

# **Netaji Subhas University of Technology**

Department of Electronics and Communication  
Engineering



## **PRACTICAL FILE RF AND MICROWAVE ENGINEERING ECECC20**

Name: Ronak Ramuka

Roll no: 2021UEC2598

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# **EXPERIMENT-1**

**AIM:-** Study of microwave components and Instruments

**Apparatus Used:-** Klystron power supply, Gunn power supply, VSWR meter, power meter, Slotted section, Frequency/wave meter, RF Generator, Vector Network Analyzer

## **Theory:**

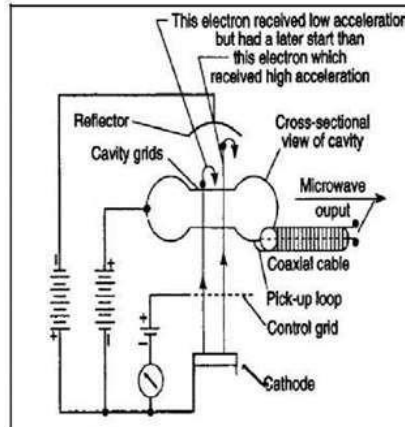
**1. Rectangular Waveguide:** Wave guides are manufactured to the highest mechanical and electrical standards and mechanical tolerances. L and S band wave guides are fabricated by precision brazing of brass-plates and all other wave guides are in extrusion quality. Waveguide sections of specified length can be supplied with flanges, painted outside and silver or gold plated in side.



**2. Klystron Power Supply:** Klystron Power supply is a regulated power supply for operating low power klystron. Klystron power supply generates voltage required for driving the reflex klystron tubes like 2k25, 2k56, 2k22. It is absolutely stable, regulated and short circuit protected power supply. It has the facility to vary the Beam Voltage continuously and built in facility of square wave and saw tooth generators, for amplitude and frequency modulation.



**3. Reflex Klystron (Klystron mount with tube) :** A waveguide of suitable length having octal base on the broad wall of the waveguide for mounting the klystron tube. It consists of movable short at one end of the waveguide to direct the microwave energy generated by the klystron tube. A small hole located exactly at the center of the broad wall of the waveguide is used to put the coupling pin of the tube as the electric field vector of EM energy is maximum at the center only. The maximum power transfer can be achieved by tuning of the movable plunger.



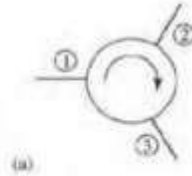
**4. Isolator:** The microwave test bench includes an attenuator, and an isolator. Both of these help to stop the reflected power from reaching the oscillator and pulling the frequency of the cavity and Gunn diode off tune when the load impedance is varied. An isolator is a two port device that transmits microwave or radio frequency power in one direction only. It is used to shield equipment on its input side, from the effects of conditions on its output side; for example, to prevent a microwave source being detuned by a mismatched load. An ideal isolator transmits all the power entering port 1 to port 2, while absorbing all the power entering port 2. An isolator is a non-reciprocal device, with a non-symmetric matrix.



**5. Circulator:** A circulator is a passive non-reciprocal three port device in which microwave or radiofrequency power entering any port is transmitted to the next port in rotation only. Model 6021 and 6022 are T and Y types of three port circulators respectively. These are precisely machined and assembled to get the desired specifications.

**Clockwise Circulator**

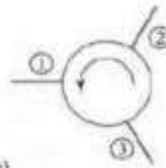
$$[S] = \begin{bmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}$$



(a)

**Counterclockwise Circulator**

$$[S] = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 1 & 0 & 0 \end{bmatrix}$$



(b)

**6. Attenuator:** Attenuators are required to adjust the power flowing in a waveguide. Attenuators are of fixed, variable and rotary vane type, i.e. Fixed: Any amount of fixed attenuation can be supplied between 3 to 40 dB. These attenuators are calibrated frequency band. Variable: Variable attenuators provide a convenient means of adjusting power level very accurately.



**7. Direct reading frequency meter:** This Frequency Meter has convenient readout with high resolution is provided by long spiral dials. These dials have all frequency calibrations visible so you can tell at a glance the specific portion of each band you are measuring. Overall accuracy of these frequency meters is 0.17% and includes such variables as dial calibration. It is constructed from a cylindrical cavity resonator with a variable short circuit termination. The shorting plunger is used to change the resonance frequency of the cavity by changing the cavity length. DRF measures the frequency directly. It is particularly useful when measuring frequency

differences of small changes. The cylindrical cavity forms a resonator that produces a suck-out in the frequency response of the unit. This you would turn the knob until a dip in the response is observed.



**8. Slotted line section with probe carriage:** The slotted line represented the basic instrument of microwave measurements. With its help it is possible to determine the VSWR, attenuation, phase and impedances. The position of carriage (probe) can be read from a scale with its vernier. The total travel of probe carriage is more than three time of half of guide wavelength. This system consists of a transmission line (waveguide), a traveling probe carriage and facility for attaching/detecting instruments. The slot made in the center of the broad face do not radiate for any power of dominant mode. The precision built probe carriage having centimeter scale with a vernier reading of 0.1 mm least count is used to note the position of the probe. Additionally slotted section can be used to measure reflection coefficient and the return loss.



