# RBE 500 Group Assignment #1

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# Problem 1

# Create SCARA Robot in Gazebo

The 3 DOF SCARA robot we have built is shown below.

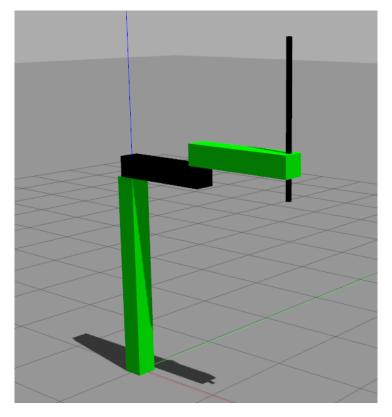


Figure 1: Final SCARA built by our team

We undertook the following steps to create our SCARA robot.

# 1 — Modify joint locations

In the downloaded package, the RRBot robot has its revolute joints on the 'sides' of its links, as shown in the following figure.

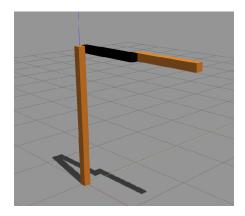


Figure 2: Initial RRBot in Gazebo

However, for a standard SCARA robot, we want the revolute joints to sweep angles in the XY plane of the world frame, not in the XZ plane.

Hence, we edited the <joint> element blocks in the URDF file rrbot\_description.urdf.xacro. For the first joint, we made the following change.

In the above code snippet, we changed the type attribute of the joint element from continuous to revolute. We also added the limit sub-element, and modified the origin and axis sub-elements. We made similar changes for the second joint, for which the code snippet is shown below.

As a result, our robot now looked like the following image.



Figure 3: RRBot with top-joints

In order to test our changes, we moved our robot by publishing joint values in the format of the following ROS command in our terminal.

```
ros2 topic pub --once /forward_position_controller/commands ...
std_msgs/msg/Float64MultiArray "{data: [0.75 0.82]}"
```

#### 2 — Add prismatic joint

Now our revolute joints resemble those of a SCARA robot, but we still need a prismatic joint. In order to do this, we first made the following changes to the rrbot\_description.urdf.xacro file.

```
<!-- Tool Joint -->
1
         <joint name="${prefix}tool_joint" type="prismatic">
2
3
           <parent link="${prefix}link2"/>
           <child link="${prefix}tool_link" />
           <!-- Set limits of prismatic joint -->
           limit lower="${prismatic_offset * -1}" upper="1.1" effort="1000" velocity="1"/>
           <origin xyz="${prismatic_offset - height4} 0 ${height3 - axel_offset*2}" rpy="0 ...</pre>
7
               1.5708 0" />
           <axis xyz="0 0 1"/>
           <dynamics damping="0.7"/>
9
         </joint>
10
11
         <!-- Tool Link -->
12
         <link name="${prefix}tool_link">
13
           <collision>
14
             <origin xyz="0 0 ${height4/2 - axel_offset}" rpy="0 0 0"/>
15
16
               <box size="${prismatic_width} ${prismatic_width} ${height4}"/>
17
             </geometry>
18
           </collision>
           <visual>
21
             <origin xyz="0 0 ${height4/2 - axel_offset}" rpy="0 0 0"/>
22
23
             <geometry>
               <box size="${prismatic_width} ${prismatic_width} ${height4}"/>
24
25
             </geometry>
           </visual>
26
27
28
           <inertial>
             <origin xyz="0 0 ${height4/2 - axel_offset}" rpy="0 0 0"/>
29
             <mass value="${mass}"/>
30
             <inertia
31
               ixx="${mass / 12.0 * (prismatic_width*prismatic_width + height4*height4)}" ...
32
                   ixy="0.0" ixz="0.0"
               iyy="${mass / 12.0 * (height4*height4 + prismatic_width*prismatic_width)}" ...
33
                   iyz="0.0"
34
               izz="${mass / 12.0 * (prismatic_width*prismatic_width + ...
                   prismatic_width*prismatic_width)}"/>
             </inertial>
         </link>
```

In the above code snippet, we have changed the tool joint from fixed to prismatic, defined its translation axis, set its limits, and defined its origin. We defined a special prismatic\_width so that we could make the tool link thinner than the regular links. We also defined a prismatic\_offset so that the tool link is slightly 'lowered'. This makes it so that the zero position of the tool link is at the same height as our first link, which makes our calculations consistent with our forward-kinematics derivation.

