

# HW 1

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## Problem 1

The energy of a photon can be quantified as:

$$E = \frac{hc}{\lambda},$$

where,  $E, h, c$  and  $\lambda$  are energy, Planck's constant, speed of light and wavelength respectively. To create electron-hole pairs, the following condition needs to be satisfied:

$$E \geq E_{gap}, \quad (1)$$

where  $E_{gap}$  is the band gap energy of the material in which the electron-hole pairs are required to be created. From (1),

$$\begin{aligned} \frac{hc}{\lambda} &\geq E_{gap} \\ \Rightarrow \lambda &\leq \frac{hc}{E_{gap}}. \end{aligned} \quad (2)$$

Plugging in the values of  $E_{gap} = 1.42 \text{ eV}$ ,  $h = 6.63 \times 10^{-34} \text{ m}^2\text{kg/s}$  and  $c = 3 \times 10^8 \text{ m/s}$  in (2),

$$\begin{aligned} \lambda &\leq \frac{6.63 \times 10^{-34} \times 3 \times 10^8}{1.42 \times 1.6 \times 10^{-19}} \text{ m} \\ &= 0.875 \text{ } \mu\text{m}. \end{aligned}$$

Therefore, a photon can have a maximum wavelength of  $0.875 \text{ } \mu\text{m}$  to create electron-hole pairs in Gallium Arsenide.

## Problem 2.1

The system needs to deliver 4000 kWhr/yr energy. Now, Las Vegas receives  $6.4 \text{ kWhr/m}^2\text{day}$  of average insolation. It can be interpreted as  $6.4 \text{ hr/day}$  of  $1\text{kW/m}^2$  solar irradiation. Therefore, the AC rated power (kW) of the system should be

$$\begin{aligned} P_{ac} &= \frac{4000}{365 \times 6.4} \\ &= 1.71. \end{aligned}$$

## Problem 2.2

We know that,

$$P_{ac} = P_{dc, stc} [1 - ((T - 25)l_t)] (1 - l_d)(1 - l_m)\eta_{inv}, \quad (3)$$

where,  $P_{dc, stc}, T, l_t, l_d, l_m$  and  $\eta_{inv}$  are DC power (kW) at STC (standard test condition), cell temperature, percentage drop in voltage/ $^{\circ}\text{C}$ , percentage loss due to dirt, percentage loss due to cell condition mismatch and inverter efficiency respectively.

Plugging in the values of  $P_{ac} = 1.71 \text{ kW}$ ,  $T = 45^{\circ}\text{C}$ ,  $l_t = 0.0036$ ,  $l_d = 0.03$ ,  $l_m = 0.03$ ,  $\eta_{inv} = 0.92$ , we get

$$\begin{aligned} P_{dc, stc} &= \frac{1.71}{0.928 \times 0.97 \times 0.97 \times 0.92} \\ &= 2.13. \end{aligned}$$

### Problem 2.3

Let  $A \in \mathbb{R}$  denote the required area ( $\text{m}^2$ ) of the system. We previously calculated the DC power,  $P_{dc,stc}$  kW, under STC. This power has to come from a system with  $A \text{ m}^2$  area with  $1 \text{ kW/m}^2$  irradiation. If the PV module efficiency is 13%, then,

$$\begin{aligned} P_{dc,stc} &= A \times 0.13 \\ \implies A &= \frac{2.13}{0.13} \\ \implies A &= 16.38. \end{aligned}$$

### Problem 2.4

DC output power of the system is  $P_{ac}/\eta_{inv} = 1.86 \text{ kW}$ . Therefore, total capital cost (\$) of installation is  $C = 6 \times 1860 = 11160$ .

Interest rate,  $d$  is 0.06 and duration of investment is  $n = 30$  years.

The renewable energy credit pays the owner  $\$0.05/\text{kWhr}$  generated. In the question, it is not clear that if this payment is done upfront or annual. Here I assume that the payment of credit is annual. Let  $A \in \mathbb{R}$  denote the annual installment for the loan. Therefore, the net present value of the system is

$$\begin{aligned} C &= A \frac{(1+d)^n - 1}{d(1+d)^n} \\ \implies A &= C \frac{d(1+d)^n}{(1+d)^n - 1} \\ \implies A &= \frac{(11160)(0.06)(1.06)^{30}}{(1.06)^{30} - 1} \\ \implies A &= 810.76. \end{aligned}$$

Annual energy yield is  $4000 \text{ kWhr}$ . Therefore, considering the renewable energy credit, the cost of electricity should be

$$\text{cost of electricity } (\$/\text{kWhr}) = \frac{810.76}{4000} - 0.05 = 0.153.$$

### Problem 3.1

Absolute value of the slope of I-V curve near the open circuit voltage is approximately equal to  $\frac{1}{R_s}$ . From the given graph, we can calculate the slope and find

$$\begin{aligned} \frac{1}{R_s} &= \frac{1.4 - 1.0}{0.58 - 0.56} \\ \implies R_s &= 0.05 \Omega. \end{aligned}$$

### Problem 3.2

The absolute value of the slope of I-V curve near the short circuit current is approximately equal to  $\frac{1}{R_p}$ . From the given graph,

$$\begin{aligned} \frac{1}{R_p} &= 0 \\ \implies R_p &= \infty \Omega. \end{aligned}$$

### Problem 3.3

From the graph, approximately it looks maximum power point, for the curve labeled as  $R_s = 0$  is near  $V = 0.56 \text{ V}$  and  $I = 3.8 \text{ A}$ . Therefore, the maximum power that can be delivered is  $P_{max} = (0.56)(3.8) = 2.13 \text{ W}$ .

