

PROBLEMA P1

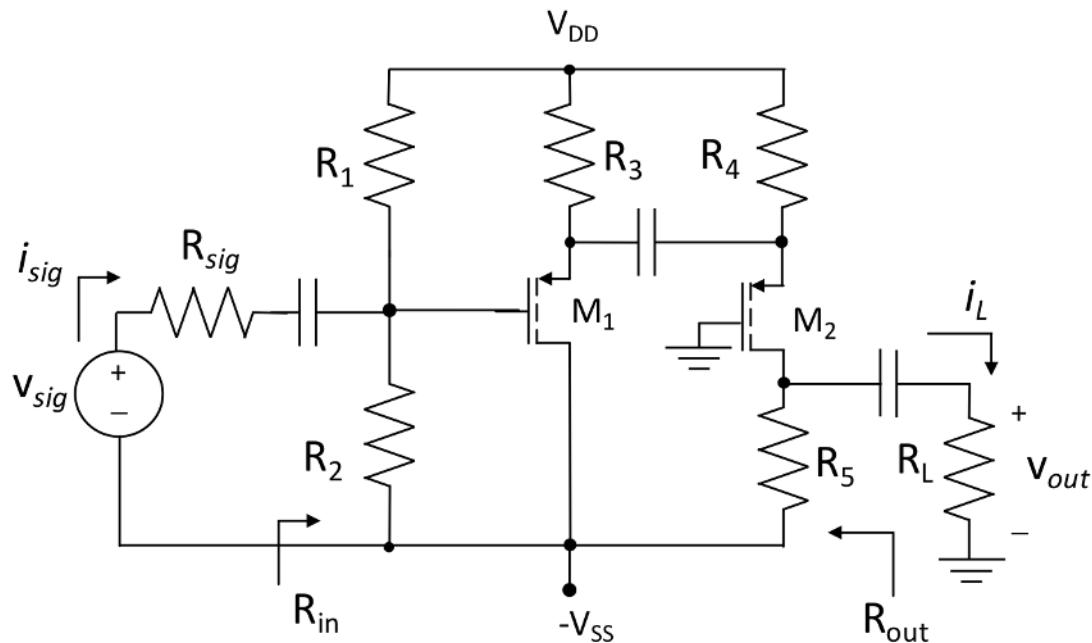
Dato il circuito riportato nella figura sottostante, determinare:

- 1) il valore della resistenza R_3 in modo che la corrente di drain di M_1 valga $I_{D1} = 10 \text{ mA}$;
- 2) il punto di lavoro dei transistor M_1, M_2 ,
- 3) il guadagno di tensione ai piccoli segnali ac $A_v = v_{out}/v_{sig}$;
- 4) Il guadagno di corrente $A_i = i_L/i_{sig}$;
- 5) le resistenze di ingresso e uscita ai piccoli segnali ac R_{in} e R_{out} .

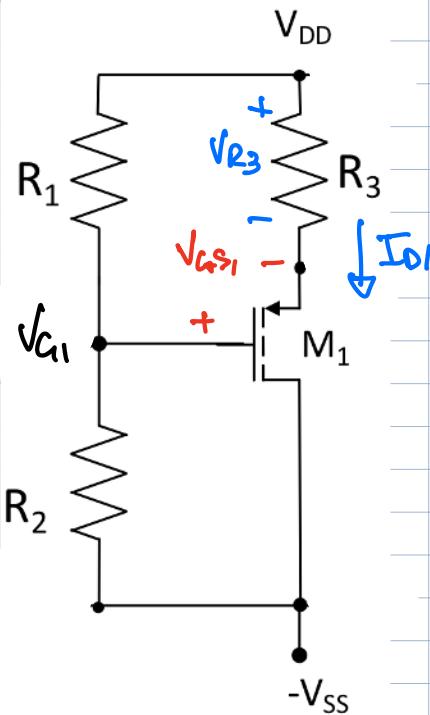
Dati:

$$\begin{aligned} V_{DD} &= 15 \text{ V} \\ V_{SS} &= 15 \text{ V} \\ R_I &= 200 \text{ k}\Omega, \\ R_2 &= 200 \text{ k}\Omega, \\ R_4 &= 1 \text{ k}\Omega, \\ R_5 &= 1.0 \text{ k}\Omega, \\ R_L &= 1.0 \text{ k}\Omega, \\ R_{sig} &= 1.0 \text{ k}\Omega, \end{aligned}$$

$$\begin{aligned} M_1: \quad k_{p1} &= 10 \text{ mA/V}^2, \\ V_{TP1} &= -1 \text{ V}, \\ \lambda_{p1} &= 0 \text{ V}^{-1}; \\ M_2: \quad k_{p2} &= 5 \text{ mA/V}^2, \\ V_{TP2} &= -2 \text{ V}, \\ \lambda_{p2} &= 0 \text{ V}^{-1}; \end{aligned}$$



POLARIZZAZIONE.



$$V_{G1} = V_{DD} \cdot \frac{R_2}{R_1 + R_2} - V_{SS} \cdot \frac{R_1}{R_1 + R_2}$$

$$I_{D1} = \frac{k_{p1}}{2} (V_{GS1} - V_{TP1})^2$$

$$\Rightarrow V_{GS1} = V_{TP1} - \sqrt{\frac{2I_{D1}}{k_{p1}}} = -1V - \sqrt{2V} \quad \underline{\underline{-2,414}}$$

$$V_{GS1} = V_{G1} - V_{S1} = -V_{S1} \quad (V_{G1} = 0)$$

$$\Rightarrow V_{S1} = -V_{GS1} = 2,414$$

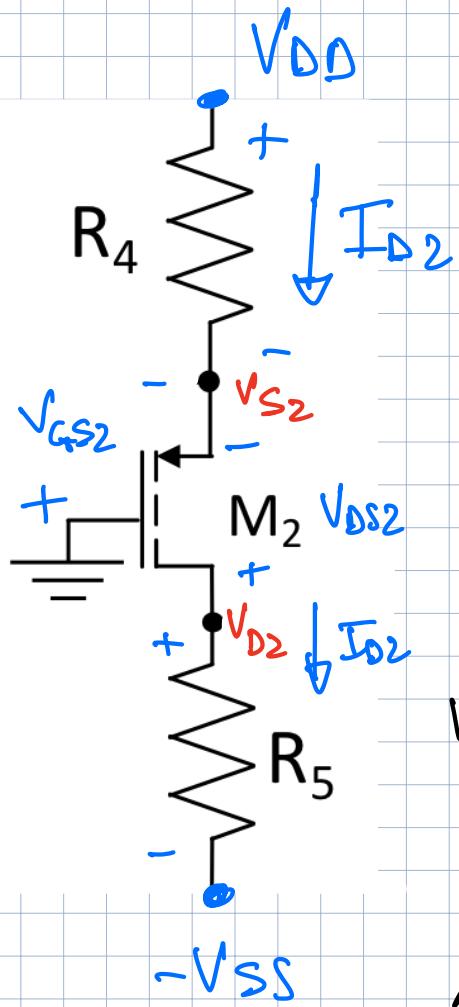
$$V_{S1} = V_{DD} - V_{R3} = V_{DD} - R_3 I_{D1}$$