Next, we defined the tool joint in the rrbot.ros2\_control.xacro file, so that the command and state interfaces

for ROS2 could be made available for that joint. Finally, we also edited the gazebo\_controllers.yaml file to define the tool joint as part of the three controllers — forward\_position\_controller, forward\_velocity\_controller, and forward\_effort\_controller. All these modified files have been included as part of our submission inside the rrbot\_description.zip compressed directory.

At this point, our robot looked as follows.

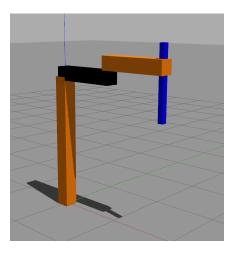


Figure 4: SCARA configuration without finishing touches

After this, we tweaked some offsets, adjusted some link lengths, changed the colors of the robot, and decreased the thickness of the tool link in order to arrive at our finished implementation of the SCARA robot. We also used the same ROS command as earlier (except with 3 data-points this time) to ensure that we were able to move all the joints of our robot.

# Question 2

## Forward Kinematics for SCARA

Before implementing forward kinematics in ROS, we worked out a derivation for the forward kinematics of the SCARA robot model.

### Derviation

The image below shows the frame assignments for the robot.

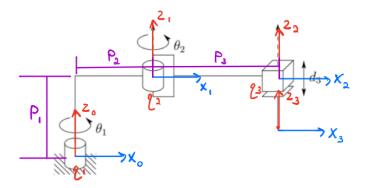


Figure 5: Frame assignments for forward kinematics

Based on this, we can form the DH table as shown below.

Link	$\alpha_i$	$a_i$	$\theta_i$	$d_i$
1	0	$p_2$	$q_1$	$p_1$
2	0	$p_3$	$q_2$	0
3	0	0	0	$q_3$

Next, we create a MATLAB script as shown below. We use the matrix obtained from equation 3.10 of the textbook to write  $A_1, A_2, A_3$ . By multiplying these matrices, we obtain the  $T_3^0$ .

```
1 %% Forward Kinematics
 2 clc
 3 clear
 5 syms P1 P2 P3 q1 q2 q3
 a = [P2 P3 0];
       theta = [ q1 q2 0];
 s d = [P1 0 q3];
       alpha = [ 0 0 0];
        % NOTE: Please enter theta in degrees
11
12
13 i = 1;
14 Al = [\cos d(theta(i)) (-\sin d(theta(i)) * \cos d(alpha(i))) (sind(theta(i)) * sind(alpha(i))) ...
                      (a(i)*cosd(theta(i)));
                     \verb|sind(theta(i))| (\verb|cosd(theta(i))| *| cosd(theta(i))| *| cosd(theta(i))| *| sind(theta(i))| *| cosd(theta(i))| *| cosd(thet
15
                                 (a(i)*sind(theta(i)));
16
                     0 sind(alpha(i)) cosd(alpha(i)) d(i);
                     0 0 0 11;
17
18
       i = 2;
19
 20 \quad A2 = [\cos d(\text{theta(i)}) \ (-\sin d(\text{theta(i)}) * \cos d(\text{alpha(i)})) \ (\sin d(\text{theta(i)}) * \sin d(\text{alpha(i)})) \ \dots ] 
                     (a(i)*cosd(theta(i)));
                    sind(theta(i)) (cosd(theta(i))*cosd(alpha(i))) (-cosd(theta(i))*sind(alpha(i))) ...
                                 (a(i)*sind(theta(i)));
                     0 sind(alpha(i)) cosd(alpha(i)) d(i);
                     0 0 0 1];
24
25 i = 3;
26 A3 = [\cos d(theta(i)) (-\sin d(theta(i)) * \cos d(alpha(i))) (sind(theta(i)) * sind(alpha(i))) ...
                     (a(i)*cosd(theta(i)));
                     \verb|sind(theta(i))| (\verb|cosd(theta(i))| *cosd(alpha(i))|) (-cosd(theta(i))| *sind(alpha(i))|) ... \\
27
                                 (a(i)*sind(theta(i)));
                     0 sind(alpha(i)) cosd(alpha(i)) d(i);
28
                     0 0 0 1];
29
30
31 \quad T30 = A1 * A2 * A3;
32
        % Export to latex
33
34 latex(T30)
```