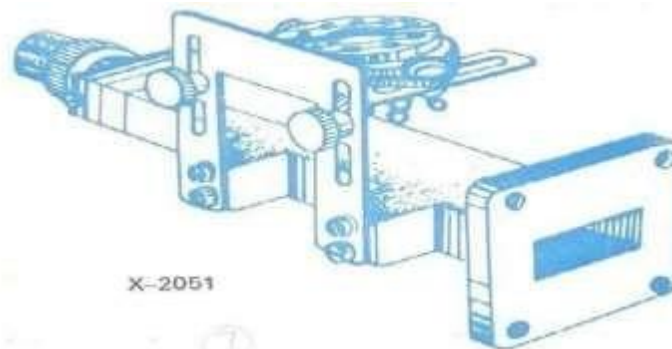
**9. Crystal Detector:** The crystal detector (Detector mount) can be used for the detection of microwave signal. RF choke is built into the crystal mounting to reduce leakage from BNC connector. Square law characteristics may be used with a high

gain selective amplifier having a square law meter calibration. At low level of microwave power, the response of each detector approximate to square law characteristics and may be used with a high gain selective amplifier having a square law meter calibration.



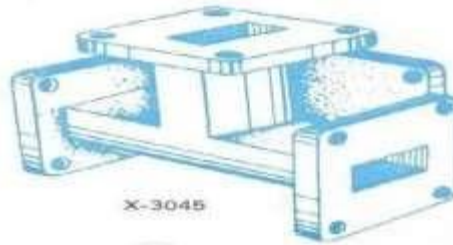
**10. VSWR Meter:** The SWR meter or VSWR (voltage standing wave ratio) meter measures the standing wave ratio in a transmission line. The meter can be used to indicate the degree of mismatch between a transmission line and its load (usually a radio antenna), or evaluate the effectiveness of impedance matching efforts.

**11. Klystron Mount:** Model 2051 Klystron mounts are meant for mounting corresponding Klystrons such as 2K25, 723A/B, 726A or RK - 5976 etc. These consists of a section of wave guide flanged on one end and terminated with a movable short on the other end. An octal base with cable is provided for Klystron.

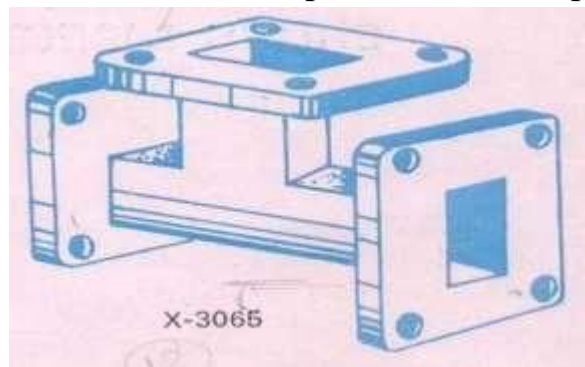


**12. E-Plane Tee: Model 3061 E - plane tee** are series type T - junction and consists of three section of wave guide joined together in order to divide or compare power levels. The signal entering the first port of this T - junction will be equally dividing at second and third ports of the same magnitude but in opp. Phase

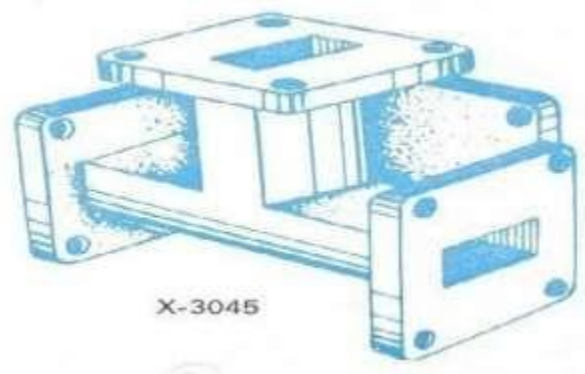




**13. H-Plane Tee: Model 3065** H - Plane Tee are shunt type T - junction for use in conjunction with VSWR meters, frequency - meters and other detector devices. Like in E-plane tee, the signal fed through first port of H - plane Tee will be equally divided in magnitude at second and third ports but in same phase.



**14. Magic Tee: Model 3045** E - H Tee consists of a section of wave guide in both series and shunt wave guide arms, mounted at the exact midpoint of main arm. Both ends of the section of wave guide and both arms are flanged on their ends. These Tees are employed in balanced mixers, AFC circuits and impedance measurement circuits etc. This becomes a four terminal device where one terminal is isolated from the input terminal.



## RESULT:-

Thus all the microwave components were studied in detail.