$$\Rightarrow R_3 = \frac{V_{DD} - V_{S1}}{I_{D1}} = \frac{10V}{5mA} = 1,26k\Omega$$

$$V_{DS1} = -V_{SS} - V_{S1} = -17,414 \text{ V}$$

$V_{DS1} < V_{GS1} - V_{TP1}$?
 $-17,41 \text{ V} < -1 \text{ V}$ OK

M₁ IN SATURATION



$$V_{DD} = R_4 I_{D2} - V_{GS2}$$

$$\Rightarrow I_{D2} = \frac{V_{DD} + V_{GS2}}{R_4}$$

$$I_{D2} = \frac{K_P}{Z} (V_{GS2} - V_{TP2})^2$$

$$\frac{2(V_{DD} + V_{GS2})}{R_4 K_P} = V_{GS2}^2 + V_{TP2}^2 - 2 V_{GS2} V_{TP2}$$

$$V_{GS2}^2 + V_{GS2} \left(-\frac{2}{R_4 K_P} - 2 V_{TP2} \right) + V_{TP2}^2 - \frac{2 V_{DD}}{R_4 K_P} = 0$$

$$a = 1 \quad b = 3,6 \quad c = -2$$

$$\Delta = (3,6)^2 - 4 \times (-2) = 20,96$$

$$V_{GS2} = \frac{-b - \sqrt{\Delta}}{2a} = \frac{-3,6 - 4,59}{2} \text{ V} = -4,09 \text{ V}$$

$$I_{D2} = \frac{K_P}{Z} (V_{GS2} - V_{TP2})^2 = 10,81 \text{ mA}$$

$$V_{S2} = V_{DD} - R_4 I_{D2} = 4,09 \text{ V}$$

$$V_{D2} = -V_{SS} + R_5 I_{D2} = -4,09 \text{ V}$$

$$V_{DS2} = V_{D2} - V_{S2} = -8,18 \text{ V} < V_{GS2} - V_{TP2} ?$$

$$-8,18 < -1,32 \text{ V}$$

OK M₂ IN SATURATION

$$M_1: I_{D1} = 10 \text{ mA}, V_{DS1} = -17,61 \text{ V}, V_{GS1} = -2,41 \text{ V.}$$

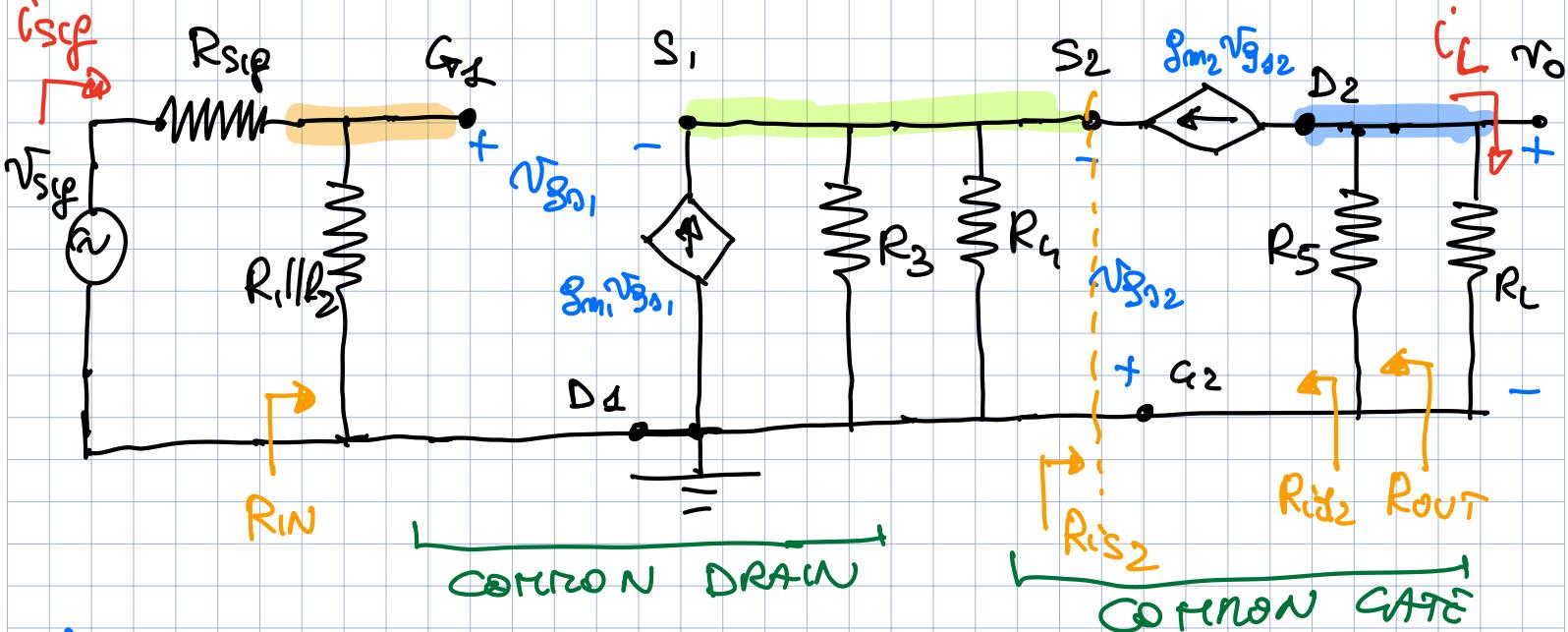
$$M_2: I_{D2} = 10,81 \text{ mA}, V_{DS2} = -8,18 \text{ V}, V_{GS2} = -4,09 \text{ V.}$$

ANALISI AL PICCOLO SEGNALE

$$\gamma_{m1} = \frac{2I_{D1}}{V_{GS1} - V_{TP1}} = \sqrt{2I_{D1}K_P} = 14,14 \text{ mS}; Z_{o1} = \infty$$

$$\gamma_{m2} = \frac{2I_{D2}}{V_{GS2} - V_{TP2}} = \sqrt{2I_{D2}K_P} = 10,45 \text{ mS}; Z_{o2} = \infty$$

SCHEMA AL PICCOLO SEGNALE



$$R_{IN} = R_1 \parallel R_2$$

$$R_{OUT} = R_6$$

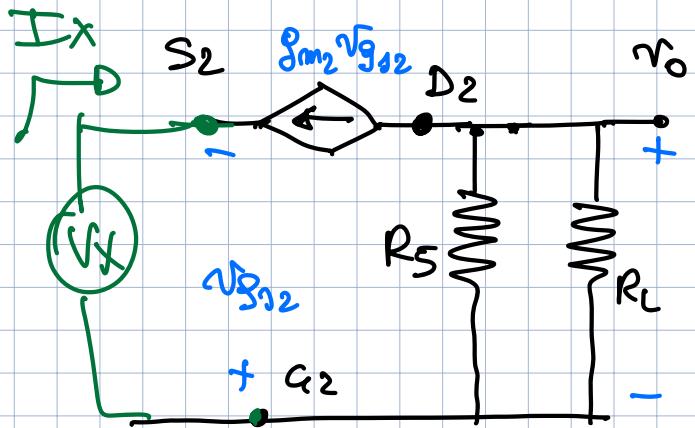
(in quanto $R_{id2} = \infty$ con 20∞)