This MATLAB script gives us the following  $T_3^0$  matrix, which is the homogeneous transformation for the end-effector with respect to the base frame.

```
\begin{bmatrix} \cos q_1 & \cos q_2 - \sin q_1 & \sin q_2 & -\cos q_1 & \sin q_2 - \cos q_2 & \sin q_1 & 0 & P_2 & \cos q_1 + P_3 & \cos q_1 & \cos q_2 - P_3 & \sin q_1 & \sin q_2 \\ \cos q_1 & \sin q_2 + \cos q_2 & \sin q_1 & \cos q_1 & \cos q_2 - \sin q_1 & \sin q_2 & 0 & P_2 & \sin q_1 + P_3 & \cos q_1 & \sin q_2 + P_3 & \cos q_2 & \sin q_1 \\ 0 & 0 & 1 & P_1 + q_3 \\ 0 & 0 & 1 & 1 \end{bmatrix}
```

#### **ROS** Implementation of Forward Kinematics

For implementing the forward kinematics in ROS, a new package was created (this package has been submitted as a zip file along with this report). Inside this package, a file was created to house all of the code for the forward kinematics subscriber, calculations, and publisher. In the code, we first create the Subscriber class which houses both the \_\_init\_\_ and calculate\_forward\_kinematics functions. The \_\_init\_\_ function initializes certain attributes to be used later. Here, the link lengths, as provided by the Gazebo model, are defined. Next, the subscriber and publisher are each created and defined by their respective message types and topics. Inside of the calculate\_forward\_kinematics function, the message containing each joint value is accepted and split apart into each individual value as a variable. These joint values, along with the link lengths are then plugged into the overall transformation matrix as previously calculated by hand and solved with Matlab. From this 3x4 matrix, the first three rows and columns are extracted as the rotation matrix. Once this matrix is obtained, an open source scipy package is used to calculate the quaternion. Elements of the rotation matrix as well as the quaternion are then extracted and placed into the pose, which will be published. Once this pose message is published, it can be accessed through terminal to obtain the location of the end effector. Below are the commands used with this system to obtain the desired results:

```
# Moves the Gazebo robot to the desired position
ros2 topic pub --once /forward_position_controller/commands ...
std_msgs/msg/Float64MultiArray "{data: [0.349066 0.610865 0.5]}"

# Kicks off the subscriber so that it can start calculating from the joint values ...
that are repeatedly published
ros2 run group_project calculate
```

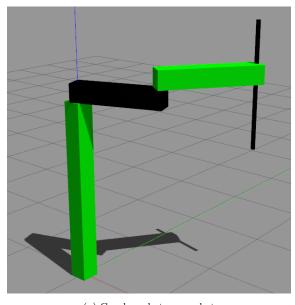
#### Gazebo Screenshots with ROS Output

# $\underline{\text{Pose } 1}$

First we moved our SCARA robot by changing the joint values to  $q_1 = 20^{\circ}$ ,  $q_2 = 35^{\circ}$ ,  $q_3 = 0.5$ . We did this by executing the following command

```
ros2 topic pub --once /forward_position_controller/commands ... std_msgs/msg/Float64MultiArray "{data: [0.349066 0.610865 0.5]}"
```

Next, we launced our forward kinematics calculation ROS node. The screenshots obtained are shown in Figure 6.



