Project 2.1: Brake Disc Design

MAE 598: Design Optimization

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CAD Model

For the CAD model in this project, the same geometry was used as the one given in the tutorial. In the geometry, the rotor thickness, outer rotor diameter, and inner rotor diameter were set as parameters. The brake disk was solid and was later assigned gray cast iron as its material. The frozen parts were the brake pads and were assigned structural steel as their material.

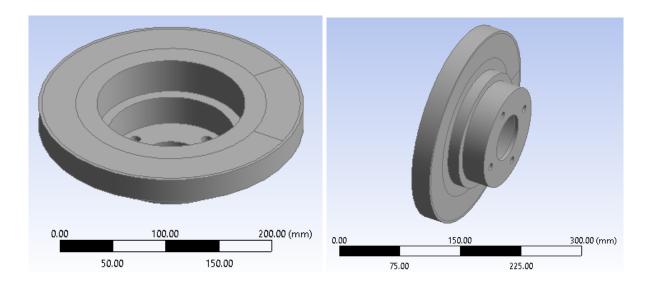


Figure 1: Solid Geometry

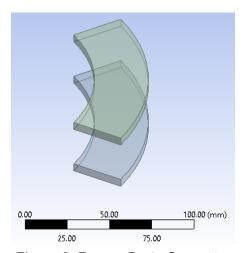


Figure 2: Frozen Parts Geometry

CAE Analysis (Structural, Modal, and Thermal)

The initial analysis shown in figures 3 - 5 below was performed in order to set the parameters: volume, maximum equivalent stress, frequency, and maximum temperature.

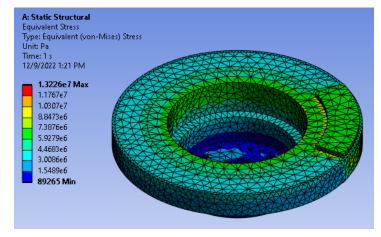


Figure 3: Initial Equivalent Stress From Static Structural Analysis

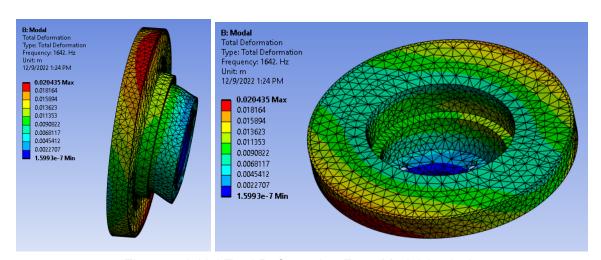


Figure 4: Initial Total Deformation From Modal Analysis

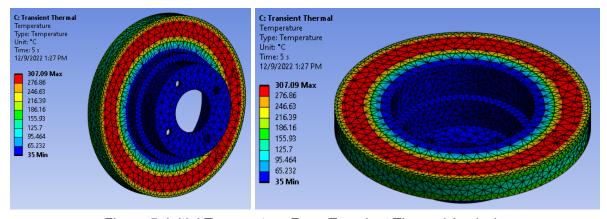


Figure 5: Initial Temperature From Transient Thermal Analysis

Design of Experiments

For the design of experiments, the Latin hypercube sampling design was used. Many samples were gathered with different bounds in order to reach a point were there were no errors in the samples. Additionally, many iterations were run to later narrow the bounds for each parameter. One of the final iterations that led to the last one was a sample of 50 with bounds of [5 27], [124 150], and [66 90] for thickness, outer diameter, and inner diameter respectively. Based on the optimization results from that sample, the final bounds were chosen. In the end, the final design points used were 20. The bounds were [12 15], [123 125], and [75 82] for thickness, outer diameter, and inner diameter respectively.

