

# Three-dimensional bin packing with vertical support

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### Abstract

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## Abstract in lingua italiana

Qui va l'Abstract in lingua italiana della tesi seguito dalla lista di parole chiave.

Parole chiave: qui, vanno, le parole chiave, della tesi



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# 1 Introduction

The problem addressed by our contribution is the 3D-SBSBPP (3D Single Bin-Size Bin Packing Problem) which is strongly NP-hard and is the generalization of the one-dimensional bin packing problem Martello et al. [2000].

Case study

Overview



## 2 Literature review

#### Static stability

Static stability or vertical support received most of its contributions from the fields of Pallet Loading Problems (PLP) and Cargo Loading Problems (CLP). In [Elhedhli et al., 2019] a second order cone programming formulation was provided as a solution to a spacing problem between layers of a pallet. The pubblication further described the concept of minimizing the area of overlap between items of different layers to increase spacing between items of the same layer and increase the amount of potential support for higher layers. In [Paquay et al., 2016] a formulation of the CLP was given with practical constraints like weight distributiom, non-regular container shapes and vertical stability through vertex support.



# 3 Problem description and mathematical formulation

In this thesis, we address the 3D single bin-size bin packing problem (3D-SBSBPP) with the addition of a few practical constraints. Starting from a set of items of different sizes the goal is to arrange them in the least amount of bins of a given fixed size without any overlap between each other. In addition to the standard formulation of the problem, three practical constraints need to be taken into account:

- each item inside a bin should have static stability, meaning that every item should be supported either by the ground or by other items in the same bin,
- the cage ratio of each used bin should be maximized,
- each item can be rotated orthogonally along its vertical axis.

Given a certain placement of items inside a bin of base  $W \times D$  with the top of the highest item being at  $z_{\text{max}}$  and the sum of the volume of each item being V, the bin's cage ratio is defined as eq. (3.1).

$$CR = \frac{V}{W \cdot D \cdot z_{\text{max}}} \tag{3.1}$$

A high cage ratio means that even if a bin isn't fully occupied, it could be used as a base for other structures. This property is desirable in some industrial settings. It is also noted that in a single bin configuration, maximizing cage ratio is equivalent to minimizing  $z_{\text{max}}$ . Finally, a visual representation of the cage ratio metric is provided in fig. 3.1.

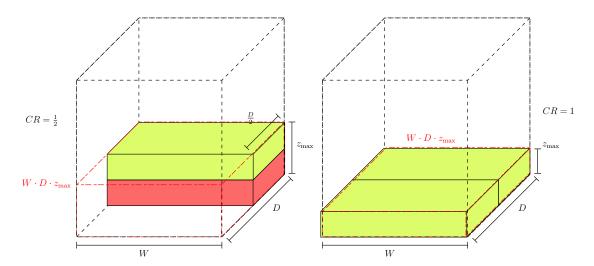


Figure 3.1: Cage ratio of two different bin configurations

Our notion of vertical support stems from rules imposed by the industry and from the literature on Pallet Loading Problems and Container Loading Problems. Vertical stability is usually ensured between horizontal or vertical slices of items as a constraint on the minimum amount of area which rests on other items (as for ex. [Elhedhli et al., 2019; Kurpel et al., 2020; Paquay et al., 2016]). Given a support area threshold  $\alpha_s$  and a vertical tolerance  $\beta_s$  we can define an item as supported if one of the following holds

- 1. the sum of the overlap area over the XY-plane with every other item on which it is resting is greater than  $\alpha_s$  times its base area. (area support)
- 2. the number of its corners resting on another item is greater than 3, and condition 1 holds with a lower threshold  $\alpha'_s < \alpha_s$ . (vertex support)

A visual representation of the condition of support is illustrated in fig. 3.2.

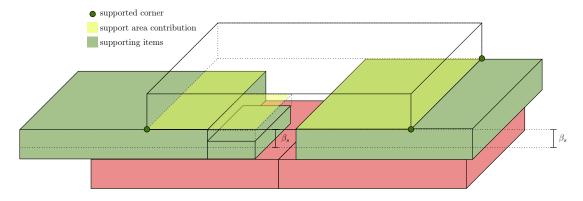


Figure 3.2: Representation of an item with vertical support given  $\alpha_s = 0.5, \beta_s$ 

Given the definitions of our practical constraints, a conceptual formulation of our model would be

minimize number of used bins the unused volume of each bin under  $z_{\rm max}$  subject to all items assigned to one and only one bin all items within the bin dimensions no overlaps between items in the same bin all items with vertical support

In section 3.1 a mixed-integer linear programming model for the 3D-SBSBPP is presented and it's later extended to include orthogonal rotations in section 3.1.1 and vertical support constraints limited to condition 1 (area support) in section 3.1.2. Cage ratio isn't directly included in the proposed MILP formulation since the evaluation of the heuristic with the model was done in a single bin configuration where minimizing the maximum height of the bin is equivalent to minimizing the cage ratio.

#### 3.1. 3D single bin-size bin packing problem

Let  $I = \{1, \ldots, n\}$  be the set of items that need to be packed,  $B = \{1, \ldots, m\}$  the set of bins to evaluate of fixed dimensions  $W \times D \times H$ . Each item  $i \in I$  is characterized by a given width, depth, and height  $(w_i, d_i, h_i)$ . Let us introduce three continuous variables that identify the position of an item's bottom front left corner  $(x_i, y_i, h_i)$  as seen in fig. 3.3. We can now introduce a set of integer variables  $v_b$  which will be 1 if bin  $b \in B$  will be used in the solution and 0 otherwise. A set of integer variables  $u_{ib}$  which will be 1 if item  $i \in I$  will be placed in bin  $b \in B$  and 0 otherwise. To check for overlaps, we introduce three sets of integer variables for each axis of possible overlap to determine if there is a clear order of precedence on at least one axis. This formulation is also usually used in scheduling problems. One of the introduced sets is the set  $x_{ij}^p$ , which will take the value of 1 if item  $i \in I$  precedes item  $j \in I$  over axis x and 0 otherwise. This condition is verified if  $x_i + w_i \leq x_j$ . The other two sets are defined in a similar way over the remaining axis  $y_{ij}^p$  and  $z_{ij}^p$ . An additional set of continuous variables  $z_b^{\max}$  is introduced which will assume the value of the maximum  $x_i + h_i$  of the items  $i \in I$  placed in bin  $b \in B$ .

The 3D-SBSBPP can then be formulated as a mixed-integer linear programming problem:

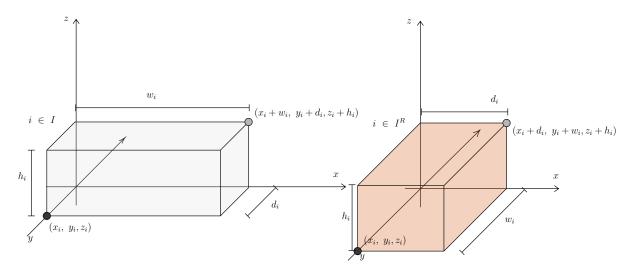


Figure 3.3: Coordinate system representation for a generic item i and its rotated clone  $i \in I^R$ 

The objective function 3.2 seeks to minimize the number of opened bins and the maximum height at which items were placed across bins. In a single bin configuration, since all the volume mass is concentrated inside one bin, it maximizes the cage ratio. Constraint 3.3

ensures that each item is packed in one and only one bin, while constraint 3.4 ensures that items are only packed in bins used in the solution. Since the solution has lots of symmetries with respect to the number of bins, a symmetry-breaking constraint 3.5 can be added on the opening of bins to improve solve times. Each item is also ensured to be placed inside the bin thanks to eqs. (3.6) to (3.8). The value of  $z_b^{max}$  is forced to converge to the maximum height of a given bin thanks to constraint 3.9. Constraints from 3.10 to 3.15 are used to define the precedence binary variables  $x_{ij}^p$ ,  $y_{ij}^p$ ,  $z_{ij}^p$  over each axis as described in the problem formulation. Constraint 3.16 then ensures that if two items are in the same bin, there needs to be at least one axis with a clear order of precedence; otherwise, the two items would overlap.

#### 3.1.1. Orthogonal rotations

Let us extend the definition of the bin packing problem without rotations with a new formulation that allows 90 degrees rotations of each item. Let  $I = I^O \cup I^R$  be the new set of items where  $I^O$  is the set of original non-rotated items, and  $I^R$  is the set of items rotated by 90 degrees. Given the set of tuples  $(i, j) \in I^{OR}$  where i is the original item with dimensions  $(w_i, d_i, h_i)$  and j is the corresponding rotated clone with dimensions  $(w_j, d_j, h_j) = (d_i, w_i, h_i)$ , we can now rewrite constraint 3.3 as 3.17 to force only one of them to be part of the solution.

$$\sum_{b \in B} u_{ib} + \sum_{b \in B} u_{jb} = 1 \qquad \forall (i, j) \in I^{OR}$$
 (3.17)

#### 3.1.2. Discrete vertical support formulation

We now extend the model to address the constraint of vertical support. In the literature, some mathematical formulations tackle the concept of area support and, in some cases, vertex support. For example, in Elhedhli et al. a SOCP formulation of the support constraint was used but was limited to the problem of spacing between layers with one of them being fixed in position relative to the other. A similar formulation would lead to a non-linear support constraint in our case. By introducing a discretization over the XY-plane a linear version of the constraint can be formulated similar to the one proposed in Kurpel et al. without the need to discretize the z-axis as well.

Let us introduce some additional parameters to the model, let  $0 \le \alpha_s \le 1$  be the amount of area that an item needs to have supported by other items. Let  $\beta_s$  be the tolerance to consider one item as being close enough to support another item (as seen in fig. 3.2). In

addition to the support parameters, a parameter  $\delta$ , which represents the discretization unit used to partition the XY-plane, is given. Let  $I^B$  be the set of all the tuples (i, j, b) such that  $(i, j) \in I \land i \neq j$  and  $b \in B$ . We can now compute a few additional parameters that we will use to reduce the number of constraints evaluated by the model. Let  $\gamma$  be the maximum size over a dimension on the XY-plane between all the items as eq. (3.18), and let  $\Delta$  be the set of all possible distances between the origins of two items along one discretized axis as eq. (3.19).

$$\gamma = \max_{\forall i \in I} \{ w_i, d_i \} \tag{3.18}$$

$$\Delta = \left[ -\left\lfloor \frac{\gamma}{\delta} \right\rfloor, \left\lfloor \frac{\gamma}{\delta} \right\rfloor \right] \tag{3.19}$$

Let  $O(i, j, h, k) \to \mathbb{R}^+$  be a function that computes the amount of overlap between two items  $(i, j) \in I$  given the discretized distance between each other  $(h, k) \in \Delta$  such that  $x_j = x_i + \delta h$  and  $y_j = y_i + \delta k$  which returns the area of overlap or 0 otherwise.

Additional new variables need to be added to the ones of the original model, let  $s_{ij}$  be a set of binary variables which will assume value 1 if item  $i \in I$  can offer support to item  $j \in I$  and 0 otherwise. A new set of binary variables  $z_{ij}^c$  will be 1 if item  $i \in I$  is close w.r.t. the z-axis to item  $j \in I$ , which would mean that  $z_j - (z_i + h_i) \leq \beta_s$ , and 0 otherwise. Let us then introduce a new set of binary variables  $g_i$  which will assume value 1 if item  $i \in I$  will be on the ground or 0 otherwise. A set of binary variables  $s_{ijb}^{kh}$  will assume value 1 if item  $i \in I$  will receive support from item  $j \in I$  and both items will be placed in bin  $b \in B$  with a discretized distance of  $(k, h) \in \Delta$  between each other and 0 otherwise.

Given all the additional parameters and variables introduced, we can give a new formulation of the model with the same objective function 3.2 and the constraints in section 3.1 with the addition of the following constraints:

$$z_{j} - (z_{i} + h_{i}) \leq \beta_{s} + H(1 - z_{ij}^{c}) \qquad \forall (i, j) \in I : i \neq j \qquad (3.20)$$

$$z_{j} - (z_{i} + h_{i}) \geq -\beta_{s} - H(1 - z_{ij}^{c}) \qquad \forall (i, j) \in I : i \neq j \qquad (3.21)$$

$$s_{ij} \leq z_{ij}^{p} \qquad \forall (i, j) \in I \qquad (3.22)$$

$$s_{ij} \leq z_{ij}^{c} \qquad \forall (i, j) \in I \qquad (3.23)$$

$$s_{ij} \geq z_{ij}^{p} + z_{ij}^{c} - 2 \qquad \forall (i, j) \in I : i \neq j \qquad (3.24)$$

$$\sum_{j \in I} s_{ij} \leq \sum_{b \in B} u_{ib} \qquad \forall i \in I \qquad (3.25)$$

$$z_{i} \leq H(1 - g_{i}) \qquad \forall i \in I \qquad (3.26)$$

$$\sum_{(k,h) \in \Delta; O(i,j,k,h) \neq 0} s_{ijb}^{kh} \leq s_{ij} \qquad \forall (i, j, b) \in I^{B} \qquad (3.28)$$

$$\sum_{(k,h) \in \Delta; O(i,j,k,h) \neq 0} s_{ijb}^{kh} \leq u_{ib} \qquad \forall (i, j, b) \in I^{B} \qquad (3.29)$$

$$\sum_{(k,h)\in\Delta:O(i,j,k,h)\neq 0} s_{ijb}^{kh} \le u_{jb} \qquad \forall (i,j,b)\in I^B$$
 (3.29)

Constraints 3.20 and 3.21 ensure that  $z_{ij}^c$  is forced to 1 only when the distance over the z-axis between item i and item j is within the range  $[-\beta_s, \beta_s]$ . The value of  $s_{ij}$  is then assigned to the logical equation  $z_{ij}^p \wedge z_{ij}^c$  thanks to constraints from 3.22 to 3.24. Since some items could be left out of the solution due to the formulation of orthogonal rotations, we also ensure that support can only come from placed items thanks to constraint 3.25. Constraint 3.26 ensures that  $g_i$  will assume value 1 if item i is on the ground Constraints from 3.27 to 3.29 ensure that if a discretized support decision  $s_{ijb}^{hk}$  is 1 then every subscript of that variable must be true in the non-discretized model, so item i can give discretized support to item i in in bin b if both items are assinged to bin b and if i can give support to item j. They also force the selection of only one possible combination of  $(h,k) \in \Delta$  for which i gives support to j in bin b.

We can then define a set of constraints which given a discretized placement  $s_{ijb}^{kh}$  limits the distance between i and j to a given continuous region in space delimited by a square of the dimension of our discretization unit  $\delta$ . Given every tuple of possible discretized distances between items  $(k,h) \in \Delta$  and every tuple of different pairs of items in the same bin  $(i, j, b) \in I^B$  such they have a non-zero discretized overlap over the XY-plane

 $(O(i, j, k, h) \neq 0)$ . The resulting constraints are defined in eqs. (3.30) to (3.33).

$$x_j - x_i \ge \gamma k - 2W(1 - s_{ijb}^{kh})$$
 (3.30)

$$x_j - x_i \le \gamma(k+1) + 2W(1 - s_{ijb}^{kh}) \tag{3.31}$$

$$y_j - y_i \ge \gamma h - 2D(1 - s_{ijb}^{kh})$$
 (3.32)

$$y_j - y_i \le \gamma(h+1) + 2D(1 - s_{ijb}^{kh}) \tag{3.33}$$

We can then introduce a feasibility constraint that ensures that every item that isn't on the ground is supported by other items placed beneath it by at least  $\alpha_s$  times its area, which corresponds to condition 1 of the practical constraint of vertical support.

$$\sum_{(k,h)\in\Delta,b\in B,j\in I: i\neq j\land O(i,j,k,h)\neq 0} O(i,j,k,h) s_{jib}^{kh} \ge \alpha_s w_i d_i - w_i d_i g_i \quad \forall i\in I$$
 (3.34)

It is noted that every combination of  $(i, j, b) \in I^B$  and  $(h, k) \in \Delta$  where O(i, j, k, h) = 0 do not contribute to the support constraint. We can omit them from the formulation of the problem to reduce the number of constraints to evaluate.

## 4 | Solution algorithms

This chapter describes a heuristic algorithm to solve the 3D bin packing problem with vertical support. In section 4.1 we describe the concepts which will be used in the algorithm, like the definition of a state, insertions, and the feasibility of a solution. Since the 3D-BPP is NP-Hard, an exhaustive search for a solution is not practical, so a heuristic search is conducted by combining the beam search algorithm described in section 4.2 with the constructive heuristic described in section 4.3. The proposed algorithm takes in input the empty state (4.2), and outputs the best scoring state based on an ordering function defined in section 4.2.1.

