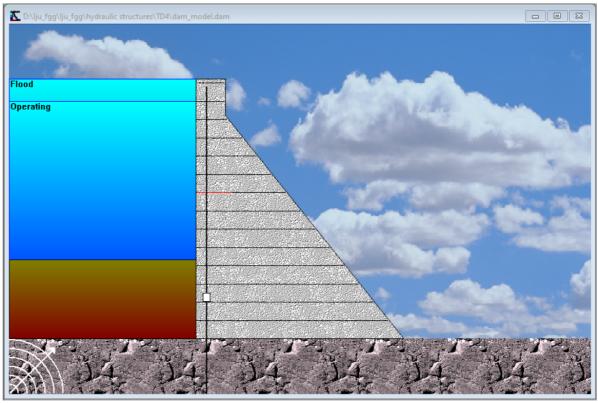
Model in CADAM

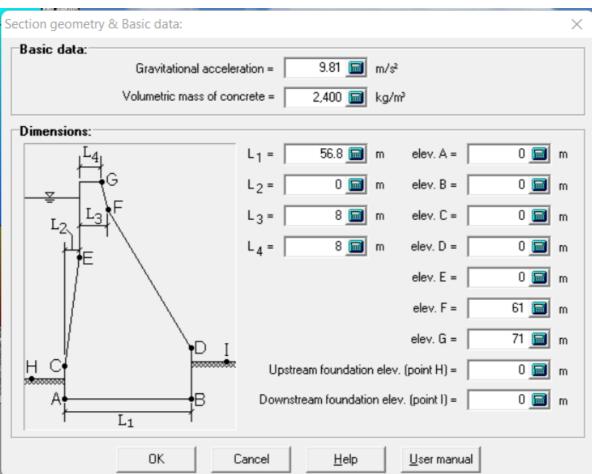
Arthur Guillot - Le Goff Autumn semester 2021-2022 | Hydroelectric power

Model in CADAM

Our model Model results

Our model





Model results

Date:

By Martin Leclerc, M. Ing.

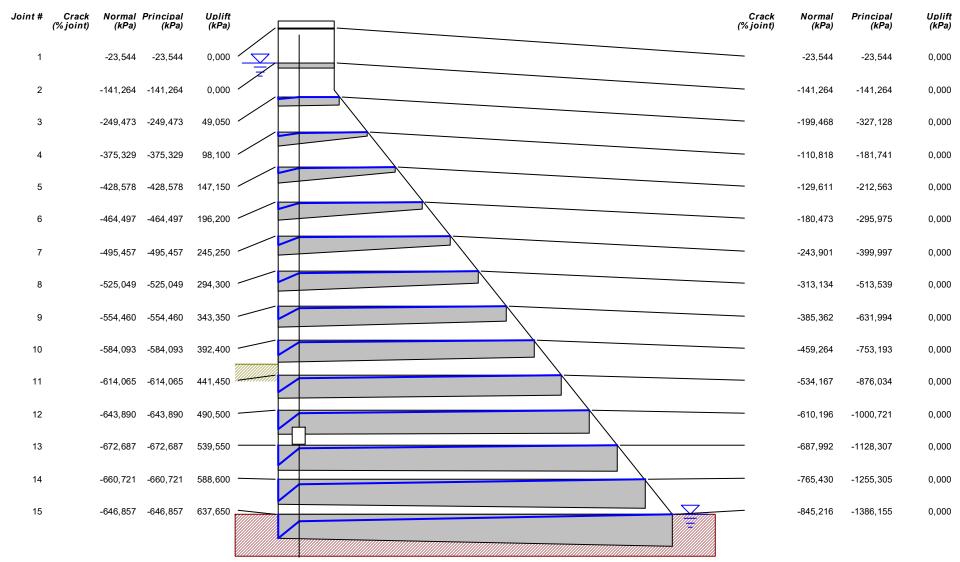
NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

Project: TD4 Dam location: FGG Analysis performed by:

30/11/2021

Dam: Owner: Example 1

Usual combination (effective stress analysis)



Arthur Guillot - Le Goff

Project engineer:

By Martin Leclerc, M. Ing.

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Dam location: FGG Analysis performed by: Project: Example 1 30/11/2021 Project engineer: Dam: Date: Arthur Guillot - Le Goff

Owner:

| Owner: | | | | | | | | | | |
|--|---------|---------------|-------------------|-----------------|-----------------|--------|----------------|---------------|----------|------------------------|
| Usual combination (stability analysis) | | | | | | | | | | |
| | Joint # | SSF (peak) | SSF (residual) | OSF (U/S <-) | OSF (-> D/S) | USF | Normal (kN) | Shear (kN) | | Res. Pos. (% joint) |
| | 1 | > 100 | > 100 | > 100 | > 100 | > 100 | -188,4 | 0,0 | 0,0 | 50,000 |
| | 2 | > 100 | > 100 | > 100 | > 100 | > 100 | -1130,1 | 0,0 | 0,0 | 50,000 |
| | 3 | 28,747 | 23,006 | 42,655 | 10,633 | 19,644 | -1975,3 | 122,6 | -322,7 | 48,144 |
| | 4 | 11,147 | 9,059 | 26,346 | 6,765 | 13,893 | -3111,3 | 490,5 | -3611,5 | 40,932 |
| | 5 | 7,285 | 6,068 | 23,399 | 5,260 | 12,545 | -4688,8 | 1103,6 | -7031,7 | 41,073 |
| | 6 | 5,731 | 4,883 | 22,862 | 4,502 | 12,173 | -6707,7 | 1962,0 | -10240,0 | 42,661 |
| | 7 | 4,918 | 4,271 | 22,935 | 4,058 | 12,126 | -9168,0 | 3065,6 | -12893,1 | 44,329 |
| | 8 | 4,427 | 3,905 | 23,168 | 3,772 | 12,205 | -12069,8 | 4414,5 | -14647,6 | 45,786 |
| | 9 | 4,100 | 3,663 | 23,428 | 3,574 | 12,336 | -15413,1 | 6008,6 | -15160,1 | 47,001 |
| | 10 | 3,869 | 3,494 | 23,676 | 3,429 | 12,485 | -19197,8 | 7848,0 | -14087,4 | 48,006 |
| | 11 | 3,695 | 3,366 | 23,898 | 3,320 | 12,636 | -23423,9 | 9937,4 | -11083,4 | 48,840 |
| | 12 | 3,541 | 3,250 | 24,101 | 3,233 | 12,784 | -28091,5 | 12343,0 | -5635,5 | 49,552 |
| | 13 | 3,402 | 3,143 | 24,294 | 3,158 | 12,925 | -33200,6 | 15086,2 | 3037,4 | 50,187 |
| | 14 | 3,192 | 2,960 | 16,736 | 2,868 | 9,727 | -37650,4 | 18167,1 | 24326,0 | 51,224 |
| | 15 _ | 3,014 | 2,804 | 13,284 | 2,652 | 8,015 | -42374,9 | 21585,6 | 53329,6 | 52,216 |
| | | 3,000 | 1,500 | 2,000 | 2,000 | 1,200 | | | | |

Date:

By Martin Leclerc, M. Ing.

