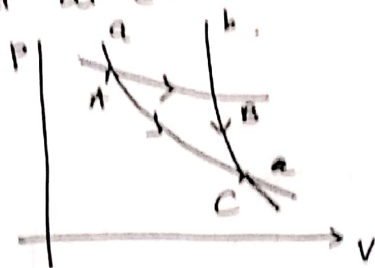


## Solution Set for HW 2

1. Assume that two reversible adiabatic lines  $a, b$  intersect at  $C$ .



Consider an isothermal line that intersects with  $a, b$  at  $A, B$ . [Convince yourself that such a line can always be found.]

Then the cycle  $A \rightarrow B \rightarrow C \rightarrow A$  can be considered as a reversible cycle in which the system takes a positive amount of heat  $Q$  from the environment only during the leg  $A \rightarrow B$  and does positive work  $W = (\text{area } ABC)$ . By first law  $Q = W$  since  $\Delta U = 0$ .

So in this cycle the system has taken a positive amount of heat  $Q$  from a source and converted it entirely into work without any other change  $\Rightarrow$  Contradicts Kelvin-Planck statement.

$\Rightarrow a, b$  cannot intersect.

Note: As brought up in class, this does not hold true for a reversible and irreversible adiabatic curve. e.g. You can start out an adiabatic quasistatic process and an adiabatic free expansion from the same initial conditions. Of course a free expansion curve cannot be plotted on a PV diagram.

- 2 (a) From Maxwell relations.

(5) 
$$\left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V = \frac{P}{T}, \quad P, T > 0$$

Here  $P = kT$ .

$$\left(\frac{\partial P}{\partial T}\right)_V = k = \frac{P}{T}.$$

$$\left(\frac{\partial S}{\partial V}\right)_T > 0.$$

entropy increases with volume.

2 (b).  $\left(\frac{\partial H}{\partial P}\right)_T$   
(5)

$$dH = TdS + VdP.$$

$\frac{\partial H}{\partial P}$  Isenthalpic process.  $(T = T')$ .

$$dH = 0$$

Joule Thomson coeff.

$$\left(\frac{\partial T}{\partial P}\right)_H > 0 \text{ for cooling.}$$

$$\text{Now; } \left(\frac{\partial H}{\partial P}\right)_T = - \frac{(\partial H / \partial T)_P}{(\partial P / \partial T)_H} = - \frac{C_P}{(\partial P / \partial T)_H}.$$

$$C_P > 0.$$

$$\therefore \left(\frac{\partial H}{\partial P}\right)_T = - \frac{C_P}{(\partial P / \partial T)_H} < 0$$

3. (i). Equation of state.

(5)  $PV = \frac{1}{3}U$  ;  $p = \frac{1}{3}u$ . — ①

we have derived in class

$$\left(\frac{\partial U}{\partial V}\right)_T = T \left(\frac{\partial P}{\partial T}\right)_V - P \text{ — ②}$$

[ using ① in ②

$$u = \frac{1}{3} T \frac{du}{dT} - \frac{1}{3} u.$$

$$4 \frac{dT}{T} = \frac{du}{u}.$$

$$\boxed{u = cT^4}.$$

(ii)  $TdS = dU + PdV.$

3 (ii)

(5)

entropy density.

$$Tds = dU + PdV \quad \left. \begin{array}{l} U = cT^4V \\ dU = cT^4dV + 4cT^3VdT \end{array} \right\}$$

$$Tds = cT^4dV + 4cT^3VdT + \frac{c}{3}T^4dV$$

$$ds = \frac{4}{3}cT^3dV + 4cT^2VdT$$

$$ds = d\left(\frac{4}{3}cT^3V\right)$$

$$S = \frac{4}{3}cT^3V + \underbrace{S_0}_{=0} \text{ by given bdy condn.}$$

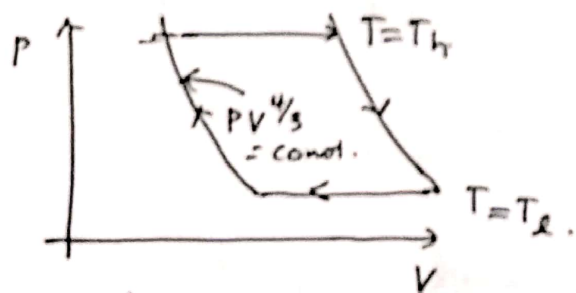
$$\boxed{s = \frac{S}{V} = \frac{4}{3}cT^3}$$

(iii) . Adiabatic for this gas.  $\Rightarrow VT^3 = \text{const.}$

isothermal  $P = \text{const}$

$$\rightarrow PV^{4/3} = \text{const}$$

(5)



↳ Carnot cycle.

4.  
(10)

Heat Capacity  $C = aT^3 = \left(\frac{\partial U}{\partial T}\right)_V$ .

$$dQ_L = aT_L^3 dT_L.$$

For the refrigerator

$$Q_L + W = Q_H.$$

$$dW = \left(1 - \frac{T_L}{T_H}\right) Q_L = \left(T_H - T_L\right) \frac{Q_L}{T_L}.$$

$$dW = (T_H - T_L) \frac{dQ_L}{T_L}.$$

$$= a \left(\frac{T_H}{T_L} - 1\right) T_L^3 dT_L \quad \left\{ \begin{array}{l} T_H = T_i, \text{ if } T_L \\ dT_L \end{array} \right.$$

$$W = \int_{T_i}^{T_H} a T_L^2 dT_L - \int_{T_i}^{T_H} a T_L^3 dT_L.$$

$$W = \frac{a}{3} (-T_i^3 T_H) + a \frac{T_i^4}{4}. \quad T_H = T_i$$

$$W = -\frac{a}{3} T_H^4 + a \frac{T_H^4}{4}.$$

$$= -\frac{a T_H^3}{3} - \frac{a T_H^4}{12}.$$

↓ work done by the system

$$\text{Electrical energy required} = \frac{a T_H^4}{12}.$$

5.

 $T_h$  and  $T_l$ 

(b)

$$W = (T_h - T_l) \frac{Q_l}{T_l}.$$

$$= \left( \frac{T_h}{T_l} - 1 \right) Q_l.$$

$$P = \left( \frac{T_h}{T_l} - 1 \right) \frac{dQ_l}{dt}.$$

$$= \left( \frac{T_h}{T_l} - 1 \right) A (T_h - T_l).$$

$$\Rightarrow \frac{P}{A} T_l = (T_h - T_l)^2.$$

$$\Rightarrow T_l^2 - 2 T_l T_h + \frac{P}{A} T_l + T_h^2 = 0.$$

$$T_l = T_h + \frac{P}{2A} - \sqrt{\left( T_h + \frac{P}{2A} \right)^2 - T_h^2}$$

minus sign taken since  
 $T_l < T_h$