#### 4.1. States

States or packings are partial solutions to the 3D-BPPWS. Since our heuristic is constructive by nature, the main idea of the algorithm is that by starting from a state representing an empty solution, we'll iteratively build new states that are always closer to a complete solution to the problem. Given the formal definition of the problem (3.1) we introduce a few new definitions to facilitate the algorithm's definition. First, it is helpful to define a collection of items that still need to be assigned to a particular bin; this collection would then be used to track how many items still need to be placed. Let us define the concept of unpacked items in relation to our MILP formulation.

**Definition 4.1** (Unpacked item). An item  $i \in I$  is unpacked iff

$$\sum_{b \in B} u_{ib} = 0$$

It is also assumed that variables identifying an item's position are independent between states (changes to their values in state s won't affect state s'). In order to simplify the algorithm representation, rotations are handled by simply swapping the dimensions  $w_i$  and  $d_i$  of item  $i \in I$  when needed. A state s can then be defined as follows:

• *U*: the set of unpacked items,

- B: the set of used bins,
- $Q = (q_1, q_2, \dots, q_b)$ : the set of supporting structures for each bin  $b \in B$ ,
- p: the insertion pending on this state (described by def. 4.4).

Since the heuristic will open new bins when the already opened ones are full, the number of bins in each state can vary and is not fixed as a parameter to the problem like in the MILP formulation. Thanks to the newly introduced definitions, we can trivially define a function that determines if a state is a final state.

**Definition 4.2.** A state s is final if there are no more items to pack

$$IsFinal(s) = \begin{cases} 1, & s.U = \emptyset \\ 0, & otherwise \end{cases}$$
(4.1)

The proposed heuristic also stores additional data for each opened bin, which will then be used by the constructive heuristic described in section 4.3. This additional information is stored in the set s.Q so that each bin  $b \in B$  has an associated supporting structure  $q_b \in s.Q$ . The collection of items placed inside a bin, for example, is one piece of data that we store in this structure. Let us then introduce the concept of packed items inside a bin.

**Definition 4.3** (Packed item). Given a state s and a bin  $b \in s.B$ , we say that item

$$i \in I$$
 is packed in  $b$  iff  $u_{ib} = 1$ 

In addition to the set of packed items, other supporting structures are needed to facilitate checks of the problem's constraints. Given a bin  $b \in s.B$  we can then define structure  $q_b$  as follows.

- J: the set of items that are packed inside b,
- Z: the set of planes inside b (section 4.3),
- T: the AABB Tree (section 4.1.1) representing the items inside b.

Both sets  $q_b.J$  and  $q_b.T$  contain the items packed in b but adding and accessing items in  $q_b.J$  has a time complexity of O(1) given an implementation as hash set while maintaining  $q_b.T$  usually has a time complexity of  $O(log(|q_b.J|))$ .

#### 4.1.1. AABB Tree

To determine the feasibility of a given state, checking for overlaps with items already placed is needed. Since every item is a cuboid and our problem formulation only allows for 90 deg rotations over the z-axis, each item is contained inside a bounding box, which is axis-aligned. An adequate structure to compute overlaps is then an Axis-Aligned Bounding Box Tree (AABB Tree) Bergen [1997].

AABB Trees are bounding volume hierarchies typically used for fast collision detection, and they usually offer a few operations:

- AABBInsert(i): which allows inserting an axis-aligned box i in the tree
- AABBOverlaps(i): which allows determining if an axis-aligned box i overlaps an element in the tree
- AABBClosest(i, d): which, given an axis-aligned box i and an axis-aligned direction d, returns the closest element following that direction starting from the box i

If the tree is appropriately balanced, each operation, on average, has a time complexity of  $O(\log(n))$  where n is the number of elements in the tree. Maintaining an AABB Tree in the state allows us to do checks for feasibility during the construction of a solution (as detailed in 4.3.1) and feasibility checks on the final states to allow for error detection.

An additional operation  $AABBGetSupporting(i, \beta_s)$  was added to compute the set of supporting boxes of item i given a vertical tolerance  $\beta_s$ . This was possible by only checking intersections over the XY-plane similarly to the AABBOverlaps implementation and filtering each item by the distance with tolerance.

#### 4.1.2. Feasibility

A state s is feasible if the currently packed items in each bin  $b \in s.B$  aren't overlapping any other item if they are all contained inside their bin and if each item is either on the ground or satisfies at least one of the support conditions (cond. 1, cond. 2). Since the proposed heuristic is constructive, it is more convenient to define the concept of feasibility relative to a change in the state. In the heuristic, we generate new states by applying insertions starting from an initial feasible one. Let us define the concept of insertion and how an insertion is feasible.

**Definition 4.4** (Insertion). Given a state s, we define an insertion p as a tuple (b, I) where  $b \in s.B$ , and I is a set of non-overlapping unpacked items such that they are

inserted at the same z.

$$I \subseteq s.U \land \exists z (z \in \mathbb{Z} \land \forall i (i \in I \land z_i = z))$$

**Observation 4.1.** Given a state s and an insertion  $p = (b, \emptyset)$  where  $b \notin s.B$ , p is an insertion that opens a new bin b in s.

**Definition 4.5** (Next). Let p be an insertion over a state s, we define s' = Next(s, p) as a "copy" of state s where p is the pending insertion (s'.p = p).

We evaluate the changes to the score of a state based on its pending insertion. In this way, we don't have to update all the structures for every evaluated state. In addition, this property let us do fewer memory clones of states that would have been discarded either way (as seen in section 4.2). We can then define an algorithm that applies a pending insertion p on a given state s with the help of a function OpenBin(b) which initializes a new structure  $q_b$  with every element at its empty value. The proposed algorithm is shown in 1.

#### Algorithm 1: Commit

Insertion feasibility An insertion p = (b, I) that is pending on a given state s is feasible if every inserted item  $i \in p.I$  satisfies the constraint of non-overlap (3.16), the constraint of support (3.34) and if it is placed within the bin. Given an item from the set of the inserted items  $i \in p.I$ , and the AABB tree for bin p.b in the current state  $q_b.T$  as T. Let  $I_{\text{support}}$  be the set of items that could support item i when placed in the bin,

which could be saved in an appropriate structure or computed through the AABB tree as defined in section 4.1.1.

Let  $HasSupport(i, I_{support})$  be the function that returns true if the considered item would verify at least one of the conditions of support (cond. 1 or cond. 2) or false otherwise. We can define a function  $IsFeasible(i, I_{support}, T)$  which returns true if the insertion of i in bin b for state s is feasible and false otherwise. If every item  $i \in p.I$  is feasible and every item in I is not overlapping the others, then insertion p is feasible. In case some items in p aren't feasible we can always define a function  $RemoveInfeasibleItems(p, I_{support}, T)$  which removes every unfeasible item and returns a new insertion p' = (b, I') where  $I' = p.I \setminus \{i \in p.I : \neg IsFeasible(i, I_{support}, T)\}$ .

Checking if a state is feasible can then be done by iteratively applying all the insertions ordered by z and updating the proper trees, or starting from an already built tree and computing the set  $I_{\text{support}}$  for each item through the tree as defined in 4.1.1.

**Proposition 4.1.** A state s' derived by committing a feasible insertion p to a feasible state s is feasible.

Observation 4.2. We can always define the empty state  $s_e$  where

$$\begin{cases} s_e.U = I \\ s_e.Q = \emptyset \\ s_e.B = \emptyset \end{cases}$$

and it is always feasible

#### 4.1.3. State Hashing

From a given state, it's possible to apply two different sequences of insertions and end up with two states that have all the items in the same positions. This undesirable behavior was observed during our computational experiments. A hashing mechanism needs to be introduced to enable checking if two states are likely the same in constant time. In a state s we can identify a packed item  $i \in I$  in a given position  $(x_i, y_i, z_i)$  with its given dimensions  $(w_i, d_i, z_i)$  in a given bin  $b \in s.B$  with a non-commutative hashing function  $hash\_nc$ . The resulting hash  $hash_{ib} = hash\_nc(b, x_i, y_i, z_i, w_i, d_i, h_i)$  can identify every similar packing of an item of the same shape in that specific bin spot. Since  $hash_{ib}$  identifies one item with the shape of i in the same spot as i, we can use a commutative function to combine every hash for every packed item in every bin to ignore the order with

which items were added to the solution. The combined hash can then be saved inside the state structure as follows.

$$s.hash = \sum_{b \in s.B} \sum_{i \in q_b.J} hash_{ib} \tag{4.2}$$

In our tests, by filtering states with the proposed hash as seen in algo. 2, with a simple 64-bit hashing function, this mechanism allowed us to filter out all equal states between iterations with a low amount of collisions. Since the combining of hashes is a simple sum with modulus, the hashing of the state can also be kept updated in constant time at each iteration by simply adding the inserted hashes in the *Commit* function (algo. 1).

#### 4.2. Beam Search

Beam Search (BS) is a heuristic tree search algorithm designed for systems with limited memory where expanding every possible node is unfeasible. The idea behind BS is to conduct an iterative truncated breadth-first search where, at each iteration, only a limited number of k nodes is expanded. After the expansion, every new node needs to be evaluated and sorted to prune the number of nodes down to the k best ones. The algorithm keeps exploring until no further node can be expanded.

To perform BS one must define the node structure, an expansion function to generate new nodes from existing ones, a ranking between nodes, and a function to determine if a node is final.

A node in the tree can be represented as the state in section 4.1 and eq. (4.1) can be used to determine if a state is final. We also know that a new state s' derived by s by applying a feasible insertion p can be computed as in definition 4.5. This state expansion procedure, with the exception of empty insertions, will generate new states in our tree which will add a positive number of bins or packed items to the solution so, eventually, it will generate a final state.

If the starting state for the search is feasible every new state generated will be feasible and if a final state is found it will be feasible (proposition 4.1). We also note that starting from state s the time complexity to compute feasible insertions can be lower than the complexity required to update the structures that will be used for further expansions (AABB Tree insertion and balancing, memory cloning, etc.) so we modified the standard BS algorithm to separate the expansion phase from the commit phase. As noted in section 4.1.3, since by evaluating different insertions on different states it is possible to end up having two equal states, a filtering mechanism should be introduced. During each iteration, it is possible to keep the hashes of the best scoring selected states in a HashSet

and discard new states with the same hash.

Given a set of initial states  $S^0$  and the number of best states to expand at each iteration k, the described BS can be represented by algorithm 2. As observed in observation 4.2, it's possible to start the search from  $S^0 = \{s_e\}$ .

```
Algorithm 2: Beam search
```

```
input : S^0, k
output: s_{best}
S^t \leftarrow S^0
S_{final} \leftarrow \emptyset
repeat
     S^{t+1} \leftarrow Expand(S^t) (algo. 3)
     S_{final} \leftarrow S_{final} \cup \{s \in S^{t+1} : IsFinal(s)\} \text{ (def. 4.2)}
     S^{t+1} \leftarrow S^{t+1} \setminus S_{final}
     S^{t+1} \leftarrow Sort(S^{t+1}) \text{ (sec. 4.2.1)}
     i \leftarrow 0
     seen \leftarrow \emptyset
     forall s \in S^{t+1} do
           if s.hash \in seen then
                 continue
           S^t \leftarrow S^t \cup Commit(s) \text{ (algo. 1)}
          seen \leftarrow seen \cup \{s.hash\}
i \leftarrow i + 1
if i > k then
     end
until S^t \neq \emptyset
S_{final} \leftarrow Sort(S_{final})
return first element of S_{final}
```

**State Expansion** An expansion of a state s can be seen as a new set of states  $S_{new}$  derived by a set of feasible insertions. In order to determine these insertions, an underlying heuristic is used (described in section 4.3).

The main idea in this phase of the algorithm is to find feasible insertions in all the bins

at the lowest possible height for items that still need to be packed. To reduce the number of possible expansions to evaluate we limit the search to insertions of items with unique shapes. With a similar concept to the one used in section 4.1.3, an hash for each item's dimensions can be computed on the fly or pre-computed as a problem's parameter. Given each item's hash we can then group items that have the same shape. The evaluation of new insertions can then be done with two different approaches:

- **PS**: where we evaluate only the possible insertion of a single item per item type, which would generate insertions of at most 1 item,
- **PM**: where we evaluate the biggest possible insertion of a group of items of the same shape, which would generate insertions of at most the size of the group of items with the same shape.

Creating insertions of groups of similar items is usually used in Pallet Loading Problems (as for ex. Elhedhli et al. [2019]) to create better bases of support for upper layers. With a similar intuition, the idea of placing groups of items of the same shape is to facilitate the creation of uniform planes (not necessarily layers) to use for further insertions.

Given a set of items I and a tolerance  $\beta_s$  we can introduce an algorithm to group them by their shape and produce a set G of tuples (h, I') where h is the hash summurizing the shape of the group and I' is the set of items grouped as in algo. 4. Once items are grouped by shape the best insertion for each class of items can be computed for each open bin. If no insertion is possible in any bin, then the only viable insertion is the bin opening insertion (observation 4.1). The described procedure is detailed in algo. 3, which can be

modified with minor changes to limit the number of items to consider when in PS mode.

```
Algorithm 3: Expand
input : S
output: S_{new}
forall s \in S do
    S_{new} \leftarrow \emptyset
    G \leftarrow GroupByHash(s.U) (algo. 4)
    placed \leftarrow false
    forall (h, I) \in G do
         forall q_b \in s.Q do
              P \leftarrow SPBestInsertion(q_b.Z, I, q_b.T) (section 4.3)
             if P \neq \emptyset then
                  placed \leftarrow true
forall p \in P do
S_{new} \leftarrow S_{new} \cup Next(s, p) \text{ (def. 4.5)}
                  \mathbf{end}
              end
         end
    end
    if placed = false then
         // Open a new bin with index |s.B| (oss. 4.1)
         S_{new} \leftarrow S_{new} \cup Next(s, (|s.B|, \emptyset))
    end
end
return S_{new}
```

#### 4.2.1. Scoring States

In order to sort states, a scoring function needs to be defined over them. Since the scoring of the states is what will influence the final solution the most, parameters that are directly related to minimizing the objective function are selected.

In the proposed solution to handle multiple objective functions, lexicographic ordering is used.

**Definition 4.6.** Let  $f_1(s), f_2(s), f_i(s), \ldots, f_n(s)$  be objective functions ordered by prece-

#### Algorithm 4: Group By Hash

```
input : I
output: G
G \leftarrow \emptyset
forall i \in I do
    generate \leftarrow true
    forall (h, I') \in G do
        if h = hash(w_i, d_i, h_i) then
             generate \leftarrow false
             I' \leftarrow I' \cup i
             break
        end
    end
    if generate = true then
        G \leftarrow G \cup (hash(w_i, d_i, h_i), \{i\})
    end
end
return G
```

dence based on index  $i \in \mathbb{Z}$ , then

$$s < s'$$
 iff  $\exists j \in \mathbb{Z} : \begin{cases} f_j(s) < f_j(s') \\ f_k(s) = f_k(s'), & \forall k \in \mathbb{Z} : 0 \le k < j \end{cases}$ 

Scoring metrics for each state s that we want to evaluate can then be computed in the Next algorithm by considering the contents of the pending insertions and updating each parameter differentially.

The defined ordering utilized is the following:

- $f_1(s) = -|s.B|$ : we prefer states that opened fewer bins.
- $f_2(s) = \operatorname{avgvol}(s)$ : we prefer states that have packed more average volume between bins.
- $f_3(s) = \operatorname{avgcageratio}(s)$ : we prefer states that have better average cage ratio (eq. (3.1)) between bins.

#### 4.3. Support Planes

Support Planes (SP) is a constructive heuristic based on an underlying 2D-BPP heuristic which is used to generate feasible insertions inside a bin starting from a set of items to

pack. Since insertions must be feasible, SP maintains an internal structure to facilitate feasibility checks. The idea at the base of SP is to build a solution to the 3D-BPP by filling 2D planes called *support planes*.

Each support plane is characterized by the tuple  $(z, I_{support}, I_{upper})$  where

- z: is the height of the plane,
- $\bullet$   $I_{support}$ : the set of the items that can offer support to items placed on the plane,
- $I_{upper}$ : the set of items that will be obstacles to potential new items placed on the plane.

Every item placed in the bin can either generate a new support plane or be part of the supporting items of other planes. Items placed above a particular plane, such that  $z_i + h_i > z$ , are considered obstacles and are added to the  $I_{upper}$  set. When evaluating a new possible insertion, given a set of items to place I, SP selects the first feasible insertion starting from the lowest plane by using a modified version of Extreme Point in two dimensions (introduced in Crainic et al. [2008]). Once no more insertions can be made on the lowest available support plane, it's removed from the set of planes. Since insertions always happen in the lowest possible planes, the set of obstacles of those planes is composed of items that have only their top face above the z of the evaluated plane, such that  $z_i \leq z < z_i + h_i$ .