(a) Gazebo robot screenshot



(b) Terminal output screenshot

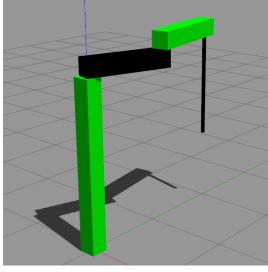
Figure 6: Pose 1 Screenshots

#### Pose 2

We moved our SCARA robot by setting the joint values to  $q_1 = 72^{\circ}$ ,  $q_2 = 28^{\circ}$ ,  $q_3 = 1.05$ . We did this by executing the following command

```
ros2 topic pub --once /forward_position_controller/commands ...
std_msgs/msg/Float64MultiArray "{data: [1.25664 0.488692 1.05]}"
```

After this we launched the forward kinematics ROS node as well. The obtained screenshots are shown in Figure 7.



(a) Gazebo robot screenshot



(b) Terminal output screenshot

Figure 7: Pose 2 Screenshots

## Pose 3

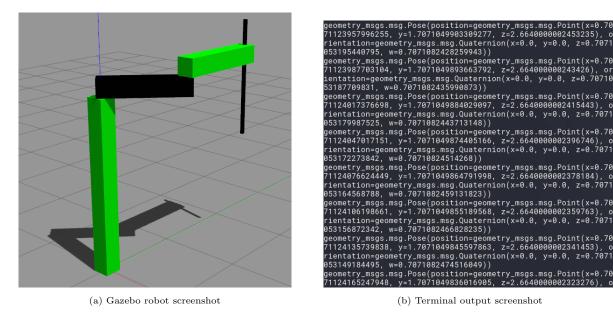


Figure 8: Pose 3 Screenshots

We moved our SCARA robot by setting the joint values to  $q_1 = 45^{\circ}$ ,  $q_2 = 45^{\circ}$ ,  $q_3 = 0.65$ . We did this by executing the following command

```
ros2 topic pub --once /forward_position_controller/commands ...
std_msgs/msg/Float64MultiArray "{data: [0.785398 0.785398 0.65]}"
```

After this we launched the forward kinematics ROS node as well. The obtained screenshots are shown in Figure 8

# Question 3

#### Inverse Kinematics for SCARA

Before implementing forward kinematics in ROS, we worked out a derivation for the inverse kinematics of the SCARA robot model.

#### Derviation

For the inverse kinematics, a side view and a top view were used to geometrically solve for the unknown joint values.

#### Top view

From Figure 9,  $q_1$  can be expressed as

$$q_1 = \arctan\left(\frac{y_3^0}{x_3^0}\right) - \gamma$$

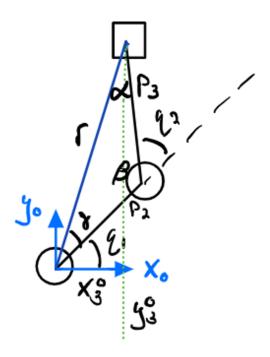


Figure 9: Top view for inverse kinematics

Similarly,  $q_2$  can be expressed as,

$$q_2 = 180^{\circ} - \beta$$

In order to find  $\alpha$  and  $\gamma$ , we can use the law of cosines. For instance,  $\alpha$  can be found as follows,

$$P_2^2 = r^2 + P_3^2 - 2rP_3\cos\alpha$$
$$2rP_3\cos\alpha = r^2 + P_3^2 - P_2^2$$
$$\alpha = \arccos\left(\frac{r^2 + P_3^2 - P_2^2}{2rP_3}\right)$$

