This document provides a comprehensive explanation of the control theory governing **Standard Second-Order Systems**, detailing the fundamental parameters, the role of poles in system stability and behavior, key transient response specifications, and visual interpretations.

### I. Standard Form and Core Parameters

The analysis of second-order systems is based on the standard closed-loop transfer function G(s):

$$G(s) = rac{Y(s)}{R(s)} = rac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

This function is defined by two core parameters:

- 1. **Undamped Natural Frequency** ( $\omega_n$ ): This parameter determines the **speed** of the system response, measured in radians per second (rad/s).
- 2. **Damping Ratio** ( $\zeta$ ): This parameter determines the **shape** of the system response (oscillatory or non-oscillatory) and is dimensionless.

### II. System Dynamics: The Poles and Stability (The s-Plane)

The system's dynamic behavior is entirely governed by its poles, which are the roots of the characteristic equation:

$$s^2 + 2\zeta\omega_n s + \omega_n^2 = 0$$

The two poles,  $s_{1,2}$ , are found using the quadratic formula:

$$s_{1,2} = -\zeta \omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

The term **Decay Rate** ( $\sigma$ ) is often defined as the real part of the poles:

$$\sigma = \zeta \omega_n$$

(This  $\sigma$  represents the distance of the pole from the imaginary axis in the s-plane).

### Stability Criteria Based on Poles

The location of the poles in the complex s-plane dictates the system's stability:

- Stable: All poles lie in the Left Half-Plane (LHP), meaning their real part is negative (Re(s) < 0). This occurs when the damping ratio  $\zeta > 0$ .
- Marginally Stable: Poles are on the imaginary axis  $(j\omega$ -axis), meaning their real part is zero ( $\mathrm{Re}(s)=0$ ). This occurs when  $\zeta=0$ .
- Unstable: Any pole lies in the Right Half-Plane (RHP), meaning their real part is positive (Re(s) > 0). This occurs when the damping ratio is negative,  $\zeta < 0$  (negative damping).

Pole Type	$\mathrm{Re}(s)$	$\zeta$ Value	Stability	Location in s-Plane
Negative Poles	Negative	$\zeta > 0$	Stable	LHP
Positive Poles	Positive	$\zeta < 0$	Unstable	RHP
Imaginary Poles	Zero	$\zeta = 0$	Marginally Stable	On $j\omega$ -axis

### III. Damping Status and Response Characteristics

The relationship between the poles and the damping ratio ( $\zeta$ ) determines the fundamental response characteristics of the system.

Damping Status	$\zeta$ Range	Pole Type	Poles $s_{1,2}$	Response Description	Common Example System
Undamped	$\zeta = 0$	Imaginary	$\pm j\omega_n$	Pure oscillation, never settles.	An ideal mass-spring system in a perfect vacuum (no friction).
Underdamped	$0 < \zeta < 1$	Complex Conjugate	$-\sigma\pm j\omega_d$	<b>Damped oscillation</b> (oscillates and settles). Fastest speed with acceptable overshoot.	A <b>shock absorber</b> on a car that is too soft.
Critically Damped	$\zeta = 1$	Real & Equal	$-\omega_n, -\omega_n$	Fastest non-oscillatory response. Ideal transition point.	A properly designed <b>door closer</b> that shuts quickly without slamming.
Overdamped	$\zeta > 1$	Real & Distinct	$-\sigma_a, -\sigma_b$	Slow, <b>non-oscillatory response</b> (lagging). Safe but sluggish.	A system with excessive friction, like a heavy bank vault door closing slowly.
Unstable	$\zeta < 0$	Positive Real Part	$\sigma \pm j\omega$	Oscillations or <b>exponential growth</b> .	A rocket balancing on its tail with an uncompensated control system.

## **IV. Transient Response Specifications**

The transient response refers to the initial behavior of the system before it settles. These specifications are primarily relevant for underdamped systems (0  $< \zeta < 1$ ).