$$R_{id2} = 1/\gamma_{m2}$$

$$I_X = -\gamma_{m2} \sqrt{\gamma_{s2}}$$

$$V_X = -\sqrt{\gamma_{s2}}$$

$$\frac{V_X}{I_X} = \frac{1}{\gamma_{m2}}$$



$$R_{L1} = R_3 // R_4 // R_{C2} = R_3 // R_4 // \frac{1}{g_m2} = 81,7 \text{ S}$$

$$R_{L2} = R_5 // R_L = 0,5 \text{ k}\Omega$$

$$\cdot A_V = \frac{V_o}{V_{sig}} = \frac{\sqrt{D2}}{\sqrt{S2}} \cdot \frac{\sqrt{S2}}{\sqrt{A_V}} \cdot \frac{\sqrt{C2}}{\sqrt{S1}} \\ = \underbrace{A_V}_{CG} \cdot \underbrace{A_V}_{CD} \cdot \alpha$$

$$\sqrt{S2} = \sqrt{S1}$$

$$\alpha = \frac{R_1 // R_2}{R_{sig} + R_1 // R_2} = 0,99$$

$$\underbrace{A_V}_{CD} = ? \quad \sqrt{S2} = g_m1 \sqrt{S1} R_{L1}$$

$$V_{C1} = \sqrt{S1} + g_{m1} \sqrt{S1} R_{C1}$$

$$\Rightarrow \underbrace{A_V}_{CD} = \frac{\sqrt{S2}}{\sqrt{S1}} = \frac{g_{m1} R_{L1}}{1 + g_{m1} R_{C1}} = 0,536$$

$$\underbrace{A_V}_{CG} = ? \quad \sqrt{D2} = - g_{m2} \sqrt{S2} R_{L2}$$

$$\sqrt{S2} = - V_{S2}$$

$$\Rightarrow \underbrace{A_V}_{CG} = \frac{\sqrt{D2}}{\sqrt{S2}} = g_{m2} R_{L2} = 5,223$$

$$\Rightarrow \boxed{A_v = \underbrace{A_V}_{CG} \cdot \underbrace{A_V}_{CD} \cdot \alpha = 2,77}$$

$$A_C = \frac{C_C}{C_{S\text{ig}}} = \frac{\frac{V_o}{R_L}}{\frac{V_{S\text{ig}}}{R_{S\text{ig}} + R_L/R_2}} = A_V \cdot \frac{R_{S\text{ig}} + R_L/R_2}{R_L} = 280$$

= 101

IN ALTERNATIVA:

$$C_C = -g_{m2} V_{GS2} \frac{R_S}{R_S + R_L}$$

$$V_{GS2} = -g_{m1} V_{GS1} \cdot R_{L1}$$

$$V_{GS1} = C_{S\text{ig}} \cdot R_L/R_2 - g_{m1} V_{GS1} R_{L1}$$

$$V_{GS1} (1 + g_{m1} R_{L1}) = C_{S\text{ig}} R_L/R_2$$

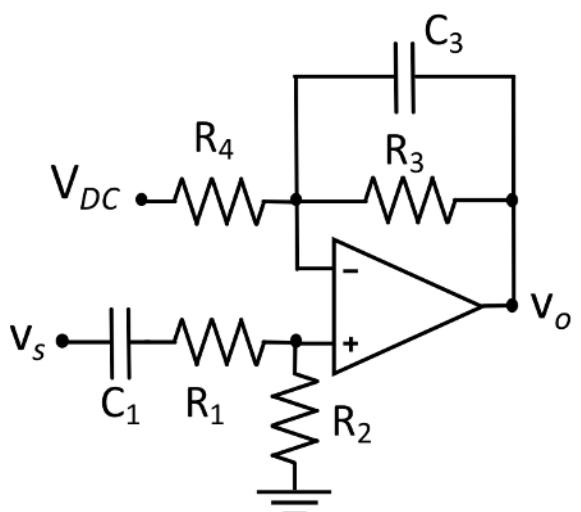
$$V_{GS1} = \frac{C_{S\text{ig}} R_L/R_2}{1 + g_{m1} R_{L1}}$$

$$\frac{C_C}{C_{S\text{ig}}} = R_L/R_2 \cdot \frac{g_{m1} R_{L1}}{1 + g_{m1} R_{L1}} \cdot g_{m2} \frac{R_S}{R_S + R_L} = 280$$

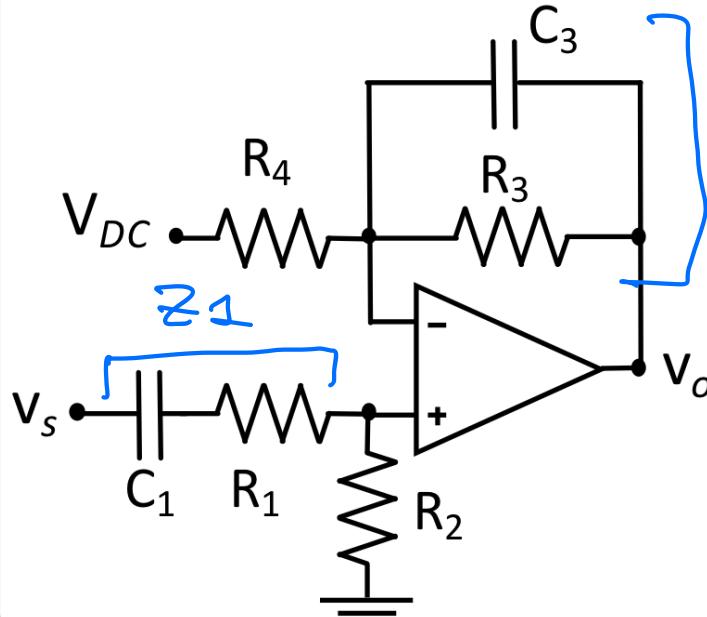
PROBLEMA P2

Sia dato il circuito in figura che usa un amplificatore operazionale ideale. Le resistenze hanno valore $R_1 = 99 \text{ k}\Omega$, $R_2 = 1 \text{ k}\Omega$, $R_3 = 990 \Omega$, $R_4 = 10 \Omega$. Le capacità valgono: $C_1 = 10 \mu\text{F}$, $C_3 = 101 \text{nF}$, $V_{DC} = 2 \text{ V}$.

