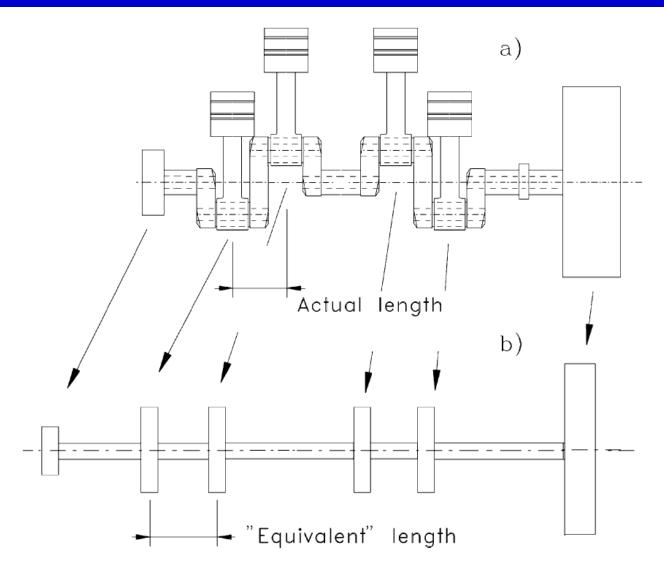
# Dynamic Design of Machines

# Tutorial 5 – Exercise 1







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Equivalent length according to Carter's model

$$L_{eq} = 2c + 0.8b + \frac{3}{4} \frac{D^4 - d^4}{D'^4 - d'^4} a + \frac{3}{2} \frac{D^4 - d^4}{bs^3} r = 0.150 m$$

Second moment of area of the Main Pin

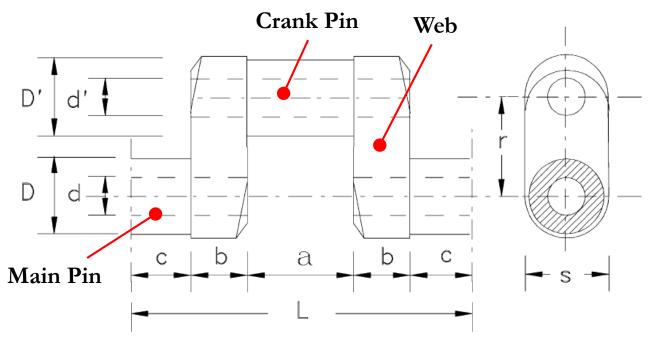
$$I_{p,MP} = \pi \frac{D^4 - d^4}{32} = 7.854 \ 10^{-8} \ m^4$$

Equivalent stiffness of the Crankshaft

$$k_{eq,C} = \frac{GI_{p,MP}}{L_{eq}} = 4.040 \ 10^4 Nm/rad$$



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Inertia of the Main Pin

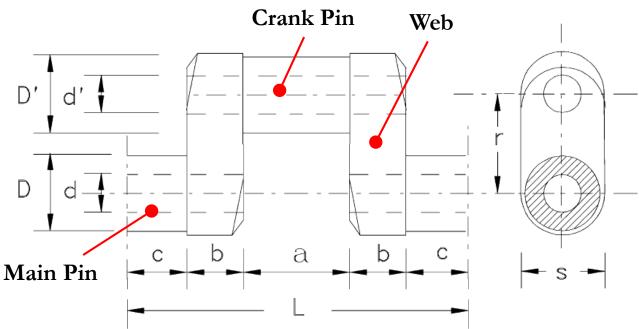
$$J_{MP} = \pi \frac{D^4 - d^4}{32} c\rho = 1.225 \ 10^{-5} \ kgm^2$$

Inertia of the Crank Pin

$$J_{CP} = \pi \frac{D'^4 - d'^4}{32} a\rho + \pi \frac{D'^2 - d'^2}{4} a\rho r^2 = 3.157 \ 10^{-4} \ kgm^2$$



