

## 3CL4 Pre Lab 5

Hemant Arora, 400440039      Warun Gumarawell, 400450068

April 3, 2025

### Question 1

From lab 4 prelab, the parameters were:

$$K_c = 11.11$$

$$z = -4$$

$$p = -9.33$$

$$K_v = 6.99$$

New system parameters:

$$P.O = 10\%$$

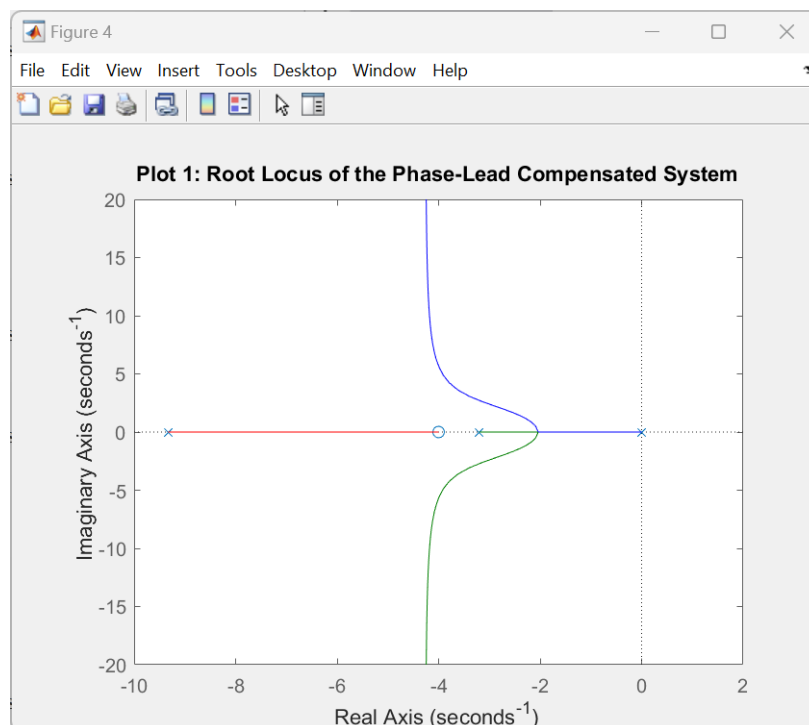
$$T_s = 1\text{ s}$$

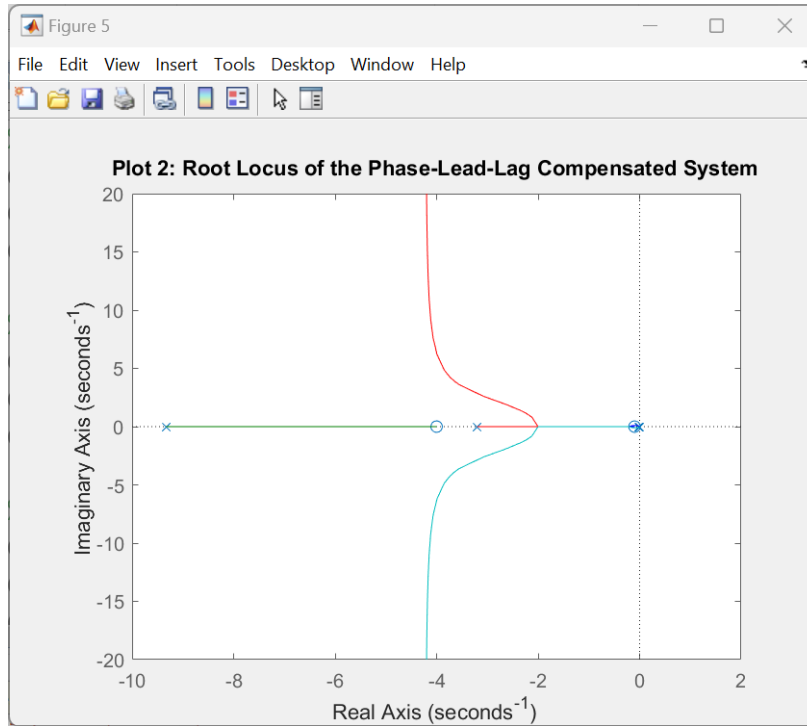
$$K_{v2} = 69.9 \quad (10 \times K_v)$$

### Question 2

To satisfy the requirement of increasing  $K_v$  by a factor of 10 while minimizing impact on overshoot and settling time, the phase lag compensator's zero ( $z_{lag}$ ) and pole ( $p_{lag}$ ) are placed close to the origin with  $\frac{z_{lag}}{p_{lag}} = 10$ . Choosing  $z_{lag} = 0.1$  and  $p_{lag} = 0.01$  ensures the  $K_v$  boost while their proximity guarantees negligible net angle contribution to the dominant poles. From the root locus perspective, since  $z_l$  and  $p_{lag}$  are near  $s = 0$ , their angles to the dominant poles nearly cancel out ( $\theta_z - \theta_p \approx 0$ ), preserving the transient response shaped by the lead compensator.