- 1) ricavare l'espressione della funzione di trasferimento $W(s) = v_o(s)/v_{in}(s)$;
- 2) tracciare il diagramma di Bode asintotico dell'ampiezza e della fase di W , (per la fase non usare l'approssimazione a gradino).
- 3) Calcolare $v_o(t)$ sapendo che $v_s = 4 \text{ V} + 5 \text{ V} \cdot \sin(\omega_0 t)$ con $\omega_0 = 10^4 \text{ rad/s}$.



$$1) \quad W(s) = \frac{V_o}{V_s} \quad (\text{non si considerare } V_{DC} !)$$



$$z_1 = R_1 + \frac{1}{SC_1}$$

$$= \frac{1 + SC_1 R_1}{SC_1}$$

$$z_3 = \frac{R_3 \cdot \frac{1}{SC_3}}{R_3 + \frac{1}{SC_3}} = \frac{R_3}{1 + SC_3 R_3}$$

$$V_f = V_s \cdot \frac{R_2}{R_2 + z_1} = \frac{R_2}{R_2 + \frac{1 + SC_1 R_1}{SC_1}} V_s$$

$$= \frac{SC_1 R_2}{1 + SC_1 (R_1 + R_2)} V_s$$

$$N_0 = V_f \left(1 + \frac{z_3}{R_u} \right) = V_f \left(\frac{R_u + z_3}{R_u} \right)$$

$$R_u + \frac{\frac{R_3}{1 + SC_3 R_3}}{R_u} V_f$$

$$= \frac{R_u + SC_3 R_3 R_u + R_3}{R_u (1 + SC_3 R_3)} V_f = \frac{R_3 + R_u}{R_u} \cdot \frac{1 + SC_3 R_3 / R_u}{1 + SC_3 R_3} V_f$$

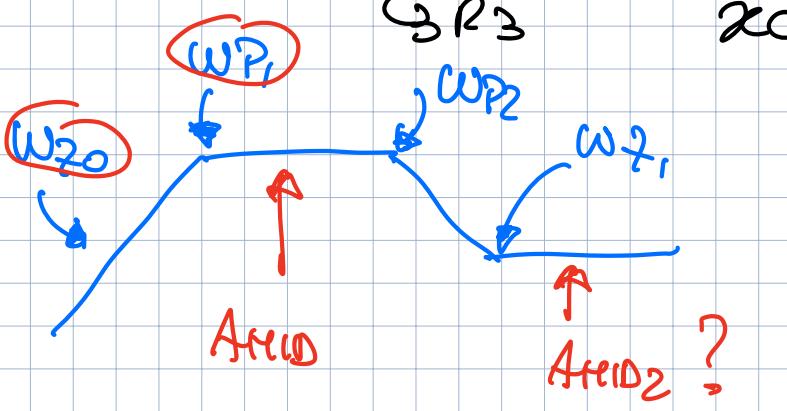
$$\Rightarrow W(s) = \frac{V_o}{V_s} = \frac{R_3 + R_4}{R_4} \cdot \frac{sC_1 R_2}{1 + sC_1(R_1 + R_2)} \cdot \frac{1 + sC_3 R_3 // R_4}{1 + sC_3 R_3}$$

$$W_{Z_0} = \frac{1}{C_1 R_2} = 10^2 \text{ rad/sec} \quad WP_1 = \frac{1}{C_1(R_1 + R_2)} = 1 \frac{\text{rad}}{\text{sec}}$$

$$W_{Z_1} = \frac{1}{C_3 R_3 // R_4} = 10^6 \text{ rad/sec} \quad WP_2 = \frac{1}{C_3 R_3} = 10^4 \frac{\text{rad}}{\text{sec}}$$

$$\frac{R_3 + R_4}{R_4} = 100 = 40 \text{ dB}$$

NON è $\omega(0)$
NON è A_{mid}

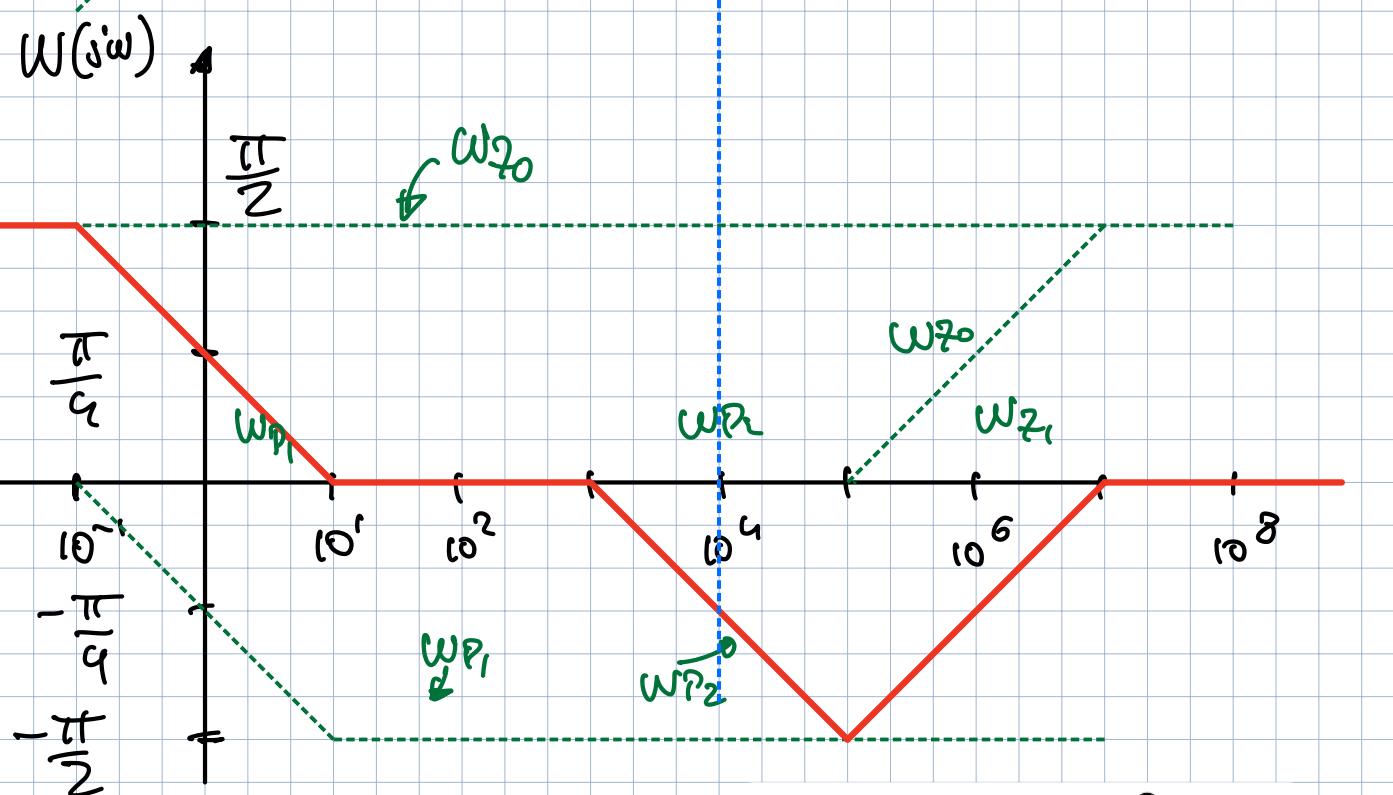
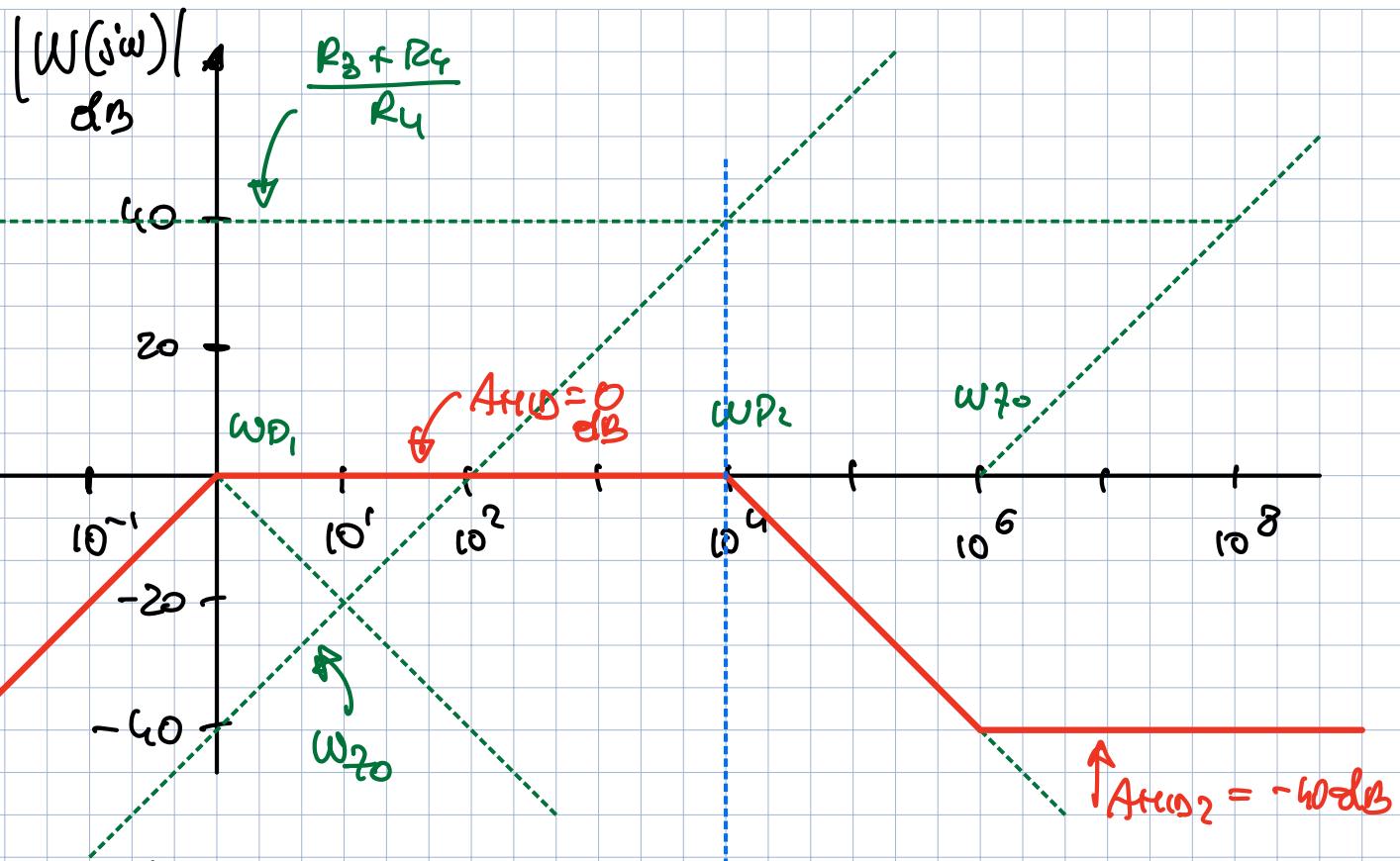