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Inertia of the Web

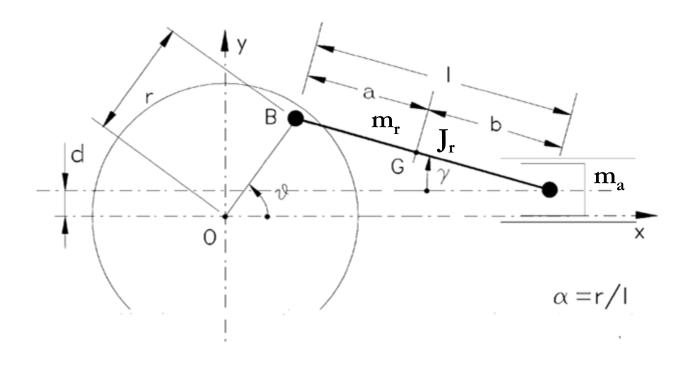
$$J_w = \frac{sr^3}{12}b\rho + m_w \left(\frac{r}{2}\right)^2 = \frac{1}{3}sbr^3\rho = 1.860\ 10^{-4}\ kgm^2$$

Inertia of the Crank

$$J_C = 2J_{MP} + 2J_w + J_{CP} = 7.122 \ 10^{-4} \ kgm^2$$



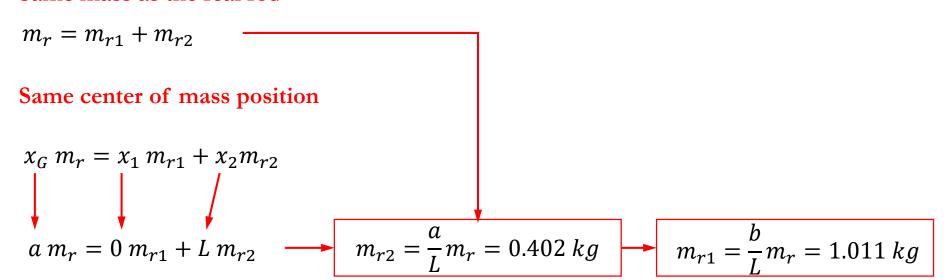
# Equivalent Rod





# Equivalent Rod

#### Same mass as the real rod



## Same moment of inertia

$$J_r = J_0 + m_{r1}a^2 + m_{r2}b^2$$

$$J_0 = J_r + m_r ab = -3.876 \ 10^{-3} \ kgm^2$$



# Equivalent average moment of inertia

$$J_{eq} = J_C + m_{r1}r^2 + (m_{r2} + m_a)r^2 f_1(\theta) + J_0 f_2(\theta)$$

$$f_1(\vartheta) \approx a_0 = \frac{8 + 2\alpha + \alpha^4}{16} = 0.514$$

First order approximation, constant terms only

$$f_2(\theta) \approx c_0 = \alpha^2 \frac{4 + \alpha^2}{8} = 0.054$$
  $\alpha = \frac{r}{L} = 0.325$ 

$$J_{eq} = J_C + m_{r1}r^2 + (m_{r2} + m_a)r^2a_0 + J_0c_0 = 4.463 \ 10^{-3} \ kgm^2$$



### Stiffness matrix

$$K = \begin{bmatrix} k_1 & -k_1 & 0 \\ -k_1 & k_1 + k_2 & -k_2 \\ 0 & -k_2 & k_2 \end{bmatrix}$$

### Mass matrix

$$M = \begin{bmatrix} J_1 & 0 & 0 \\ 0 & J_2 & 0 \\ 0 & 0 & J_3 \end{bmatrix}$$

$$det(-\omega^2[M] + [K]) = 0$$



# **Potential Energy**

$$U = \frac{1}{2}k_5(\vartheta_6 - \vartheta_5)^2 + \frac{1}{2}k_3(\vartheta_4 - \vartheta_3)^2 + \frac{1}{2}k_2(\vartheta_3 - \vartheta_2)^2 + \frac{1}{2}k_1(\vartheta_2 - \vartheta_1)^2$$