The Extreme Point (EP) heuristic evaluates the placement of rectangles in a plane based on a set of reference points with a best-fit approach. Each rectangle placement generates a new set of reference points which are usually introduced based on the projection of its corner points along the orthogonal axis of the plane. The corner points of an added rectangle r placed in  $(x_r, y_r)$  of dimensions  $(w_r, d_r)$  are the top left corner  $(x_r, y_r + d_r)$  and the bottom right corner  $(x_r + w_r, y_r)$ . In our version of the algorithm, the corner points of each item are introduced without projecting them to increase the likelihood of evaluating placements that verify the support constraint. Placements follow a first-fit approach where the algorithm selects the first point closest to the origin where a rectangle can fit with or without rotations. In order to facilitate the evaluation of reference points with support, we also generate a reference point in the bottom left corner of each item that belongs to the set of supporting items  $I_{support}$ . When a reference point is used for a placement, it is then removed from the pool of reference points. Before evaluating placements, the item to place are ordered based on their area. New planes have the origin of space (0,0) as an available reference point.

Since reference points are usually ordered based on the euclidean distance from the bottom

left corner of the plane and the corner points are usually generated and projected towards the origin of each axis, the placements over one plane are usually biased towards the bottom left corner. To address the problem, we evaluate four instances of EP where each has a different coordinate change applied to every item that moves the plane's origin to each corner of the bin. This addition is based on similar approaches from the literature where it is usually used to more uniformly fill the space (ex. Gajda et al.) and was verified to yield better cage ratio results in our internal testing.

The EP procedure is called for each item to pack on a given plane. In order to produce a valid insertion, every item in the insertion shouldn't overlap each other (as stated in definition 4.4). Since the AABB tree for a given state is shared by each evaluation of a possible insertion, it can't be modified to account for temporary placements of items. This means that we need to keep a temporary AABB tree updated composed of the items that are part of the current insertion T'. We can then define a function that uses the temporary tree and the feasibility function defined in section 4.1.2 to ensure that we are producing a feasible insertion as eq. (4.3).

$$EPCanPack(i, I_{support}, T, T') = IsFeasible(i, I_{support}, T) \land \neg AABBOverlaps(i, T')$$

$$(4.3)$$

A graphical representation of a support plane is shown in fig. 4.1 with the reference points available. In fig. 4.2 the state of two extreme point instances for the bottom left and top left coordinate changes are shown. When a bin is opened the only support plane available is the one on the ground. In the figure different coordinate changes are marked with different colors.

Given eq. (4.3) to check if a considered placement would lead to a feasible insertion, the set of items to pack I, the AABB tree of the currently packed items T and the set of currently available support planes Z. The heuristic that will output the new best possible feasible insertion for the given set of items or an empty object can be summarized in alg. 5.

**Commit Extension** We now describe an extension to *Commit* (algo. 1) to update the structures needed by SP.

When a plane is filled, new insertions become less likely to be feasible. To avoid evaluating planes where no insertion is possible a mechanism to prune dead planes can be introduced.

Since best insertions for a bin are always evaluated by considering lower planes first, if all the insertions in Expand (algo. 3) happened over a  $z_{min}$  then we can safely remove the

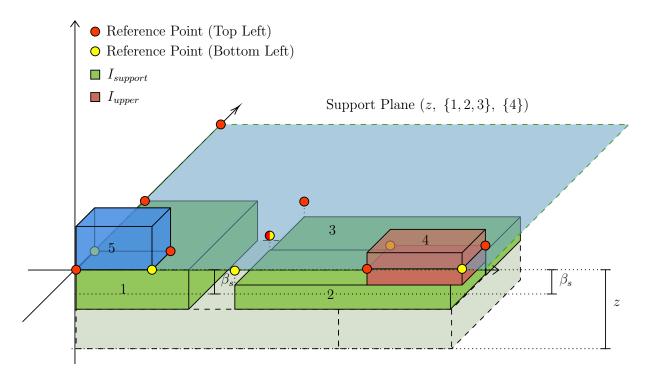


Figure 4.1: Representation of a generic support plane with a placed item

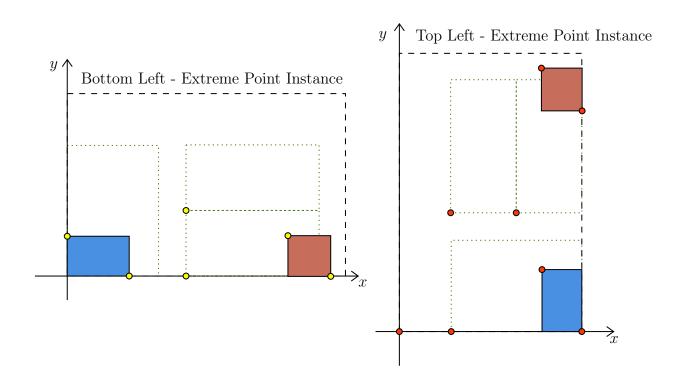


Figure 4.2: Extreme Point instances for some coordinate changes of fig. 4.1

#### Algorithm 5: SP Best Insertion

```
\overline{\text{input}}: Z, I, T
output: p
forall (z, I_{support}, I_{upper}) \in Z do
    P \leftarrow \emptyset
    forall possible coordinate changes do
        p \leftarrow (z, \emptyset)
        T' \leftarrow \text{empty AABB tree}
        //Initialize reference points
        refPoints \leftarrow (0,0)
        forall i \in I_{support} do
          refPoints \leftarrow refPoints \cup \{(x_i, y_i)\}
        end
        forall i \in I_{upper} do
           refPoints \leftarrow refPoints \cup \{(x_i + w_i, y_i), (x_i, y_i + d_i)\}
        end
        sort(refPoints) // Based on euclidean distance from (0,0)
        //Create a feasible insertion for the given items
        forall i \in I do
            //Evaluate first possible placement
            forall (x, y) \in refPoints do
                (x_i, y_i, z_i) \leftarrow (x, y, z)
                if EPCanPlace(i, T, T') then
                    EPInsertRect(p, i, T', refPoints) // alg. 6
                    break
                end
                (w_i, d_i) \leftarrow (d_i, w_i) //Try rotating i
                if EPCanPlace(i, T, T') then
                    EPInsertRect(p, i, T', refPoints) // alg. 6
                    break
                end
                (w_i, d_i) \leftarrow (d_i, w_i) //Restore original i rotation
            end
        end
        if p \neq (z, \emptyset) then
         P \leftarrow P \cup p
        end
    end
    sort(P) //Sorted as in section 4.3.1
    if P \neq \emptyset then
    return first element of P
    end
end
return none
```

#### Algorithm 6: EP Insert Rect

```
input: p, i, T, refPoints
refPoints \leftarrow refPoints \setminus \{(x_i, y_i)\}
refPoints \leftarrow refPoints \cup \{(x_i + w_i, y_i), (x_i, y_i + d_i)\}
sort(refPoints) \text{ // Based on euclidean distance from } (0, 0)
p.I \leftarrow p.I \cup \{i\}
AABBInsert(i, T') \text{ //section 4.1.1}
return
```

opened planes with  $z < z_{min}$  for that bin. Let us introduce a  $z_{min}$  variable carried over in  $q_b$  for each bin, which is updated during the Expand phase with the minimum z of all the insertions on bin b. Once the best states are computed and Commit is called we can then use its value to prune planes in each  $q_b$ . Other operations are also necessary in the Commit algorithm to allow SP to update its data structures accordingly to the insertion.

Given a state s and an insertion p where each packed item  $i \in p.I$  in bin b has  $z_i$  within tolerance of z and the minimum height for the considered bin  $q_b.z_{min}$ . The algorithm which updates the structures for a given bin b is represented by algorithm 7. This new

algorithm can be used as the last step of the Commit algorithm for each  $b \in s'.B$ .

```
Algorithm 7: SP Apply and Filter
input : s, p, z, z_{min}, \beta_s
output: s
q_b \leftarrow (q_i \in s.Q : i = p.b)
//Filter bad planes
q_b.Z \leftarrow q_b.Z \setminus \{(z', I_{support}, I_{upper}) \in q_b.Z : z' < z_{min}\}
//Apply insertion
forall i \in p.I do
    q_b.T \leftarrow InsertAABB(i, q_b.T)
    generate \leftarrow true
    forall (z', I_{support}, I_{upper}) \in q_b.Z do
         //Based on the distance from the top of the item
         dz \leftarrow z' - (z_i + h_i)
        if 0 \le dz \le \beta_s then
             generate \leftarrow false
             I_{support} \leftarrow I_{support} \cup i
         end
         else if dz < 0 then
            I_{upper} \leftarrow I_{upper} \cup i
         end
    end
    if generate then
        q_b.Z \leftarrow q_b.Z \cup (z_i + h_i, \{i\}, \emptyset)
    end
end
```

#### 4.3.1. Scoring Insertions

return s

Similarly to the scoring of states (section 4.2.1), an ordering function is also needed to evaluate different insertions for the same set of items. Given the lexicographic ordering formulation in definition 4.6 a few new statistics can be calculated and stored inside an insertion to help in the evaluation. The parameters used to sort an insertion p are then the following:

•  $f_1(p) = -|p.I|$ : maximize number of items inserted (of the same shape),

- $f_2(p) = -\sum_{i \in p.I} (w_i d_i + w_i d_i h_i)$ : maximize the sum of the area and volume of each packed item,
- $f_3(p) = \max_{i \in p, I} (z_i + h_i)$ : minimize the maximum height of the inserted items,
- $f_4(p) = \text{sum of the supported area of items in } p.I$ : minimize the support area available to the inserted items,
- $f_5(p) =$



### 5 Computational results

In this chapter, in section 5.1, we evaluate the proposed heuristic against the MILP model (3.1), and in section 5.2 against other heuristics from the literature. We then show the effectiveness of our approach for our case study in section 5.3. All the tests were run on a desktop computer with an AMD Ryzen-7 5800x processor with 8 cores at 3.8 GHz and 32GB of DDR4 system RAM with Windows 10. The algorithm was implemented in Java 11, and the model was run using the python APIs from CPLEX Optimization Studio 22.1.0. In every test, CPLEX was used with a maximum runtime of 1 hour. Each evaluation against the heuristic lists both operational modes described in section 4.2 listed as "PM" and "PS". All the instances used in each section of this chapter are available at https://github.com/artumino/BinPackingThesis/tree/main/tests/instances. Out of the 100 instances used for our case study experiments, only 80 were freely sharable with the generation procedure also described in section 5.3.

#### 5.1. Model validation

We compared our heuristic to the proposed MILP model of section 3.1 with a single bin and with no limit on the height of the bin (also referred to as the 3D strip packing problem). The heuristic was configured to run without vertex support, using only area support rules for its feasibility checks, and k was set to 200. The configured parameters for the test were  $\alpha_s = 0.7$ ,  $\beta_s = 5$ , and the discretization unit for the model was  $\delta = 10$ . Tests were run on the first generated instance of the class 1 problems from Martello et al. [2000] which we used for literature tests. These classes of problem have a bin base of  $100 \times 100$ . The test were run with an iterative approach by selecting only a limited amount of items from the selected instance, starting from the first item and increasing the number of items to pack by one at each iteration. The problem created with each iteration was saved as a test instance in the same format as the one used for literature tests. All the generated instances are available at https://github.com/artumino/BinPackingThesis/tree/main/tests/instances/model. A python script then loaded each generated instance sequentially and evaluated the solutions from both the MILP problem and the heuristic. Starting from

instance 6, the solution from the previous instance was used to mip start the new one leading to lower execution times.

Table 5.1 shows the obtained  $z_{\rm max}$  value of the heuristic and the MILP solution, the runtime in seconds, and the number of items. Since the underlying problem is NP-Hard, it is shown that starting from instances of size bigger than 8 items; the MILP model becomes too slow for practical use while our heuristic maintains negligible execution time. Due to discretization errors, some of the model instances gave solutions that didn't have the expected amount of support and were marked with an asterisk. The solution to instance number 5 and instance number 7 is also shown in fig. 5.1.

Table 5.1: Comparison with MILP model on limited set of boxes

	MILP	Model	PI	VI	P	S
$\overline{n}$	Max Z	TT(s)	Max Z	TT(s)	Max Z	TT(s)
1	85	0.01	85	0.00	85	0.00
2	85	0.09	85	0.00	85	0.00
3	85	0.24	85	0.00	85	0.00
4	85	0.64	85	0.01	85	0.01
5	85	16.48	85	0.02	85	0.02
6	158*	594.32	158	0.06	158	0.05
7	158*	3,178.00	158	0.07	158	0.08
8	-	-	160	0.10	160	0.08
9	_	-	169	0.09	161	0.10
10	-	-	218	0.12	218	0.13
11	_	-	240	0.12	240	0.12
12	_	-	310	0.13	316	0.16
13	_	-	310	0.15	333	0.18
14	_	-	310	0.20	333	0.22
15	_	-	406	0.21	397	0.27
16	_	-	435	0.23	452	0.36
17	_	-	429	0.27	515	0.41
18	_	-	432	0.32	522	0.47
19	_	-	458	0.35	522	0.55
20	-	=	539	0.37	564	0.62

<sup>\*</sup> Some boxes had lower support than expected due to discretization errors within the  $0.65 \le \alpha_s \le 0.7$  range.

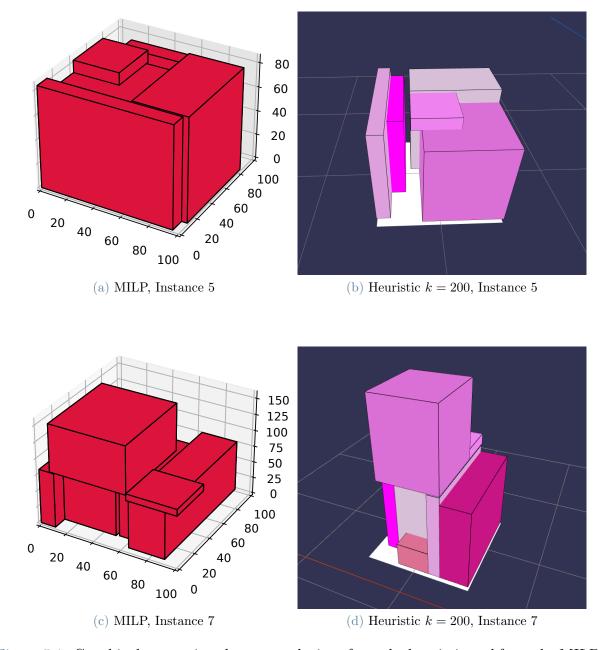


Figure 5.1: Graphical comparison between solutions from the heuristic and from the MILP model

#### 5.2. Literature results

The heuristic was also evaluated against instances from the literature defined by Martello et al. [2000]. Since these instances were designed for heuristics without the vertical support constraint and orthogonal rotations, we ran the experiments with a relaxed version of our heuristic. The heuristic was configured to ignore the support constraint with  $\alpha_s = 0$  and  $\beta_s = 1$ . We also disabled orthogonal rotations and stopped scoring insertions based on the support area available (as described in section 4.3.1).

The literature instances are divided into classes from 1 to 8, with each class having a different bin size and various distributions of types of items. Instances were generated with the C++ instance generator provided by Martello et al. [2000] at http://hjemmesider.diku.dk/~pisinger/new3dbpp/test3dbpp.c which allows the generation of problem instances with a given problem class and number of items to use. We generated 10 instances for each pair of problem class and number of items  $n \in \{50, 100, 150, 200\}$  for a total of 320 instances.

In table 5.2 we compare the average number of opened bins across 10 instances for each problem class and n number of items combinations. The results are then compared to the most effective methods from the literature ordered by publishing date and listed as TS3 [Lodi et al., 2002], GLS [Faroe et al., 2003], GASP [Crainic et al., 2009], GVND [Parreño et al., 2010], EHGH2 [Hifi et al., 2014], BRKGA [Gonçalves and Resende, 2013], BRKGA-VD [Zudio et al., 2018]. It is noted that values for other heuristics are reported as in their publications, and our generated instances weren't the same ones which, as indicated in Hifi et al. [2014], could have different optimal values. The best values of all the heuristics are marked in bold. Best scoring values across different configurations of our heuristic are marked in italic instead. Results show an average gap of 4.1% compared to the average value across the other heuristics and an average gap of 5.32% with respect to the best performing one.