### Problem 3.4

In case of 5 parallel strings of 10 series connected cells, the open circuit voltage would be  $0.63 \times 10 = 6.3$  V and short circuit current would be  $4 \times 5 = 20$  A. As for the curve labeled with  $R_s = 0$  is having approximately very large parallel resistance ( $R_p \leftarrow \infty$ ), as estimated before, and series resistance  $R_s = 0$   $\Omega$ , as indicated in the given graph. Therefore, we can assume that there will not be significant effect on the slope of the I-V curve near open circuit as well as short circuit condition. An approximate I-V curve for the series-parallel combination is shown in Fig. 1.

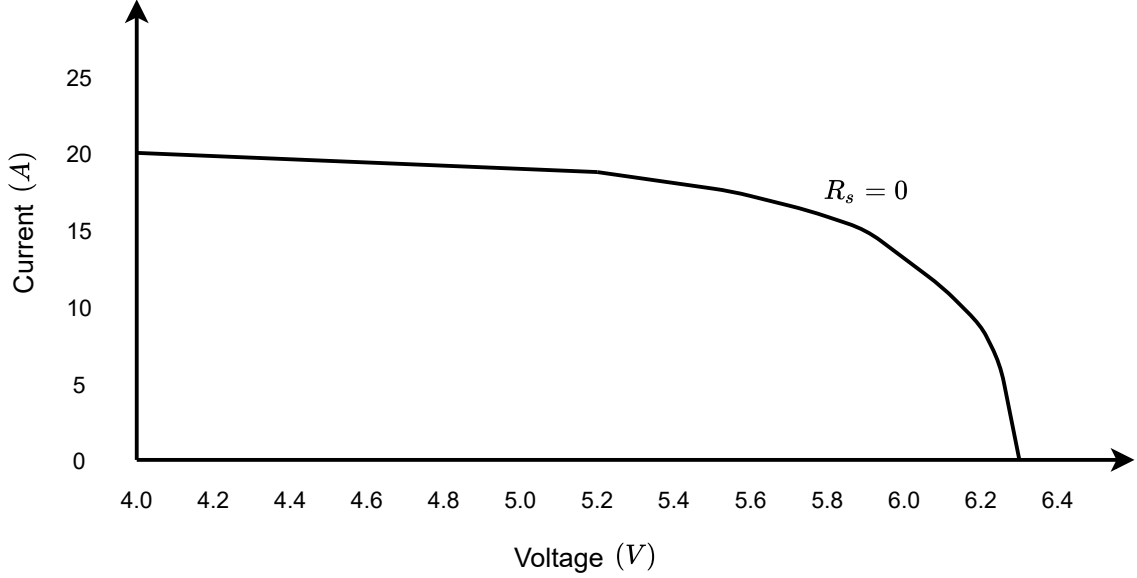


Figure 1: I-V curve of 5 parallel strings each with 10 series-connected PV cells

### Problem 4

The maximum power point corresponds to 40 V and 5 A. We need to provide power to a 12 V battery. Therefore, for maximum power point operation of the PV resource, we need to step down the input voltage,  $V_{in} = 40$  V to output voltage,  $V_{out} = 12$  V. Thus, we may use a buck converter to accomplish this. The input output voltage of a buck converter is related as follows:

$$V_{out} = DV_{in},$$

where,  $D \in [0, 1] \in \mathbb{R}$  is the duty cycle of the buck converter. Plugging in the values of  $V_{in}$  and  $V_{out}$ , we find that  $D = 0.3$ .

### Problem 5

Let  $S \in \mathbb{N}$  and  $P \in \mathbb{N}$  denote the number of PV modules connected in series and parallel respectively. Our objective is to deliver maximum power to the inverter. Let  $V_{oc}, I_{sc}, V_{mppt}, I_{mppt}$  denote the PV modules's open circuit voltage, short-circuit current, voltage at maximum power and current at maximum power respectively and let  $V_{inv}^{max}, V_{inv,mppt}^{max}, V_{inv,mppt}^{min}, I_{inv}^{max}$  denote the inverter maximum input voltage, MPPT (maximum power point tracker) voltage range maximum value, MPPT voltage range minimum value and maximum input current. In this question,

$$\begin{aligned} V_{oc} &= 43.40 \text{ V} \\ I_{sc} &= 4.80 \text{ A} \\ V_{mppt} &= 34 \text{ V} \\ I_{mppt} &= 4.40 \text{ A} \end{aligned}$$

$$\begin{aligned}
V_{inv}^{max} &= 600 \text{ V} \\
V_{inv,mppt}^{max} &= 550 \text{ V} \\
V_{inv,mppt}^{min} &= 250 \text{ V} \\
I_{inv}^{max} &= 11 \text{ A}.
\end{aligned} \tag{4}$$

For maximum power point operation of the PV module, we need to ensure the following:

$$\begin{aligned}
SV_{oc} &\leq V_{inv}^{max} \\
V_{inv,mppt}^{min} &\leq SV_{mppt} \leq V_{inv,mppt}^{max} \\
PI_{mppt} &\leq I_{inv}^{max}.
\end{aligned}$$

Plugging in the values from (4),

$$\begin{aligned}
S &\leq 13 \\
8 &\leq S \leq 16 \\
P &\leq 2.
\end{aligned}$$

Therefore, from the given combinations, I would choose (8  $S$ , 2  $P$ ) (choice no. 2 in question).