

# 1 Deriving A

As provided by T.M. Qian et al. in *Design and construction of the MUSE permanent magnet stellarator* appendix A, the magnetic field everywhere can be computed with

$$\vec{B} = \mu_0 \sum_d^D (\vec{H}_d + \vec{M}_d) \quad (1)$$

inside the magnet and

$$\vec{B} = \mu_0 \sum_d^D (\vec{H}_d) \quad (2)$$

outside the magnet, where  $\vec{M}_d$  is the magnetization vector of magnet d and  $\vec{H}_d$  is the auxiliary field given by

$$\begin{aligned} \vec{H}_d(\vec{r}_n) &= \frac{1}{4\pi} \sum_{i,j,k}^{0,1} (-1)^{i+j+k} \begin{bmatrix} \tan^{-1}\left(\frac{y_j x_i}{z_k r_{ijk}}\right) + \tan^{-1}\left(\frac{z_k x_i}{y_j r_{ijk}}\right) & \ln(z_k + r_{ijk}) & \ln(y_j + r_{ijk}) \\ \ln(z_k + r_{ijk}) & \tan^{-1}\left(\frac{x_i y_j}{z_k r_{ijk}}\right) + \tan^{-1}\left(\frac{z_k y_j}{x_i r_{ijk}}\right) & \ln(x_i + r_{ijk}) \\ \ln(y_j + r_{ijk}) & \ln(x_i + r_{ijk}) & \tan^{-1}\left(\frac{x_i z_k}{y_j r_{ijk}}\right) + \tan^{-1}\left(\frac{y_j z_k}{x_i r_{ijk}}\right) \end{bmatrix} \cdot \vec{M}_d \\ &= H'(\vec{r}_n) \vec{M}_d \end{aligned}$$

Thus inside the magnet the magnetic field can be simplified to  $\vec{B} = \mu_0 \sum_d^D (H'_d(\vec{r}_i) \vec{M}_d + \vec{M}_d) = \mu_0 \sum_d^D (H'_d(\vec{r}_i) + I) \cdot \vec{M}_d$ .

In the expression for  $\vec{H}$ ,  $x_i$ ,  $y_j$ , and  $z_k$  give the distances to each of the corners of the magnet. Thus they are evaluated as follows:

$$\begin{aligned} x_0 &= x_n + L/2 & y_0 &= y_n + W/2 & z_0 &= z_n + H/2 \\ x_1 &= x_n - L/2 & y_1 &= y_n - W/2 & z_1 &= z_n - H/2 \end{aligned}$$

where L,W,H are the dimensions of the magnet and  $\vec{r}_n = [x_n \ y_n \ z_n]$  is the position from the center of the magnet to the  $n^{th}$  point we are evaluating.  $r_{ijk} = \sqrt{x_i^2 + y_j^2 + z_k^2}$ .

From *Permanent-Magnet Optimization for Stellarators as Sparse Regression* Appendix A (Alan A. Kaptanoglu et al.) we see that  $\vec{B} \cdot \hat{n}_i = (A\vec{M})_i$ , allowing us to solve for A. The sum has been temporarily removed for simplicity.

Inside the magnet:

$$\begin{aligned} \vec{B} \cdot \hat{n}_i &= \mu_0 (H'_d(\vec{r}_i) \vec{M}_d \cdot \hat{n}_i + \vec{M}_d \cdot \hat{n}_i) \\ &= \mu_0 ((H'_d(\vec{r}_i) \vec{M}_d)^T \hat{n}_i + \vec{M}_d \cdot \hat{n}_i) \\ &= \mu_0 (\vec{M}_d^T H'_d(\vec{r}_i) \hat{n}_i + \vec{M}_d \cdot \hat{n}_i) \\ &= \mu_0 (\vec{M}_d \cdot H_d'^T(\vec{r}_i) \hat{n}_i + \vec{M}_d \cdot \hat{n}_i) \\ &= \mu_0 (H_d'^T(\vec{r}_i) \hat{n}_i + \hat{n}_i) \cdot \vec{M}_d \end{aligned}$$