### Question 3





#### Question 4

From lab 4, the parameters were:

$$\begin{aligned} K_c &= 2.180 \\ z &= -13.33 \\ p &= -32.60 \\ K_v &= 24.95 \end{aligned}$$

#### Question 5

Similar to Question 2, we select the phase lag compensator poles/zeros ( $z_l = 0.1$ ,  $p_l = 0.01$ ) to achieve:

- A  $10\times$  boost in  $K_v$  (since  $\frac{z_l}{p_l} = 10$ ),
- Minimal impact on transient response (angles from  $z_l$  and  $p_l$  cancel out near  $s = 0$ ).

The lead-lag compensator is:

$$G_c(s) = G_{\text{lead}}(s) \cdot \frac{s + 0.1}{s + 0.01}.$$

#### Question 6

The lead-lag compensator  $\bar{G}_c(s)$  and DC motor  $G(s)$  combine as:

$$\bar{G}_c(s)G(s) = \underbrace{2.180 \frac{(s + 0.1)(s + 13.33)}{(s + 0.01)(s + 32.60)}}_{\text{Lead-Lag Compensator}} \cdot \underbrace{\frac{279.3}{s(s + 9.98)}}_{\text{DC Motor}},$$

yielding:

**Question 7**

$$\overline{G}_c(s)G(s) = \frac{(2.180)(279.3)(s + 13.33)(s + 0.1)}{s(s + 9.98)(s + 32.60)(s + 0.01)}.$$

The closed loop transfer functions are:

$$T_{\text{lead}}(s) = \frac{595.8s + 7942}{s^3 + 42.58s^2 + 921.1s + 7942} \quad (\text{Lead-only}) \quad (1)$$

