

write all terms as Taylor expansion about (x, y)

$$\textcircled{\text{II}} = \rho(x,y) u(x,y) \Delta y + \frac{\partial}{\partial x} (\rho(x,y) u(x,y) \Delta y) \left(-\frac{\Delta x}{2}\right) + \dots$$

$$\textcircled{\text{IV}} = \rho(x,y) u(x,y) \Delta y + \frac{\partial}{\partial x} (\rho(x,y) u(x,y) \Delta y) \left(\frac{\Delta x}{2}\right) + \dots$$

$$\textcircled{\text{IV}} = \rho(x,y) u(x,y) v(x,y) \Delta x + \frac{\partial}{\partial y} [\rho(x,y) u(x,y) v(x,y) \Delta x] \left(-\frac{\Delta y}{2}\right) + \dots$$

$$\textcircled{\text{V}} = \rho(x,y) u(x,y) v(x,y) \Delta x + \frac{\partial}{\partial y} [\rho(x,y) u(x,y) v(x,y) \Delta x] \left(\frac{\Delta y}{2}\right) + \dots$$

plugging in the mom. balance x-direction

$$\frac{\partial}{\partial t} [\rho(x,y,t) u(x,y,t)] \Delta x \Delta y = (\textcircled{\text{II}} + \textcircled{\text{IV}}) - (\textcircled{\text{III}} + \textcircled{\text{V}}) + \text{forces}_x$$

$$= (\textcircled{\text{II}} - \textcircled{\text{III}}) + (\textcircled{\text{IV}} - \textcircled{\text{V}}) + \text{forces}_x$$

$$= - \frac{\partial}{\partial x} [\rho(x,y,t) u(x,y,t) u(x,y,t)] \Delta y \Delta x - \frac{\partial}{\partial y} [\rho(x,y,t) u(x,y,t) v(x,y,t)] \Delta x \Delta y + \text{forces}$$

divide by $\Delta x \Delta y$

$$\rho \frac{\partial u}{\partial t} + u \frac{\partial \rho}{\partial t} + \underbrace{u u \frac{\partial \rho}{\partial x} + u \rho \frac{\partial u}{\partial x}}_{\text{forces}_x} + \rho u \frac{\partial u}{\partial x} + u v \frac{\partial \rho}{\partial y} + u \rho \frac{\partial v}{\partial y} + \rho v \frac{\partial u}{\partial y} = \frac{\text{forces}_x}{\text{Vol}}$$

$$\rho \left[\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right] + \underbrace{u \left\{ \frac{\partial \rho}{\partial t} + \left[u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} \right] + \rho \left[\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right] \right\}}_{\text{continuity eq.} = 0} = \frac{\text{forces}_x}{\text{Volume}}$$