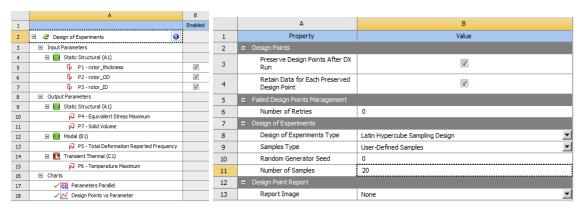


Figure 6: General Design Of Experiments Set Up

	A		В	С	D	E	F	G	Н	
1	Name	•	P1 - rotor_thickness (mm)	P2 - rotor_OD (mm)	P3 - rotor_ID (mm)	P4 - Equivalent Stress Maximum (Pa)	P5 - Total Deformation Reported Frequency (Hz)	P6 - Temperature Maximum (C)	P7 - Solid Volume (m^3)	
2	1 [DP 82	13.575	123.45	79.725	1.2218E+07	1786.8	405.58	0.00060682	
3	2 [DP 86	14.175	124.35	75.875	1.1582E+07	1662	391.01	0.00064653	
4	3 [DP 72	12.075	124.45	76.925	1.1684E+07	1647.3	432.89	0.00058103	
5	4 [DP 84	13.875	123.05	76.575	1.2381E+07	1719.3	402.8	0.00062116	
6	5 [DP 74	12.375	123.75	81.125	1.1576E+07	1786.4	428.99	0.00057253	
7	6	DP 91	14.925	123.85	80.075	1.1 444 E+07	1792.2	381.13	0.00064778	
8	7 [DP 83	13.725	124.25	81.475	1.1438E+07	1787.7	399.03	0.00061374	
9	8	DP 90	14.775	124.05	77.975	1.1761E+07	1739.5	382.64	0.00065376	
10	9 (DP 78	12.975	124.85	75.175	1.1664E+07	1597.1	411.39	0.0006169	
11	10	DP 77	12.825	123.15	76.225	1.3711E+07	1683.9	422.87	0.00059248	
12	11 [DP 80	13.275	123.95	75.525	1.1973E+07	1646.8	408.79	0.00061594	
13	12 (DP 76	12.675	124.15	80.425	1.1671E+07	1761.7	420.34	0.00058667	
14	13 (DP 81	13.425	123.65	81.825	1.2033E+07	1811.5	407.24	0.00059805	
15	14 [DP 87	14.325	124.55	78.325	1.1554E+07	1724.9	387.86	0.00064497	
16	15 [DP 79	13.125	123.25	77.275	1.1939E+07	1719.5	415.77	0.00059935	
17	16	DP 89	14.625	123.35	79.025	1.2233E+07	1785.4	388.18	0.00063758	
18	17 [DP 88	14.475	124.95	79.375	1.1804E+07	1738.4	384.2	0.00065016	
19	18 (DP 85	14.025	124.65	78.675	1.1696E+07	1726.4	392.37	0.00063606	
20	19	DP 75	12.525	123.55	77.625	1.1769E+07	1706.3	426.75	0.00058399	
21	20 [DP 73	12.225	124.75	80.775	1.162E+07	1740.1	428.2	0.00057886	