Similarly,  $\gamma$  can be expressed as,

$$\gamma = \arccos\left(\frac{r^2 + P_2^2 - P_3^2}{2rP_3}\right)$$

Hence,  $\beta$  can be written as,

$$\beta = 180^{\circ} - \alpha - \gamma$$

Also, we can express r in its norm,

$$r = \sqrt{\left(y_3^0\right)^2 + \left(x_3^0\right)^2}$$

# Side view

From Figure 10, we can find  $q_3$  as follows

$$z_3^0 = P_1 - q_3$$
$$q_3 = -(P_1 - z_3^0)$$

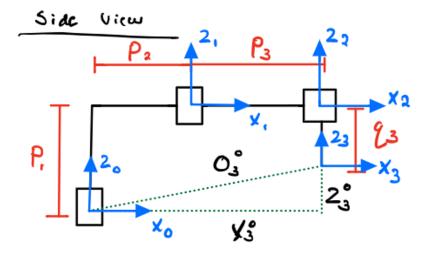


Figure 10: Side view for inverse kinematics

Now we have expressed all the joint variables in the form of constants of the system and end-effector position coordinates. These equations for each joint value can now be solved once the end effector location is known. In the following MATLAB script, these equations are written out, and when plugging in the values found in the forward kinematics, the original joint values are found, therefore proving their accuracy.

```
% Group Project Part 1 Forward and Inverse Kinematics
3
   clc; clear
   % Forward Kinematics
    % Link lengths from Gazebo
   P1 = 2;
  P2 = 1;
   P3 = 1;
12
   % This will come from ROS, current values are arbitrary for testing
13
   q1 = 45;
14 	 q2 = 45;
  q3 = 0.65;
15
16
   % DH parameters from hand-written work
17
   a = [P2 P3 0];
18
   theta = [q1 q2 0];
19
20
   d = [P1 \ 0 \ q3];
21
   alpha = [ 0 0 0 ];
22
    % AlO, A21, and A32 transformation matrices
23
^{24}
   \texttt{A1} = [\texttt{cosd}(\texttt{theta}(\texttt{i})) \ (-\texttt{sind}(\texttt{theta}(\texttt{i})) * \texttt{cosd}(\texttt{alpha}(\texttt{i}))) \ (\texttt{sind}(\texttt{theta}(\texttt{i})) * \texttt{sind}(\texttt{alpha}(\texttt{i}))) \ \dots
          (a(i)*cosd(theta(i)));
         \verb|sind(theta(i))| (\verb|cosd(theta(i))| *cosd(alpha(i))|) (-\verb|cosd(theta(i))| *sind(alpha(i))|) ... |
26
               (a(i)*sind(theta(i)));
27
         0 sind(alpha(i)) cosd(alpha(i)) d(i);
         0 0 0 1];
28
29
30
  A2 = [\cos d(\text{theta(i)}) (-\sin d(\text{theta(i)}) * \cos d(\text{alpha(i)})) (\sin d(\text{theta(i)}) * \sin d(\text{alpha(i)})) ...
          (a(i)*cosd(theta(i)));
```

```
sind(theta(i)) (cosd(theta(i))*cosd(alpha(i))) (-cosd(theta(i))*sind(alpha(i))) ...
            (a(i) *sind(theta(i)));
       0 sind(alpha(i)) cosd(alpha(i)) d(i);
33
       0 0 0 11:
34
35
36 i = 3:
37 A3 = [\cos d(\text{theta}(i)) (-\sin d(\text{theta}(i)) * \cos d(\text{alpha}(i))) (\sin d(\text{theta}(i)) * \sin d(\text{alpha}(i))) ...
       (a(i)*cosd(theta(i)));
       sind(theta(i)) (cosd(theta(i))*cosd(alpha(i))) (-cosd(theta(i))*sind(alpha(i))) ...
            (a(i)*sind(theta(i)));
       0 sind(alpha(i)) cosd(alpha(i)) d(i);
40
       0 0 0 1];
41
42 % End effector pose
43 \quad T30 = A1 * A2 * A3;
44 end_effector_pose = T30 % display whole end-effector T matrix
45 end_effector = T30(1:3,4); % use only position part of T
46
47
   % Inverse Kinematics
48
   %These will come from the forward kinematics
49
x30 = end_effector(1);
51
   y30 = end_effector(2);
52
   z30 = end_effector(3);
  q3 = z30 - P1;
54
56
   r = sqrt((y30^2) + (x30^2));
57
   % Needed angles from law of cosines
   alpha = acos(((r^2) + (P3^2) - (P2^2))/(2*r*P3));
   gamma = acos(((P2^2)+(r^2)-(P3^2))/(2*P2*r));
61 beta = 180 - alpha - gamma;
62
63 	 q2 = 180 - beta;
q1 = atan(y30/x30) - gamma;
65
  % Calculated joint values
   joint_angles = [(q1/(pi/180)); (q2/(pi/180)); q3]
```