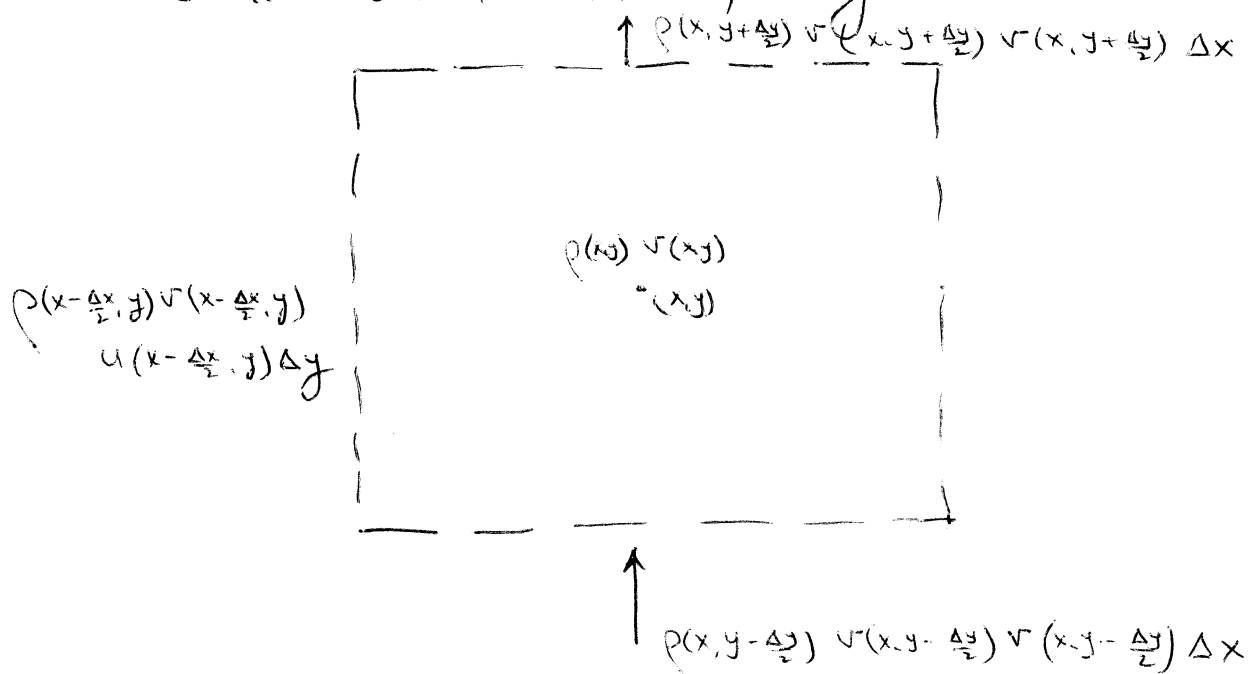
$$\therefore \rho \left[\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} \right] = \frac{\text{forces}_x}{\text{Volume}}$$

$$\rho \frac{Du}{Dt} = \frac{\text{forces}_x}{\text{Vol}}$$

$$\rho \left[\frac{\partial u}{\partial t} + \vec{v} \cdot \nabla u \right] = \frac{\text{forces}_x}{\text{Vol}}$$

$$\text{or } \rho \left(\frac{\partial}{\partial t} + \vec{v} \cdot \nabla \right) u = \frac{\text{forces}_x}{\text{Vol}}$$

Same control volume, y direction



...

$$\rho \frac{Dv}{Dt} = \frac{\text{forces}_y}{\text{Vol}}$$

also

$$\rho \frac{Dw}{Dt} = \frac{\text{forces}_z}{\text{Vol}}$$

Now let's look at forces

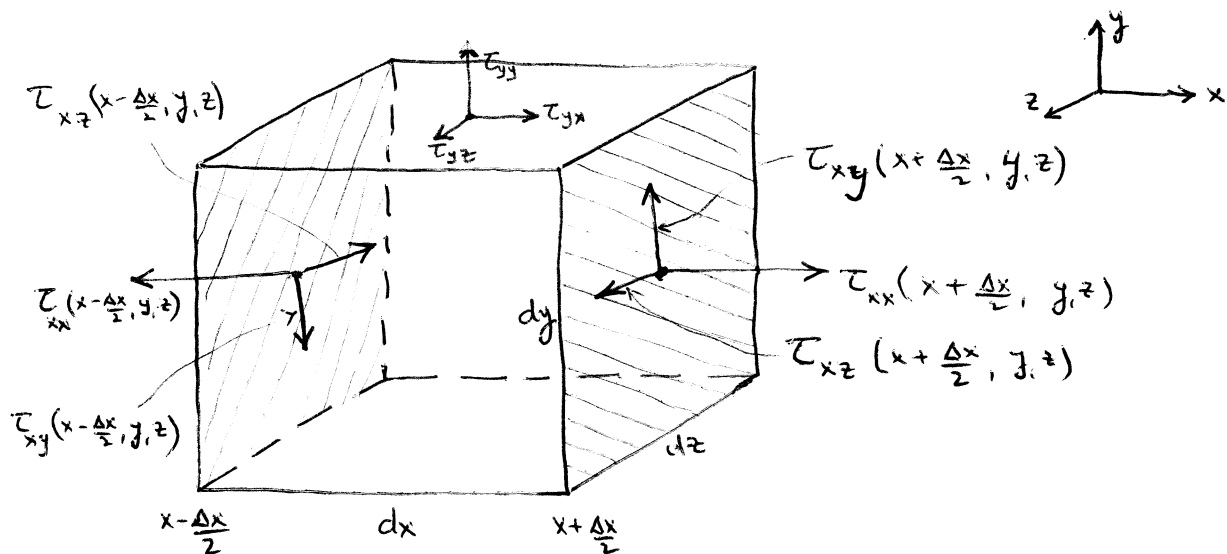
There is body force, such as gravity, $\phi \Delta x \Delta y \Delta z$