Figure 7: Final Design Points

Table of	Schematic (D2: Design	of Experiments (Latir	n Hypercube Samp	oling Design : Use	er-Defined Samples : Rando	m Generator Seed = 0 : N	umber of Samples = 50)		
		Α	В	С	D	E	F	G	Н	
1	Name	• 💌	P1 - rotor_thic (mm)	P2 - rotor_OD (mm)	P3 - rotor_ID ~ (mm)	P4 - Equivalent Stress Maximum (Pa)	P5 - Total Deformation Reported Frequency (Hz)	P6 - Temperature Maximum (C)	P7 - Solid Volume (m^3)	
2	1	DP 16	13.14	125.82	89.28	1.7148E+07	1790.3	405.98	0.00058828	
3	2	DP 16	17.1	140.9	75.84	1.1983E+07	1271.8	346.53	0.00097171	
4	3	DP 14	5.66	146.1	68.16	1.1569E+07	691.93	779.59	0.00048531	
5	4	DP 16	14.9	139.34	88.8	2.0614E+07	1403.5	372.65	0.00080168	
6	5	DP 14	6.54	129.98	70.08	1.1402E+07	1038.3	687.82	0.00044087	
7	6	DP 18	25.46	132.06	80.64	1.2795E+07	1489.1	302.91	0.0011061	
8	7	DP 16	14.46	142.98	87.84	2.064E+07	1322.4	378.88	0.00083641	
9	8	DP 18	25.02	139.86	66.24	2.0515E+07	1357.8	304.28	0.0013748	
10	9	DP 15	9.18	133.62	73.44	1.1659E+07	1163.1	518.55	0.00056529	
11	10	DP 14	7.86	149.74	68.64	1.1774E+07	753.02	587.39	0.00062726	
12	11	DP 15	10.94	124.26	69.6	2.2092E+07	1383.9	464.85	0.00055726	
13	12	DP 14	7.42	136.74	76.8	1.4231E+07	1085.5	616.25	0.00051591	
14	13	DP 15	12.7	135.7	72.48	1.1618E+07	1214.8	410.22	0.00072777	
15	14	DP 17	18.42	148.18	74.88	1.6478E+07	1144.3	334.91	0.001157	
16	15	DP 15	10.5	128.94	89.76	2.6338E+07	1711.7	469.58	0.00054835	
17	16	DP 18	22.38	144.54	85.92	1.8307E+07	1269.1	312.25	0.0012007	
18	17	DP 17	21.5	137.26	70.56	4.4757E+07	1341.1	316.14	0.0011325	
19	18	DP 16	16.66	148.7	84.96	1.7502E+07	1205.2	350.83	0.0010268	
20	19	DP 14	6.98	134.66	79.68	1.1175E+07	1183	649.1	0.0004862	
21	20	DP 14	6.1	149.22	81.6	1.1583E+07	852.16	729.44	0.00053387	
22	21	DP 15	12.26	140.38	77.76	1.2021E+07	1206.6	419.9	0.00074705	
23	22	DP 18	22.82	128.42	85.44	1.743E+07	1583.1	311.32	0.00090803	
24	23	DP 18	25.9	146.62	83.04	1.8052E+07	1217.5	301.49	0.0014282	
25	24	DP 14	8.3	127.38	75.36	1.1357E+07	1358	565.21	0.00048752	
26	25	DP 17	19.74	137.78	69.12	2.2113E+07	1273.8	325.81	0.0010725	
27	26	DP 16	16.22	134.14	79.2	1.7834E+07	1473.3	355.68	0.00082332	
28	27	DP 17	21.06	133.1	83.52	1.335E+07	1510.8	318.34	0.00095244	
29	28	DP 17	17.98	127.9	72.96	1.2877E+07	1534.7	339.72	0.00082762	

Figure 8: Semi-final Design Points

Response Surface

For the response surface, Kringing type was chosen to compensate for the small number of samples at the end. Additionally, about ¼ of the sample size was used as verification points on every set of samples run. The figures below show the response surface configuration and final response point.

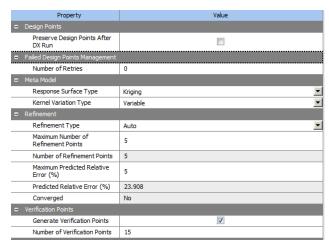


Figure 9: General Response Surface Setup

Table 1: Response Points

Name	P1 (mm)	P2 (mm)	P3 (mm)	P4 (Pa)	P5 (Hz)	P6 (C)	P7 (m^3)
Semi-final Response Point	16	137	78	16336176.1	1379.139738	357.0146723	0.0008594019427
Final Response Point	13.5	124	78.5	11624249.07	1735.973582	404.2538199	0.0006143285002

Sensitivity

In the final sample, the sensitivities were most monotonic. All but one parameter were mostly monotonic, which was equivalent stress. The sensitivities are shown in figures 10-14. From these figures, thickness seems to have the highest impact. For both temperature and volume, thickness has the steepest curve.