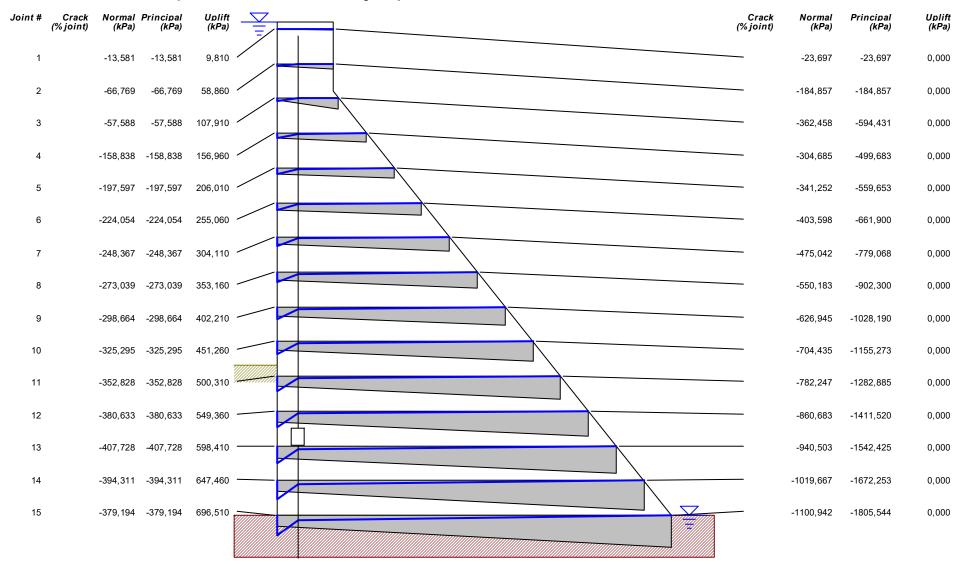
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Project: TD4 Dam location: FGG Analysis performed by:

30/11/2021

Dam: Owner: Example 1

Flood combination (effective stress analysis)



Arthur Guillot - Le Goff

Project engineer:

By Martin Leclerc, M. Ing.

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Dam location: FGG Analysis performed by: Project: Example 1 30/11/2021 Project engineer: Dam: Date: Arthur Guillot - Le Goff

Owner:

| lood combination (stability analysis) | | | | | | | | | | |
|---------------------------------------|---------|---------------|-------------------|-----------------|-----------------|--------|----------------|---------------|------------------|------------------------|
| | Joint # | SSF (peak) | SSF (residual) | OSF (U/S <-) | OSF (-> D/S) | USF | Normal (kN) | Shear (kN) | Moment (kN·m) | Res. Pos. (% joint) |
| | 1 | > 100 | 43,416 | 7,216 | 3,572 | 4,800 | -149,1 | 4,9 | 54,0 | 54,523 |
| | 2 | 11,765 | 8,140 | 22,378 | 4,021 | 9,143 | -1006,5 | 176,6 | 629,8 | 57,822 |
| | 3 | 5,633 | 4,447 | 23,850 | 2,629 | 8,929 | -1848,2 | 593,5 | 1967,4 | 62,097 |
| | 4 | 4,189 | 3,374 | 21,385 | 2,602 | 8,683 | -2966,5 | 1255,7 | 1991,3 | 55,24 |
| | 5 | 3,610 | 2,988 | 21,473 | 2,528 | 8,961 | -4526,3 | 2163,1 | 3378,8 | 54,443 |
| | 6 | 3,313 | 2,812 | 22,010 | 2,482 | 9,363 | -6527,6 | 3315,8 | 6473,2 | 54,768 |
| | 7 | 3,139 | 2,718 | 22,561 | 2,457 | 9,779 | -8970,3 | 4713,7 | 11617,9 | 55,22 |
| | 8 | 3,026 | 2,663 | 23,036 | 2,445 | 10,171 | -11854,4 | 6356,9 | 19156,2 | 55,61 |
| | 9 | 2,948 | 2,629 | 23,431 | 2,439 | 10,531 | -15180,0 | 8245,3 | 29431,5 | 55,91 |
| | 10 | 2,891 | 2,607 | 23,756 | 2,438 | 10,856 | -18947,0 | 10379,0 | 42787,2 | 56,13 |
| | 11 | 2,847 | 2,591 | 24,025 | 2,439 | 11,150 | -23155,5 | 12762,6 | 59569,0 | 56,30 |
| | 12 | 2,800 | 2,568 | 24,256 | 2,440 | 11,414 | -27805,5 | 15462,6 | 80290,0 | 56,44 |
| | 13 | 2,751 | 2,540 | 24,464 | 2,440 | 11,654 | -32896,9 | 18500,1 | 105731,0 | 56,58 |
| | 14 | 2,630 | 2,437 | 17,356 | 2,296 | 9,052 | -37329,0 | 21875,3 | 145282,6 | 57,37 |
| | 15 | 2,524 | 2,346 | 13,923 | 2,181 | 7,589 | -42035,8 | 25588,1 | 194044,3 | 58,12 |
| | _ | 2,000 | 1,300 | 1,100 | 1,100 | 1,100 | | | | |