## EXPERIMENT 2

**AIM:-** Set up an experiment to measure frequency, power and wavelength of microwave signal.

**APPARATUS REQUIRED:-** Klystron tube 2k25, klystron power supply 5kps-610, klystron mount, XM-251, isolator XI-621, Frequency meter XF-455, Variable attenuator, Slotted section XS-651, Tunable Probe Xp-655, VSWR Meter SW-115, Waveguide Stand, Movable short XT-481, Matched Termination XL-400

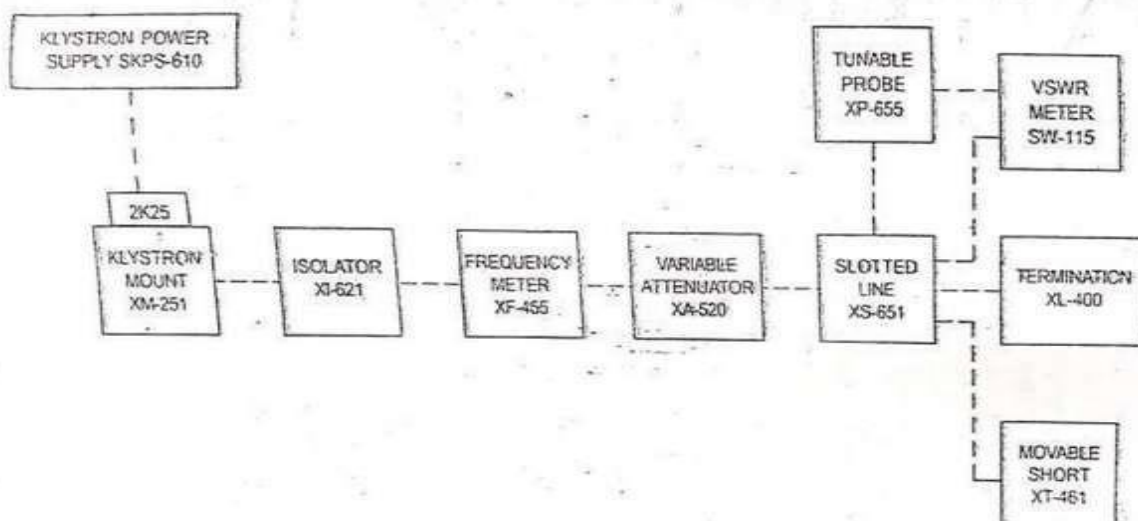
### **THEORY:-**

For dominant TE<sub>10</sub> mode

$$1/\lambda_b^2 = 1/\lambda_g^2 + 1/\lambda_c^2$$

where  $\lambda_b$  is the free-space wavelength,  $\lambda_g$  is the wavelength of the radio waves in the guiding medium (such as a waveguide or coaxial cable), and  $\lambda_c$  is the cutoff wavelength of the guiding medium.

For TE<sub>10</sub> mode  $\lambda_c = 2a$  where  $a$  is broad dimension of waveguide.



## **OBSERVATIONS:**

$a=2.286\text{cm}$ ,  $\lambda_c=2a=4.572\text{cm}$

S.No	Repeller Voltage(V)	Frequency(f) (GHz)	$\lambda_g$ $=2(d_2 \sim d_1)$	$f = c/\lambda = \sqrt{\frac{1}{\lambda_g^2} + \frac{1}{\lambda_c^2}}$ (GHz)
1	-106	11.5	$2*1.87=3.74$	10.3GHz
2	-5	11.1	$2*2.33=4.66$	9.2GHz

## **RESULT:-**

Frequency, power and wavelength of microwave signal were determined.

## **EXPERIMENT 3**

**AIM:-**Set up an experiment to study the mode characteristics of reflex klystron and to determine mode number, transit time, electronic tuning range (etr) and electronic tuning sensitivity.

**APPARATUS REQUIRED:-** Klystron power supply, klystron with mount, isolator, frequency meter, variable attenuator, slotted section with probe carriage, CRO, movable short.

### **THEORY:-**

Klystron is a microwave vacuum tube employing velocity modulation. These electrons move towards the repeller (ie) the electrons leaving the cavity during the positive half cycle are accelerated while those during negative half cycle are decelerated. the faster ones penetrate further while slower ones penetrate lesser in the field of repeller voltage. but, faster electrons leaving the cavity take longer time to return and hence catch up with slower ones. in the cavity the electrons bunch and interact with the voltage between the cavity grids.

It consists of an electron gun producing a collimated electron beam. It bunches pass through grids at times the grid potential is such that electrons are decelerated they give by energy. the electrons are then collected by a positive cavity wall near the cathode. to protect repeller from damage, repeller voltage is applied before accelerating voltage.

### **CALCULATION:-**

Knowing mode top voltages of two adjacent modes, mode numbers of the modes is computed from the equation,

$$n_2/n_1 = v_1/v_2 = [(n + 1) + 3/4]/[n + 3/4]$$

where  $v_1$  and  $v_2$  are the values of repeller voltages required to operate the klystron in mode numbers  $n_1$  and  $n_2$ .

Knowing mode number, transit time of each mode is calculated from

$$t_1 = [n + 3/4]/f_{01} = n_1/f_{01}$$

$f_{01} \rightarrow$  frequency of microwave operation in one mode.

etr – electronic tuning range i.e, the frequency band from one end of the mode to another is calculated by

$$\text{etr} = f_{1\text{max}} - f_{1\text{min}} \text{ for } n_1 \text{ mode (ghz)}$$

$f_{1\text{max}} - f_{1\text{min}} \rightarrow$  half power frequencies

ets – electronic tuning sensitivity

$$\text{ets} = (f_{1\text{max}} - f_{1\text{min}})/(v_{1\text{max}} - v_{1\text{min}})$$

$v_{1\text{max}} - v_{1\text{min}} \rightarrow$  half power frequency

$v_{1\text{max}}, v_{1\text{min}} \rightarrow$  corresponding repeller voltages for a particular mode.