And so (reintroducing the sum)

$$\begin{aligned}(A\vec{M})_i &= \mu_0 \sum_d^D (H_d'^T(\vec{r}_i) \hat{n}_i + \hat{n}_i) \cdot \vec{M}_d \\ &= \mu_0 ((H_1'^T(\vec{r}_i) \hat{n}_i + \hat{n}_i) \cdot \vec{M}_1 + \dots + (H_D'^T(\vec{r}_i) \hat{n}_i + \hat{n}_i) \cdot \vec{M}_D)\end{aligned}$$

Outside the magnet:

$$\begin{aligned}\vec{B} \cdot \hat{n}_n &= \mu_0 (H_d'^T(\vec{r}_n) \vec{M}_d) \cdot \hat{n}_n \\ &= \mu_0 H_d'^T(\vec{r}_n) \hat{n}_n \cdot \vec{M}_d\end{aligned}$$

And so

$$\begin{aligned}(A\vec{M})_i &= \mu_0 \sum_d^D (H_d'^T(\vec{r}_i) \hat{n}_i) \cdot \vec{M}_d \\ &= \mu_0 ((H_1'^T(\vec{r}_i) \hat{n}_i) \cdot \vec{M}_1 + \dots + (H_D'^T(\vec{r}_i) \hat{n}_i) \cdot \vec{M}_D)\end{aligned}$$

If  $\vec{M} = [M_1^x \ M_1^y \ \dots \ M_D^z]$ , then

$$A = \mu_0 \begin{bmatrix} g_1^x(1) & g_1^y(1) & \dots & g_D^z(1) \\ \dots & & & \\ g_1^x(N) & g_1^y(N) & \dots & g_D^z(N) \end{bmatrix} \quad (3)$$

where  $g_d^x(i) = (H_d'^T(\vec{r}_i) \hat{n}_i + \hat{n}_i)_x$  inside the magnet and  $g_d^x(i) = (H_d'^T(\vec{r}_i) \hat{n}_i)_x$  outside the magnet.

When solving for  $\vec{g}_d(i)$  it is important to realize that  $H_d'^T(\vec{r}_i)$  is in the local coordinate system of magnet  $d$ , defined such that the  $+\hat{x}$ -direction (and thus one of the magnet's faces) points normal away from the toroidal surface. Meanwhile,  $\hat{n}_i$  is in a global coordinate system with the origin at the center of the device. Thus we introduce the rotation matrix which translates from the global to the local system:

$$P_d = \begin{bmatrix} \cos \theta & 0 & \sin \theta \\ 0 & 1 & 0 \\ -\sin \theta & 0 & \cos \theta \end{bmatrix} \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \theta \cos \phi & -\cos \theta \sin \phi & \sin \theta \\ \sin \phi & \cos \phi & 0 \\ -\sin \theta \cos \phi & \sin \theta \sin \phi & \cos \theta \end{bmatrix} \quad (4)$$

where  $\phi$  is the  $d^{th}$  local system's rotation around the z-axis and  $\theta$  is its rotation around the new y-axis (ie, the resulting y-axis after the first rotation). It turns out that, as long as we set the  $(\phi, \theta)$  toroidal coordinate system such that  $(0, 0)$  lies on the global x-axis (and angles increase in the counter-clockwise direction) then the rotation angles of each local system are just their magnet's  $(\phi, \theta)$  coordinate on the torus.

Then  $\vec{g}_d(i) = H_d'^T(\vec{r}_i) \hat{n}_i^{local} + \hat{n}_i^{local}$  where  $\hat{n}_i^{local} = P_d \hat{n}_i$ .

Now we have  $A$  expressed in  $D$  different local coordinate systems and  $\vec{M}$  expressed in the global coordinate system, so we have to make another transformation. Here we have two options:

1. We transform each  $\vec{g}_d(i)$  into the global system with  $\vec{g}_d^{global}(i) = P_d^T \vec{g}_d(i)$
2. We transform each  $\vec{M}_d$  in  $\vec{M}$  into their respective local systems with  $\vec{M}_d^{local} = P_d \vec{M}_d$

Since there are  $N \times D$   $\vec{g}_d(i)$ 's but only  $D$   $\vec{M}_d$ 's, the second option has a factor of  $N$  fewer operations. However since we would then have columns of  $A$  in  $D$  different coordinate systems, it complicates out final operation to solve for  $B$ .