PER A mid "RACCOLGO" $W_{Z_0} \in WP_1 \in L_C$
SCURO COGLI $(S + \omega)$ INVECE DI $1 + \frac{S}{\omega}$

$$W(s) = \frac{R_3 + R_4}{R_4} \cdot \frac{R_2}{R_1 + R_2} \cdot \frac{\frac{s}{1 + sC_1(R_1 + R_2)}}{C_1(R_1 + R_2)} \cdot \frac{1 + sC_3 R_3 // R_4}{1 + sC_3 R_3}$$

$$A_{mid} = 1 = 0 \text{ dB}$$

$$A_{mid2} = \frac{R_3 + R_4}{R_4} \cdot \frac{R_2}{R_1 + R_2} \cdot \frac{R_3 // R_4}{R_3} = \frac{R_2}{R_1 + R_2} = 0,01 \\ = -40 \text{ dB}$$

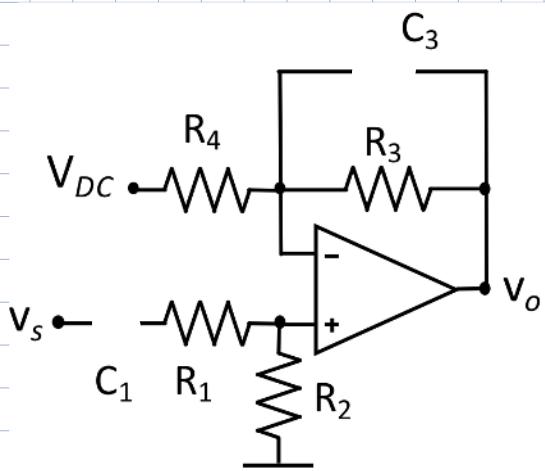


PARCOLO delle ω_0

Considero ora la V_{DC} !

In continua i "C"

Sono circuiti aperti



V_S viene ANNULLATO (SOVRAPP. EFFETTI)

Comunque il FATTO che C_1 è "OPEN" V_S non avrebbe avuto nessun effetto!

$\bar{V}_f = \text{MASSA}$ (NON CIRCOLA CORRENTE
su $R_1 > R_2$)

$$V_0 = V_{DC} \left(-\frac{R_3}{R_1} \right) = -99V_{DC} = -99V = V_{DC}$$

per $\omega_0 = 10 \text{ rad/sec}$

$$|W(j\omega_0)| = 0 \text{ dB} = 1$$

(VISTO CHE SONO NELLO SPETTRORESONO
POSso DIRE $|A(j\omega_0)| = \frac{1}{\sqrt{2}} = 0,707$)

$$\underline{W(j\omega_0)} = -\frac{\pi}{4}$$

$W(0) = 0$ NOTA BENE, C'È
ZERO NELL'ORIGINE!

$$\bar{V}_S = 2V + 5V \sin(\omega_0 t)$$

$$\underline{V_0} = V_{DC} + 2V \cdot W(0) + 5V \cdot |W(j\omega_0)| \sin \left(\omega_0 t + \underline{W(j\omega_0)} \right)$$