and there are surface forces acting by contact

In terms of the stress tensor τ

$$\tau = \begin{bmatrix} \tau_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \tau_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \tau_{zz} \end{bmatrix}$$

each component is force per unit area in a certain direction



Similar forces also exist on $y = \text{const.}$ & $z = \text{const.}$ surfaces

$$\begin{aligned}
 \text{forces in } x\text{-direction} &= \left[\tau_{xx}(x + \frac{\Delta x}{2}, y, z) - \tau_{xx}(x - \frac{\Delta x}{2}, y, z) \right] \Delta y \Delta z \\
 &+ \left[\tau_{yx}(x, y + \frac{\Delta y}{2}, z) - \tau_{yx}(x, y - \frac{\Delta y}{2}, z) \right] \Delta x \Delta z \\
 &+ \left[\tau_{zx}(x, y, z + \frac{\Delta z}{2}) - \tau_{zx}(x, y, z - \frac{\Delta z}{2}) \right] \Delta y \Delta x \\
 &= \frac{\partial}{\partial x} \tau_{xx}(x, y) \Delta x \Delta y \Delta z \\
 &+ \frac{\partial}{\partial y} \tau_{yx} \Delta x \Delta y \Delta z \\
 &+ \frac{\partial}{\partial z} \tau_{zx} \Delta x \Delta y \Delta z
 \end{aligned}$$

Similarly,

$$\begin{aligned}
 \text{forces in } y\text{ direction} &= \frac{\partial}{\partial x} \tau_{xy}(x, y) \Delta x \Delta y \Delta z \\
 &+ \frac{\partial}{\partial y} \tau_{yy}(x, y, z) \Delta x \Delta y \Delta z \\
 &+ \frac{\partial}{\partial z} \tau_{zy}(x, y, z) \Delta x \Delta y \Delta z
 \end{aligned}$$

Hence, the fundamental force balance is

$$\rho \frac{Du(x,y,z,t)}{Dt} = \rho \Phi_x + \frac{\partial \tau_{xx}(x,y,z,t)}{\partial x} + \frac{\partial \tau_{yx}}{\partial y} + \frac{\partial \tau_{zx}}{\partial z}$$

$$\rho(x,y,z,t) \frac{Dv(x,y,z,t)}{Dt} = \rho \Phi_y + \frac{\partial \tau_{xy}}{\partial x} + \frac{\partial \tau_{yy}}{\partial y} + \frac{\partial \tau_{yz}}{\partial z}$$

$$\rho(x,y,z,t) \frac{Dw(x,y,z,t)}{Dt} = \rho \Phi_z + \frac{\partial \tau_{xz}}{\partial x} + \frac{\partial \tau_{yz}}{\partial y} + \frac{\partial \tau_{zz}}{\partial z}$$

but what are the τ_{ij} ?

we are interested in ρ, u, v, w . Along with the continuity eqn, we have 4 eqns (scalar) and 4 + 9 unknowns.

Get rid of the 9 unknowns (the τ_{ij} terms) in favor of the other four (ρ, u, v, w); using constitutive relations.