### **OBSERVATION:-**

Mode	Frequency (ghz)	Repeller voltage (v)	Output voltage (mv)
1	9.84	140	50
	9.85	150	325
	9.85	160	275
2	9.895	110	100
	9.87	1000	300
	9.85	90	175

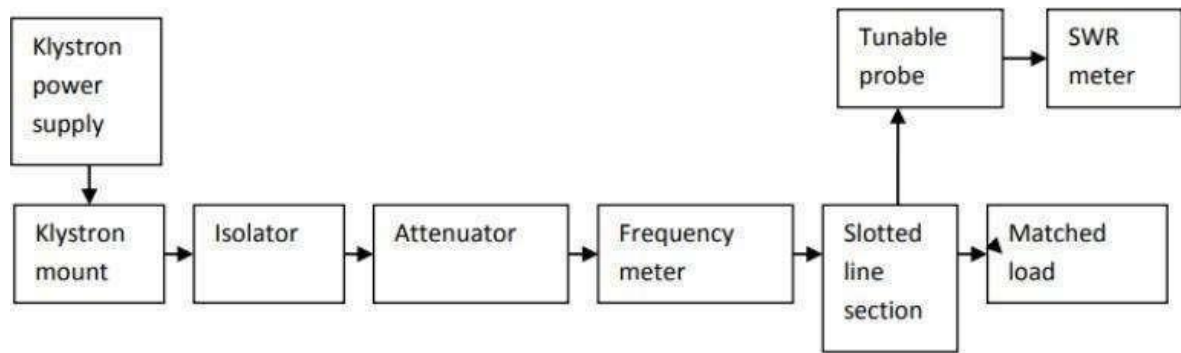
**RESULT:-** Characteristics of reflex klystron were studied and mode number, transit time, electronic tuning range (etr) and electronic tuning sensitivity were determined.

## **EXPERIMENT - 4**

**AIM:** Set up an experiment to measure SWR and reflection coefficient.

**APPARATUS:** Klystron Power supply, klystron mount isolator, frequency meter, variable attenuator, slotted section, tunable probe, VSWR meter, Waveguide stand, movable short/matched termination.

**THEORY:**



**Fig 1.Set up for frequency and wavelength measurement.**

### **TERMINOLOGIES USED**

Reflection Coefficient :

$$\Gamma = (VSWR - 1)/(VSWR + 1)$$

$$VSWR = 1 + |\Gamma| / 1 - |\Gamma|$$

$$\text{Return Loss} : |\Gamma|^2$$

$$\text{Mismatch Loss(mi)} : -\log(1 - |\Gamma|^2)$$

$$\text{Reflected Power (Pr)}: 100 * |\Gamma|^2$$

$$\text{Forward Power(Pf)} : 100 [1 - |\Gamma|^2]$$

**Range of VSWR = 1 to  $\infty$**

**Range of Reflection Coefficient = 0 to 1**

VSWR Meter :



Slotted Line :



## OBSERVATION TABLE:

SNO:	Slotted line reading	VSWR	$\Gamma$	Pf	Pr	mi
1	9	1.43	0.177	3.13%	96.87%	0.013
2	9.5	2.1	0.359	12.88%	87.12%	0.059
<b>3</b>	<b>10</b>	<b>1.09</b>	<b>0.043</b>	<b>0.18%</b>	<b>99.82%</b>	<b>0.007</b>
4	10.5	1.7	0.259	6.7%	93.3%	0.03
5	11	1.4	0.166	2.75%	97.25%	0.012
6	11.5	1.5	0.2	4%	96%	0.017

## RESULT :

VSWR = 1.09

$\Gamma = 0.043$

VSWR and reflection has been calculated from the following calculations for maximum power delivery and minimum mismatch loss.



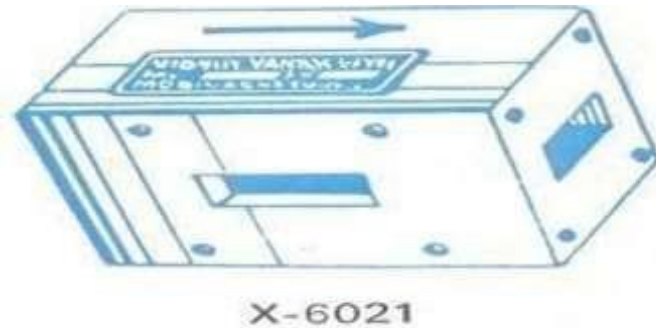
## **EXPERIMENT - 5**

**AIM:** Set up and experiment to study the function of Isolator and circulator.

**APPARATUS:** Klystron Power supply, klystron mount isolator, frequency meter, variable attenuator, slotted section, tunable probe, VSWR meter, Waveguide stand, movable short/matched termination, isolator, circulator.

### **THEORY :**

#### **ISOLATOR**



The three port circulators Model 6021 may be converted into isolators by terminating one of its port into matched load. these will work over the frequency range of circulators. These are well matched devices offering low forward insertion loss and high reverse isolation.