In table 5.3 we give an approximate comparison between the average execution time of our heuristic with respect to BRKGA-VD. Execution times for BRKGA-VD were normalized by comparing directly the floating-point operations per second of the processors used, which resulted in dividing BRKGA-VD execution times by a normalization term of 9.3. The values presented are the times averaged across 8 classes of problems divided according to the size of the instance and the heuristic configuration. In the last column, we also included the average gap of each configuration of the heuristic with respect to the values of BRKGA-VD.

Table 5.2: Literature results for k = 50

BRKGA-VD		13.4	26.6	36.3	50.8	13.8	25.5	36.6	49.4	13.3	25.9	37.5	49.8	29.4	58.9	8.98	118.8	8.3	15	19.9	27.1	9.7	18.9	29	37.3	7.4	12.2	15.2	23.4	9.2	18.8	23.6	29.3
BRKGA		13.4	26.6	36.4	50.8	13.8	25.6	36.6	49.4	13.3	25.9	37.5	49.8	29.4	59	8.98	118.8	8.3	15	20.1	27.1	9.7	18.9	29	37.3	7.4	12.2	15.3	23.4	9.2	18.9	23.6	29.3
GVN		13.4	26.6	36.4	50.9	13.8	25.7	36.9	49.4	13.3	26	37.6	20	29.4	59	8.98	118.8	8.3	15	20.4	27.1	9.8	19	29.5	37.4	7.4	12.5	16	23.5	9.2	18.9	24.1	29.8
EHGH2		13.8	27.6	39.8	50.6	1	1	ı	1	ı	ı	ı	ı	29.4	59.5	90.4	119	7.9	14.6	21.5	29.6	11.8	19.2	29.8	38.7	7.4	13.5	18.2	24.1	9.4	18.9	56	35.8
GASP		13.4	26.9	37	51.6	1	1	1	1	1	ı	1	1	29.4	59	8.98	118.8	8.4	15.1	20.6	27.7	9.6	19.1	29.5	38	7.5	12.7	16.6	24.2	9.3	19	24.8	31.1
GLS		13.4	26.6	37	51.2	1	1	ı	ı	1	ı	1	1	29.4	59	8.98	119	8.3	15.1	20.2	27.2	8.6	19.1	29.4	37.7	7.4	12.3	15.8	23.5	9.2	18.9	23.9	29.9
TS3		13.4	26.6	36.7	51.2	13.8	25.7	37.2	50.1	13.3	56	37.7	50.5	29.4	59	86.8	118.8	8.4	15	20.4	27.6	9.6	19.1	29.4	37.7	7.5	12.5	16.1	23.9	9.3	18.9	24.1	30.3
$\mathbf{PS}$	k = 50	14	27.7	37.9	52.7	14.8	26.7	39	51.7	13.9	27.3	39	51.2	29.7	59.2	87.7	119.5	9.8	15.6	21.4	28.4	10.3	19.7	30.2	38.5	9.7	13.2	16.8	24.7	9.7	20	25.8	31.2
$_{ m PM}$	k = 50	14.10	28	38.4	53	14.6	26.6	38.3	51	13.9	27.8	39.2	51.8	29.7	59.2	97.8	119.5	8.6	16	21.7	29	10	19.8	30.3	38.9	7.8	13.2	17.1	24.9	6.6	9.61	25.7	31.6
u		20	100	150	200	50	100	150	200	50	100	150	200	20	100	150	200	50	100	150	200	50	100	150	200	50	100	150	200	50	100	150	200
Class		1				2				3				4				ಬ				9				2				$\infty$			

Table 5.3: Average execution time of literature results with bin gap

He	uristic		Execution	n Time (s	s)	Bin Gap %
		n = 50	n = 100	n = 150	n = 200	
$\mathbf{PM}$	k = 1	0.03	0.11	0.28	0.54	5.82
	k = 5	0.08	0.38	1.00	2.09	5.56
	k = 10	0.15	0.73	1.93	4.00	5.54
	k = 20	0.29	1.40	3.77	7.71	5.30
	k = 50	0.70	3.50	9.39	19.59	5.19
PS	k = 1	0.05	0.18	0.50	1.05	5.61
	k = 5	0.12	0.72	2.10	4.62	5.26
	k = 10	0.23	1.38	4.11	8.95	5.19
	k = 20	0.46	2.67	8.21	17.64	4.98
	k = 50	1.12	6.45	20.39	43.50	4.75
BRK	GA-VD	1.85	8.69	20.53	39.85	0.00

#### 5.3. Case study results

Case study experiments were conducted on a series of problem instances that were divided between 20 real-world instances and 80 generated instances composed of items sampled from a population of real-world products. Each instance was anonymized and converted to a format similar to the one used for the literature tests thanks to a Rust program available at https://github.com/artumino/BinPackingThesis/tree/main/additional/testConverter. Support parameters for the heuristic were set to  $\alpha_s = 0.7$  and  $\beta_s = 10$  with both area and vertex support enabled. All dimensions of the bin, items, and tolerances are assumed to be in millimeters. Different values of  $k \in \{1, 5, 10, 20, 50, 100, 200\}$  were tested as well as both placement modes.

Each generated instance is composed of a random number of n items sampled from a given range of possible instance sizes. All generated instances had a bin of standard size  $800 \times 1200 \times 2000$ . We identified four ranges of interest and generated 20 instances for each range as follows:

- Class 1-20: a class of instances with the target sizes for our case-study  $n \in [70, 100]$
- Class 21-40: a class of small sized instances with number of items  $n \in [50, 70]$
- Class 41-60: a class of medium sized instances with number of items  $n \in [70, 120]$
- Class 61-80: a class of big instances with number of items  $n \in [120, 200]$

Given an input n (the size of the test instance), the generation procedure uniformly sampled an item type from a population of real-world products. The quantity of items of that type to add to the test instance was then sampled from a normal distribution  $\mathcal{N}(\mu=4.6,\sigma=1.8)$  with parameters calculated from the real-world instances. The sampled quantity was then floored to be an integer value and clamped to avoid generating more items than n. This uniform sampling of item types was done until the instance was composed of n items.

Real-world instances are listed as Class 81-100 and have a variable number of items between [25, 345], a variable bin size (although similar to the one used for the generated instances), and a variable number of items of the same type. Some instances were homogeneous with only a few unique items, and some were heterogeneous with every item of a different type. An example of real-world instances is shown in fig. 5.2 where items of the same shape are marked with the same color.

Table 5.3 shows the average results over the 20 instances per class, divided by each configuration of the heuristic with different values of k. The results shown include the

total execution time in milliseconds (TT), the number of opened bins (B), and the average cage ratio between the opened bins (CR). It is clear that although the "PS" method had better results when dealing with a relaxed version of the problem, grouping items by type shows considerable improvements under all measured metrics when taking vertical support into account. Most of the configurations lead to an average cage ratio of more than 70%, which was the target value for our case study. It is also possible to see that increasing the value of k improves the quality of the solutions, on average, at the expense of a higher execution time. By doing a case-by-case analysis of each experiment, we discovered that increasing k can temporarily worsen the solution in some instances. A further study of the problematic instances highlighted that the current greedy scoring mechanism of the states leads to cutting out good solutions too early. Further improvements are proposed in chapter 6.

Table 5.4: Summary of case study tests

Instanc	e	]	PS		I	PM	
		TT (ms)	B	CR	TT (ms)	B	CR
Class 1-20	k = 1	187.25	1.15	64.10	54.95	1.05	70.69
	k=5	489.40	1.05	70.38	111.75	1.00	75.36
	k = 10	861.30	1.05	71.94	182.20	1.00	75.77
	k = 20	1,588.15	1.05	72.04	308.45	1.00	76.60
	k = 50	3,896.40	1.05	73.07	690.80	1.00	76.95
	k = 100	7,789.90	1.00	75.45	1,204.35	1.00	78.46
	k = 200	15,817.20	1.05	74.99	$2,\!192.75$	1.00	78.27
Class 21-40	k = 1	50.90	1.00	68.21	17.80	1.00	73.66
n = [50, 70]	k=5	138.40	1.00	71.92	39.20	1.00	74.78
	k = 10	253.10	1.00	73.15	74.95	1.00	75.28
	k = 20	483.85	1.00	73.86	124.30	1.00	76.46
	k = 50	$1,\!193.55$	1.00	74.77	288.50	1.00	77.02
	k = 100	$2,\!358.50$	1.00	75.08	535.30	1.00	77.11
	k = 200	4,769.85	1.00	76.69	1,033.00	1.00	78.64
Class 41-60	k = 1	292.35	1.30	65.62	60.55	1.25	71.34
n = [70, 120]	k=5	1,025.65	1.30	67.97	172.35	1.30	72.53
	k = 10	1,910.60	1.30	68.46	304.25	1.25	72.04
	k = 20	3,666.40	1.30	68.68	571.90	1.25	74.01
	k = 50	7,649.95	1.25	71.32	$1,\!152.40$	1.25	75.25
	k = 100	$15,\!848.15$	1.25	72.90	1,956.55	1.20	75.67
	k = 200	32,420.40	1.25	73.29	3,472.50	1.20	76.10
Class 61-80	k=1	1,371.00	2.20	64.68	158.00	2.05	69.11
n = [120, 200]	k=5	5,751.95	2.15	66.66	531.80	1.95	71.31
	k = 10	9,040.85	2.05	68.56	1,033.15	1.90	72.69
	k = 20	$19,\!116.60$	2.15	67.81	1,881.70	1.90	73.84
	k = 50	52,937.40	2.05	69.94	3,744.70	2.00	71.25
	k = 100	$98,\!271.55$	2.10	70.04	7,010.65	1.90	73.80
	k = 200	170,191.55	2.00	71.15	13,544.15	1.90	75.01
Class 81-100	k=1	217.85	1.20	66.74	34.60	1.20	68.68
	k = 5	582.30	1.20	69.03	71.00	1.20	71.41
	k = 10	1,071.75	1.20	69.65	129.95	1.20	72.00
	k = 20	2,013.95	1.20	71.52	218.40	1.20	71.97
	k = 50	5,338.20	1.20	71.44	523.40	1.20	72.57
	k = 100	10,402.95	1.20	72.68	995.00	1.20	71.74
	k = 200	21,525.50	1.20	73.30	2,086.50	1.15	73.95
Global Avg	k = 1	423.87	1.37	65.87	65.18	1.31	70.70
	k=5	1,597.54	1.34	69.19	185.22	1.29	73.08
	k = 10	2,627.52	1.32	70.35	344.90	1.27	73.56
	k = 20	5,373.79	1.34	70.78	620.95	1.27	74.57
	k = 50	14,203.10	1.31	72.11	1,279.96	1.29	74.61
	k = 100	26,934.21	1.31	73.23	2,340.37	1.26	75.36
	k = 200	48,944.90	1.30	73.89	4,465.78	1.25	76.39

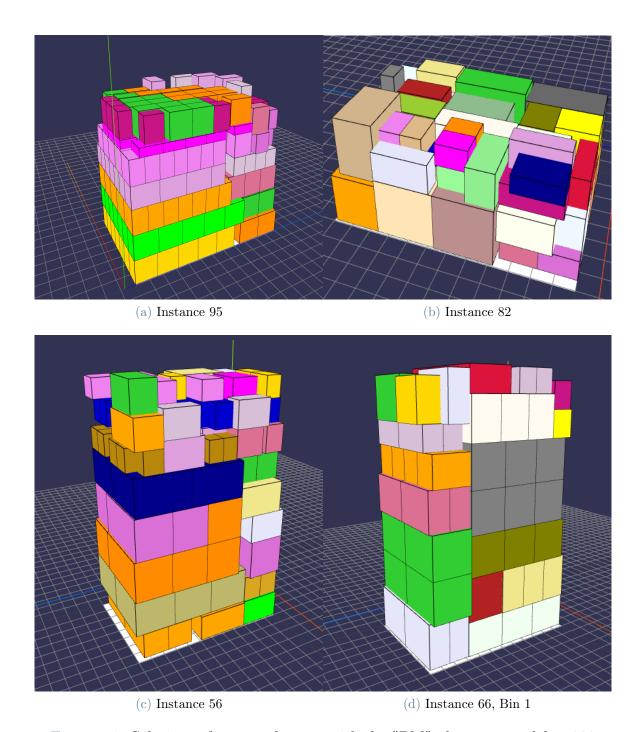


Figure 5.2: Solutions of case study tests with the "PM" placement and k=200

# 6 Conclusions and future developments

A final chapter containing the main conclusions of your research/study and possible future developments of your work have to be inserted in this chapter.



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## $\mathbf{A} \mid \mathbf{A}$

Table A.1: Case study results 1-5

Iı	nstance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
1	k=1	403	1	69.54	218	1	69.82
	k=5	384	1	70.9	157	1	74.64
	k = 10	502	1	71.47	151	1	74.64
	k = 20	786	1	71.47	187	1	73.33
	k = 50	1732	1	71.47	357	1	74.26
	k = 100	3524	1	71.47	613	1	76.54
	k = 200	6892	1	74.71	1020	1	74.64
2	k = 1	266	2	48.2	67	1	77.19
	k=5	835	1	78.58	196	1	84.69
	k = 10	1537	1	78.58	311	1	86.65
	k = 20	2045	1	83.22	607	1	87.59
	k = 50	5233	1	83.22	1706	1	87.84
	k = 100	11422	1	83.22	3226	1	86.94
	k = 200	22911	1	83.22	3860	1	85.87
3	k = 1	169	1	73.36	62	1	65.48
	k=5	335	1	73.36	104	1	73.31
	k = 10	532	1	73.36	141	1	72.73
	k = 20	1003	1	73.36	245	1	74.86
	k = 50	2621	1	73.46	457	1	74.51
	k = 100	5209	1	73.46	897	1	75.02
	k = 200	10781	1	74.2	1676	1	78.9
4	k = 1	384	1	53.7	57	1	79.2
	k=5	1048	1	59.27	153	1	79.91
	k = 10	1934	1	59.27	203	1	76.37
	k = 20	3754	1	59.27	313	1	79.44
	k = 50	9266	1	65.04	754	1	82.18
	k = 100	18445	1	72.44	1467	1	82.18
	k = 200	36636	1	72.44	2956	1	82.18
5	k = 1	52	1	67.48	25	1	74.44
	k=5	192	1	73.22	75	1	76.16
	k = 10	324	1	73.22	104	1	69.76
	k = 20	641	1	73.22	144	1	69.18
	k = 50	1613	1	73.22	255	1	68.65
	k = 100	3466	1	73.22	518	1	68.65
	k = 200	7149	1	73.22	1050	1	68.74

Table A.2: Case study results 6-10

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT (ms)	B	CR	TT (ms)	B	CR
6	k = 1	357	2	35.53	76	1	78.78
	k=5	939	1	65.88	196	1	79.74
	k = 10	1638	1	74.23	419	1	82.46
	k = 20	3257	1	73.74	624	1	80.73
	k = 50	8533	1	73.74	1295	1	80.52
	k = 100	16594	1	75.36	2019	1	78.53
	k = 200	33658	1	75.36	3925	1	77.35
7	k = 1	308	1	62.38	32	1	68.32
	k = 5	774	1	62.38	98	1	71.36
	k = 10	1052	1	69.06	148	1	81.03
	k = 20	2003	1	69.06	299	1	82.35
	k = 50	4828	1	71.32	697	1	79.09
	k = 100	10009	1	71.32	1138	1	82.12
	k = 200	19931	1	71.32	2289	1	82.12
8	k = 1	50	1	74.2	36	1	79.27
	k = 5	142	1	74.2	46	1	78.78
	k = 10	240	1	76.51	66	1	83.85
	k = 20	472	1	80.77	126	1	83.85
	k = 50	1196	1	82.12	317	1	83.85
	k = 100	2410	1	82.12	617	1	83.85
	k = 200	4844	1	82.12	1212	1	83.85
9	k = 1	188	1	67.28	41	1	69.6
	k = 5	580	1	74.36	135	1	73.26
	k = 10	989	1	74.36	319	1	81.8
	k = 20	1795	1	75.21	364	1	77.87
	k = 50	4573	1	78.8	1377	1	80.34
	k = 100	8641	1	78.8	1557	1	76.19
	k = 200	18028	1	78.8	3058	1	76.07
10	k = 1	37	1	75.91	24	1	72.18
	k=5	229	1	76.34	65	1	74.73
	k = 10	321	1	76.34	102	1	74.73
	k = 20	645	1	76.34	186	1	74.73
	k = 50	1641	1	76.34	413	1	80.24
	k = 100	3177	1	76.34	685	1	79.76
	k = 200	6562	1	76.34	1376	1	79.76

