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## Part -1

Discretize the system departure:

$$\frac{\partial}{\partial x} = V_{2x}, \quad m\dot{v}_{x} = -(v_{1} + v_{2})\sin\theta, \quad 0 = \omega$$
 $\dot{y} = V_{y}, \quad m\dot{v}_{y} = (v_{1} + v_{2})\cos\theta, \quad T\dot{\omega} = \omega(v_{1} - v_{2})$ 
 $\frac{\partial}{\partial x} = \left[ x, V_{x}, \frac{v}{2}, v_{y}, 0, \omega \right]^{T}$ 
 $\frac{\partial}{\partial x_{1} + 1} = X_{1} + \Delta t V_{2}$ 
 $\frac{\partial}{\partial x_{1} + 1} = V_{2} + \Delta t \left( -\frac{(v_{1} + v_{2})\sin\theta}{m} \right)$ 
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Q Given: 
$$V_{N,2} O$$
,  $V_{Y,2} O$ ,  $W_{2} O$ 

Aubstituting the vedues we get:
$$O = -(v_{1}+v_{2}) \text{ find}$$

$$\boxed{v_{1} = -v_{2}}$$

$$d = v_{1}+v_{2}$$

$$\log O = 0 : \cos O = 1$$

$$\boxed{v_{1}+v_{2} = mg}$$

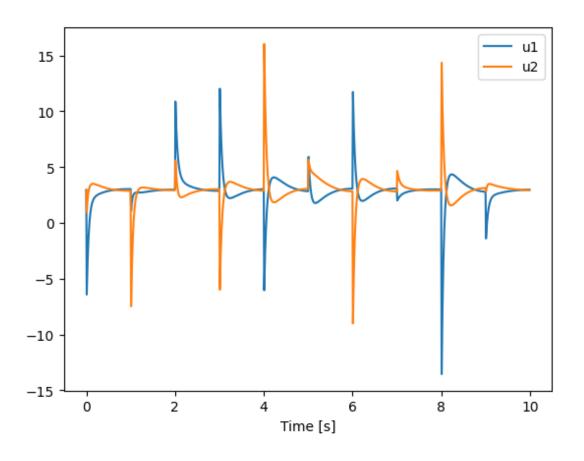
(3) It 
$$0=0$$
:

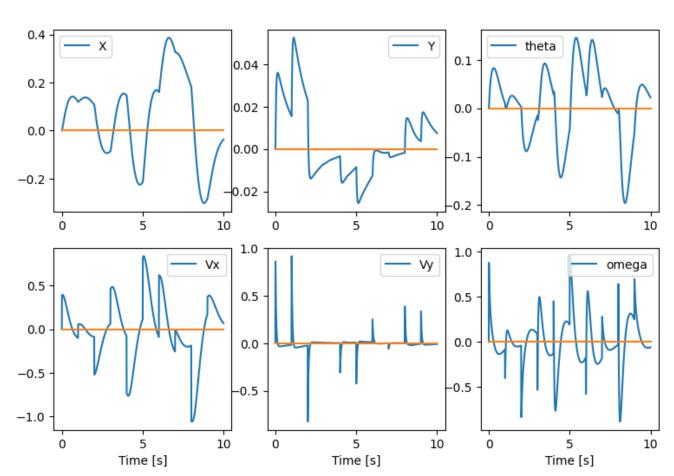
 $m\dot{v}_x = -(v_1+v_2)\sin\theta$ 
 $fx = 0$ 
 $m\dot{v}_x = (v_1+v_2)-mg$ 
 $f_y = v_1+v_2-mg$ 

.. We see that  $F_{\mathcal{K}}$  is 0 meaning when 0=0 there in no force in the X direction and hence it is not possible for it to move.

(i) If 
$$\theta = T_2$$
 $m\dot{v}_{il} = -(v_1 + v_2)$  who  $T_1$ 
 $m\dot{v}_{il} = -(v_1 + v_2)$ 
 $m\dot{v}_{il} = -(v_1 + v_2)$ 
 $m\dot{v}_{il} = -mg$ 
 $m\dot{v}_{il$ 

Part -2
Infinite-horizon LQR





## Part -3

4. One of the main benefit of this design is that it tracks the position of the robot.

An issue with this design is that it is not suitable for much more complex tasks for example like in a real robot.

5. When theta = pi/4 we see that the y position is tracked whereas the x position isn't tracked.

## Part -4

7. Benefit of this approach is that it allows us to calculate the position of the robot at every state.

An issue is that it can not be used for very complex tasks

9. Application of this controller can be run on a real controller in the real world. However we will have to keep in mind the computation cost associated with this naive approach and therefore there are more efficient approaches with ILQR.