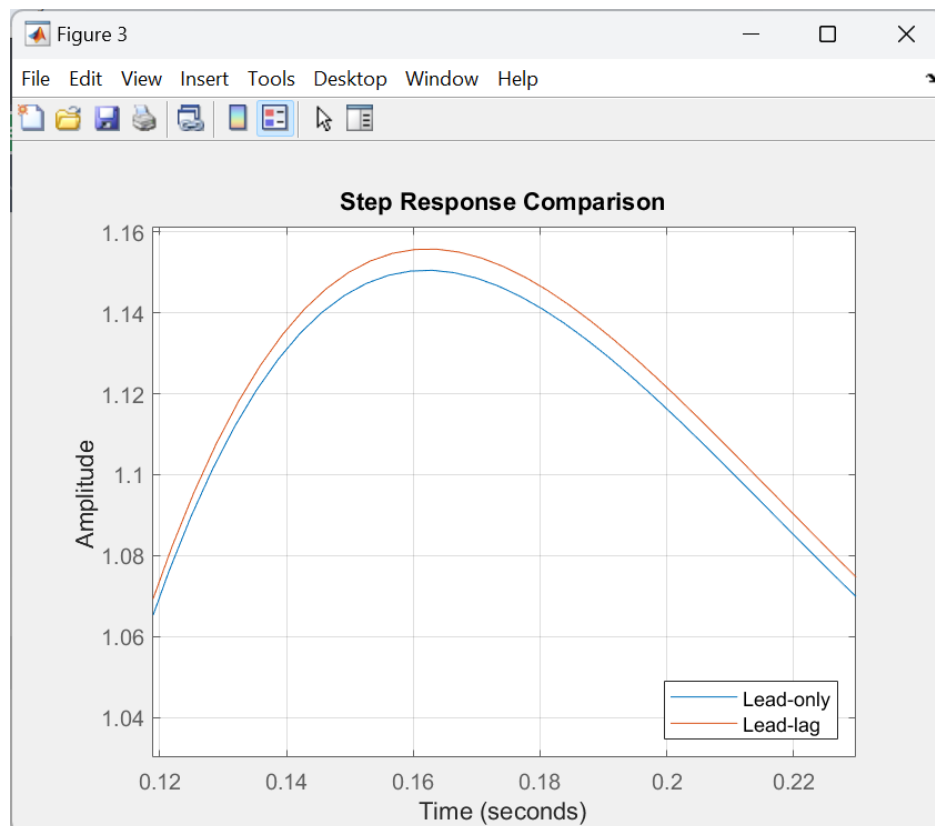
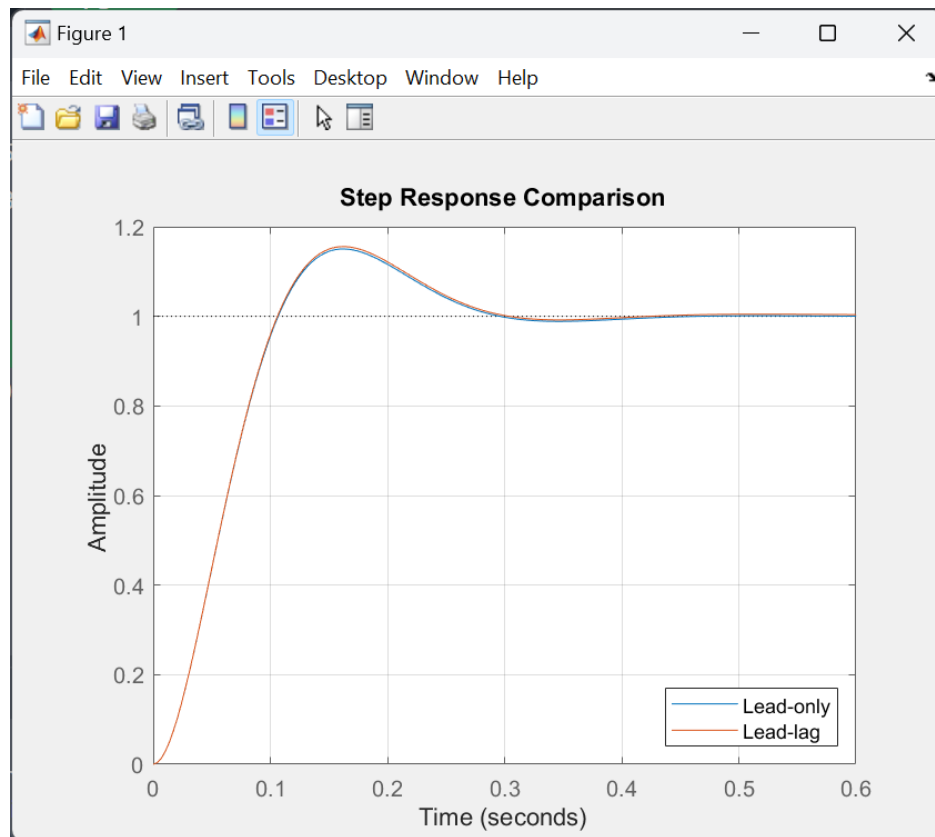
$$T_{\text{lead-lag}}(s) = \frac{595.8s^2 + 8002s + 794.2}{s^4 + 42.59s^3 + 921.6s^2 + 8005s + 794.2} \quad (\text{Lead-lag}) \quad (2)$$