Model No. : X - 6022

Frequency Range (GHz) : 8.6 - 10.6 or 10.2 - 12.2

Min Isolation (dB) : 20

Max Insertion Loss (dB) : 0.4

Max VSWR : 1.20

### OBSERVATION TABLE:

Port	VSWR	$P_{forward}$	$P_{reflected}$	Return Loss	Mismatch Loss
1	1.89	91%	9%	10.45dB	0.4dB
2	1.5	96%	4%	13.97dB	0.01dB

**CALCULATIONS:**

$$S_{11} = VSWR_1 - 1/VSWR_1 + 1$$

$$1.89 - 1/1.89 + 1 = 0.3$$

$$S_{22} = VSWR_2 - 1/VSWR_2 + 1$$

$$1.5 - 1/1.5 + 1 = 0.2$$

$$S_{12} = P_o/P_i = 0.09/0.91 = 0.1$$

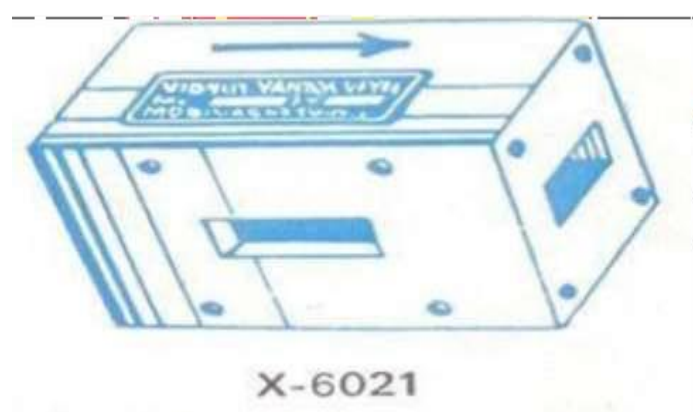
$$S_{21} = P_i/P_o = 0.91/0.09 = 10.1$$

Thus, the scattering matrix is calculated to be

$$S =$$

$$\begin{bmatrix} 0.3 & 0.1 \\ 10.1 & 0.2 \end{bmatrix}$$

# CIRCULATOR



Model 6021 and 6022 are T and Y types of three port circulators respectively. These are precisely machined and assembled to get the desired specifications. Circulators are matched three port devices and these are meant for allowing Microwave energy to flow in clockwise direction with negligible loss but almost no transmission in the anti-clockwise direction.

Model No. : X - 6021

Frequency Range (Ghz) : 8.6 - 10.6 or 10.2 - 12.2

Min. Isolation (dB) : 20

Max. Insertion Loss (dB) : 0.4 Max.

VSWR : 1.20

### **OBSERVATION TABLE:**

Sno	<u>Frequency</u> (GHz)	P1	P2	P3	<u>Insertion</u> <u>loss</u> (Db)	Isolation loss(dB)
1	11.5	45	48	60	3	15
2	11	40	43	57	3	17

### **RESULT:**

Characteristics of isolator and circulator were studied.

## **EXPERIMENT-6**

**AIM:** Set up an experiment to study the functions of Directional coupler.

### **APPARATUS:**

Klystron tube 2k25, klystron power supply 5kps-610, Klystron mount, Directional Coupler, XM-251, Frequency meter X F710, Variable Attenuator, Slotted section Xs-651, Tunable Probe Xp-655, VSWR Meter SW-115, Waveguide Stand, Movable short XT-481, Matched Termination XL-400.

### **THEORY:**

Directional Coupler is a four-port waveguide junction as shown in Figure.



Multi-hole Directional Coupler

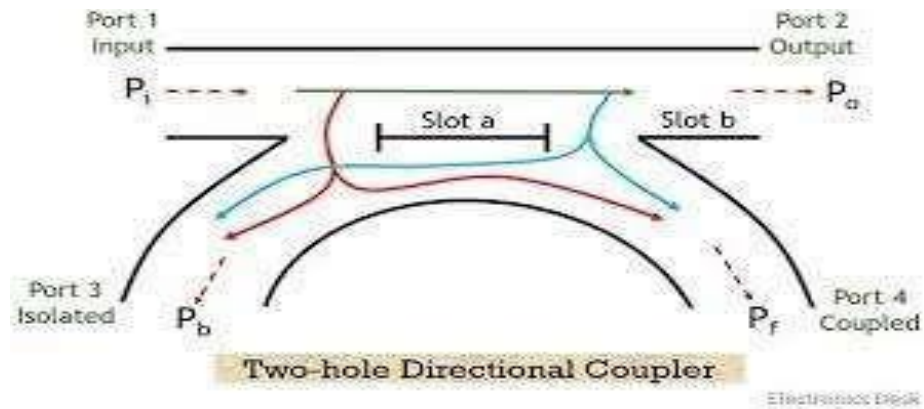
The characteristics of Directional coupler can be expressed in terms of its coupling factor and directivity.

