups from Nuclear Fuel Cycle Evaluation and Screening study [21].

RESULTS

This section presents calculation results, such as neutron flux spectrum for full-core and unit cell models, fuel and fertile salt composition evolution during the reactor operation, and evaluation metrics.

Full-core vs unit cell neutron spectrum

Figures 2 to 5 show neutron flux energy spectrum normalized by lethargy for full-core 3D models obtained with SERPENT2 and simplified unit cell 2D models obtained with SCALE/TRITON. Calculated correlation coefficient (r) and approximation error (δ) in total neutron spectrum for unit cell model indicated in right upper corner of each plot. The most accurate approximation is obtained for the MOSART, while the MCSFR has the worse approximation quality. The main reason of discrepancy is low energy groups resolution in fast energy region in 238 group nuclear data library which was developed for thermal reactors. This issue could be resolved by using problem-oriented multi-group cross-section libraries for SCALE/TRITON for fast reactors but it would significantly increase computational time.

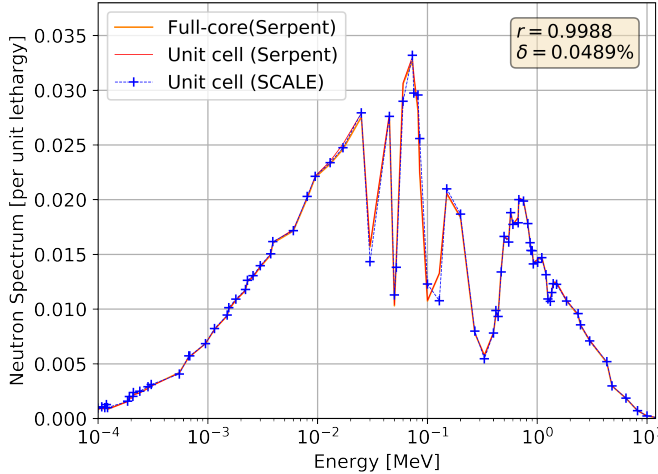


Fig. 2. Neutron flux energy spectrum for full-core and unit cell models for two-fluid MSFR.

Fuel Cycle Performance analysis

Figure 6

Equations, such as Eq. (1), should be centered and sequentially numbered to the flush right of the formula.

$$\text{Speedup} = \frac{1}{\frac{f}{p} + (1 - f)} \quad (1)$$

The continuation of a paragraph after an equation should not be indented. All paragraphs, as well as section or subsection headings, are separated by just one single empty line.

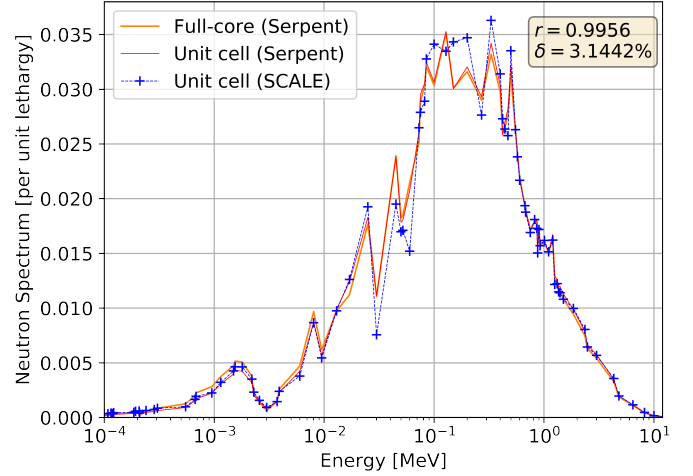


Fig. 3. Neutron flux energy spectrum for full-core and unit cell models for two-fluid MCSFR.