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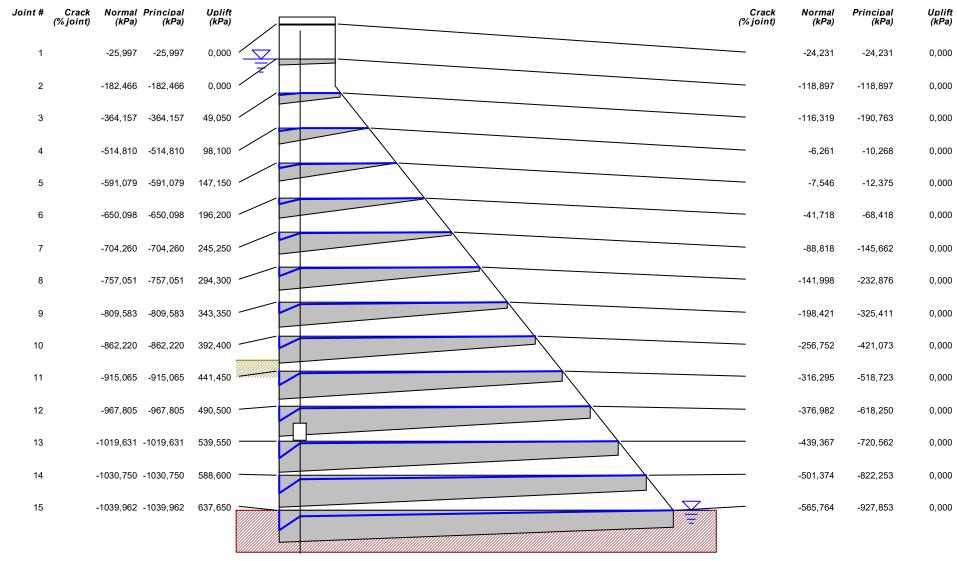
NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismic #1 combination - Peak accelerations (stress analysis) (effective stress analysis)



By Martin Leclerc, M. Ing.

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Project: Dam location: FGG Analysis performed by: 30/11/2021 Dam: Example 1 Date: Project engineer: Arthur Guillot - Le Goff

Owner:

Seismic, #1 combination - Peak accelerations (stress analysis) (stability analysis) Joint # SSF SSF (peak) (residual) USF Normal Moment Res. Pos. (U/S <-) (-> D/S) (kN) (kN) (kN·m) (% joint) 49,213 15,234 85,333 > 100 > 100 -200,9 -18,8 -9.4 49,414 46,484 20,897 15,234 14,222 > 100 > 100 -1205,5-113,0 -339,0 23.934 41,403 29.514 6.406 12,649 20.954 -2114.1 -126,2-1599.495,548 5,039 7,932 14,819 -3334,949,8 -6943,4 33,734 20.591 17.345 4,977 6,136 13,381 -5028.5 414,0 -13724,7 33,754 10,578 12,291 5,189 5,235 12,984 -7194,9 971,4 -21934,1 35,343 9,292 8,142 5,452 4,708 12,934 -9834,2 1725,0 -31543,4 37,066 7,769 6,908 5,708 4,367 13,019 -12946,3 2676,6 -42512,5 38,598 6,853 6,168 5,943 4,131 13,158 -16531,3 3827,7 -54792,6 39,895 10 6,245 5,677 6,155 3,957 13,317 -20589,1 5179,6 -68329,1 40,982 5,812 3,826 13,479 -25119,7 -83061,4 41,896 11 5,327 6,346 6734,4 12 5,454 5,035 6,516 3,720 13,636 -30123,2 8544,5 -98817,1 42,678 13 5,144 4,777 6,669 3,631 13,787 -35599,6 10642,6 -115155,4 43,371 14 4,756 4,432 6,063 3,294 10,375 -40448,1 13032,8 -122984,7 44,241 4,433 4,144 5,639 3,044 8,549 -45602,6 15717,4 -127489,9 45,078 1,100 1,300 1,000 1,100 1,100

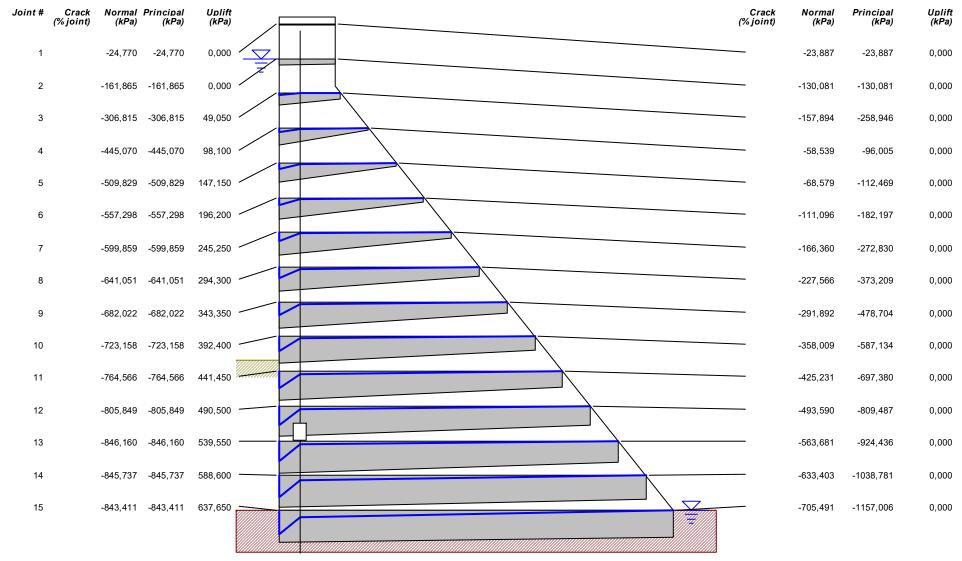
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Project: Dam location: FGG Analysis performed by: Example 1 30/11/2021 Dam: Date: Project engineer: Arthur Guillot - Le Goff

Owner:

Seismic #1 combination - Sustained accelerations (stability analysis) (effective stress analysis)



Date:

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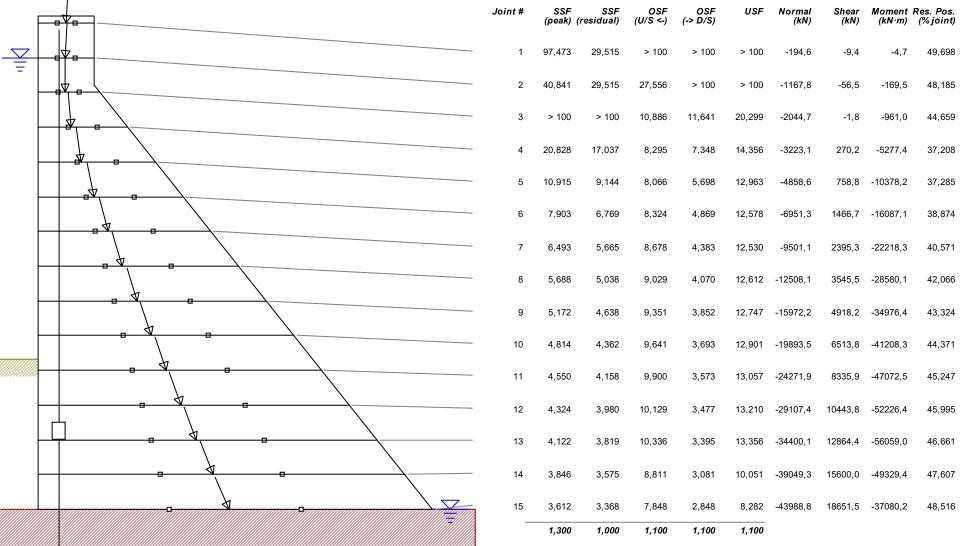
Project engineer:

Arthur Guillot - Le Goff

Project: Dam location: FGG Analysis performed by: 30/11/2021

Dam: Owner: Example 1

Seismic, #1 combination - Sustained accelerations (stability analysis) (stability analysis)



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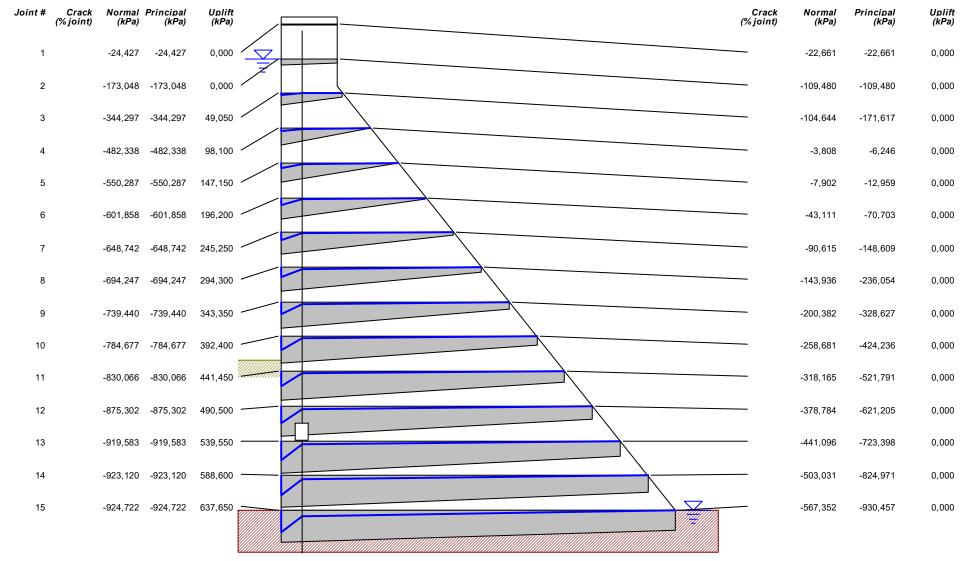
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 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismic #2 combination - Peak accelerations (stress analysis) (effective stress analysis)



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 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismic, #2 combination - Peak accelerations (stress analysis) (stability analysis) Joint # SSF SSF (peak) (residual) USF Normal Moment Res. Pos. (U/S <-) (-> D/S) (kN) (kN·m) (% joint) 48,260 14,281 80,000 > 100 > 100 -188,4-18,8 -9.4 49,375 14,281 13,333 > 100 > 100 -1130,1 -113,0 -339,0 46,250 19,945 22.363 6,015 -1975.3 -126,2 41,103 27.944 11,940 19.644 -1546.6 89,144 4,753 7,481 13,893 -3111,3 49,8 -6533,5 33,594 19.420 16.174 4,714 5,785 12,545 -4688.8 414,0 -12756,9 33,805 11,574 9,861 4,929 4,935 12,173 -6707,7 971,4 -20144,7 35,561 8,741 7,591 5,189 4,438 12,126 -9168,0 1725,0 -28605,9 37,419 7,301 6,440 5,441 4,116 12,205 -12069,8 2676,6 -38037,5 39,057 6,436 5,751 5,672 3,892 12,336 -15413,1 3827,7 -48328,3 40,440 10 5,862 5,293 5,879 3,729 12,485 -19197,8 5179,6 -59360,4 41,598 5,452 3,604 12,636 -23423,9 42,570 4,967 6,066 6734,4 -71010,9 4,695 3,505 43,401 12 5,115 6,232 12,784 -28091,5 8544,5 -83044,4 13 4,822 4,455 6,381 3,420 12,925 -33200,6 10642,6 -94957,2 44,139 14 4,450 4,126 5,803 3,103 9,727 -37650,4 13032,8 -97595,0 45,091

4,139

1,300

3,850

1,000

5,399

1,100

2,867

1,100

15717,4 -96080,0

46,008

-42374,9

1,100

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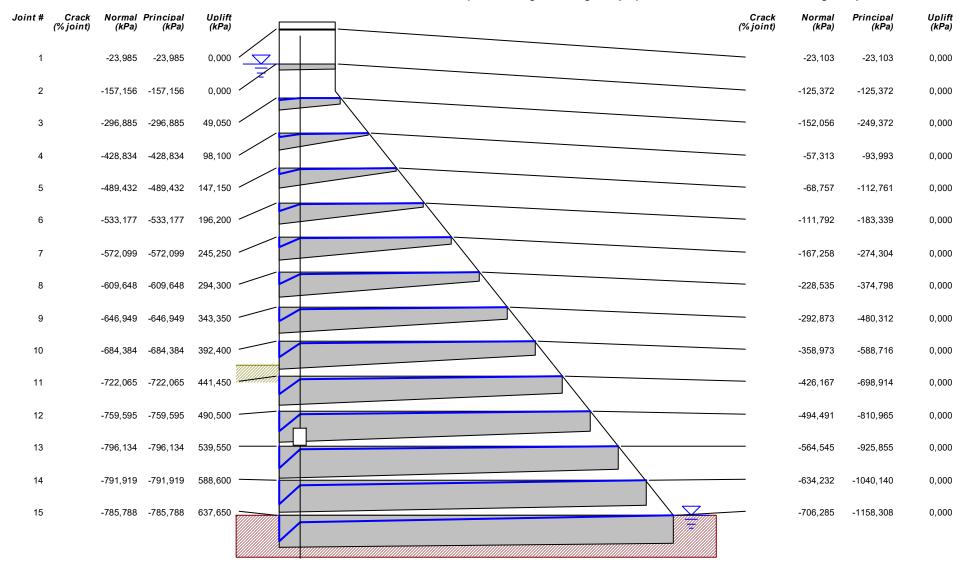
NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismic #2 combination - Sustained accelerations (stability analysis) (effective stress analysis)



By Martin Leclerc, M. Ing.

NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

Project: Dam location: FGG Analysis performed by: 30/11/2021 Dam: Example 1 Date: Project engineer: Arthur Guillot - Le Goff

Owner:

Seismic, #2 combination - Sustained accelerations (stability analysis) (stability analysis) Joint # SSF SSF (peak) (residual) OSF (-> D/S) Moment Res. Pos. (U/S <-) (kN) (kN) (kN·m) (% joint) 96.521 28,563 > 100 > 100 > 100 -188,4-9,4 49,688 -4,728,563 > 100 > 100 -1130,1 -56,5 48,125 39,889 26,667 -169,5-1975.3 > 100 > 100 10,543 11,286 19.644 -1,8 -934.6 44,623 20.237 16,447 8,053 7,123 13,893 -3111,3 270,2 -5072,5 37,263 10.596 8.825 7.847 5,522 12,545 -4688.8 758,8 -9894.3 37,439 8,110 7,666 6,531 4,719 12,173 -6707,7 1466,7 -15192,3 39,111 6,295 5,466 8,464 4,248 12,126 -9168,0 2395,3 -20749,5 40,874 5,512 4,862 8,813 3,944 12,205 -12069,8 3545,5 -26342,5 42,422 5,009 4,476 9,133 3,733 12,336 -15413,1 4918,2 -31744,1 43,721 10 4,661 4,209 9,420 3,579 12,485 -19197,8 6513,8 -36723,7 44,802 4,405 4,013 3,462 12,636 -23423,9 8335,9 -41047,0 45,705 9,676 3,841 10443,8 -44339,6 46,477 12 4,185 9,903 3,369 12,784 -28091,5 13 3,989 3,686 10,107 3,289 12,925 -33200,6 12864,4 -45959,5 47,163 14 3,718 3,447 8,618 2,985 9,727 -37650,4 15600,0 -36634,0 48,157 3,488 3,245 7,678 2,760 -42374,9 18651,5 -21374,6 49,112 1,100 1,300 1,000 1,100 1,100

Arthur Guillot - Le Goff

Project engineer:

CADAM - Stability drawing

Date:

By Martin Leclerc, M. Ing.

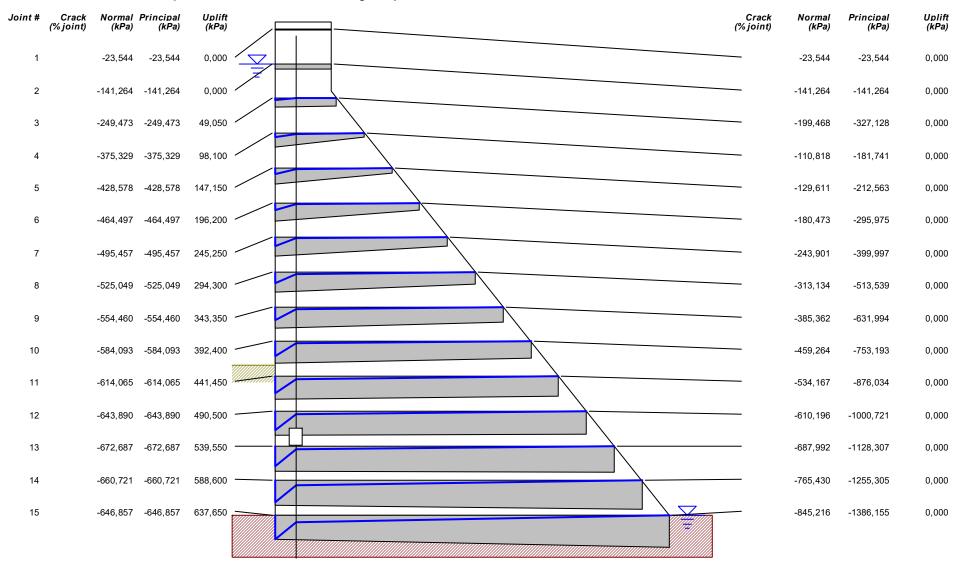
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Project: TD4 Dam location: FGG Analysis performed by:

30/11/2021

Dam: Owner: Example 1

Usual combination (effective stress analysis)



By Martin Leclerc, M. Ing.

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Dam location: FGG Analysis performed by: Project: Example 1 30/11/2021 Project engineer: Dam: Date: Arthur Guillot - Le Goff

Owner:

| Usual combina | tion (stability analysis) | | | | | | | | | | |
|---------------|---------------------------|---------|---------------|-------------------|-----------------|-----------------|--------|----------------|---------------|----------|------------------------|
| - | | Joint # | SSF (peak) | SSF (residual) | OSF (U/S <-) | OSF (-> D/S) | USF | Normal (kN) | Shear (kN) | | Res. Pos. (% joint) |
| <u>_</u> | | 1 | > 100 | > 100 | > 100 | > 100 | > 100 | -188,4 | 0,0 | 0,0 | 50,000 |
| = | | 2 | > 100 | > 100 | > 100 | > 100 | > 100 | -1130,1 | 0,0 | 0,0 | 50,000 |
| | | 3 | 28,747 | 23,006 | 42,655 | 10,633 | 19,644 | -1975,3 | 122,6 | -322,7 | 48,144 |
| | | 4 | 11,147 | 9,059 | 26,346 | 6,765 | 13,893 | -3111,3 | 490,5 | -3611,5 | 40,932 |
| | | 5 | 7,285 | 6,068 | 23,399 | 5,260 | 12,545 | -4688,8 | 1103,6 | -7031,7 | 41,073 |
| | | 6 | 5,731 | 4,883 | 22,862 | 4,502 | 12,173 | -6707,7 | 1962,0 | -10240,0 | 42,661 |
| | | 7 | 4,918 | 4,271 | 22,935 | 4,058 | 12,126 | -9168,0 | 3065,6 | -12893,1 | 44,329 |
| | | 8 | 4,427 | 3,905 | 23,168 | 3,772 | 12,205 | -12069,8 | 4414,5 | -14647,6 | 45,786 |
| | | 9 | 4,100 | 3,663 | 23,428 | 3,574 | 12,336 | -15413,1 | 6008,6 | -15160,1 | 47,001 |
| | | 10 | 3,869 | 3,494 | 23,676 | 3,429 | 12,485 | -19197,8 | 7848,0 | -14087,4 | 48,006 |
| | | 11 | 3,695 | 3,366 | 23,898 | 3,320 | 12,636 | -23423,9 | 9937,4 | -11083,4 | 48,840 |
| | | 12 | 3,541 | 3,250 | 24,101 | 3,233 | 12,784 | -28091,5 | 12343,0 | -5635,5 | 49,552 |
| | | 13 | 3,402 | 3,143 | 24,294 | 3,158 | 12,925 | -33200,6 | 15086,2 | 3037,4 | 50,187 |
| | | 14 | 3,192 | 2,960 | 16,736 | 2,868 | 9,727 | -37650,4 | 18167,1 | 24326,0 | 51,224 |
| | | 15 — | 3,014 | 2,804 | 13,284 | 2,652 | 8,015 | -42374,9 | 21585,6 | 53329,6 | 52,216 |
| | | | 3,000 | 1,500 | 2,000 | 2,000 | 1,200 | | | | |

Date:

By Martin Leclerc, M. Ing.

