

Design of a reservoir hydropower scheme

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Task 1: Determine the design of a gravity dam, height H to satisfy safety factors against sliding and overturning.

Finding measurement

Stability analysis

Load Combination

Checking safety factors

Annex: calculation code

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Finding measurement

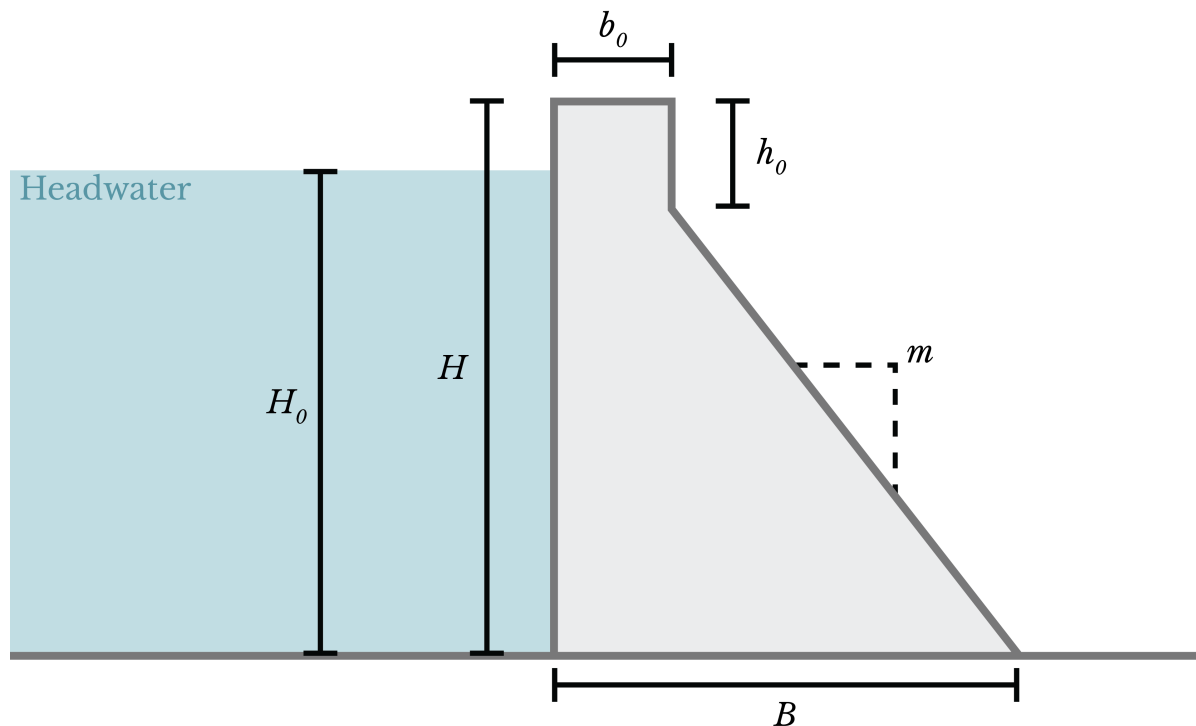


Figure 1 : Introduction to notations for the gravity dam measurements

According to the Bureau of Reclamation of the USA department of the interior "Design of gravity dams" paper we can calculate the missing dimensions according to the current standards.

$$m = \frac{B}{H} = \frac{b_0}{h_0} \simeq 0,8$$
$$b_0 = \frac{H}{10} \geq 8m$$

We can therefore calculate :

- $B = m \cdot H = 0,8 \times 71 = 56,8m$
- $b_0 = \frac{H}{10} = \frac{71}{10} = 7,1m \leq 8$, so we choose $b_0 = 8m$
- $h_0 = \frac{b_0}{m} = \frac{8}{8,0} = 10m$

Stability analysis

Now we have to figure out the weakpoints and the critical failure modes. We can identify three of them:

- **Sliding** : too much pressure causes the dam to move in the horizontal plane. The following safety factor is then considered: $n_{SL} = \frac{\sum V}{\sum H}$. Where $\sum V$ represent the sum of the vertical efforts and $\sum H$ for the horizontal ones. To meet the safety requirements $n_{SL} > 3$ for the usual load case.
- **Overturning** : the dam rotates around a fixed point. In our case and as shown in the diagram the lower end on the right. The safety factor is described as, $n_{OV} = \frac{M_{stab}}{M_{dest}} > 2$.
- **Crushing** : in this case we are looking at compression and tension failure.

Load Combination

For this example we have chosen to consider the usual load case. It is then a question of determining the set of forces wich have a reasonable probability of simultaneous occurrence. The calculations could have been made in an even less favourable scenario (unusual or extreme flood case, dynamic cases by considering waves, wind, earthquakes). The problem will be solved with the following assumptions :

- The reservoir is at his operational level (H_0),
- we are considering the dead load of the dam,
- the uplift pressure is at his full drainage capacity,
- there is a presence of silt that affect the dam.