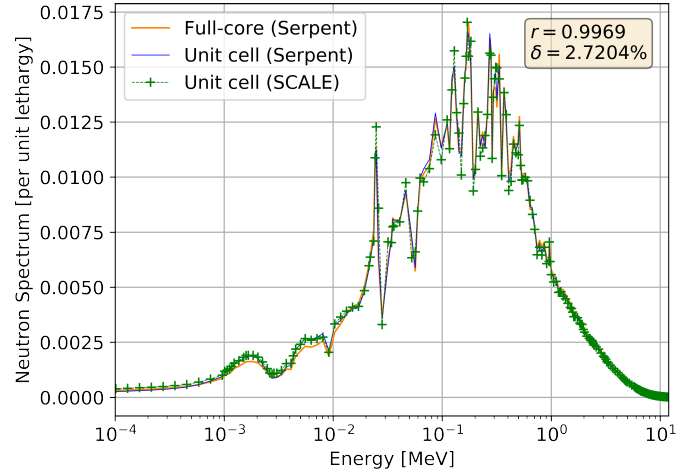


Fig. 4. Neutron flux energy spectrum for full-core and unit cell models for single-fluid REBUS-3700.

Sub-subsection level and lower: only first character uppercase

See Table III for a sample table. The “tbls” package is recommended for improved row and column spacing. Notice the caption appears above the table by setting the `\caption` command immediately after the `\begin{table}`. Tables are numbered in Roman numerals, with the caption centered above the table, in **boldface**. Triple-space before and after the table.

CONCLUSIONS

Present your summary and conclusions here.

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TABLE II. Fuel Cycle Performance metrics of selected fast spectrum MSRs designs.

Parameter	MSFR	MCSFR	REBUS	MOSART
Evaluation Group	EG28	EG23	EG24	EG28
Natural Uranium or Thorium Utilization, t/GWe-yr	TBD	TBD	0.835 (U)	TBD
Mass of SNF+HLW disposed, t/GWe-yr	TBD	TBD	0.813	TBD
Mass of DU+RU+RTh disposed, t/GWe-yr	TBD	TBD	0.0	TBD
Products from Reprocessing/Separation technology, t: RU/TRU/Fission Product (FP)	TBD	TBD	92.3/19.2/79.6	TBD

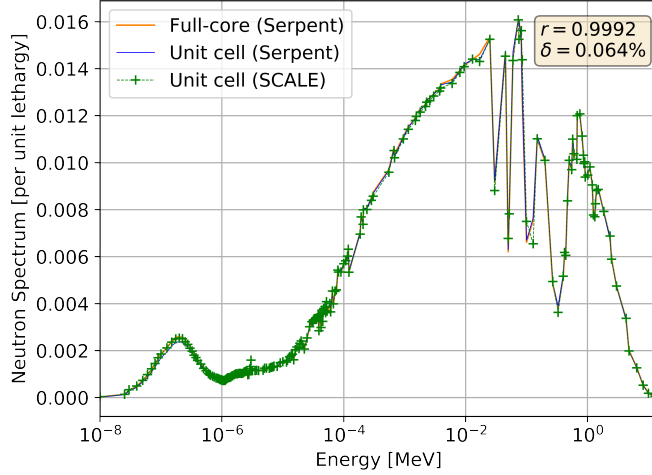


Fig. 5. Neutron flux energy spectrum for full-core and unit cell models for single-fluid MOSART with graphite reflector.

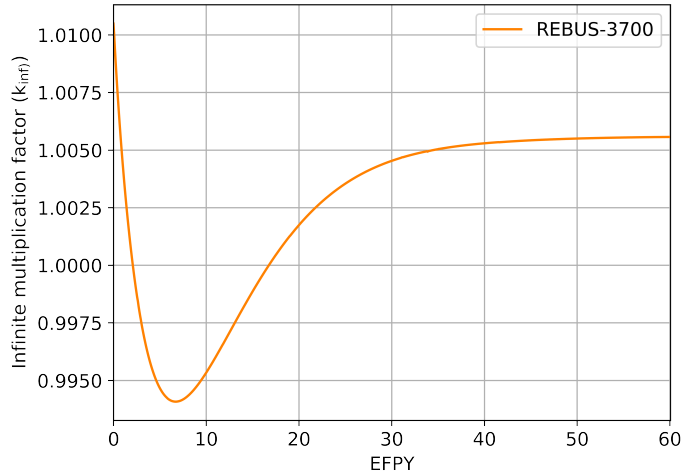


Fig. 6. Infinite multiplication factor converging to equilibrium after 35 years of operation with full separations and feeds.

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TABLE III. Parallel Performance for the Sample Problem

Parameter			
MSFR	(T_s/T_p)	(%)	
1	100.0	—	—
2	52.6	1.9	95.0

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