Table A.3: Case study results 11-15

In	stance	P	$\mathbf{S}$		P	M	
		TT $(ms)$	B	CR	TT (ms)	B	CR
11	k=1	83	1	66.82	26	1	69.88
	k=5	227	1	66.82	88	1	73.04
	k = 10	437	1	73.04	94	1	73.04
	k = 20	901	1	73.04	182	1	73.73
	k = 50	2163	1	74.9	374	1	72.55
	k = 100	4271	1	75.09	656	1	70.51
	k = 200	8965	1	75.09	1338	1	73.61
12	k = 1	290	2	54.85	41	2	38.76
	k=5	905	2	49.36	149	1	79.67
	k = 10	1746	2	49.36	153	1	77.74
	k = 20	3048	2	40.42	304	1	76.43
	k = 50	6768	2	40.91	526	1	77.53
	k = 100	13867	1	73.25	1054	1	79.32
	k = 200	29292	2	42.83	2136	1	79.32
13	k = 1	161	1	53.61	23	1	68.76
	k=5	333	1	69.77	62	1	72.32
	k = 10	585	1	69.77	120	1	73.12
	k = 20	1140	1	70.64	156	1	64.05
	k = 50	2821	1	70.64	420	1	65.88
	k = 100	5610	1	70.64	833	1	73.76
	k = 200	11427	1	75.46	1119	1	72.44
14	k = 1	209	1	66.77	30	1	70.43
	k=5	512	1	66.77	71	1	69.51
	k = 10	959	1	71.72	229	1	80.74
	k = 20	1773	1	71.72	442	1	73.78
	k = 50	4093	1	72	993	1	78.03
	k = 100	8228	1	72	1915	1	77.62
	k = 200	16602	1	75.58	2885	1	74.15
15	k=1	216	1	79.47	74	1	78.65
	k=5	710	1	79.47	161	1	66.78
	k = 10	1415	1	80.62	245	1	70.17
	k = 20	2661	1	80.62	365	1	77.37
	k = 50	6673	1	80.62	865	1	80.52
	k = 100	12879	1	80.62	1530	1	85.66
	k = 200	25418	1	80.62	3552	1	85.66

Table A.4: Case study results 16-20

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT~(ms)	B	CR	TT $(ms)$	B	CR
16	k = 1	114	1	68.8	125	1	80.6
	k = 5	471	1	71.42	139	1	76.27
	k = 10	808	1	71.42	265	1	76.27
	k = 20	1529	1	72.13	473	1	78.77
	k = 50	3901	1	72.92	1081	1	78.77
	k = 100	7624	1	76.33	1654	1	79.27
	k = 200	15602	1	76.33	3217	1	78.91
17	k = 1	98	1	71.2	27	1	73.37
	k = 5	263	1	77.41	61	1	71.09
	k = 10	535	1	77.41	148	1	72.96
	k = 20	1014	1	77.41	276	1	76
	k = 50	2540	1	78.54	616	1	75.31
	k = 100	4890	1	78.54	989	1	79.99
	k = 200	10395	1	78.54	1790	1	79.92
18	k = 1	108	1	60.55	36	1	69.39
	k = 5	244	1	75.18	59	1	80.2
	k = 10	434	1	75.18	127	1	78
	k = 20	801	1	75.18	204	1	78
	k = 50	1957	1	77.61	376	1	78.85
	k = 100	3807	1	77.61	796	1	78.85
	k = 200	7824	1	80	1575	1	77.54
19	k = 1	113	1	67.04	52	1	66.58
	k = 5	330	1	77.57	133	1	77.82
	k = 10	623	1	77.57	172	1	59.29
	k = 20	1289	1	77.57	435	1	77.44
	k = 50	2977	1	77.57	589	1	74.24
	k = 100	6064	1	77.57	1235	1	83.16
	k = 200	12258	1	78.13	2461	1	83.16
20	k = 1	139	1	65.36	27	1	63
	k = 5	335	1	65.36	87	1	73.91
	k = 10	615	1	66.36	127	1	70.1
	k = 20	1206	1	66.36	237	1	72.51
	k = 50	2799	1	66.92	348	1	65.81
	k = 100	5661	1	69.53	688	1	71.21
	k = 200	11169	1	75.42	1360	1	71.21

Table A.5: Case study results 21-25

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT (ms)	B	CR	TT $(ms)$	B	CR
21	k=1	33	1	67.44	18	1	77.23
	k=5	97	1	75.35	38	1	71.08
	k = 10	166	1	75.35	60	1	72.69
	k = 20	298	1	76.28	108	1	71.65
	k = 50	741	1	76.28	173	1	69.42
	k = 100	1399	1	76.28	349	1	69.42
	k = 200	2870	1	76.28	692	1	71.4
22	k = 1	29	1	72.11	9	1	72.94
	k=5	69	1	73.29	26	1	74.94
	k = 10	141	1	74.21	50	1	74.14
	k = 20	277	1	74.94	80	1	74.65
	k = 50	706	1	74.94	184	1	75.91
	k = 100	1385	1	78.81	354	1	75.91
	k = 200	2802	1	78.81	716	1	75.91
23	k=1	34	1	63.84	13	1	81.33
	k=5	94	1	73.15	31	1	78.01
	k = 10	173	1	75.99	57	1	77.42
	k = 20	329	1	75.99	84	1	81.09
	k = 50	808	1	76.28	211	1	83.06
	k = 100	1594	1	76.28	381	1	83.06
	k = 200	3164	1	79.14	743	1	84.51
24	k=1	26	1	73.86	8	1	73.12
	k=5	65	1	75.64	23	1	73.12
	k = 10	110	1	79.19	40	1	78.76
	k = 20	207	1	79.45	77	1	77
	k = 50	511	1	81.14	173	1	70.35
	k = 100	1076	1	81.14	349	1	70.35
	k = 200	2148	1	81.14	682	1	79.63
25	k=1	82	1	70.7	37	1	71.53
	k=5	229	1	70.7	99	1	69.62
	k = 10	431	1	70.7	181	1	69.62
	k = 20	816	1	70.7	283	1	78.27
	k = 50	2005	1	70.7	462	1	75.37
	k = 100	4011	1	71.74	933	1	75.37
	k = 200	8134	1	72.09	1759	1	75.37

Table A.6: Case study results 26-30

In	stance	P	$\mathbf{S}$		P	M	
		TT $(ms)$	B	CR	TT (ms)	B	CR
26	k = 1	35	1	71.69	16	1	73.01
	k = 5	102	1	75.92	26	1	77.99
	k = 10	194	1	75.92	49	1	76.17
	k = 20	400	1	75.92	68	1	72.31
	k = 50	1008	1	75.92	161	1	73.89
	k = 100	2126	1	76.05	327	1	73.89
	k = 200	4295	1	76.05	644	1	73.89
27	k = 1	63	1	66.47	22	1	76.56
	k = 5	164	1	70.9	38	1	77.73
	k = 10	276	1	70.9	59	1	72.99
	k = 20	522	1	70.9	105	1	77.81
	k = 50	1291	1	71.76	249	1	77.81
	k = 100	2563	1	71.76	483	1	77.81
	k = 200	5463	1	77.81	947	1	77.81
28	k = 1	55	1	68.54	17	1	77.78
	k = 5	136	1	68.54	36	1	78.32
	k = 10	236	1	70.2	59	1	79.3
	k = 20	429	1	73.5	103	1	83.47
	k = 50	1096	1	73.5	272	1	83.95
	k = 100	2151	1	73.5	451	1	83.95
	k = 200	4486	1	74.86	931	1	86.45
29	k = 1	48	1	73.14	17	1	73.85
	k = 5	144	1	75.49	41	1	74.03
	k = 10	244	1	79.77	68	1	76.69
	k = 20	462	1	79.77	132	1	77.94
	k = 50	1104	1	81.33	459	1	80.83
	k = 100	2230	1	81.33	706	1	84.8
	k = 200	4511	1	84.64	1425	1	84.8
30	k = 1	25	1	72.31	8	1	75.76
	k = 5	111	1	72.31	18	1	75.63
	k = 10	199	1	76.44	34	1	75.63
	k = 20	349	1	76.44	71	1	75.76
	k = 50	946	1	76.44	163	1	80.23
	k = 100	1865	1	76.57	317	1	80.23
	k = 200	3472	1	79.56	645	1	82.23

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Table A.7: Case study results 31-35

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT (ms)	B	CR	TT $(ms)$	B	CR
31	k=1	37	1	59.65	14	1	74.05
	k=5	106	1	71.6	38	1	72.43
	k = 10	191	1	72.36	61	1	72.43
	k = 20	365	1	72.36	103	1	73.48
	k = 50	918	1	75.08	247	1	80.34
	k = 100	1745	1	75.08	406	1	77.23
	k = 200	3442	1	77.46	798	1	78.02
32	k = 1	61	1	65.02	24	1	69.44
	k=5	148	1	72.09	30	1	78.06
	k = 10	253	1	73.71	45	1	72.09
	k = 20	515	1	73.71	83	1	72.09
	k = 50	1229	1	73.71	214	1	72.09
	k = 100	2481	1	73.71	425	1	72.09
	k = 200	5037	1	73.71	850	1	72.37
33	k=1	106	1	71.14	40	1	79.25
	k=5	239	1	75.74	64	1	78.21
	k = 10	462	1	75.74	120	1	78.21
	k = 20	854	1	78.73	192	1	78.21
	k = 50	2130	1	78.73	412	1	83.68
	k = 100	4239	1	78.73	837	1	83.68
	k = 200	8519	1	80.04	1685	1	83.68
34	k=1	36	1	61.8	12	1	62.54
	k=5	95	1	64.99	50	1	69.19
	k = 10	170	1	64.99	78	1	73.28
	k = 20	321	1	67.87	150	1	73.28
	k = 50	735	1	73.08	250	1	75.11
	k = 100	1390	1	73.08	504	1	75.11
	k = 200	2791	1	79.15	868	1	72.67
35	k=1	36	1	69.35	13	1	69.86
	k=5	106	1	69.35	37	1	71.2
	k = 10	253	1	72.43	81	1	71.2
	k = 20	480	1	74.53	85	1	73.06
	k = 50	1277	1	74.58	188	1	71.65
	k = 100	2378	1	74.58	373	1	71.65
	k = 200	4929	1	74.58	755	1	71.65

Table A.8: Case study results 36-40

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
36	k = 1	121	1	66.81	28	1	75
	k = 5	343	1	66.81	53	1	73.69
	k = 10	618	1	66.81	180	1	78.01
	k = 20	1136	1	67.11	291	1	82.68
	k = 50	2664	1	71.94	711	1	76.98
	k = 100	5253	1	73.12	1223	1	80.92
	k = 200	10658	1	75.67	2579	1	81.79
37	k = 1	44	1	73.94	13	1	68.3
	k = 5	106	1	73.94	36	1	71.96
	k = 10	184	1	73.94	92	1	74.65
	k = 20	384	1	73.94	124	1	76.03
	k = 50	909	1	73.94	270	1	76.34
	k = 100	1883	1	73.94	461	1	68.16
	k = 200	3836	1	73.94	907	1	79.57
38	k = 1	39	1	70.69	17	1	74.76
	k = 5	132	1	70.69	43	1	77.39
	k = 10	259	1	70.69	83	1	77.39
	k = 20	522	1	71.28	160	1	77.39
	k = 50	1289	1	72.24	396	1	77.39
	k = 100	2606	1	72.24	950	1	78.95
	k = 200	5212	1	72.24	1208	1	79.17
39	k = 1	24	1	62.25	7	1	76.42
	k = 5	71	1	69.91	14	1	79.74
	k = 10	121	1	71.76	23	1	79.74
	k = 20	230	1	71.76	47	1	80.77
	k = 50	559	1	71.76	110	1	80.77
	k = 100	1065	1	71.76	216	1	80.77
	k = 200	2097	1	74.15	444	1	80.77
40	k = 1	84	1	63.4	23	1	70.51
	k = 5	211	1	71.97	43	1	73.19
	k = 10	381	1	71.97	79	1	75.09
	k = 20	781	1	71.97	140	1	72.27
	k = 50	1945	1	71.97	465	1	75.22
	k = 100	3730	1	71.97	661	1	78.91
	k = 200	7531	1	72.51	1382	1	81.13

Table A.9: Case study results 41-45

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
41	k = 1	326	1	68.36	38	1	70.62
	k = 5	697	1	74.25	104	2	52.93
	k = 10	1062	1	75.63	122	1	74.21
	k = 20	1948	1	77.68	262	1	78.73
	k = 50	4790	1	77.68	668	1	74.45
	k = 100	10170	1	79.15	1062	1	77.1
	k = 200	20996	1	79.15	2013	1	78.91
42	k = 1	149	1	70.28	20	1	67.43
	k = 5	479	1	75.83	108	1	68.59
	k = 10	849	1	75.83	214	1	73.76
	k = 20	1623	1	75.83	374	1	75.83
	k = 50	4004	1	75.83	907	1	81.2
	k = 100	8093	1	75.83	1923	1	77.36
	k = 200	16798	1	75.83	2991	1	77.3
43	k = 1	174	2	64.74	96	2	65.13
	k = 5	1628	2	71.89	370	2	64.66
	k = 10	3028	2	71.89	515	2	58.88
	k = 20	6518	2	70.91	1089	2	67.08
	k = 50	9427	2	68.02	2335	2	80.84
	k = 100	21206	2	71.12	3015	2	76.47
	k = 200	67001	2	67.51	5429	2	77.53
44	k = 1	367	1	61.69	61	1	71.18
	k=5	868	1	69.72	205	1	83
	k = 10	1506	1	69.72	310	1	78.48
	k = 20	3062	1	69.72	760	1	76.04
	k = 50	7259	1	69.72	1567	1	80.62
	k = 100	14367	1	69.72	3204	1	81.5
	k = 200	29580	1	69.72	5594	1	80.33
45	k = 1	604	2	46.66	65	1	75.62
	k=5	1502	2	44.05	359	1	83.12
	k = 10	2890	2	43.78	529	1	83.12
	k = 20	4877	2	38.4	810	1	78.72
	k = 50	9384	1	76.94	2070	1	83.31
	k = 100	22382	1	76.94	4241	1	86.62
	k = 200	36854	1	79.15	6044	1	85.35

Table A.10: Case study results 46-50

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
46	k = 1	259	2	77.06	78	2	71.7
	k = 5	2706	2	72.32	101	2	66.68
	k = 10	4194	2	70.3	280	2	72.68
	k = 20	8229	2	70.3	456	2	77.02
	k = 50	14847	2	76.33	1201	2	73.15
	k = 100	26144	2	76.15	1841	2	74.16
	k = 200	45738	2	75.98	4028	2	75.2
47	k = 1	395	1	70.04	73	1	72.15
	k = 5	1082	1	70.04	188	1	75.28
	k = 10	2024	1	70.04	439	1	72.72
	k = 20	3741	1	70.04	737	1	78.82
	k = 50	8428	1	70.04	1798	1	78.82
	k = 100	17165	1	72.83	3143	1	78.82
	k = 200	34689	1	72.83	6153	1	78.82
48	k = 1	208	2	63.3	75	2	62.24
	k = 5	1616	2	69.72	179	2	61.82
	k = 10	3395	2	63.35	410	2	54.88
	k = 20	6845	2	62.39	749	2	66.88
	k = 50	7946	2	65.44	913	2	63.9
	k = 100	20583	2	65.15	2056	2	64.02
	k = 200	43066	2	70.5	4014	2	66.03
49	k = 1	152	1	64.08	36	1	79
	k = 5	617	1	69.12	79	1	76.7
	k = 10	1140	1	72.53	128	1	76.11
	k = 20	2039	1	72.53	252	1	79.88
	k = 50	4622	1	74.03	603	1	79.88
	k = 100	8767	1	74.03	1170	1	81.7
	k = 200	16856	1	74.03	2384	1	81.7
50	k = 1	421	1	63.37	63	1	70.85
	k = 5	899	1	67.26	279	1	74.19
	k = 10	1950	1	70.81	283	1	74.19
	k = 20	3077	1	70.81	670	1	67.69
	k = 50	6702	1	70.81	1476	1	74.15
	k = 100	14720	1	72.07	1272	1	67.3
	k = 200	31094	1	72.29	2618	1	67.3