Recall, heat conduction eq: the heat fluxes q_x, q_y, q_z were eliminated using Fourier's law $q_x = -k \frac{\partial T}{\partial x}$ a constitutive relation based on empirical evidence (defines k)

Now τ s are forces per unit area. τ_{ii} are normal to the surface in direction i , & τ_{ij} ($i \neq j$) are parallel to the surface (shear stress)

Physics behind shear stress: adjacent layers w/ different velocities

Constitutive Relations are

$$\tau_{xx} = -P + 2\mu \frac{\partial u}{\partial x} - \frac{2}{3}\mu \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

$$\tau_{yy} = -P + 2\mu \frac{\partial v}{\partial y} - \frac{2}{3}\mu \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

$$\tau_{zz} = -P + 2\mu \frac{\partial w}{\partial z} - \frac{2}{3}\mu \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right)$$

for a fluid at rest ($\vec{v} = 0$)

$$P = -\frac{1}{3}(\tau_{xx} + \tau_{yy} + \tau_{zz})$$

Stokes hypothesis says that even for a fluid in motion, the above holds

For relations constitutive for off diagonal elements

$$\tau_{xy} = \mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) = \tau_{yx}$$

$$\tau_{xz} = \mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) = \tau_{zx}$$

$$\tau_{yz} = \mu \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) = \tau_{zy}$$

μ is the dynamic viscosity

(λ : bulk coeff. of viscosity)
 $3\lambda + 2\mu = 0$

Substituting τ_{ij} in the force balance

x -direction :

$$\rho \frac{Du}{Dt} = \rho \phi_x + \frac{\partial}{\partial x} \left[-P + 2\mu \frac{\partial u}{\partial x} - \frac{2}{3}\mu \nabla \cdot \vec{v} \right] + \frac{\partial}{\partial y} \left[\mu \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \right]$$

for constant viscosity μ

$$= \rho \phi_x - \frac{\partial P}{\partial x} + \mu \left\{ 2 \frac{\partial^2 u}{\partial x^2} - \frac{2}{3} \frac{\partial}{\partial x} \nabla \cdot \vec{v} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 v}{\partial x \partial y} + \frac{\partial^2 u}{\partial z^2} + \frac{\partial^2 w}{\partial z \partial x} \right\}$$

$$= \rho \phi_x - \frac{\partial P}{\partial x} + \mu \nabla^2 u + \mu \frac{\partial}{\partial x} \left\{ -\frac{2}{3} \nabla \cdot \vec{v} + \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right\}$$

$$\rho \frac{Du}{Dt} = \rho \phi_x - \frac{\partial P}{\partial x} + \mu \nabla^2 u + \frac{1}{3} \frac{\partial}{\partial x} (\nabla \cdot \vec{v})$$

$$\rho \frac{Dv}{Dt} = \rho \phi_y - \frac{\partial P}{\partial y} + \mu \nabla^2 v + \frac{1}{3} \frac{\partial}{\partial y} (\nabla \cdot \vec{v})$$

$$\rho \frac{Dw}{Dt} = \rho \phi_z - \frac{\partial P}{\partial z} + \mu \nabla^2 w + \frac{1}{3} \frac{\partial}{\partial z} (\nabla \cdot \vec{v})$$

for incompressible flow, ($\rho \approx \text{const}$)
 continuity eqn $\Rightarrow \nabla \cdot \vec{V} = 0$

\therefore

$$\rho \frac{Du}{Dt} = \rho \Phi_x - \frac{\partial P}{\partial x} + \mu \nabla^2 u$$

$$\rho \frac{Dv}{Dt} = \rho \Phi_y - \frac{\partial P}{\partial y} + \mu \nabla^2 v$$

$$\rho \frac{Dw}{Dt} = \rho \Phi_z - \frac{\partial P}{\partial z} + \mu \nabla^2 w$$

each is a scalar eqn.

Vector form is

$$\rho \frac{D\vec{V}}{Dt} = \rho \vec{\Phi} - \nabla P + \mu \nabla^2 \vec{V}$$

\approx

$$\rho \frac{\partial \vec{V}}{\partial t} + \rho \vec{V} \cdot \nabla \vec{V} = \rho \vec{\Phi} - \nabla P + \mu \nabla^2 \vec{V}$$

const viscosity and density.

See form of Navier-Stokes eqn in other
 orthogonal curvilinear coordinate system.