**Coupling Factor:** The coupling factor of a directional coupler is the ratio of incident power to the forward power, measured in dB.

$$C = 10 \log_{10} \frac{P_i}{P_f} \text{ dB}$$

**Directivity:** The Directivity of a Directional coupler is the ratio of forward power to the back power, measured in dB.

$$D = 10 \log_{10} \frac{P_f}{P_b} \text{ dB}$$



Two Hole Directional Coupler

### S-Matrix of Directional Coupler:

a) In a directional coupler all four ports are completely matched. Thus the diagonal elements of the S matrix are zeroes.

$$S_{11} = S_{22} = S_{33} = S_{44} = 0$$

b) There is no coupling between port 1 and port 3 and between port 2 and port 4. So

$$S_{13} = S_{31} = S_{24} = S_{42} = 0$$

Consequently, the S matrix of directional coupler becomes:

$$\mathbf{S} = \begin{bmatrix} 0 & S_{12} & 0 & S_{14} \\ S_{21} & 0 & S_{23} & 0 \\ 0 & S_{32} & 0 & S_{34} \\ S_{41} & 0 & S_{43} & 0 \end{bmatrix}$$

### RESULT:

Functions of directional coupler were studied.

## **EXPERIMENT 7**

**AIM:-** Simulate an air-filled WR-90 waveguide Using ANSYS HFSS as shown in Fig. 1 to obtain the field patterns, intrinsic Impedance and wavelength for the first 4 modes.

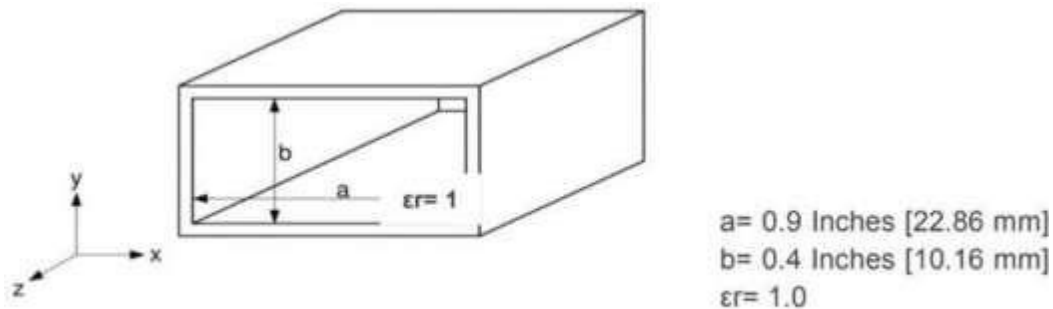


Fig.1 WR-90 Waveguide

### **SOFTWARE REQUIRED:- ANSYS HFSS**

### **PROCEDURE:-**

- 1) Launch ANSYS HFSS and create a new project.
- 2) Create a new design and specify the frequency range as 8.2 GHz to 12.4 GHz, which corresponds to the operating frequency range of the WR-90 waveguide.
- 3) Create a new waveguide structure by selecting "Insert" from the main menu and then selecting "Waveguide" and "WR-90" from the dropdown menu.
- 4) Set the boundary conditions for the waveguide by selecting "Boundaries" from the main menu and then selecting "Waveport". In the "Waveport Excitation" dialog box, select "TE10" as the mode and set the excitation amplitude to 1 V.
- 5) Define the mesh settings by selecting "Mesh Operations" from the main menu and then selecting "Mesh". In the "Mesh" dialog box, select "Fast" as the meshing option and set the maximum mesh size to 1/20th of the wavelength at the lowest frequency of the frequency range.
- 6) Run the simulation by selecting "Solve" from the main menu and then selecting "Setup". In the "Setup" dialog box, select "Driven Modal" as the solution type and set the number of modes to 4.

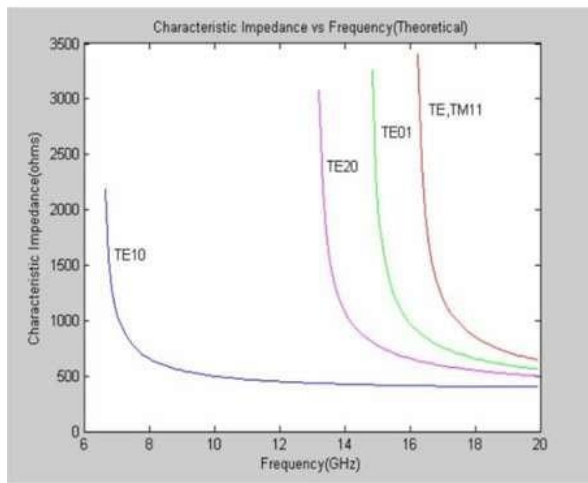
7) Analyze the results by selecting "Results" from the main menu and then selecting "Fields" and "Vector Fields". In the "Vector Fields" dialog box, select "E Field" and "z" component to obtain the field patterns.

8) Calculate the intrinsic impedance by selecting "Results" from the main menu and then selecting "Parameters". In the "Parameters" dialog box, select "Z0" to obtain the intrinsic impedance for each mode.