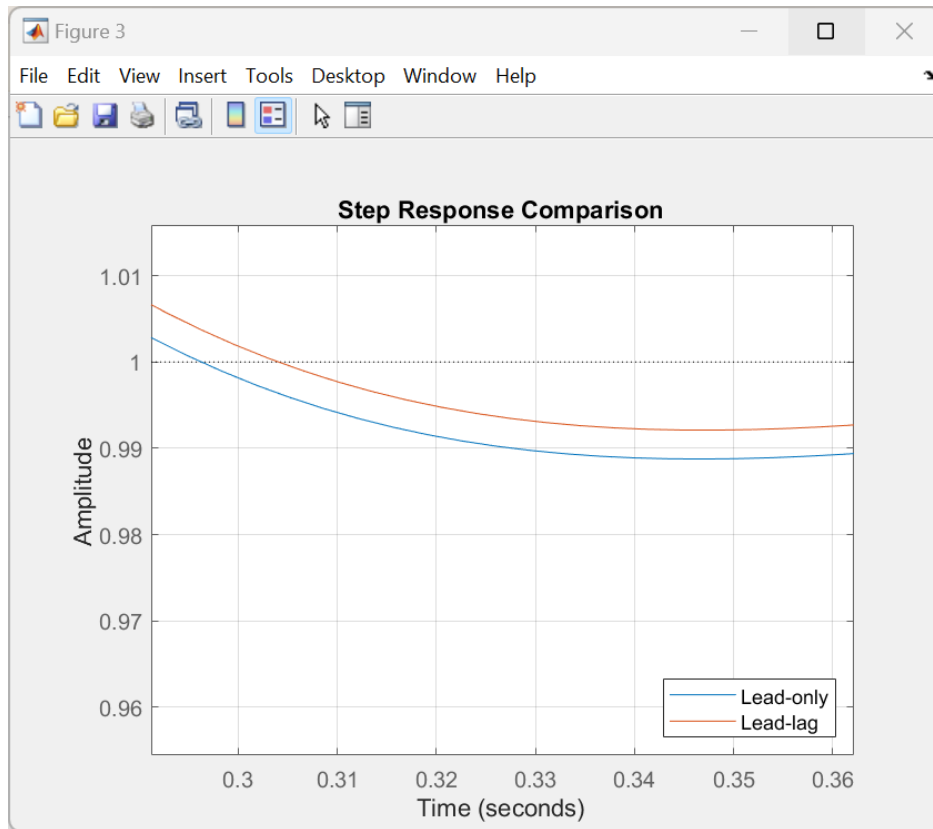
Table 1: Comparison of System Characteristics

| Feature                                  | Lead-Only                   | Lead-Lag                             |
|--|-----------------------------|--------------------------------------|
| <b>Transfer Function Characteristics</b> |                             |                                      |
| System Order                             | 3rd                         | 4th                                  |
| Number of Zeros                          | 1                           | 2                                    |
| <b>Pole-Zero Locations</b>               |                             |                                      |
| Zeros                                    | -13.33                      | -13.33, -0.1                         |
| Poles                                    | $-13.28 \pm 17.87j, -16.02$ | $-13.22 \pm 17.84j, -16.05, -0.1004$ |
| <b>Performance Characteristics</b>       |                             |                                      |
| Dominant Poles                           | $-13.28 \pm 17.87j$         | $-13.22 \pm 17.84j$                  |
| Additional Dynamics                      | None                        | Pole at -0.1004, Zero at -0.1        |
| $K_v$ Improvement                        | 1×                          | 10×                                  |

The lead-lag compensator introduces a pole-zero pair near the origin (pole at -0.1004 and zero at -0.1). These additions produce two key effects: First, their ratio  $\frac{0.1}{0.1004} \approx 1$  boosts  $K_v$  by 10×, improving the system's ability to track ramp inputs, reducing steady-state error. Second, the dominant poles governing transient response shift only minimally from  $-13.28 \pm 17.87j$  to  $-13.22 \pm 17.84j$ , preserving the system's overshoot and settling time characteristics. The physical proximity of the new pole and zero ensures their angle contributions effectively cancel out in the root locus plot, leaving the dominant pole locations and consequently the system's speed and stability margins virtually unchanged.

**Question 8** The lead and lead-lag systems show nearly identical step responses, with similar overshoot and settling time. The lag compensator's extra pole-zero pair (-0.01 and -0.1) has minimal effect on transient performance.





**Question 9** For ramp inputs, the lead-lag system reduces steady-state error by 10× due to its 0.1/0.01 pole-zero ratio. This improves  $K_v$  as designed, while maintaining the lead compensator's good transient response.