We can report on the following efforts :

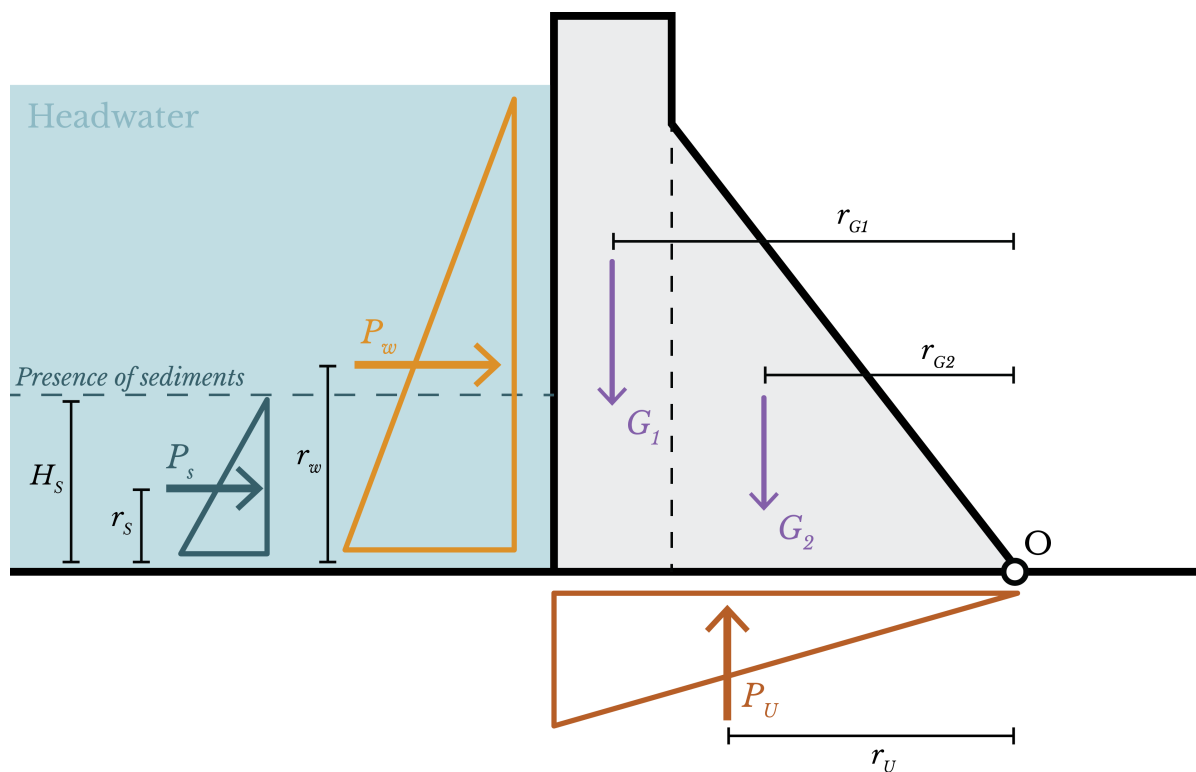


Figure 2 : Efforts on the dam

Where :

- G_1 and G_2 represent the **dead load** of the dam. The following formulas describing the effort are then considered :
 - $\gamma_{conc} = 24 \text{ kN/m}^3$
 - $G_1 = b_0 \cdot H \cdot \gamma_{conc} \cdot e = 13632 \text{ kN}$
where e is the thickness of the study section ($e = 1 \text{ m}$), so we won't consider it in the next equations
 - $G_2 = \frac{1}{2}(B - b_0)(H - H_0)\gamma_{conc} = 35721 \text{ kN}$
 - $r_{G1} = B - \frac{b_0}{2} = 52,8 \text{ m}$
 - $r_{G2} = \frac{2}{3}(B - b_0) = 32,5 \text{ m}$
- P_w the **hydrostatic pressure** on the dam :
 - $\gamma_w = 10 \text{ kN/m}^3$
 - $P_w = \gamma_w \cdot \frac{H_0^2}{2} = 21125 \text{ kN}$
 - $r_w = \frac{1}{3} \cdot H_0 = 21,7 \text{ m}$
- P_u the **uplift pressure** on the dam :
 - To reduce the effect of uplift, draingaes to the ground are installed in the dam. This reduction is associated with the coefficient $\lambda = 0,85$
 - $P_u = \lambda \cdot H_0 \cdot \gamma_w \cdot \frac{B}{2} = 15691 \text{ kN}$
 - $r_u = \frac{2}{3} \cdot B = 37,8 \text{ m}$
- P_s the **silt pressure** on the dam :
 - $\gamma_s = 18 \text{ kN/m}^3$
 - $H_s = \frac{H_0}{3} = 21,6 \text{ m}$
 - $P_s = \gamma_s \cdot \frac{H_s^2}{2} = 4225 \text{ kN}$
 - $r_s = \frac{H_s}{3} = 7,2 \text{ m}$

Checking safety factors

We can therefore calculate our safety factors.

$$n_{SL} = \frac{G_1 + G_2 - P_u}{P_w - P_s} = 1,99$$

$$n_{OV} = \frac{G_1 \cdot r_{G1} + G_2 \cdot r_{G2}}{P_w \cdot r_w + P_s \cdot r_s + P_u \cdot r_u} = 1,74$$

We can now conclude that the current design of the dam **does not satisfy the safety criteria** because $n_{SL} < 3$ and $n_{OV} < 2$.

Annex: calculation code

```

"Finding measurement"
H=71
m=0.8
B=m*H
b0=H/10
if b0<=8:
    b0=8
h0=b0/m
"Load combination"
#dead load
gconc=24
H0=H-6
G1=b0*H*gconc
G2=0.5*(B-b0)*(H-h0)*gconc
rG1=B-(b0/2)

```

```
rG2=(2/3)*(B-b0)
#hydrostatic pressure
gw=10
Pw=gw*0.5*H0*H0
rw=(1/3)*H0
#uplift pressure
lamb=0.85
Pu=lamb*H0*gw*B/2
ru=(2/3)*B
#silt pressure
gs=18
Hs=H0/3
Ps=gs*0.5*Hs*Hs
rs=Hs/3
"security factors check"
nsl=(G1+G2-Pu)/(Pw-Ps)
nov=(G1*rG1+G2*rG2)/(Pw*rw+Ps*rs+Pu*ru)
```