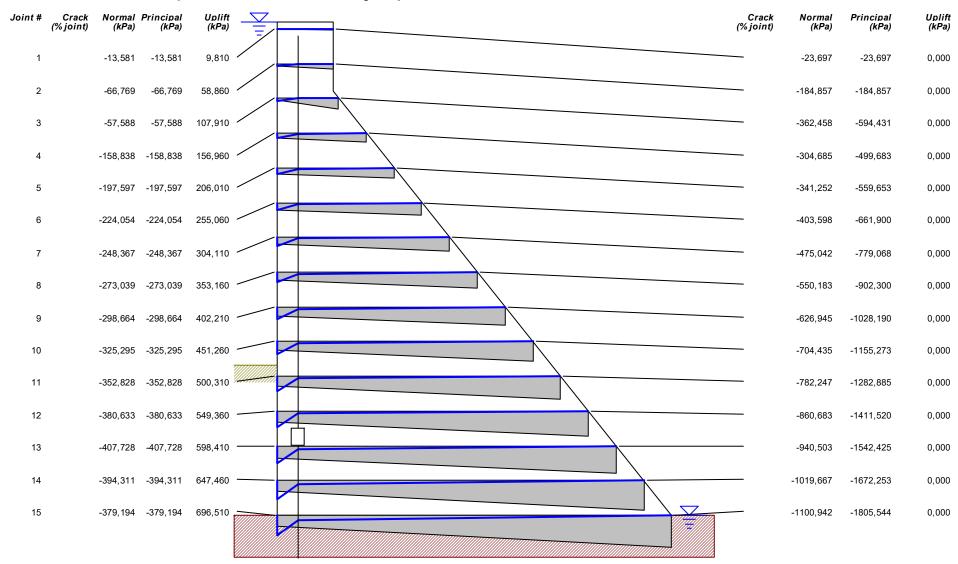
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Project: TD4 Dam location: FGG Analysis performed by:

30/11/2021

Dam: Owner: Example 1

Flood combination (effective stress analysis)



Arthur Guillot - Le Goff

Project engineer:



By Martin Leclerc, M. Ing.

NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

| Flood combination (stability analysis) | | | | | | | | | | |
|--|---------|---------------|-------------------|-----------------|-----------------|--------|----------------|---------------|------------------|------------------------|
| = | Joint # | SSF (peak) | SSF (residual) | OSF (U/S <-) | OSF (-> D/S) | USF | Normal (kN) | Shear (kN) | Moment (kN·m) | Res. Pos. (% joint) |
| | 1 | > 100 | 43,416 | 7,216 | 3,572 | 4,800 | -149,1 | 4,9 | 54,0 | 54,523 |
| | 2 | 11,765 | 8,140 | 22,378 | 4,021 | 9,143 | -1006,5 | 176,6 | 629,8 | 57,822 |
| | 3 | 5,633 | 4,447 | 23,850 | 2,629 | 8,929 | -1848,2 | 593,5 | 1967,4 | 62,097 |
| | 4 | 4,189 | 3,374 | 21,385 | 2,602 | 8,683 | -2966,5 | 1255,7 | 1991,3 | 55,244 |
| | 5 | 3,610 | 2,988 | 21,473 | 2,528 | 8,961 | -4526,3 | 2163,1 | 3378,8 | 54,443 |
| | 6 | 3,313 | 2,812 | 22,010 | 2,482 | 9,363 | -6527,6 | 3315,8 | 6473,2 | 54,768 |
| | 7 | 3,139 | 2,718 | 22,561 | 2,457 | 9,779 | -8970,3 | 4713,7 | 11617,9 | 55,222 |
| | 8 | 3,026 | 2,663 | 23,036 | 2,445 | 10,171 | -11854,4 | 6356,9 | 19156,2 | 55,611 |
| | 9 | 2,948 | 2,629 | 23,431 | 2,439 | 10,531 | -15180,0 | 8245,3 | 29431,5 | 55,911 |
| | 10 | 2,891 | 2,607 | 23,756 | 2,438 | 10,856 | -18947,0 | 10379,0 | 42787,2 | 56,137 |
| | 11 | 2,847 | 2,591 | 24,025 | 2,439 | 11,150 | -23155,5 | 12762,6 | 59569,0 | 56,305 |
| | 12 | 2,800 | 2,568 | 24,256 | 2,440 | 11,414 | -27805,5 | 15462,6 | 80290,0 | 56,445 |
| | 13 | 2,751 | 2,540 | 24,464 | 2,440 | 11,654 | -32896,9 | 18500,1 | 105731,0 | 56,586 |
| | 14 | 2,630 | 2,437 | 17,356 | 2,296 | 9,052 | -37329,0 | 21875,3 | 145282,6 | 57,371 |
| | 15 | 2,524 | 2,346 | 13,923 | 2,181 | 7,589 | -42035,8 | 25588,1 | 194044,3 | 58,127 |
| | _ | 2,000 | 1,300 | 1,100 | 1,100 | 1,100 | | | | |

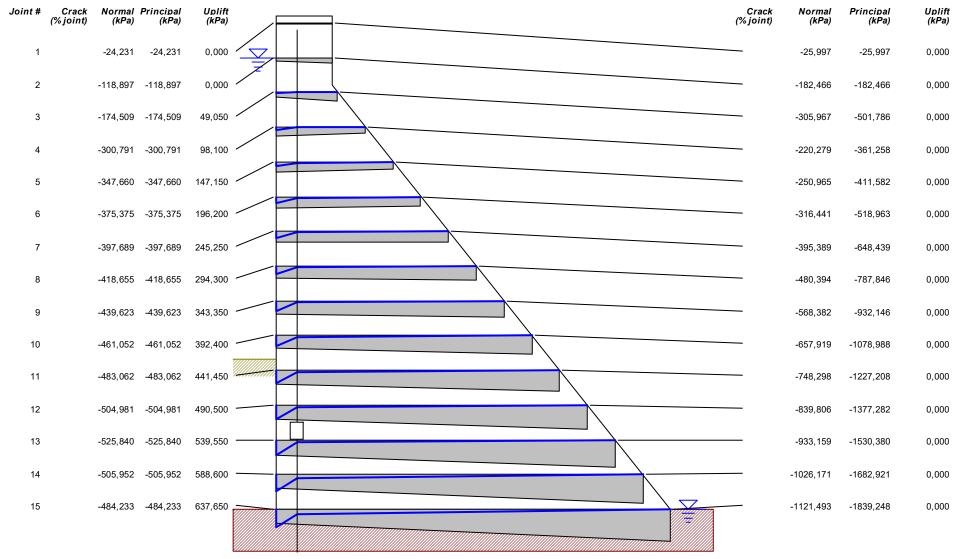
By Martin Leclerc, M. Ing.