# Kinetic Energy

$$T = \frac{1}{2}J_6\dot{\vartheta_6}^2 + \frac{1}{2}J_5\dot{\vartheta_5}^2 + \frac{1}{2}J_4\dot{\vartheta_4}^2 + \frac{1}{2}J_3\dot{\vartheta_3}^2 + \frac{1}{2}J_2\dot{\vartheta_2}^2 + \frac{1}{2}J_1\dot{\vartheta_1}^2$$

$$\tau = \frac{\vartheta_5}{\vartheta_4} = \frac{\dot{\vartheta}_5}{\dot{\vartheta}_4}$$

$$U = \frac{1}{2}k_5(\vartheta_6 - \tau\vartheta_4)^2 + \frac{1}{2}k_3(\vartheta_4 - \vartheta_3)^2 + \frac{1}{2}k_2(\vartheta_3 - \vartheta_2)^2 + \frac{1}{2}k_1(\vartheta_2 - \vartheta_1)^2$$

$$T = \frac{1}{2}J_6\dot{\vartheta}_6^2 + \frac{1}{2}J_5\tau^2\dot{\vartheta}_4^2 + \frac{1}{2}J_4\dot{\vartheta}_4^2 + \frac{1}{2}J_3\dot{\vartheta}_3^2 + \frac{1}{2}J_2\dot{\vartheta}_2^2 + \frac{1}{2}J_1\dot{\vartheta}_1^2$$



$$\vartheta_6^* = \frac{\vartheta_6}{\tau}$$

$$U = \frac{1}{2}k_5\tau^2(\theta_6^* - \theta_4)^2 + \frac{1}{2}k_3(\theta_4 - \theta_3)^2 + \frac{1}{2}k_2(\theta_3 - \theta_2)^2 + \frac{1}{2}k_1(\theta_2 - \theta_1)^2$$

$$k_5^*$$

$$T = \frac{1}{2}J_{6}\tau^{2}\dot{\vartheta_{6}^{*}}^{2} + \frac{1}{2}J_{5}\tau^{2}\dot{\vartheta_{4}}^{2} + \frac{1}{2}J_{4}\dot{\vartheta_{4}}^{2} + \frac{1}{2}J_{3}\dot{\vartheta_{3}}^{2} + \frac{1}{2}J_{2}\dot{\vartheta_{2}}^{2} + \frac{1}{2}J_{1}\dot{\vartheta_{1}}^{2}$$

$$J_{6}^{*} \qquad J_{5}^{*}$$



### Stiffness matrix

$$\mathbf{K} = \begin{bmatrix} k_1 & -k_1 & 0 & 0 & 0 \\ -k_1 & k_1 + k_2 & -k_2 & 0 & 0 \\ 0 & -k_2 & k_2 + k_3 & -k_3 & 0 \\ 0 & 0 & -k_3 & k_3 + k_5^* & -k_5^* \\ 0 & 0 & 0 & -k_5^* & k_5^* \end{bmatrix}$$

### Mass matrix

$$\mathbf{M} = \begin{bmatrix} J_1 & 0 & 0 & 0 & 0 \\ 0 & J_2 & 0 & 0 & 0 \\ 0 & 0 & J_3 & 0 & 0 \\ 0 & 0 & 0 & J_4 + J_5^* & 0 \\ 0 & 0 & 0 & 0 & J_6^* \end{bmatrix}$$

$$det(-\omega^2 \mathbf{M} + \mathbf{K}) = 0$$

With degrees of freedom 
$$\begin{cases} \vartheta_2 \\ \vartheta_3 \\ \vartheta_4 \end{cases}$$

$$egin{cases} artheta_1 \ artheta_2 \ artheta_3 \ artheta_4 \ artheta_6 \ \end{cases}$$