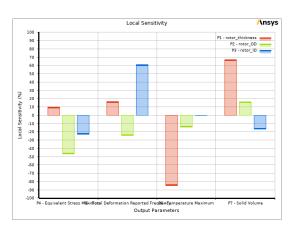


Figure 10: Local Sensitivity

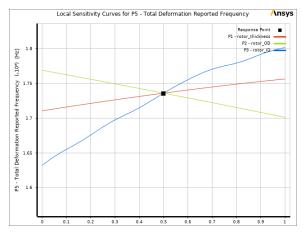


Figure 11: Frequency Sensitivity

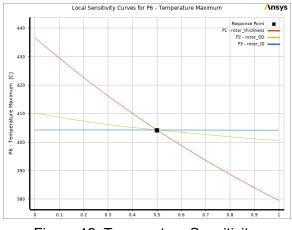


Figure 12: Temperature Sensitivity

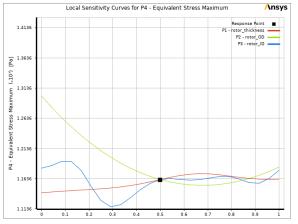


Figure 13: Equivalent Stress Sensitivity

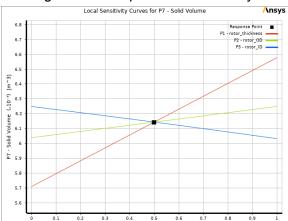


Figure 14: Volume Sensitivity

Optimization (MOGA)

For optimization, the MOGA method was used. In this method, volume was chosen as the main objective to minimize. Then, stress, frequency, and temperature were set as constraints. Their bounds were determined based on the average of the corresponding set of samples.

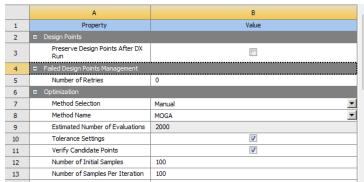


Figure 15: General Optimization Setup

Reference	Name 🔻	P1 - r (P2 -	P3 -	P4 - Equivalent S Maximum (Pa		P5 - Total Deformation Reported Frequency (Hz)		P6 - Temperature Maximum (C)		P7 - Solid Volume (m^3)															
Reference	Name		(r 💌 (Parameter Value	Variation from Reference	Parameter Value	Variation from Reference	Parameter Value	Variation from Reference	Parameter Value	Variation from Reference														
0	Candidate Point 1			83.511	1.6033E+07	14.56%	1783.9	1.28%	416.23	-0.88%	★ 0.00058516	-0.49%														
0	Candidate Point 1 (verified)	12.653	124.95		1.2585E+07	-10.08%	1793.3	1.82%	× 417.95	-0.47%	★ 0.00058516	-0.49%														
0	Candidate Point 2					1.5521E+07	10.90%	1745	-0.93%	415.69	-1.01%	★ 0.00058806	0.00%													
•	Candidate Point 2 (verified)	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	12.692	124.13	80.011	1.3996E+07	0.00%	1761.3	0.00%	× 419.94	0.00%	★ 0.00058805	0.00%
0	Candidate Point 3		125.58					1.5834E+07	13.13%	1751.2	-0.57%	415.25	-1.12%	★ 0.00059398	1.01%											
0	Candidate Point 3 (verified)	12.676		82.874	1.1223E+07	-19.81%	1757.3	-0.23%	415.69	-1.01%	★ 0.00059399	1.01%														

Figure 16: Candidate Points From Semi-final Optimization

		Object	ive		Constraint				
Name	Parameter	Туре	Targ	et erar	Туре	Lower Bound	Upper Bound	Tolerance	
Minimize P7	P7 - Solid Volume	Minimize	0		No Constraint	1			
P4 <= 1.3226E+07 Pa	P4 - Equivalent Stress Maximum	No Objective	-		Values <= Upper Bound	1	1.3226E+07	0.001	
P5 >= 1642 Hz	P5 - Total Deformation Reported Frequency	No Objective	-		Values >= Lower Bound	1642		0.001	
P6 <= 405.9 C	P6 - Temperature Maximum	No Objective			Values <= Upper Bound	1	405.9	0.001	

Figure 17: Objective And Constraints For Final Optimization

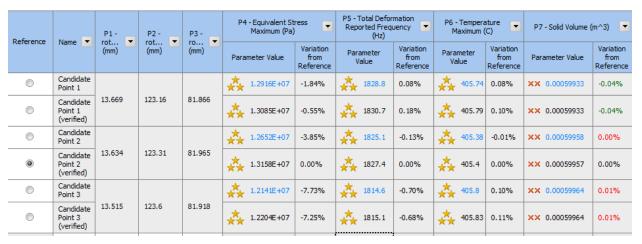


Figure 18: Candidate Points From Final Optimization

From Figure 18 above, the variation from both candidate points to verified points and candidate points to candidate points is relatively low. This is a good indicator of approaching an optimal solution.