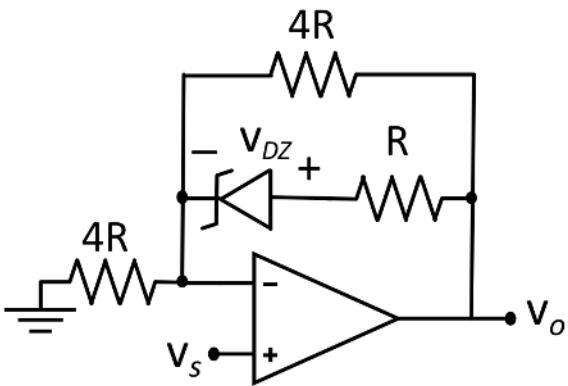
$$= -99V + 5V \sin \left(\omega_0 t - \frac{\pi}{4} \right)$$

$$\text{OPPUA } \frac{5V}{\sqrt{2}} = 3,535V$$

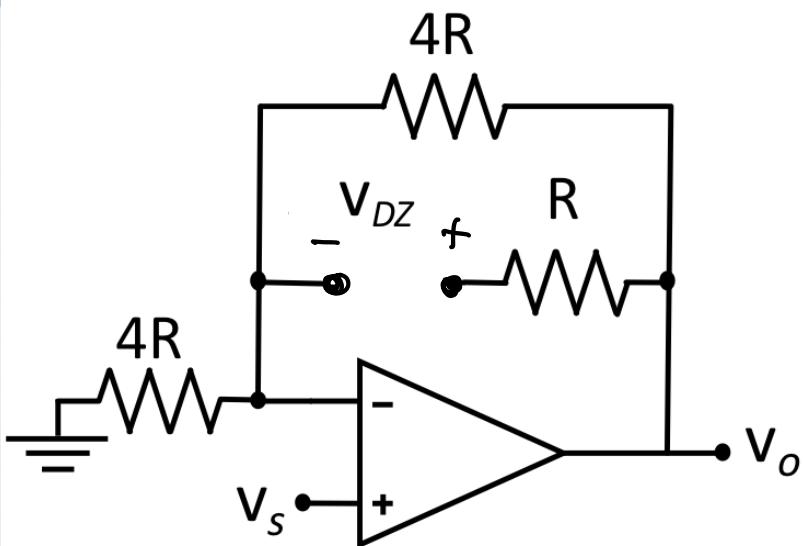
PROBLEMA Q1

L'amplificatore in figura è realizzato con un amplificatore operazionale ideale e un diodo Zener ideale.

- 1) Determinare i valori della tensione di ingresso per la quale il diodo è ON, OFF e in Breakdown.
- 2) Determinare v_o quando $v_s = +5$ V.
- 3) (facoltativo) tracciare la transcaratteristica del circuito.



Dati: $R_1 = 1 \text{ k}\Omega$, $V_{ON} = 0$, $V_Z = 5\text{V}$



HP D_Z = OFF

$$v_o = v_s \left(1 + \frac{4R}{4R}\right)$$

$$= 2v_s$$

$$\bar{v}_{DZ} = v_o - v_s$$

$$= 2v_s - v_s$$

$$= +v_s$$

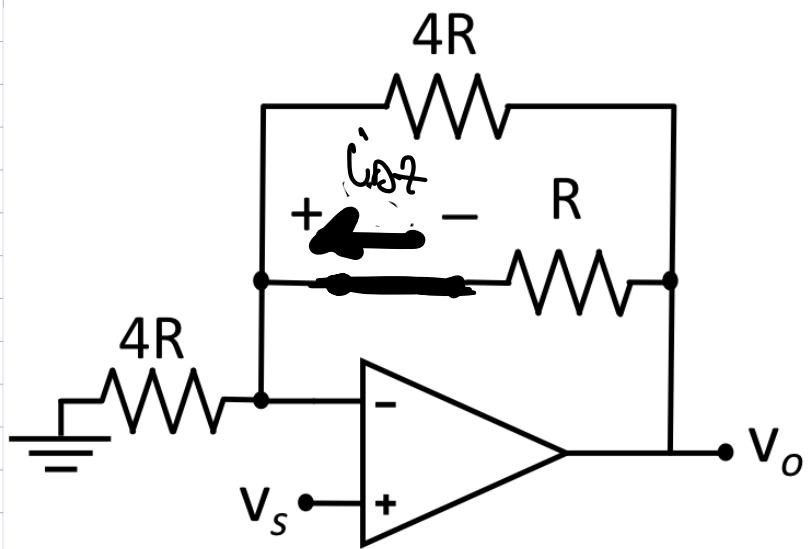
DIODO ON $v_{DZ} > 0 \Rightarrow v_s > 0$

DIODO BREAK. $v_{DZ} < -V_Z$ $v_s < -V_Z$

DIODO OFF $-V_Z \leq v_{DZ} \leq 0$ $v_{o2} \leq v_s \leq 0$



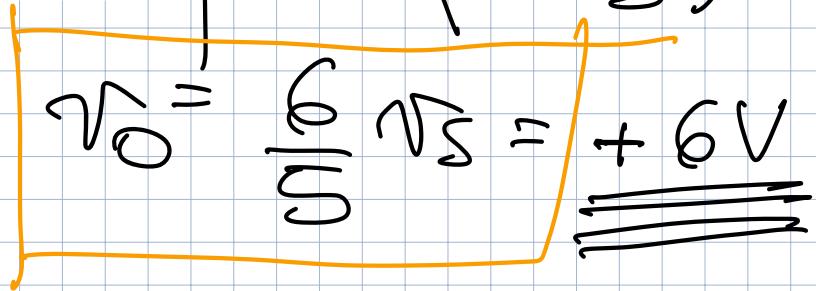
2) Con $v_s = +5V \Rightarrow D2 = "ON"$



$$4R//R = \frac{4R^2}{5R} = \frac{4}{5}R$$

$$v_o = v_s \left(1 + \frac{\frac{4}{5}R}{4R} \right)$$

$$= 2v_s \left(1 + \frac{1}{5} \right)$$



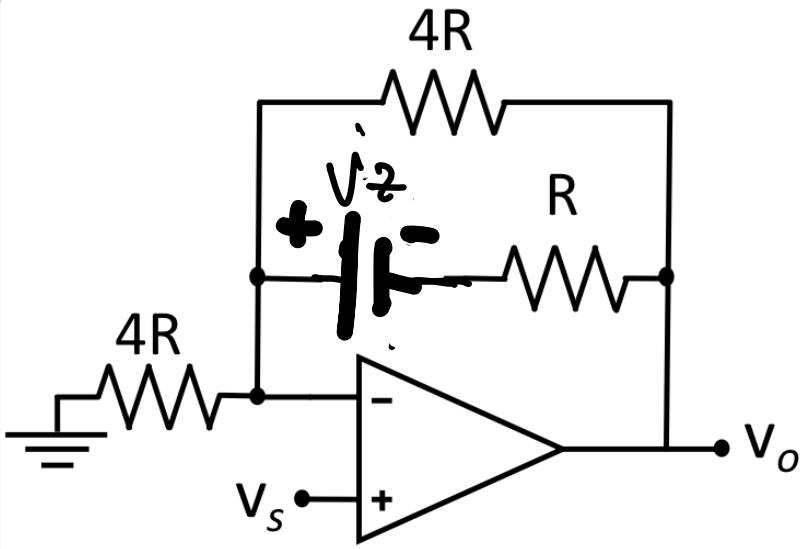
FACOLTATIVO

HO già calcolato:

a) Diodo OFF $v_o = 2v_s \quad -5V \leq v_s \leq 0V$

b) Diodo ON $v_o = \frac{6}{5} v_s = 1,2v_s \quad v_s > 0V$

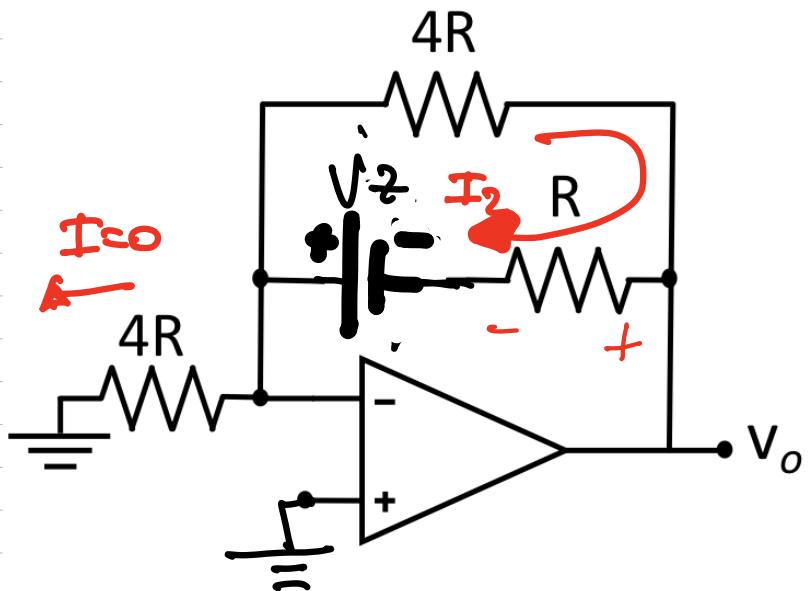
c) Diodo BREAKDOWN $v_s < -5V$



CONVIENE USARE
SOURAPP. EFFETTI

i) Con $V_S = 0$ e $V_2 = 0$
HO LA CONDIZIONE
DIODO "ON"
 $\Rightarrow V_o = \frac{6}{5} V_S$

2) Con $V_S = 0$ e V_2 ATTIVO



$$I_2 = \frac{V_2}{R+4R} = \frac{5V}{5R} = 1mA$$

$$\begin{aligned} V_o'' &= -V_2 + I_2 R \\ &= -V_2 + \frac{V_2}{5} \\ &= -\frac{4}{5} V_2 = -4V \end{aligned}$$

CON DIODO BREAK:

$$\Rightarrow V_o = \frac{6}{5} V_S - 4V$$

RACCORDI:

$V_S = 0$

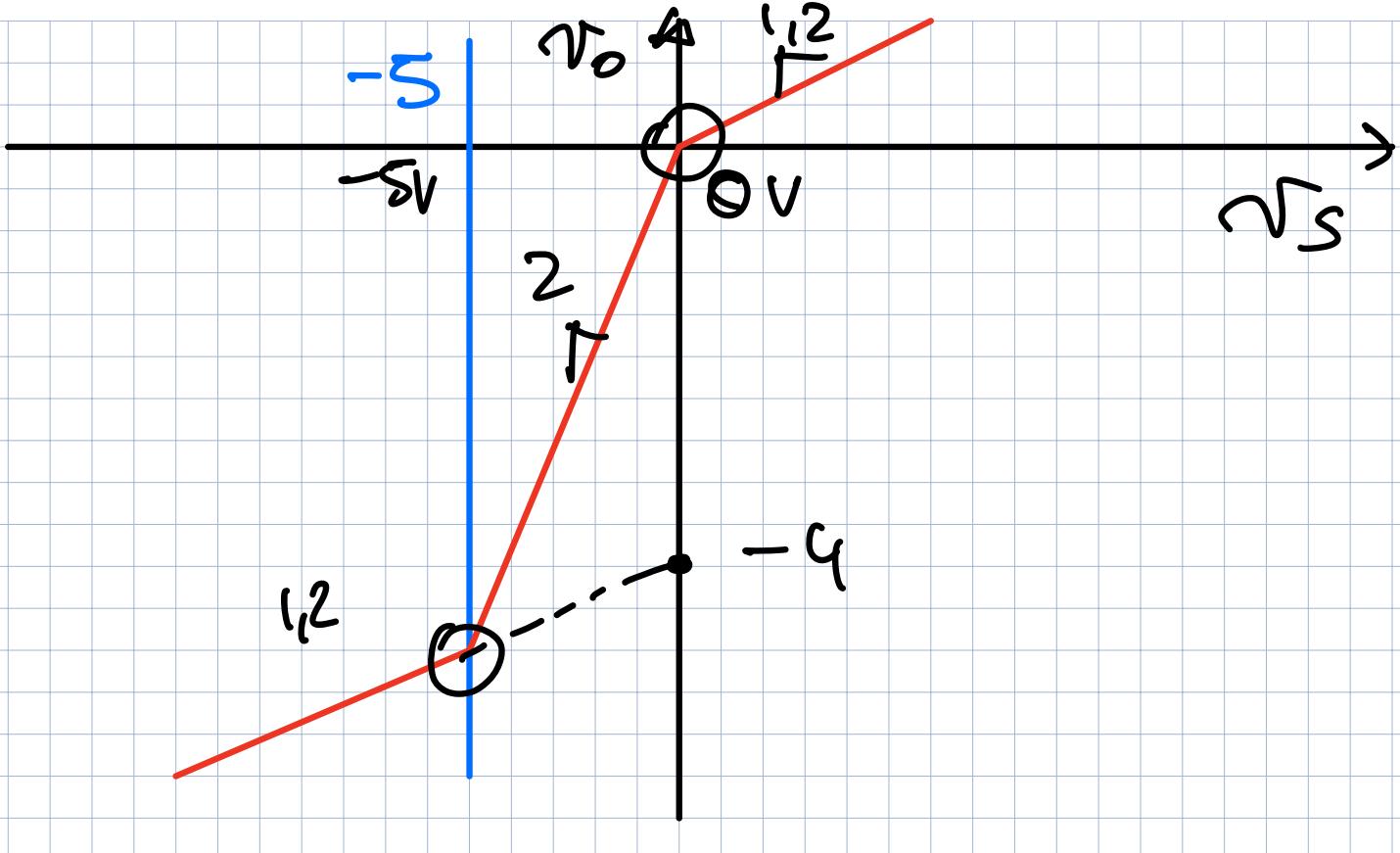
$$2V_S = 0$$

$$\frac{6}{5} V_S = 0$$

OK |

|

$$\begin{aligned} V_2 &= 2V_S = -10V \\ V_o &= \frac{6}{5} V_S - 4V = -10V \end{aligned}$$

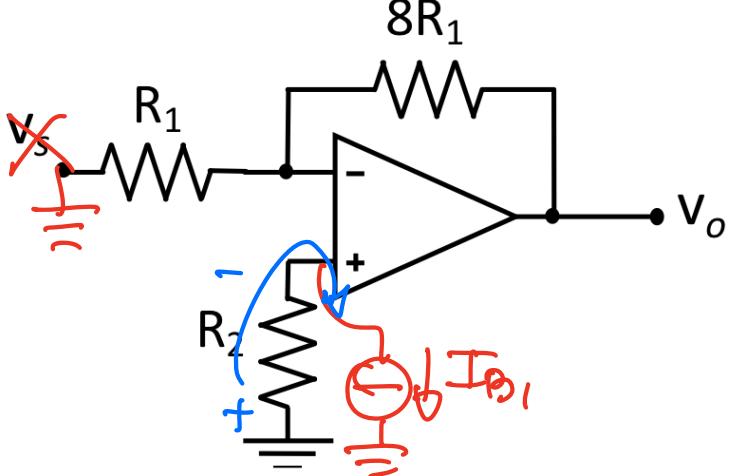
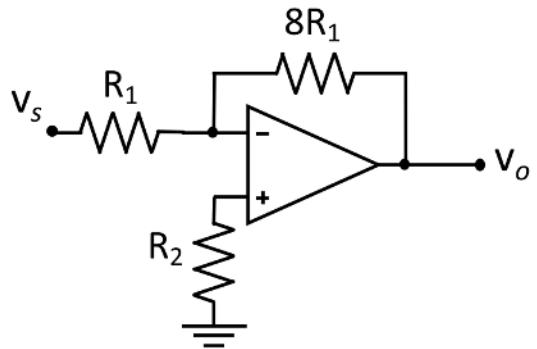


PROBLEMA Q2

Il circuito di figura impiega un AO quasi ideale con correnti di polarizzazione pari a $I_{B1}=100\text{nA}$ (morsetto non invertente), $I_{B2}=60\text{nA}$ (morsetto invertente).