Table A.11: Case study results 51-55

In	stance	P	$\mathbf{S}$		P	M	
		TT $(ms)$	B	CR	TT (ms)	B	CR
51	k=1	199	1	70.66	62	1	71.17
	k=5	1189	1	71.25	157	1	70.5
	k = 10	2375	1	71.25	297	1	69.81
	k = 20	4786	1	71.25	1206	1	71.6
	k = 50	11267	1	71.25	879	1	64.67
	k = 100	20929	1	71.25	1761	1	64.67
	k = 200	41807	1	73.87	3514	1	64.67
<b>52</b>	k = 1	54	1	71.22	22	1	77.21
	k=5	170	1	74.69	51	1	80.62
	k = 10	332	1	74.69	85	1	76.17
	k = 20	589	1	76.01	169	1	78.28
	k = 50	1589	1	76.01	424	1	80.14
	k = 100	3017	1	77.1	517	1	81.3
	k = 200	6764	1	77.1	1030	1	81.3
53	k=1	434	1	63.73	54	1	70.09
	k=5	1510	1	63.73	217	1	75.61
	k = 10	2843	1	63.73	365	1	69.2
	k = 20	5270	1	63.73	544	1	75.31
	k = 50	12437	1	68.54	1198	1	77.54
	k = 100	22733	1	69.71	1561	1	72.15
	k = 200	46766	1	70.13	3089	1	71.75
54	k=1	889	2	71.9	75	2	71.76
	k=5	1611	2	74.52	186	2	77.16
	k = 10	3338	2	74.52	452	2	70.11
	k = 20	7081	2	72.86	771	2	77.55
	k = 50	17401	2	72.55	1609	2	77.67
	k = 100	36080	2	77.76	2773	2	71.73
	k = 200	69866	2	71.95	5305	2	75.45
55	k=1	136	1	58.5	46	1	69.04
	k=5	455	1	70.35	89	1	71.56
	k = 10	786	1	74.32	168	1	71.98
	k = 20	1501	1	78.76	303	1	72.31
	k = 50	3475	1	78.76	748	1	72.31
	k = 100	7132	1	78.76	1376	1	72.53
	k = 200	14863	1	79.02	1909	1	79.6

Table A.12: Case study results 56-60

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
56	k = 1	319	1	63.92	141	1	79.42
	k = 5	828	1	71.46	236	1	77.95
	k = 10	1476	1	74.87	420	1	80.12
	k = 20	2840	1	74.87	550	1	76.63
	k = 50	7310	1	74.87	1478	1	81.85
	k = 100	15072	1	74.87	2233	1	75.5
	k = 200	30574	1	78.73	3703	1	73.29
57	k = 1	249	2	64.23	53	2	55.11
	k = 5	743	2	47.8	137	2	58.35
	k = 10	1343	2	45.86	295	2	48
	k = 20	2089	2	42.54	398	2	48.64
	k = 50	5008	2	44.26	1116	2	54.39
	k = 100	13920	2	53.72	2074	1	82.3
	k = 200	26749	2	51.17	2753	1	82.01
58	k = 1	106	1	65	34	1	77.03
	k = 5	809	1	65	135	1	76.3
	k = 10	1525	1	67.19	195	1	76.3
	k = 20	3043	1	67.99	328	1	74.82
	k = 50	7037	1	67.99	539	1	76.89
	k = 100	14984	1	71.01	1032	1	76.84
	k = 200	29794	1	71.48	2064	1	77.89
59	k = 1	64	1	69.12	54	1	78.11
	k = 5	278	1	69.66	131	1	78.2
	k = 10	658	1	69.66	250	1	77.18
	k = 20	1229	1	75.21	440	1	76.43
	k = 50	3024	1	75.21	643	1	77.6
	k = 100	5983	1	75.21	1248	1	77.6
	k = 200	11839	1	75.21	2491	1	77.6
60	k = 1	342	1	64.54	65	1	71.84
	k = 5	826	1	66.78	136	1	77.47
	k = 10	1498	1	69.14	328	1	82.87
	k = 20	2941	1	71.75	570	1	81.86
	k = 50	7042	1	72.18	876	1	71.62
	k = 100	13516	1	75.64	1629	1	73.71
	k = 200	26714	1	80.19	2324	1	69.89

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Table A.13: Case study results 61-65

In	stance	P	$\mathbf{S}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
61	k = 1	2470	3	61.14	194	2	75.03
	k=5	7566	3	61.46	458	2	79.58
	k = 10	7705	2	71.35	882	2	74.15
	k = 20	30277	3	57.73	2574	2	78.49
	k = 50	41450	2	71.61	4022	2	79.87
	k = 100	69808	3	58.95	6114	2	79.77
	k = 200	197317	2	71.15	13254	2	77.35
62	k=1	2572	2	66.32	179	2	73.37
	k=5	10605	2	69.85	507	2	73.55
	k = 10	17406	2	73.78	1380	2	73.49
	k = 20	45291	2	66.46	2006	2	72.71
	k = 50	44703	2	72.57	6606	2	77.29
	k = 100	147556	2	69.57	7603	2	76.6
	k = 200	103674	2	73.59	20459	2	76.31
63	k=1	1665	2	64.66	269	2	75.39
	k=5	11233	2	63.95	956	2	77.32
	k = 10	13900	2	68.69	1656	2	77.37
	k = 20	28438	2	72.53	2944	2	75.38
	k = 50	99439	2	72.61	9805	2	75.62
	k = 100	71230	2	72.6	15467	2	77.67
	k = 200	137283	2	73.18	12330	2	78.89
64	k=1	2452	2	66.08	156	2	76.31
	k=5	5607	2	71.17	392	2	75.41
	k = 10	4290	2	67.29	713	2	72.47
	k = 20	7240	2	65.83	1005	2	76.43
	k = 50	60548	2	69.7	2428	2	77.74
	k = 100	70161	2	73.64	6411	2	79.81
	k = 200	144912	2	73.64	10006	2	80.02
65	k=1	1391	2	61.23	126	2	62.06
	k=5	8206	2	61.29	482	2	62.92
	k = 10	17117	2	64.36	1116	2	61.67
	k = 20	15367	2	69.79	2358	2	65.05
	k = 50	78715	2	63.81	3023	2	60.12
	k = 100	146277	2	72.45	7925	2	61.3
	k = 200	406884	2	63.72	15111	2	64.17

Table A.14: Case study results 66-70

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
66	k = 1	1904	3	58.8	175	2	81.55
	k = 5	10568	3	67.91	485	2	79.54
	k = 10	5507	3	65.99	1231	2	77.61
	k = 20	11187	3	65.99	1804	2	78.44
	k = 50	119767	3	56.88	3802	2	81.5
	k = 100	256247	3	68.01	6740	2	80.58
	k = 200	222528	2	77.34	13746	2	82.84
67	k = 1	925	2	70.81	122	2	68.56
	k = 5	5226	2	69.78	439	2	66.14
	k = 10	10700	2	65.29	901	2	66.67
	k = 20	10307	2	70.82	1418	2	75.99
	k = 50	48933	2	69.91	2782	2	68.27
	k = 100	72109	2	68.5	6219	2	70.04
	k = 200	80496	2	72.21	13593	2	75.07
68	k = 1	662	2	67.89	266	2	74.12
	k = 5	2206	2	70.69	485	2	71.13
	k = 10	3601	2	70.59	933	2	72.56
	k = 20	6176	2	69.41	3152	2	75.02
	k = 50	21427	2	72.94	3732	2	75.85
	k = 100	46567	2	74.75	5835	2	73.27
	k = 200	136385	2	72.67	13022	2	72.26
69	k = 1	533	2	67.01	164	2	70.51
	k=5	2336	2	66.89	645	2	56.89
	k = 10	3697	2	69.5	906	2	57.8
	k = 20	34601	2	68.7	1629	2	63.27
	k = 50	25976	2	68.5	2795	2	55.69
	k = 100	45713	2	68.21	7779	2	57.47
	k = 200	95060	2	69.61	11836	2	67.42
70	k = 1	706	2	66.92	114	2	48.99
	k = 5	3006	2	66.92	228	2	50.21
	k = 10	9862	2	67.94	923	2	49.66
	k = 20	18979	2	67.95	1259	2	47.25
	k = 50	47210	2	67.95	3296	2	45.48
	k = 100	93287	2	67.94	5671	2	50.66
	k = 200	175227	2	69.96	10166	2	46.7

Table A.15: Case study results 71-75

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
71	k = 1	1937	2	68.46	275	2	78.92
	k=5	6324	2	67.23	923	2	79.06
	k = 10	12072	2	60.76	1845	2	77.33
	k = 20	43571	2	69.7	2488	2	77.21
	k = 50	107498	2	69.7	4843	2	79.95
	k = 100	196533	2	74.01	9836	2	80.56
	k = 200	165421	2	70.67	30888	2	77.79
72	k = 1	3135	2	69.36	180	2	75.19
	k=5	12714	2	70.89	841	2	78.12
	k = 10	13866	2	73.13	1489	2	75.76
	k = 20	17588	2	74.99	2531	2	80.41
	k = 50	63019	2	72.49	4930	2	82.07
	k = 100	99912	2	73.73	8868	2	76.87
	k = 200	202486	2	73.73	15071	2	80.41
73	k = 1	543	2	62.87	106	2	59.24
	k=5	1435	2	61.18	434	2	49.78
	k = 10	2961	2	61.18	912	1	81.44
	k = 20	5741	2	61.18	1491	1	78.06
	k = 50	14454	2	59.95	2519	2	61
	k = 100	48160	2	53.75	3573	1	81.19
	k = 200	55897	2	56.57	16018	1	81.52
74	k = 1	1141	3	59.03	110	3	51.47
	k=5	2047	2	74.12	573	2	78.35
	k = 10	11023	2	75.26	647	2	81.52
	k = 20	21326	2	78.24	1739	2	78.18
	k = 50	22942	2	73.59	3399	3	52.15
	k = 100	99298	2	76.12	4867	2	80.29
	k = 200	187444	2	76.64	5707	2	78.08
75	k = 1	1626	3	67.53	146	3	56.95
	k=5	7600	3	63.87	548	2	79.31
	k = 10	14729	3	63.87	1095	2	82.81
	k = 20	22788	3	68.43	1881	2	79.28
	k = 50	124694	3	76.24	3366	2	78.77
	k = 100	205410	3	66.02	7725	2	80.9
	k = 200	537763	3	65.18	24478	2	84.28

Table A.16: Case study results 76-80

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT (ms)	B	CR	TT (ms)	B	CR
<b>76</b>	k = 1	1376	2	63.96	177	2	74.41
	k = 5	8926	2	74.31	519	2	72.4
	k = 10	17086	2	74.31	751	2	78.52
	k = 20	33521	2	74.31	1159	2	78.81
	k = 50	60053	2	73.48	3003	2	84.23
	k = 100	135048	2	73.09	7363	2	78.8
	k = 200	231300	2	71.65	16926	2	80.54
77	k = 1	1023	2	49.84	120	1	71.99
	k=5	4338	2	39.27	651	1	82.65
	k = 10	5616	1	71.67	1016	1	76.75
	k = 20	10976	2	40.22	2028	1	80.46
	k = 50	29232	1	72.87	3568	1	75.93
	k = 100	41278	1	77.2	8318	1	73.59
	k = 200	88763	1	77.2	5868	1	80.87
78	k = 1	265	2	69.04	49	2	63.24
	k=5	1194	2	71.41	262	2	67.07
	k = 10	2336	2	65.69	571	2	68.79
	k = 20	4516	2	69.82	902	2	68.92
	k = 50	12694	2	69.79	2142	2	68.06
	k = 100	37343	2	70.11	3265	2	71.6
	k = 200	68154	2	69.01	5888	2	68.1
79	k = 1	619	2	65.18	142	2	68.24
	k=5	2508	2	68	521	2	73.19
	k = 10	4839	2	68	912	2	73.2
	k = 20	9629	2	68	1748	2	73.2
	k = 50	24561	2	68	2860	2	69.99
	k = 100	59050	2	70.69	6388	2	68.51
	k = 200	119607	2	68.91	8898	2	70.83
80	k = 1	475	2	67.45	90	2	76.64
	k=5	1394	2	73	287	2	73.64
	k = 10	2504	2	72.45	784	2	74.19
	k = 20	4813	2	76.09	1518	2	74.19
	k = 50	11433	2	76.26	1973	2	75.36
	k = 100	24444	2	71.36	4246	2	76.51
	k = 200	47230	2	76.39	7618	2	76.66

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Table A.17: Case study results 81-85

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
81	k = 1	8	1	71.74	9	1	73.14
	k = 5	32	1	71.74	17	1	71.74
	k = 10	49	1	73.14	27	1	71.74
	k = 20	94	1	73.14	49	1	71.74
	k = 50	226	1	73.14	99	1	71.74
	k = 100	451	1	74.59	185	1	71.74
	k = 200	916	1	74.59	345	1	74.59
82	k = 1	30	1	62.99	67	1	73.56
	k = 5	128	1	75.39	124	1	77.7
	k = 10	242	1	75.39	244	1	77.7
	k = 20	460	1	75.89	577	1	75.39
	k = 50	1150	1	75.89	1658	1	76.65
	k = 100	2312	1	75.89	3109	1	76.14
	k = 200	4703	1	75.89	4769	1	76.65
83	k = 1	6	1	63.86	4	1	59.07
	k = 5	16	1	63.86	11	1	65.64
	k = 10	31	1	63.86	19	1	65.64
	k = 20	52	1	64.13	39	1	65.64
	k = 50	125	1	65.64	87	1	65.64
	k = 100	245	1	65.64	173	1	65.64
	k = 200	489	1	65.64	347	1	65.64
84	k = 1	3	1	66.1	2	1	73.29
	k=5	9	1	73.29	5	1	74.06
	k = 10	17	1	73.29	8	1	74.06
	k = 20	32	1	73.29	11	1	74.06
	k = 50	75	1	73.29	10	1	74.06
	k = 100	150	1	73.29	10	1	74.06
	k = 200	307	1	73.29	10	1	74.06
85	k = 1	24	1	69.56	21	1	66.42
	k = 5	75	1	69.56	33	1	79.68
	k = 10	140	1	69.56	54	1	79.68
	k = 20	267	1	69.56	94	1	80.26
	k = 50	670	1	69.56	208	1	80.26
	k = 100	1311	1	69.56	378	1	80.26
	k = 200	2645	1	69.56	798	1	80.26

Table A.18: Case study results 86-90

In	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
86	k = 1	34	1	82.3	17	1	75.61
	k = 5	80	1	82.3	20	1	82.3
	k = 10	133	1	82.3	28	1	82.3
	k = 20	259	1	82.3	53	1	82.3
	k = 50	604	1	82.3	104	1	82.3
	k = 100	1174	1	82.3	180	1	82.3
	k = 200	2400	1	82.3	359	1	82.3
87	k = 1	250	1	68.79	111	1	71.46
	k = 5	380	1	70.77	189	1	76.67
	k = 10	617	1	70.77	138	1	70.1
	k = 20	1072	1	72.52	274	1	75.49
	k = 50	2504	1	76.27	771	1	78.3
	k = 100	4903	1	76.27	1531	1	78.3
	k = 200	9892	1	77.89	2544	1	77.07
88	k = 1	109	1	63.76	53	1	77.67
	k = 5	244	1	67.29	98	1	77.67
	k = 10	375	1	69.53	145	1	76.85
	k = 20	690	1	73.38	310	1	73.38
	k = 50	1581	1	75.66	752	1	76.45
	k = 100	3019	1	77.26	1447	1	76.45
	k = 200	6146	1	77.26	2800	1	76.45
89	k = 1	32	1	67.75	22	1	75.37
	k = 5	210	1	75.72	24	1	66.46
	k = 10	376	1	75.72	41	1	66.46
	k = 20	601	1	75.72	76	1	75.37
	k = 50	1500	1	75.72	176	1	75.37
	k = 100	3224	1	75.72	321	1	75.37
	k = 200	5858	1	76.95	619	1	76.59
90	k = 1	12	1	80.24	10	1	80.24
	k = 5	41	1	80.24	18	1	80.24
	k = 10	76	1	80.24	20	1	80.24
	k = 20	148	1	80.24	23	1	80.24
	k = 50	372	1	80.24	20	1	80.24
	k = 100	738	1	80.24	20	1	80.24
	k = 200	1517	1	80.24	20	1	80.24