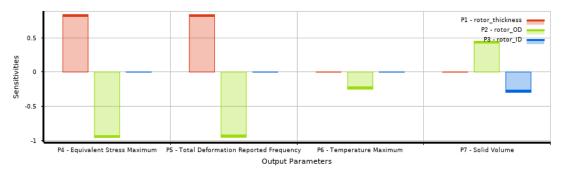


Figure 19: Sensitivities for Final Optimization

Optimal Solution

The figures below are a visual representation of the final solution.

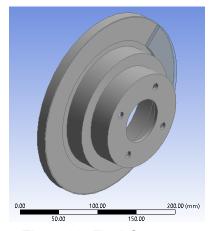


Figure 20: Final Geometry

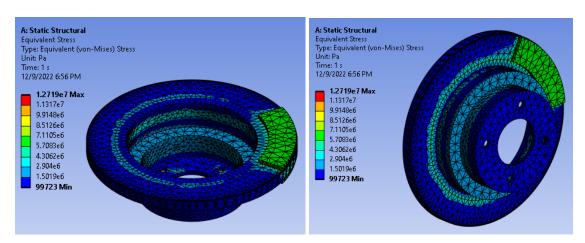


Figure 21: Final Equivalent Stress From Static Structural Analysis

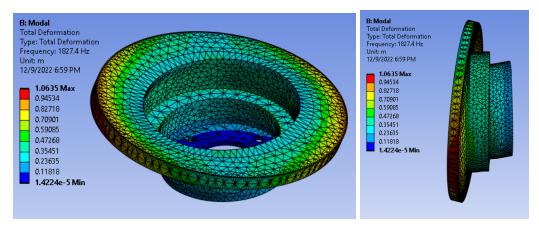


Figure 22: Final Total Deformation From Modal Analysis

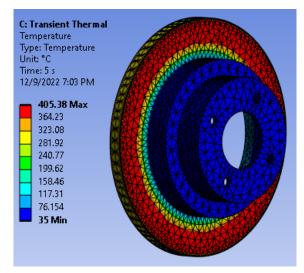


Figure 23: Final Temperature From Transient Thermal Analysis

Result Validation

The optimal solution reached was a pretty reasonable optimization of the initial design. It minimized volume, minimized stress, and maximized frequency as shown in the table below. Specifically, the main objective, the volume, was significantly improved. The only aspect in which it was unsuccessful was it increased the temperature instead of decreasing it.

Table 2: Results Comparision

Parameter	Initial Value	Optimal value	% Difference
P1 - rotor_thickness (mm)	25	13.63381702	-58.84%
P2 - rotor_OD (mm)	125	123.305501	-1.36%
P3 - rotor_ID (mm)	75	81.96505569	8.87%
P4 - Equivalent Stress Maximum (Pa)	13226000	13157839.5	-0.52%
P5 - Total Deformation Reported Frequency (Hz)	1642	1827.424017	10.69%
P6 - Temperature Maximum (C)	307.09	405.401825	27.60%
P7 - Solid Volume (m^3)	0.00099667	0.0005995741148	-49.75%

Although the design failed in one aspect, that is a tradeoff of MOGA optimization in ANSYS. You can only set one variable as the objective, the rest have to be set as constraints that can exist in the samples.

Ultimately, I believe the optimal design was reasonable based on the iterations ran. A bigger sample was first used and then the optimal design from there was used to create a new set of bounds and samples. Additionally, the sensitivity of the final sample was mostly monotonic. Finally, the variance percentage in the candidate points from optimization was pretty low.