- 1) Calcolare v_o considerando l'effetto delle sole correnti di polarizzazione ($v_s=0$). Trovare il valore di R_2 che annulla l'effetto delle correnti di BIAS.
- 2) Calcolare il valore di v_o considerando la sola tensione $v_s=+3\text{ V}$ sapendo che l'AO è alimentato con $\pm V_{cc}$ e determinare il valore della tensione del morsetto invertente, v_- .

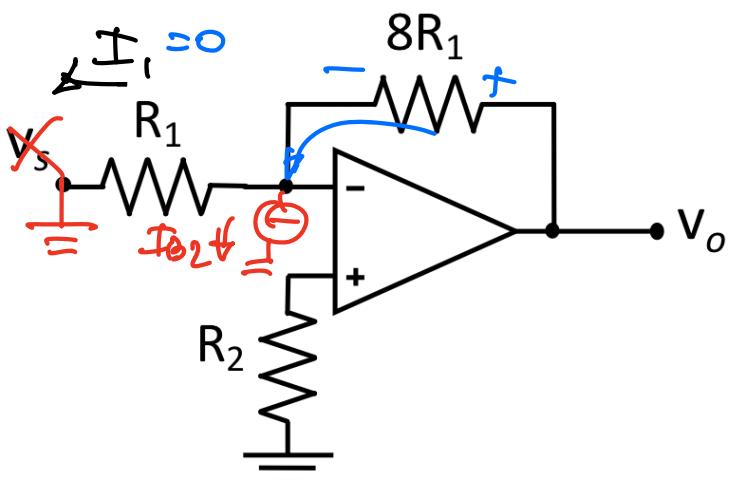
Dati: $R_1 = 1\text{k}\Omega$, $R_2 = 1\text{k}\Omega$, $v_s = +2\text{ V}$, $V_{cc} = 15\text{V}$.



EFFETTO DI I_{B1}

$$V_f = -I_{B1}R_2$$

$$\begin{aligned} V_o^1 &= V_f \left(1 + \frac{8R_1}{R_1} \right) \\ &= -9I_{B1}R_2 = 0,9\text{mV} \end{aligned}$$



$$V_0'' = 8R_1 I_{B2} = 0,48 \text{ mV}$$

$$\Rightarrow V_0 = V_0' + V_0'' = -0,42 \frac{\text{mV}}{\text{mV}}$$

X ANNULLARE EFFETTO $I_{B1,2}$:

$$8R_1 I_{B2} - 8I_{B1} R_2 = 0 \Rightarrow R_{2\text{new}} = \frac{8}{8} \frac{I_{B2}}{I_{B1}} R_1 = 533,3 \Omega$$

2) Con $V_s = 3 \text{ V}$

$$V_0 = V_s \left(-\frac{8R_1}{R_1} \right) = -8V_s = -24 \text{ V}$$

VISTO CHE AO È ACCRESCENDO A $\pm 15 \text{ V}$

$\Rightarrow V_0$ SATURA A $-\pm 15 \text{ V}$

$$\Rightarrow V_0 = -15 \text{ V}$$

Quando AO. SATURA $\Rightarrow V_0$ NON È PIÙ

TRASCRIBILE e
NON VALE PIÙ LA TASSA
VIRTALE

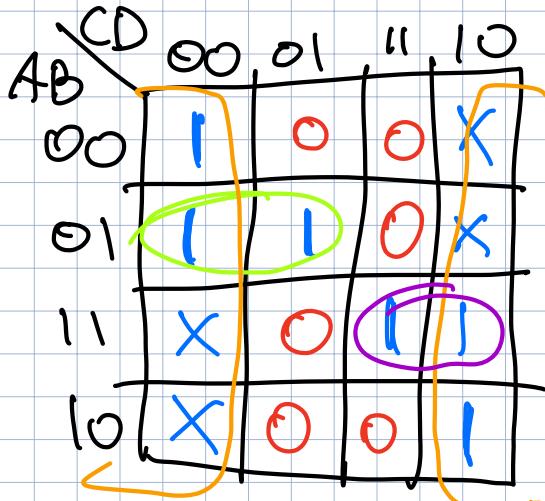
$$V_- = V_s \cdot \frac{8R_1}{R_1 + 8R_1} - V_A \cdot \frac{R_1}{R_1 + 8R_1} = 1 \text{ V}$$

PROBLEMA Q3

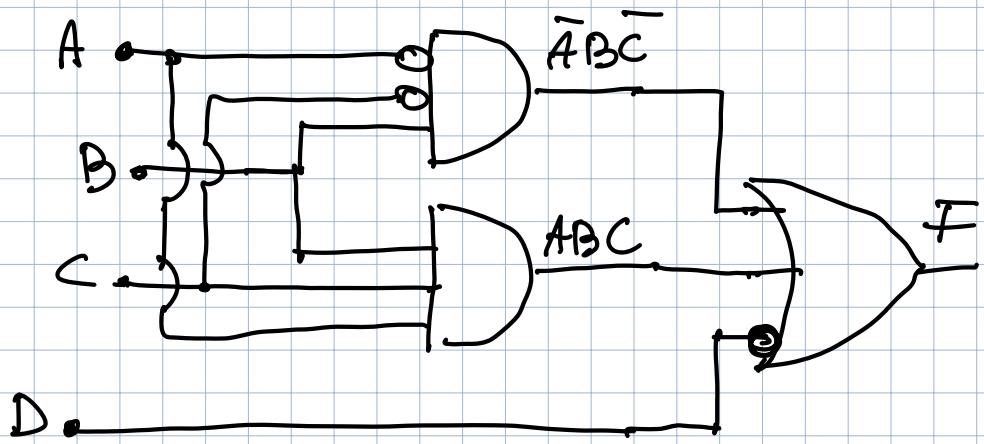
Data la seguente mappa di Karnaugh

- 1) Trovare una F minimizzata
- 2) Disegnare la rete logica minimizzata tramite porte logiche fondamentali.

CD \ AB	00	01	11	10
00	1	0	0	X
01	1	1	0	X
11	X	0	1	1
10	X	0	0	1



$$F = \bar{D} + \bar{A}\bar{B}\bar{C} + A\bar{B}C$$



$$F' = \bar{D} + B(\bar{A}\bar{C} + AC)$$

N.B. $\bar{A}\bar{C} \neq \bar{AC}$
 $(\bar{AC} + AC = 1)$