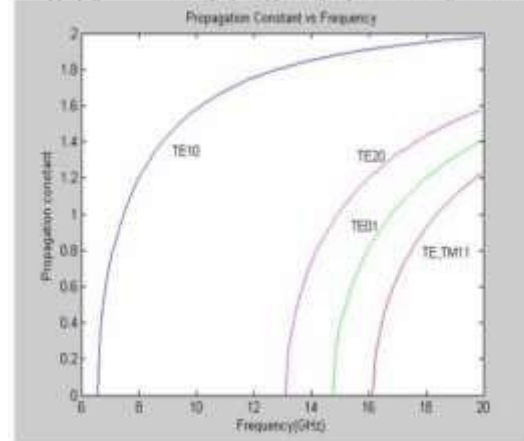
9) Calculate the wavelength for each mode by selecting "Results" from the main menu and then selecting "Fields" and "Vector Fields". In the "Vector Fields" dialog box, select "E Field" and "x" component. Then, select "Calculate Wavelength" from the dropdown menu to obtain the wavelength for each mode.

## OBSERVATIONS:-

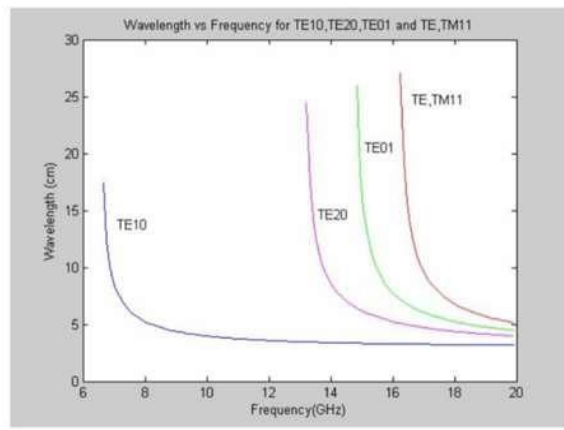
### Impedance vs. Frequency for the first four modes



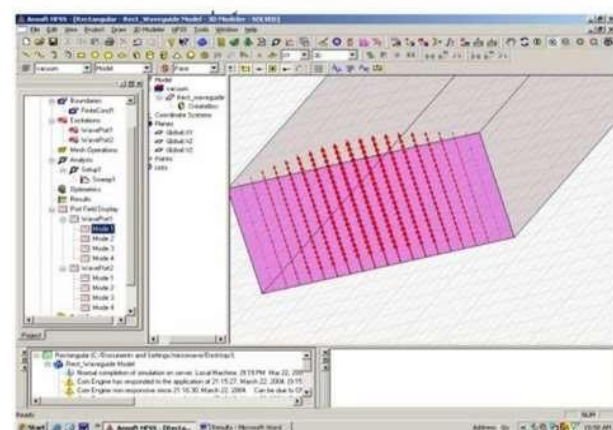
### Plot of propagation constant vs. frequency for the first four modes using Theoretical values



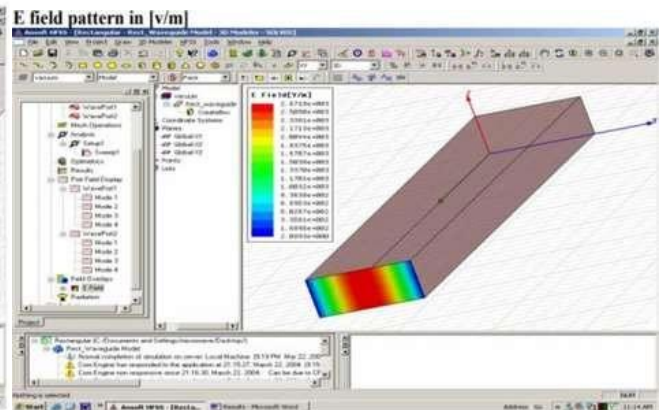
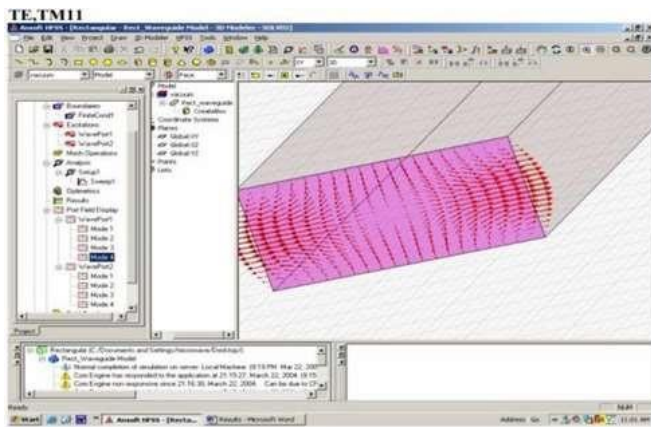
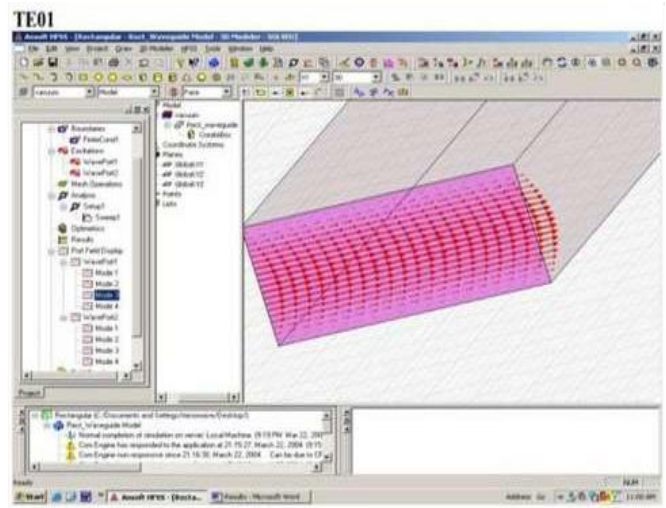
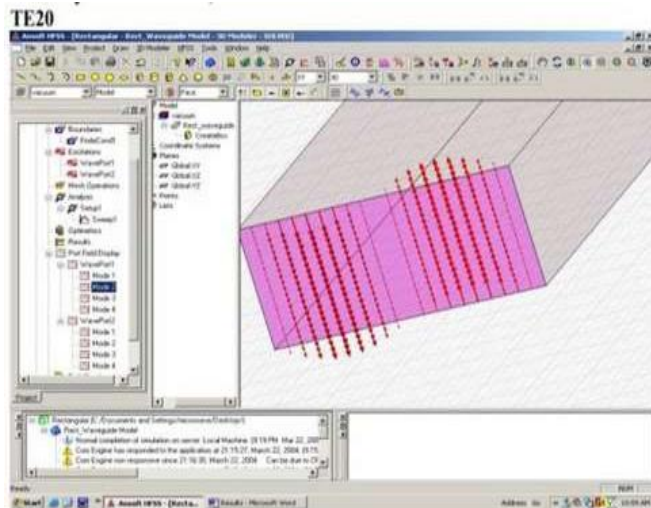
### Wavelength vs. frequency for the first four modes