Table A.19: Case study results 91-95

In	stance	P	$\mathbf{S}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
91	k=1	27	2	61.65	23	2	62.87
	k=5	167	2	60.72	51	2	67.36
	k = 10	285	2	65.81	99	2	69.17
	k = 20	596	2	67.21	189	2	70.48
	k = 50	1239	2	64.03	422	2	73.88
	k = 100	2370	2	71.91	631	2	64.22
	k = 200	4631	2	71.91	1244	2	63.94
92	k = 1	41	2	68.98	17	2	64.7
	k=5	102	2	68.5	46	2	60.91
	k = 10	180	2	68.5	87	2	63.43
	k = 20	343	2	68.5	200	2	64.45
	k = 50	1081	2	68.5	481	2	64.45
	k = 100	2487	2	75.09	848	2	62.44
	k = 200	4615	2	74.62	1428	2	61.01
93	k = 1	11	2	53.18	6	2	49.39
	k=5	29	2	60.58	13	2	63.43
	k = 10	62	2	60.75	23	2	63.43
	k = 20	114	2	60.97	44	2	62.4
	k = 50	251	2	53.59	102	2	62.4
	k = 100	480	2	53.59	207	1	70.47
	k = 200	1141	2	53.59	408	1	70.85
94	k = 1	7	2	60.41	6	2	61.33
	k=5	18	2	60.41	10	2	62.49
	k = 10	32	2	60.41	17	2	64.19
	k = 20	65	2	72.49	30	2	64.19
	k = 50	166	2	72.49	72	2	64.19
	k = 100	332	2	72.49	146	2	74.4
	k = 200	675	2	75.2	247	2	71.17
95	k=1	2596	1	71.15	217	1	80.4
	k=5	5493	1	71.15	345	1	81.11
	k = 10	10208	1	71.15	859	1	78.75
	k = 20	19066	1	71.15	1031	1	76.3
	k = 50	53469	1	71.15	2902	1	82.38
	k = 100	101264	1	71.15	5778	1	82.38
	k = 200	198827	1	71.15	11145	1	82.38

Table A.20: Case study results 96-100

Ins	stance	P	$\overline{\mathbf{S}}$		P	M	
		TT $(ms)$	B	CR	TT $(ms)$	B	CR
96	k = 1	447	1	60.54	29	1	64.78
	k = 5	1417	1	60.54	108	1	67.96
	k = 10	2778	1	60.54	191	1	68.33
	k = 20	5405	1	66.23	685	1	71.57
	k = 50	13724	1	66.23	1133	1	68.28
	k = 100	26596	1	67	2122	1	68.28
	k = 200	55258	1	67	3725	1	69.27
97	k = 1	625	1	56.36	40	1	70.47
	k = 5	2977	1	61.41	228	1	69.38
	k = 10	5436	1	61.41	459	1	68.66
	k = 20	10287	1	62.02	458	1	66.34
	k = 50	26357	1	63.42	988	1	58.96
	k = 100	53737	1	65.76	1873	2	36.16
	k = 200	123811	1	72.94	9152	1	74.29
98	k = 1	78	1	79.05	23	1	64.42
	k = 5	172	1	79.05	51	1	64.42
	k = 10	288	1	81.04	94	1	77.16
	k = 20	530	1	81.04	137	1	67.57
	k = 50	1193	1	81.04	319	1	73.63
	k = 100	2307	1	81.04	621	1	73.75
	k = 200	4741	1	81.04	1182	1	77.16
99	k = 1	8	1	71.74	9	1	73.14
	k = 5	26	1	71.74	17	1	71.74
	k = 10	55	1	73.14	27	1	71.74
	k = 20	97	1	73.14	53	1	71.74
	k = 50	234	1	73.14	93	1	71.74
	k = 100	464	1	74.59	186	1	71.74
	k = 200	921	1	74.59	338	1	74.59
100	k = 1	9	1	54.55	6	1	56.35
	k = 5	30	1	56.35	12	1	67.25
	k = 10	55	1	56.35	19	1	70.44
	k = 20	101	1	67.45	35	1	70.44
	k = 50	243	1	67.45	71	1	70.44
	k = 100	495	1	70.22	134	1	70.44
	k = 200	1017	1	70.44	250	1	70.44

Table A.21: Summary of opened bins by heuristic

BRKGA-VD		13.4	26.6	36.3	50.8	13.8	25.5	36.6	49.4	13.3	25.9	37.5	49.8	29.4	58.9	8.98	118.8	8.3	15	19.9	27.1	9.7	18.9	29	37.3	7.4	12.2	15.2	23.4	9.5	18.8	23.6	29.3
		4.	9.	4.	<u>∞</u> .	∞.	9:	9.	4.	6.3	6.	٠. -	<u> </u>	4.		<u>∞</u> .	8.8	3	ىر -	T:		7	6.	6		4	7.	نن 	4.	2	6:	9:	.3 -
BRKGA		13	26	36	20	13	25	36	49	13	25	37	49	29	വ	98	118	8	1	20	27	9.	18	2	37.3	7.	12	15	23	.6	18	23	29
GVN		13.4	26.6	36.4	50.9	13.8	25.7	36.9	49.4	13.3	26	37.6	20	29.4	59	8.98	118.8	8.3	15	20.4	27.1	8.6	19	29.2	37.4	7.4	12.5	16	23.5	9.2	18.9	24.1	29.8
EHGH2		13.8	27.6	39.8	9.02	1	ı	ı	,	-	ı	ı		29.4	59.5	90.4	119	6.7	14.6	21.5	29.6	11.8	19.2	29.8	38.7	7.4	13.5	18.2	24.1	5.4	18.9	56	35.8
$_{ m GASP}$		13.4	56.9	37	51.6		,	,	1	-	1	,	1	29.4	59	8.98	118.8	8.4	15.1	20.6	27.7	9.6	19.1	29.5	38	7.5	12.7	16.6	24.2	9.3	19	24.8	31.1
GLS		13.4	26.6	37	51.2	1	1	1	1	-	1	1	1	29.4	59	8.98	119	8.3	15.1	20.2	27.2	8.6	19.1	29.4	37.7	7.4	12.3	15.8	23.5	9.2	18.9	23.9	29.9
TS3		13.4	26.6	36.7	51.2	13.8	25.7	37.2	50.1	13.3	56	37.7	50.5	29.4	59	8.98	118.8	8.4	15	20.4	27.6	6.6	19.1	29.4	37.7	7.5	12.5	16.1	23.9	9.3	18.9	24.1	30.3
	k = 50	14	27.7	37.9	52.7	14.8	26.7	39	51.7	13.9	27.3	39	51.2	29.7	59.2	7.78	119.5	9.8	15.6	21.4	28.4	10.3	19.7	30.2	38.5	9.7	13.2	16.8	24.7	6.7	20	25.8	31.2
	k = 20	14.4	27.9	38.3	52.6	14.9	26.7	39.1	51.8	14	27.3	39	51.3	29.7	59.2	9.78	119.5	9.8	15.6	21.3	28.4	10.2	19.7	30	38.6	7.7	13.4	16.8	24.7	9.6	20	25.8	31.4
$\mathbf{PS}$	k = 10	14.3	27.8	38.5	52.6	14.8	56.9	39.1	51.9	13.9	27.2	38.9	51.4	29.7	59.2	9.78	119.5	9.8	15.6	21.3	28.3	10.4	19.8	30.3	38.8	7.9	13.5	16.9	24.8	9.6	19.9	25.7	31.6
	k=5	14.3	27.8	38.5	52.7	14.8	26.9	39.2	51.8	14.1	27.5	38.9	51.4	29.7	59.2	87.7	119.5	8.7	15.6	21.3	28.2	10.5	19.7	30.3	38.6	7.9	13.5	16.7	24.5	9.6	20	25.8	31.6
	k = 1	14.4	27.7	38.4	52.7	14.9	27.1	39.2	51.9	14	27.6	39.1	51.4	29.7	59.2	9.78	119.5	8.7	15.7	21.3	28.4	10.7	19.8	30.4	39.1	7.7	13.5	17.1	24.9	2.6	20	56	31.6
	k = 50	14.10	28	38.4	53	14.6	26.6	38.3	51	13.9	27.8	39.2	51.8	29.7	59.2	9.78	119.5	9.8	16	21.7	29	10	19.8	30.3	38.9	7.8	13.2	17.1	24.9	6.6	19.6	25.7	31.6
	k = 20	14.5	28.4	38.3	52.9	14.7	26.6	38.3	51.3	13.8	27.5	39.5	51.6	29.7	59.2	9.78	119.5	8.7	16	21.7	29	10.2	19.5	30.3	38.6	7.8	13.3	16.9	25.2	8.6	19.6	25.7	31.3
$_{ m PM}$	k = 10	14.5	28.3	38.4	53	14.7	56.6	38.2	51.1	13.9	27.7	39.5	51.7	29.7	59.2	9.78	119.5	8.7	16	21.6	28.9	10.1	20	30.3	39.2	7.9	13.4	17	25	6.6	19.7	25.6	31.6
	k = 5	14.5	28.3	38.5	53.2	14.7	26.6	38.3	51.2	14.1	27.7	39.4	51.8	29.7	59.2	9.78	119.5	8.7	16	21.6	28.9	10.3	19.8	30.4	39.2	7.7	13.2	16.9	25	10.1	19.7	25.6	31.5
	k = 1	14.5	28.4	38.5	53.1	14.8	26.5	38.4	51.3	14.2	27.7	39.4	51.8	29.7	59.2	9.78	119.5	8.7	16	21.6	28.9	10.5	19.8	30.4	39.1	6.7	13.5	16.9	25.1	10	19.6	25.8	31.5
S	u	20	100	150	200	20	100	150	200	20	100	150	200	20	100	150	200	50	100	150	200	20	100	150	200	20	100	150	200	20	100	150	200
Class	Instance					2				3				4				2				9				2				8			