#### 1. Damped Natural Frequency ( $\omega_d$ )

This is the actual frequency of oscillation of the decaying response in an underdamped system.

$$\omega_{\mathbf{d}} = \omega_n \sqrt{1 - \zeta^2}$$

Relation to Poles:  $\omega_d$  is the magnitude of the imaginary part of the complex conjugate poles.

### 2. Peak Time $(T_p)$

The time required for the response to reach the first peak of the overshoot. This is a measure of the speed of response.

$$\mathbf{T_p} = rac{\pi}{\omega_d} = rac{\pi}{\omega_n \sqrt{1-\zeta^2}}$$

Relation to Poles: Primarily determined by the imaginary part of the pole ( $\omega_d$ ).

### 3. Percent Overshoot ( or $M_p$ )

The amount the response overshoots the final steady-state value, expressed as a percentage. This is a measure of relative stability.

$$\mathbf{\%OS} = 100 \cdot e^{-\frac{\zeta\pi}{\sqrt{1-\zeta^2}}}$$

Alternatively, it can be defined as:

$$\mathbf{\%OS} = rac{c(T_p) - c(\infty)}{c(\infty)} imes 100$$

Finding  $\zeta$  from Overshoot: If  $M_p$  is the fractional overshoot (e.g.,  $M_p = 0.1$  for 10% overshoot), the damping ratio can be found by inversion:

$$\zeta = rac{|\ln(M_p)|}{\sqrt{\pi^2 + (\ln(M_p))^2}}$$

*Relation to Poles:* Depends only on the **Damping Ratio**  $\zeta$ .

### 4. Settling Time $(T_s)$

The time required for the response to settle within a defined percentage (usually 2% or 5%) of the final steady-state value. This is a measure of system speed and stability.

 $T_s$  is inversely proportional to the **Decay Rate** ( $\sigma = \zeta \omega_n$ ):

Criterion	Formula for Settling Time $\mathbf{T}_{\mathrm{s}}$
2% Criterion (More common)	$\mathbf{T_{s,2\%}}pprox rac{4}{\zeta\omega_n}=rac{4}{\sigma}$
5% Criterion (Less conservative)	$\mathbf{T_{s,5\%}}pprox rac{3}{\zeta\omega_n}=rac{3}{\sigma}$

*Relation to Poles*: Primarily determined by the **real part** of the pole ( $\sigma$ ).

### 5. Rise Time $(T_r)$

The time required for the response to rise from 10% to 90% of its final value (for overdamped/critically damped) or from 0% to 100% (for underdamped). A common approximation for  $0.1 < \zeta < 1.0$  is used:

$$\mathbf{T_r} pprox rac{1.8}{\omega_n}$$

## V. Impact of Damping Ratio ( $\zeta$ ) on System Specifications

The damping ratio  $\zeta$  is a crucial design parameter that controls the character and stability margin of the response. Optimal control design often targets a  $\zeta$  close to  $\approx 0.707$  to balance speed and overshoot (resulting in roughly 4% to 5% overshoot).

Specification	Relationship with $\zeta$ (Assuming $\omega_n$ is constant)	Impact of Larger $\zeta$
Percent Overshoot ()	Exponentially decreases as $\zeta$ increases.	<b>Shorter overshoot.</b> For $\zeta \geq 1$ , overshoot is zero.
Settling Time $(T_s)$	Inversely proportional to $\zeta$ (via $\sigma=\zeta\omega_n$ ).	Shorter settling time (faster decay), up to the critical point $\zeta=1$ . (Past $\zeta=1$ , $T_s$ increases).
Peak Time ( $T_p$ )	Increases as $\zeta$ increases.	Longer peak time (slower to reach the first peak).
Damped Frequency ( $\omega_d$ )	Decreases as $\zeta$ increases.	Lower oscillation frequency (slower oscillations).

Specification	Relationship with $\zeta$ (Assuming $\omega_n$ is constant)	Impact of Larger $\zeta$
Response Speed (General)	A trade-off between $\zeta$ and $\omega_n$ .	Less oscillatory but potentially slower if $\zeta\gg 1$ . The fastest response is achieved at $\zeta=1$ .