### TE10 MODE:





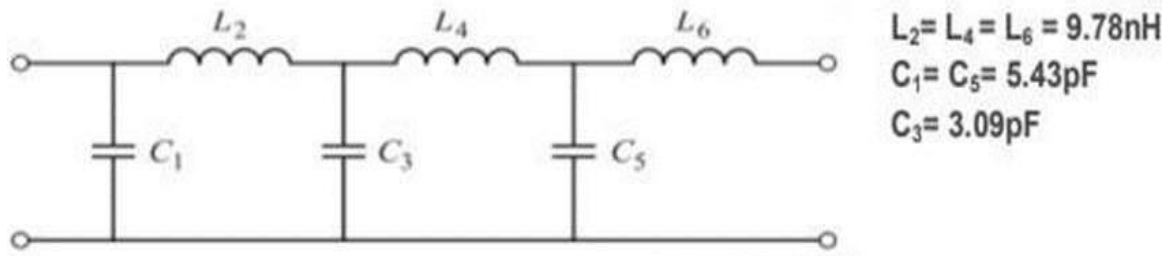


## RESULT:

An air-filled WR-90 waveguide has been designed successfully using ANSYS HFSS.

## EXPERIMENT 8

**AIM:-**For the circuit shown below, determine the ABCD Matrix and then convert it to S-parameters. Plot the return loss and insertion loss over a frequency range of 0.1GHz to 2GHz using MATLAB



**SOFTWARE REQUIRED:-** MATLAB

**THEORY:-**

$$S_{21} = \frac{2}{A + \frac{B}{Z_0} + CZ_0 + D}$$

$$S_{11} = \frac{A + \frac{B}{Z_0} - CZ_0 - D}{A + \frac{B}{Z_0} + CZ_0 + D}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & Z \\ 0 & 1 \end{bmatrix} \Rightarrow \text{Series Impedance } Z$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ Y & 1 \end{bmatrix} \Rightarrow \text{Shunt Admittance } Y$$

T matrix of a cascade of network is the product of T matrix of each network. Therefore ,T matrix is found for any network and they are then converted to S matrix using the above formulas.

$$\text{Return loss} = -20\log(|S_{11}|)$$

$$\text{Insertion loss} = -20\log(|S_{21}|)$$

## MATLAB CODE:

```
L2=9.78.*(10.^(-9));
C1=5.43.*(10.^(-12));
C3=3.09.*(10.^(-12));
f=linspace(0.1,2);
len=length(f);
w=2.*pi.*f.*(10.^9);
s11=zeros(1,len);
s21=zeros(1,len);
Z0=50;
log10s21=zeros(1,len);
log10s11=zeros(1,len);
for i=1:
lenYc=complex(0,w(i)*C1);
X1=complex(0,w(i)*L2);
Yc3=complex(0,w(i)*C3);
TC1=[1,0;Yc,1];
Tl1=[1,X1;0,1];
TC3=[1,0;Yc3,1];
T=TC1*Tl1*TC3*Tl1*TC1*Tl1;
den=T(1,1)+(T(1,2)./Z0)+(T(2,1).*Z0)+T(2,2);
s21(i)=abs(2./den);
log10s21(i)=log10(s21(i));
s11(i)=abs((T(1,1)+(T(1,2)./Z0)-(T(2,1).*Z0)-T(2,2))./den);
log10s11(i)=log10(s11(i));
end figure();
plot(f,s21);
title("s21");
figure();
plot(f,log10s21);
title("insertion loss");
figure();
plot(f,s11); title("s11")
figure();
plot(f,log10s11);
title("return loss");
```

## OUTPUT:-