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Project: Dam location: FGG Analysis performed by: Example 1 30/11/2021 Dam: Date: Project engineer: Arthur Guillot - Le Goff

Owner:

Seismic #1 combination - Peak accelerations (stress analysis) (effective stress analysis)



By Martin Leclerc, M. Ing.

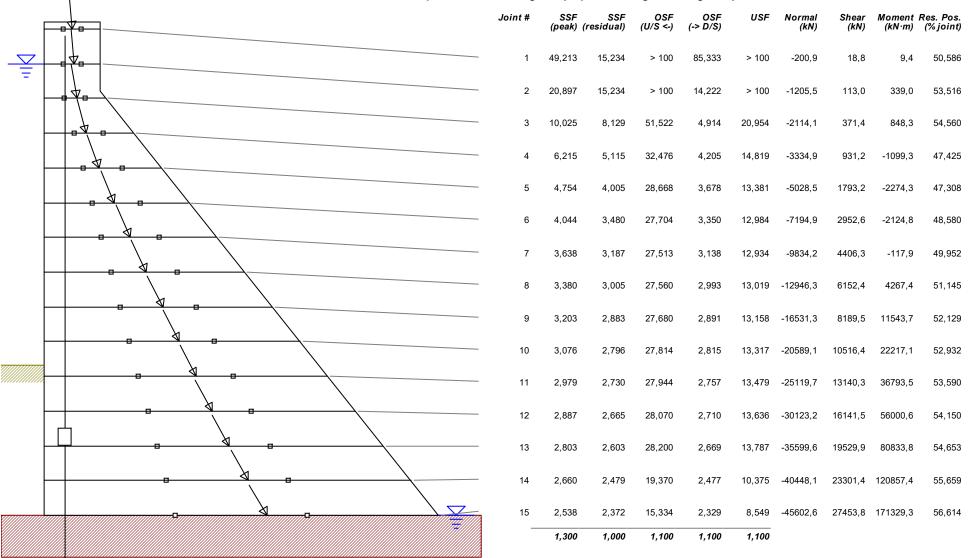
NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismiç #1 combination - Peak accelerations (stress analysis) (stability analysis)



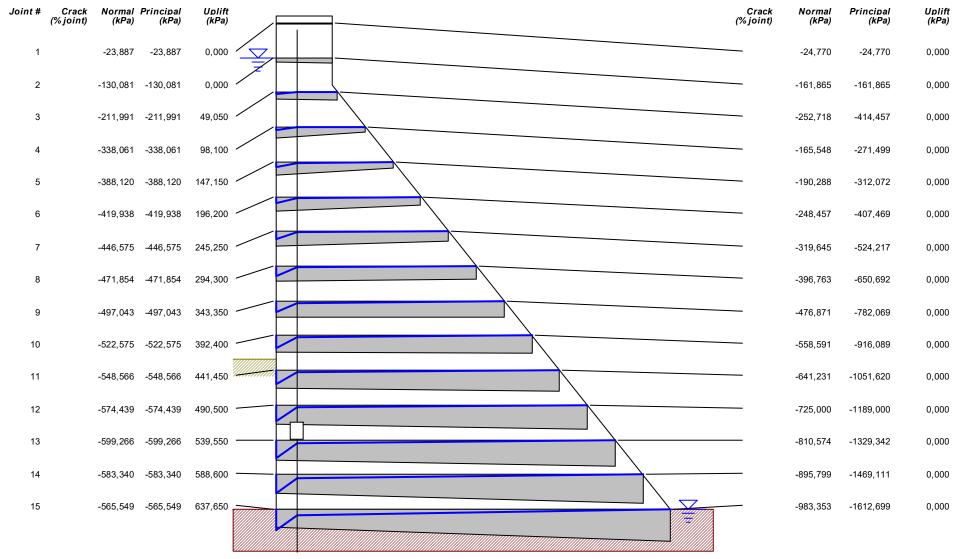
By Martin Leclerc, M. Ing.

NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

Project: Dam location: FGG Analysis performed by: Example 1 30/11/2021 Dam: Date: Project engineer: Arthur Guillot - Le Goff

Owner:

Seismic #1 combination - Sustained accelerations (stability analysis) (effective stress analysis)



Date:

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Project engineer:

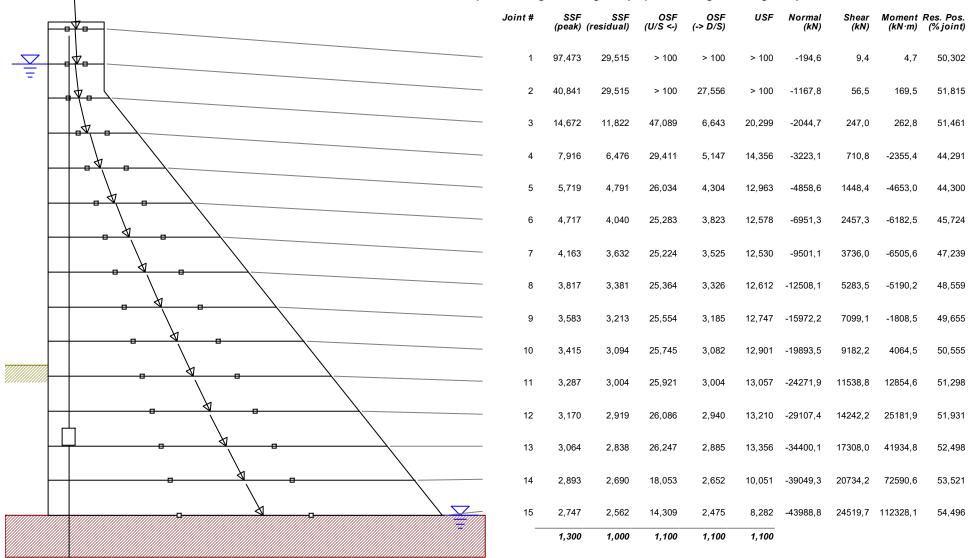
Arthur Guillot - Le Goff

Project: TD4 Dam location: FGG Analysis performed by:

Dam: Owner: Example 1

Seismiç #1 combination - Sustained accelerations (stability analysis) (stability analysis)