Both the forward and inverse kinematics are now solved and ready to be plugged into ROS.

## **ROS** Implementation of Inverse Kinematics

For implementing the ROS portion of inverse kinematics, we need to implement a service. However, before implementing the service itself we need a custom interface for the request/response structure of the service. Hence, we created a new CMake package called <code>rbe\_custom\_interfaces</code>. Under this package, we created a new directory srv, in which we defined our custom <code>InvKinscara.srv</code> file. After this, we edited the CMakeLists to import the <code>rosidl\_default\_generators</code> so that our custom interface could be generated in the intended manner in ROS. Our custom interface is then built and loaded locally using . <code>install/setup.bash</code>.

After our custom interface became ready, we created a new ROS Python package called <code>inv\_kin\_serv</code>. Inside this package, under the directory of the same name as the package, we created a file called <code>inverse\_kin\_service.py</code>. Inside this file, we declared a class for our service, which we called <code>InverseKinService</code>. The constructor of this class initializes its super class and assigns the link-lengths of our robot system as its

member variables. The constructor then creates our service, which uses our custom interface, and assigns a callback function called calculate\_inverse\_kin that we have defined. This calculate\_inverse\_kin function calculates the joint variables from the end-effector position, as we have shown in the preceding Derviation section. After building our package, we used the following commands run and communicate with it.

```
# This command launches our service, which waits for a "call", or client request.

ros2 run inv_kin_serv service

# This command calls out to the service

ros2 service call /inverse_kin_service rbe500_custom_interfaces/srv/InvKinSCARA ...

"{x: 1.5133, y: 1.1612, z: 2.5}"
```

Both ROS packages for inverse kinematics have been zipped and included in the submission with this report.

# Terminal Screenshot of ROS Output

In the screenshot below (which has also been included in the inverse kinematics server package), we can see the calculated ROS output for the three end-effector positions that we used as examples in the forward kinematics portion of this report. Therefore this additionally proves our forward and inverse kinematics implementations.

```
### received an end effector position of x:0.1353999723434448 y:1.935899729156494 z:3.0499998
### received an end effector position of x:0.1353999723434448 y:1.9358999729156494 z:3.0499999
### received an end effector position of x:0.1353999723434448 y:1.9358999729156494 z:3.0499999
### received an end effector position of x:0.1353999723434448 y:1.9358999729156494 z:3.0499999
### received an end effector position of x:0.1353999723434448 y:1.9358999729156494 z:3.0499999
### received an end effector position of x:0.1353999723434448 y:1.9358999729156494 z:3.0499999
### received an end effector position of x:0.1767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
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### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.767899974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position of x:0.76789974155426 y:1.7071080337680708 z:2.558808095
### received an end effector position
```