### VI. Geometrical Interpretation

#### A. Poles in the s-Plane

In the Left Half-Plane (LHP), the stable poles are geometrically related to the core parameters:

- 1. Radius: The poles lie on a semi-circle whose radius is equal to  $\omega_n$ .
- 2. **Angle** ( $\theta$ ): The angle  $\theta$  a pole makes with the negative real axis is directly related to the damping ratio:

$$\zeta = \cos(\theta)$$

### B. Trajectory Graphs (Phase Plane Analysis)

A trajectory graph (or phase portrait) plots the system's output variable (position, c(t)) versus its derivative (velocity,  $\dot{c}(t)$ ). This visualizes the system's path from its initial state to the equilibrium point.

For a unit step input, the equilibrium point (where the system settles) is at (1,0). Arrows on the trajectories indicate the direction of time.

#### **Phase Plane Descriptions**

Damping Status	Trajectory Description	Key Behavior
Undamped ( $\zeta=0$ )	Center (Stable Orbit). The trajectory is a closed loop (ellipse/circle) centered on the equilibrium point.	Sustained oscillations, never settles.
Underdamped ( $0<\zeta<1$ )	<b>Stable Focus</b> . The trajectory is an <b>inward spiral</b> that converges toward the equilibrium point.	<b>Decaying oscillations</b> (the spiraling reflects the sinusoidal response).
Critically/Overdamped ( $\zeta \geq 1$ )	<b>Stable Node</b> . The trajectory is a <b>smooth</b> , <b>non-oscillatory curve</b> that moves directly to the equilibrium point.	Fastest non-oscillatory path ( $\zeta=1$ ); slower path ( $\zeta>1$ ).
Unstable ( $\zeta < 0$ )	Unstable Focus (or Node). The trajectory is an outward spiral (or curve) that moves away from the equilibrium point.	Response exhibits <b>exponentially</b> increasing amplitude.

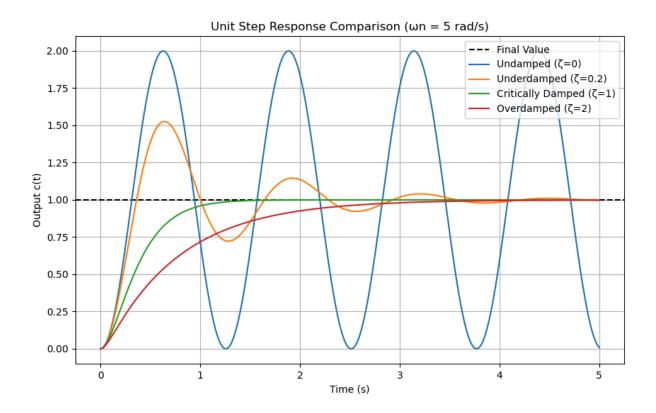
# VII. System Response Visualizations

### 1. Example System Step Response Graph

This simulated output compares the unit step response for the four stable damping statuses with a fixed  $\omega_n = 5 \; \mathrm{rad/s}$ .

- Undamped ( $\zeta = 0$ ): Oscillates indefinitely.
- Underdamped (0 <  $\zeta$  < 1): Shows **overshoot** and decaying oscillations.

- Critically Damped ( $\zeta=1$ ): Reaches the final value fastest without overshoot.
- Overdamped ( $\zeta > 1$ ): Slowest response, approaches value asymptotically without oscillation.



### 2. Trajectory Graph (Phase Plane Comparison)

This conceptual visualization plots velocity ( $\dot{c}$ ) vs. position (c) on the phase plane, showing the path taken by the system towards or away from the equilibrium point (1,0).

- Undamped ( $\zeta = 0$ ): Closed ellipse/circle (Red Dashed).
- **Underdamped** (0  $< \zeta <$  1): Converging spiral (Blue Solid).
- Critically Damped ( $\zeta = 1$ ): Direct, quick path to equilibrium (Green Solid).
- **Overdamped** ( $\zeta > 1$ ): Slower, direct path to equilibrium (Magenta Solid).
- Unstable ( $\zeta$  < 0): Diverging spiral (Black Dotted).

### Conceptual Phase Plane Trajectories for Second-Order System (Unit Step Response)