30/11/2021



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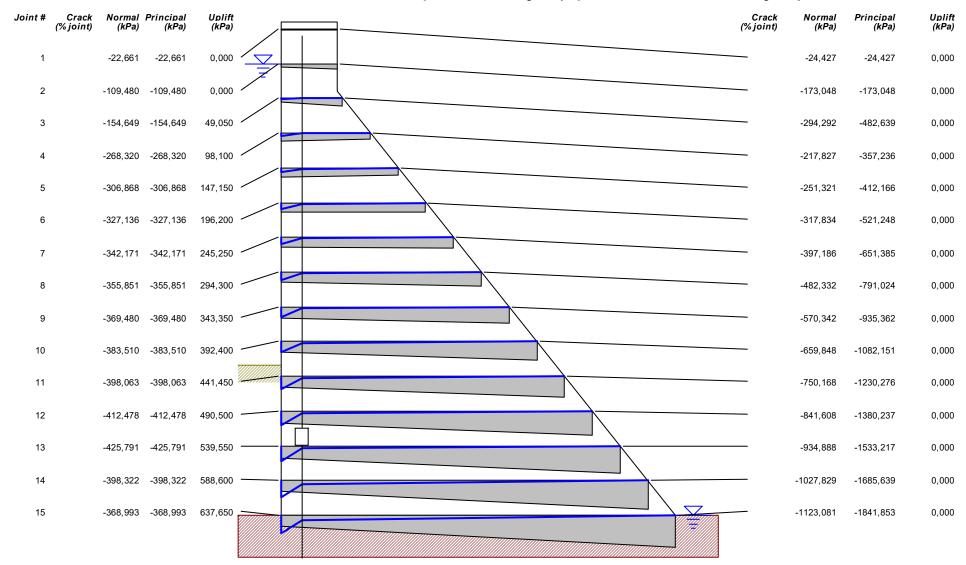
NSERC / Hydro-Quebec / Alcan Industrial Chair on Structural Safety of Concrete Dams, École Polytechnique de Montréal, Canada

 Project:
 TD4
 Dam location:
 FGG
 Analysis performed by:

 Dam:
 Example 1
 Date:
 30/11/2021
 Project engineer:
 Arthur Guillot - Le Goff

Owner:

Seismic #2 combination - Peak accelerations (stress analysis) (effective stress analysis)



Date:

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Project engineer:

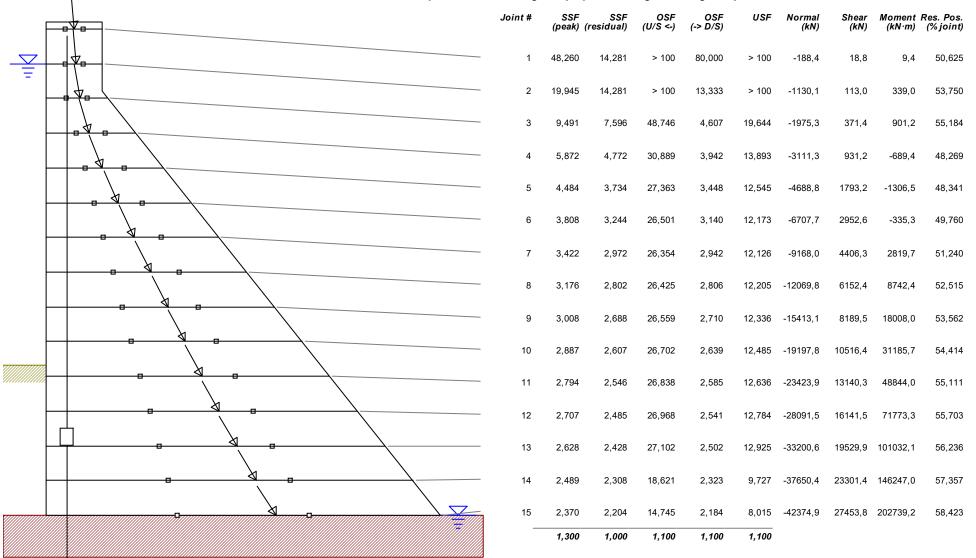
Arthur Guillot - Le Goff

Project: TD4 Dam location: FGG Analysis performed by:

30/11/2021

Dam: Owner: Example 1

Seismiç #2 combination - Peak accelerations (stress analysis) (stability analysis)



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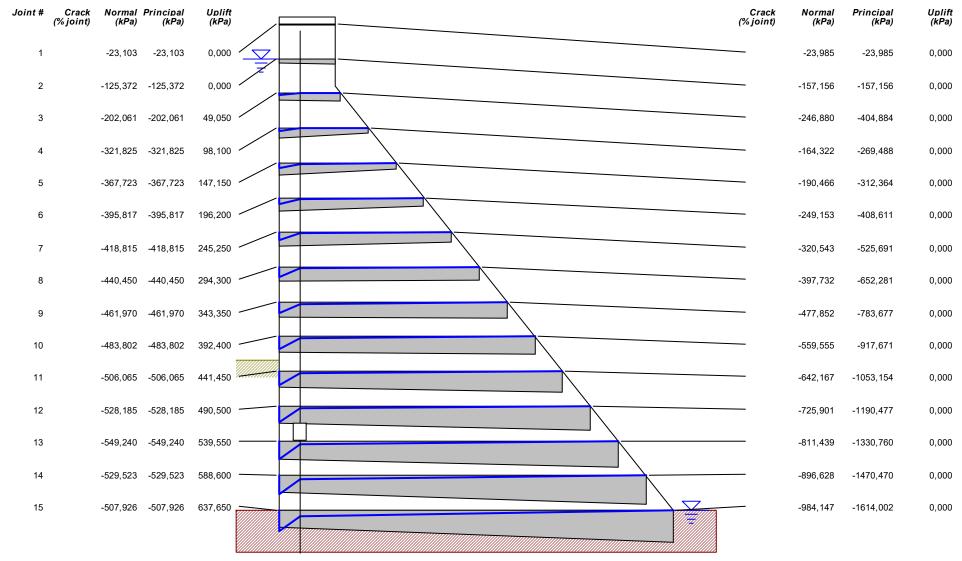
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 Project:
 TD4
 Dam location:
 FGG
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 Example 1
 Date:
 30/11/2021
 Project engineer:
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Owner:

Seismic #2 combination - Sustained accelerations (stability analysis) (effective stress analysis)



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Owner:

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Project: TD4 Dam location: FGG Analysis performed by:

Dam:Example 1Date:30/11/2021Project engineer:Arthur Guillot - Le Goff

Seismiç #2 combination - Sustained accelerations (stability analysis) (stability analysis)