Table A.22: Detailed execution times for literature tests in milliseconds

Instantor         h         k=1         k=2         k=20         k=8         k=10         k=20         k=80         k=10         k=2         k=10         k=20         k=20         k=20         k=90         k=90         k=20         k=10         k=20         k=10         k=20         k=10         k=20         k=10         k=20         k	Class	S			$_{ m PM}$					PS			BRKGA-VD
50         80,50         85,20         150,70         820,30         85,00         192,80         390,60         982,00           100         137,70         439,10         373,70         177,20         634,80         1,181,20         1,245,00         1,214,30         1,182,90         1,180,20         3,210,10         1,214,30         1,182,90         1,180,20         3,181,20         1,237,10         1,247,20         6,477,0         1,243,20         1,182,20         3,144,60         1,182,20	Instance	n	k = 1	k = 5	k = 10	k = 20	k = 50	k = 1	k = 5	k = 10	k = 20	k = 50	
100         137.90         489.10         819.60         1500.60         3777.60         177.20         (64.80         1.181.50         2.469.10         5.540.10           150         341.50         1,227.10         1,207.10         1,273.00         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20         1,273.20	П	50	80.50	85.20	150.70	307.00	820.30	85.00	109.40	192.80	390.60	968.20	1,293.25
150         341.50         1.237.10         2.478.60         4.677.30         12.143.30         4.94.10         1.885.90         3.817.80         7.625.60         18.751.70         1.237.10         2.478.60         1.677.40         2.808.20         3.417.80         1.679.40         1.808.90         3.817.80         1.724.50         3.817.70         1.00.20           100         105.80         3.42.50         6.47.50         1.528.70         3.921.30         1.60.90         1.724.50         3.391.50         1.479.20           100         105.80         3.42.50         6.47.50         1.528.70         1.940.00         869.00         1.724.50         3.991.30         1.909.00           100         105.80         3.42.50         6.47.50         1.528.70         1.329.40         1.67.20         4.931.70         1.170.30         3.891.20         1.170.20         3.891.20         1.170.20         3.891.20         1.170.20         3.891.20         1.170.20         3.891.20         1.170.20         3.891.20         3.891.70         3.891.20         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.891.70         3.		100	137.90	439.10	819.60	1,500.60	3,737.60	177.20	634.80	1,181.50	2,409.10	5,540.10	7,005.10
200         697.40         2.888.20         5.144.30         10.319.20         2.6679.40         1.087.30         4.629.80         9.134.60         18.256.50         4.1727.70           50         10.41.00         1.65.80         2.20.10         5.55.70         3.59.02         1.25.80         125.60         1.140.30         1.190.30           100         1.65.80         3.42.50         647.50         1.528.70         3.290.30         125.00         1.742.45         3.30.13         1.190.30           150         266.00         974.60         1.842.70         1.728.50         1.260.30         2.590.20         4.719.40         1.30.30         2.410.20         2.43.60         1.190.30         1.20.30         2.40.20         3.20.20         1.20.20         2.590.20         4.719.40         1.590.30         2.590.20         4.719.40         1.590.30         2.20.70         4.719.40         1.150.20         2.24.30         0.00.10         3.80.20         0.00.10         3.80.20         1.10.20         3.80.20         0.00.10         3.80.20         1.10.20         3.80.20         1.10.20         3.24.30         0.00.10         3.80.20         1.10.20         3.24.30         0.00.10         3.80.20         3.80.20         3.80.20         3.80.20         3.80		150	341.50	1,237.10	2,478.60	4,677.30	12,143.30	494.10	1,865.90	3,817.80	7,625.60	18,751.70	17,674.42
50         24.70         72.80         126.50         29.0.10         555.70         35.80         125.60         24.10         17.80         11.05.00         11.00.30         <		200	697.40	2,808.20	5,144.30	10,319.20	26,679.40	1,087.30	4,629.80	9,134.60	18,256.50	44,792.70	34,702.21
100         105.80         342.50         647.50         1,528.70         3,921.30         194.00         869.00         1,724.50         3,391.50         8,489.30           150         266.00         974.01         1,828.70         1,528.70         1,528.50         1,010.85         2,649.20         2,535.02         2,493.20         2,532.40         401.30         2,432.20         2,492.20         2,532.40         401.30         3,81.20         2,532.40         401.30         3,81.20         2,532.40         401.30         3,81.20         2,532.40         401.30         3,81.490         2,630.41         3,81.490         3,821.490         2,630.41         3,81.490         3,821.490         2,630.41         3,81.490         1,71.790.20         2,530.41         6,042.70         1,730.10         40.30.80         3,821.490         40.40.70         3,81.49	2	50	24.70	72.80	126.50	220.10	555.70	35.80	125.60	243.20	510.80	1,190.30	1,293.25
150         266 00         974.60         1.842 70         3.399 20         8,160.60         590.30         2,599 20         4,943 70         10,118 50         24,492 20           200         532.40         1,971.00         3,817.30         7,228.50         17,694.30         1,230.60         22,535.00         22,535.00         23,044.0           50         28.10         82.70         1,503.80         3,025.50         4,719.40         1,506.80         4,013.0         204.00         2,634.10         6,027.70         1,231.80         2,234.10         6,027.70         2,234.10         6,027.70         3,234.10         6,027.70         3,234.10         6,027.70         982.40         982.40         982.40         982.40         1,209.90         690.00         2,044.00         1,209.90         1,209.00         94,520         4,027.40         8,214.90         1,209.20         1,209.20         4,027.40         8,214.90         1,209.20         1,708.20         2,044.00         1,209.20         1,708.20         2,074.20         1,209.20         1,209.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         1,708.20         <		100	105.80	342.50	647.50	1,528.70	3,921.30	194.00	869.00	1,724.50	3,391.50	8,489.30	7,112.88
200         532.40         1,971.00         3,817.30         7,228.50         1,709.50         1,770.20         22,535.60         530.24.40           50         28.10         82.70         1,528.50         17,020         32.50         112.00         204.00         10.00         165.50         710.20         32.50         112.00         204.00         204.00         165.50         4713.90         11.50         11.20         20.04.00         20.49.00         2,455.60         4719.40         11.50         41.318.50         8.788.70         17,801.60         44.03.80         20.57.70         10.418.30         25.855.20         1,018.20         40.74.0         82.44.0         60.42.70         20.04.00         5.307.70         10,418.30         25.855.20         1,018.20         28.78.80         1,7801.60         44.038.80         1.20.80         1,00.70         40.00         20.04.00         3.04.40         7.778.10         1,108.20         28.788.70         1,7801.60         44.431.70         1,00.20         28.04.0         58.28.0         1,00.70         1,00.20         20.04.00         3.04.40         1,777.80         20.07.00         3.00.00         1,00.00         3.00.00         1,00.00         3.00.00         3.00.00         1,00.00         1,00.00         1,00.00		150	266.00	974.60	1,842.70	3,399.20	8,160.60	590.30	2,599.20	4,943.70	10,118.50	24,492.20	17,782.19
50         28.10         82.70         156.30         302.50         710.20         32.50         112.00         204.00         401.30         982.40           100         120.10         489.30         910.70         1,655.50         4,131.30         162.20         621.70         1,231.80         2,234.10         6,042.70           120         341.20         1,263.80         2,475.60         4,719.40         1,596.80         6,21.70         1,231.80         2,234.10         6,045.70           200         690.00         2,694.00         2,567.0         1,714.83         2,585.0         1,377.00         8,737.70         1,209.80         36.60         1,718.80         2,234.0         1,377.00         6,045.70         1,380.80         2,273.30         7,125.80         2,601.60         5,089.70         3,998.20         1,377.00         8,690.00         1,370.00         3,590.70         1,370.00         1,3		200	532.40	1,971.00	3,817.30	7,228.50	17,694.90	1,320.50	5,792.70	11,790.20	22,535.60	53,024.40	34,486.67
100         120.10         489.30         910.70         1,625.50         4,313.90         162.20         621.70         1,231.80         2,234.10         6,042.70           150         341.20         1,263.80         910.70         1,625.50         4,313.90         162.20         621.70         1,231.80         2,234.10         6,042.70           200         690.00         2,694.00         5,307.70         10,418.30         25,865.20         1,018.20         28,783.00         1,377.00         4,903.80           100         220.70         2,694.00         2,566.10         1,208.00         96.00         9,682.20         24,431.50           100         220.70         817.40         1,9574.70         6,44.20         2,601.60         5,089.70         9,682.20         24,431.50           100         220.70         817.40         1,778.10         19,574.70         644.20         2,601.60         5,089.70         9,685.20         1,377.00           100         639.70         2,074.00         375.10         1,44.21.60         1,415.90         6,077.40         1,588.20         58,029.70         2,647.50         1,44.31.50           100         638.70         1,133.40         2,415.50         2,727.40         1,415.80 </th <th>က</th> <th>20</th> <th>28.10</th> <th>82.70</th> <th>156.30</th> <th>302.50</th> <th>710.20</th> <th>32.50</th> <th>112.00</th> <th>204.00</th> <th>401.30</th> <th>982.40</th> <th>1,293.25</th>	က	20	28.10	82.70	156.30	302.50	710.20	32.50	112.00	204.00	401.30	982.40	1,293.25
150         341.20         1,263.80         2,455.60         4,719.40         11,596.80         461.40         1,979.50         4,027.40         8,214.90         20,657.80           200         690.00         2,694.00         5,307.70         10,418.30         25,886.20         1,018.20         4,318.50         8,788.70         17,801.60         44,903.80           100         220.70         12,940         2,556.00         2,973.30         7,125.80         246.00         945.50         1,742.80         3,532.90         8,636.00           100         220.70         2,074.50         3,944.40         17,728.10         1,415.00         9,968.20         3,532.90         8,636.00           100         259.70         2,074.50         3,944.40         17,294.00         44,421.60         1,415.00         9,588.70         1,415.90         3,532.90         8,636.00           100         69.80         230.80         438.70         861.00         2,222.40         1,703.40         3,547.50         1,617.20           100         69.80         230.80         1,134.80         2,415.50         5,727.40         618.10         2,532.90         3,547.50         2,543.60           100         69.80         23.80         1,035.90 <th></th> <th>100</th> <th>120.10</th> <th>489.30</th> <th>910.70</th> <th>1,625.50</th> <th>4,313.90</th> <th>162.20</th> <th>621.70</th> <th>1,231.80</th> <th>2,234.10</th> <th>6,042.70</th> <th>6,897.33</th>		100	120.10	489.30	910.70	1,625.50	4,313.90	162.20	621.70	1,231.80	2,234.10	6,042.70	6,897.33
200         690.00         2,694.00         2,694.00         1,418.30         25,865.20         1,018.20         4,318.50         8,788.70         17,801.60         44,903.80           50         45.10         129.40         25,866.10         1,200.90         95.60         150.20         280.40         1,582.90         1,377.00           150         220.70         817.40         1,582.80         2,973.30         7,125.80         246.00         945.50         1,742.80         3,532.90         8,636.00           100         220.70         2,074.50         3,944.40         7,712.91.40         44.421.60         145.90         260.80         23.898.0         17.291.40         44.421.60         145.90         36.899.70         9,988.20         24.431.50           100         69.80         230.80         438.70         861.00         2,229.90         212.40         957.60         1,703.40         3,547.50         7,580.70           100         69.80         230.80         438.70         861.00         2,229.90         212.40         957.00         1,617.20         3,641.50         1,617.20           100         69.80         230.80         2,415.50         5,727.40         618.10         253.20         1,617.20		150	341.20	1,263.80	2,455.60	4,719.40	11,596.80	461.40	1,979.50	4,027.40	8,214.90	20,657.80	18,428.81
50         45.10         129.40         255.60         506.10         1,200.30         95.60         150.20         280.40         532.50         1,377.00           100         220.70         817.40         1,582.80         2,973.30         7,125.80         246.00         945.50         1,742.80         3,532.90         8,636.60           150         220.70         817.40         1,582.80         2,973.30         7,125.80         246.00         945.50         1,742.80         3,532.90         8,636.60           200         1,143.20         4,685.50         8,938.80         17,291.40         44,421.60         1,415.90         1,1581.60         3,682.90         8,636.00           100         69.80         230.80         1,7291.40         44,421.60         1,455.90         318.80         631.80         1,617.20         8,636.00         1,617.80         1,759.00         1,759.00         1,759.00         1,759.00         1,759.00         1,759.00         1,770.40         1,758.00         1,377.70         1,377.70         1,770.40         1,876.70         1,770.40         1,880.00         1,377.70         1,890.00         1,289.70         1,289.70         1,703.40         1,893.70         1,100.00         1,990.00         1,749.50         1,770.40<		200	00.069	2,694.00	5,307.70	10,418.30	25,865.20	1,018.20	4,318.50	8,788.70	17,801.60	44,903.80	35,672.15
100         220.70         817.40         1,582.80         2,973.30         7,125.80         246.00         945.50         1,742.80         3,532.90         8,636.60           150         259.70         2,074.50         3,944.40         7,778.10         19,574.70         644.20         2,601.60         50.89.70         9,968.20         24,431.50           200         1,143.20         4,685.50         8,938.80         17,291.40         44,421.60         1,415.90         6,027.40         11,581.60         23,292.0         24,431.50           100         69.80         233.80         17,291.40         44,421.60         1,415.90         438.20         318.80         1,617.20           100         69.80         230.80         4,415.80         2,124.0         40.60         1,559.0         1,617.20         7,580.70           100         69.80         1,055.90         2,415.50         5,774.40         4,688.80         1,773.40         3,547.50         1,617.20           200         222.40         73.20         2,016.70         2,688.00         2,688.80         1,773.40         3,547.50         1,138.00         2,688.80         1,773.40         3,547.50         1,138.00         2,688.00         1,361.00         4,456.70 <td< th=""><th>4</th><th>50</th><th>45.10</th><th>129.40</th><th>255.60</th><th>506.10</th><th>1,200.90</th><th>95.60</th><th>150.20</th><th>280.40</th><th>532.50</th><th>1,377.00</th><th>1,185.48</th></td<>	4	50	45.10	129.40	255.60	506.10	1,200.90	95.60	150.20	280.40	532.50	1,377.00	1,185.48
150         559.70         2,074.50         3,944.40         7,778.10         19,574.70         6,40.20         2,601.60         5,089.70         9,968.20         24,431.50           200         1,143.20         4,685.50         8,938.80         17,291.40         44,421.60         1,415.90         318.80         631.80         58,029.70           50         23.40         75.40         152.80         275.10         701.90         40.60         1,581.60         23,829.20         58,029.70           100         69.80         230.80         438.70         861.00         2,229.90         212.40         937.60         1,703.40         3,547.50         7,580.70           100         69.80         230.80         1,34.80         2,415.50         3,727.40         618.10         2,532.10         4,824.10         3,547.50         7,580.70           200         283.80         1,065.90         2,415.50         3,617.70         3,944.0         1,617.20         3,547.50         7,580.70           100         88.10         2,529.90         1,134.80         2,415.50         3,547.50         1,617.20         3,547.50         1,617.20           200         2,230         1,134.80         2,629.90         2,629.90		100	220.70	817.40	1,582.80	2,973.30	7,125.80	246.00	945.50	1,742.80	3,532.90	8,636.60	6,574.02
200         1,143.20         4,685.50         8,938.80         17,291.40         44,421.60         1,415.90         6,027.40         11,581.60         23,829.20         58,029.70           50         23.40         75.40         152.80         275.10         701.90         40.60         155.90         318.80         631.80         1,617.20           100         69.80         230.80         438.70         861.00         2,229.90         212.40         937.60         1,703.40         3,547.50         7,580.70           100         69.80         230.80         438.70         861.00         2,229.90         212.40         937.60         1,703.40         3,547.50         7,580.70           200         283.80         1,055.90         2,011.50         2,229.90         212.40         937.60         1,703.40         5,734.60         27,346.00           200         283.80         1,055.90         2,011.20         2,629.00         2,610.60         1,703.40         1,839.40         2,684.80         1,360.10         2,532.10         4,988.80         1,773.40         1,839.80         2,617.80         2,617.80         2,686.00         2,693.00         1,389.40         2,684.80         1,360.10         2,532.00         2,611.90         2,532.		150	559.70	2,074.50	3,944.40	7,778.10	19,574.70	644.20	2,601.60	5,089.70	9,968.20	24,431.50	17,135.56
50         23.40         75.40         152.80         275.10         701.90         40.60         155.90         318.80         631.80         1,617.20           100         69.80         230.80         438.70         861.00         2,229.90         212.40         937.60         1,703.40         3,547.50         7,580.70           100         69.80         230.80         438.70         861.00         2,229.90         212.40         618.10         2,532.10         4,824.10         9,131.20         7,346.00           200         283.80         1,055.90         2,071.00         3,899.90         9,916.70         1,210.60         4,882.41         9,131.20         27,346.00           50         22.40         73.20         136.10         262.90         568.60         26.90         88.80         177.70         349.40         836.40           100         88.50         315.00         583.50         1,139.40         2,684.80         1,360.10         2,561.50         2,734.60         275.30         1,777.80         36.77.80         36.778.90         36.778.90         36.778.90         36.778.90         36.778.90         36.778.90         36.778.90         36.778.90         36.777.80         37.777.40         37.56.00         37.		200	1,143.20	4,685.50	8,938.80	17,291.40	44,421.60	1,415.90	6,027.40	11,581.60	23,829.20	58,029.70	34,271.13
100         69.80         230.80         438.70         861.00         2,229.90         212.40         937.60         1,703.40         3,547.50         7,580.70           150         164.90         596.50         1,134.80         2,415.50         5,727.40         618.10         2,532.10         4,824.10         9,131.20         27,346.00           200         283.80         1,055.90         2,071.00         3,899.90         9,916.70         1,210.60         4,988.80         9,872.90         20,611.90         56,078.50           100         88.50         1,055.90         2,071.00         3,899.90         9,916.70         1,210.60         4,988.80         177.70         349.40         86.078.80           100         88.50         1,055.90         1,139.40         2,684.80         1,360.10         2,561.50         5,367.50         11,886.10           200         401.90         1,555.60         2,820.30         12,899.70         624.40         2,561.50         5,261.20         5,377.80           50         401.90         1,555.60         2,820.30         190.80         1,938.70         1,255.30         1,943.60         9,218.90         2,561.20         2,561.20         2,561.20         2,583.50         1,774.60         2,	ಬ	20	23.40	75.40	152.80	275.10	701.90	40.60	155.90	318.80	631.80	1,617.20	3,233.13
150         164.90         596.50         1,134.80         2,415.50         5,727.40         618.10         2,532.10         4,824.10         9,131.20         27,346.00           200         283.80         1,055.90         2,071.00         3,899.90         9,916.70         1,210.60         4,988.80         9,872.90         20,611.90         56,078.50           50         22.40         73.20         136.10         262.90         568.60         26.90         88.80         177.70         349.40         836.40           100         88.50         315.00         583.50         1,139.40         2,684.80         136.40         555.30         1,030.40         1,886.10         26.61.70         349.40         836.40         836.70         1,886.10         27.20         1,139.40         2,684.80         136.40         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,886.10         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,106.60         1,105.60 </th <th></th> <th>100</th> <th>08.69</th> <th>230.80</th> <th>438.70</th> <th>861.00</th> <th>2,229.90</th> <th>212.40</th> <th>937.60</th> <th>1,703.40</th> <th>3,547.50</th> <th>7,580.70</th> <th>13,040.27</th>		100	08.69	230.80	438.70	861.00	2,229.90	212.40	937.60	1,703.40	3,547.50	7,580.70	13,040.27
200         283.80         1,055.90         2,071.00         3,899.90         9,916.70         1,210.60         4,988.80         9,872.90         20,611.90         56,078.50           50         22.40         73.20         136.10         262.90         568.60         26.90         88.80         177.70         349.40         56,078.50           100         88.50         315.00         583.50         1,139.40         2,684.80         136.40         555.30         1,030.40         1,839.80         4,456.70           150         88.50         315.00         583.50         1,139.40         2,684.80         136.40         5561.50         2,611.30         84.456.70           200         401.30         1,555.60         2,820.30         12,899.70         624.40         2,521.50         1,986.10         1,886.10         1,105.60           100         68.30         2,295.60         19,89.80         15,300.90         1,255.30         1,255.30         1,105.60         1,105.60           100         68.30         2,295.60         1,987.00         15,430.00         2,521.20         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60         1,105.60		150	164.90	596.50	1,134.80	2,415.50	5,727.40	618.10	2,532.10	4,824.10	9,131.20	27,346.00	29,960.29
5022.4073.20136.10262.90568.6026.9088.80177.70349.40836.4010088.50315.00583.501,139.402,684.80136.40555.301,030.401,839.804,456.70150223.40796.901,448.703,019.107,749.502,33.801,360.102,561.505,367.5011,886.10200401.901,555.602,820.305,229.5012,899.70624.402,523.204,943.609,218.9023,577.8010068.302,95.604,33.30846.801,993.60154.30656.701,255.302,261.205,893.50150153.10547.601,164.102,190.905,292.60413.901,894.103,777.407,156.6017,704.60200270.00976.902,056.003,804.1010,078.00808.704,513.507,854.1014,518.6032,642.1010065.00208.00395.90758.201,983.70160.20576.301,179.102,155.504,981.50150151.70516.30937.801,970.204,837.304,149.507,612.0014,338.2034,916.60		200	283.80	1,055.90	2,071.00	3,899.90	9,916.70	1,210.60	4,988.80	9,872.90	20,611.90	56,078.50	57,226.32
100         88.50         315.00         583.50         1,139.40         2,684.80         136.40         555.30         1,030.40         1,839.80         4,456.70           150         223.40         796.90         1,448.70         3,019.10         7,749.50         323.80         1,360.10         2,561.50         5,367.50         11,886.10           200         401.90         1,555.60         2,820.30         5,229.50         12,899.70         624.40         2,523.20         4,93.60         23,577.80           100         68.30         2,29.50         483.30         846.80         1,993.60         154.30         656.70         1,255.30         4,53.50         1,105.60           150         68.30         2,29.50         433.30         846.80         1,993.60         154.30         656.70         1,255.30         2,218.50         2,261.20         5,893.50           150         68.30         2,20.50         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           100         65.00         20.40         119.30         220.30         228.50         29.50         109.00         20.09         4,981.50         3,815.50         3,815.50         3,815.50<	9	50	22.40	73.20	136.10	262.90	568.60	26.90	88.80	177.70	349.40	836.40	969.94
150223.40796.901,448.703,019.107,749.50323.801,360.102,561.505,367.5011,886.10200401.901,555.602,820.305,229.5012,899.70624.402,523.204,943.609,218.9023,577.8050401.901,555.602,820.30190.80487.4032.80113.30218.20453.501,105.6010068.30229.50433.30846.801,993.60413.901,894.103,777.407,156.6017,704.60150270.00976.902,056.003,804.1010,078.00808.704,513.507,854.1014,518.6032,642.10200270.00976.902,056.003,804.1010,078.00808.704,513.507,854.1014,518.6032,642.1010065.00208.00395.90758.201,983.70160.20276.301,179.102,155.504,981.50150151.70516.301,970.204,837.30433.101,964.403,815.508,109.5017,854.20200296.801,004.901,835.803,471.709,174.80896.004,149.507,612.0014,338.2034,916.60		100	88.50	315.00	583.50	1,139.40	2,684.80	136.40	555.30	1,030.40	1,839.80	4,456.70	5,065.23
200         401.90         1,555.60         2,820.30         5,229.50         12,899.70         624.40         2,523.20         4,943.60         9,218.90         23,577.80           50         18.00         53.70         103.60         190.80         487.40         32.80         113.30         218.20         453.50         1,105.60           100         68.30         229.50         433.30         846.80         1,993.60         154.30         656.70         1,255.30         2,261.20         5,893.50           150         68.30         229.50         4,164.10         2,190.90         5,292.60         413.90         1,894.10         3,777.40         7,156.60         17,704.60           200         270.00         976.90         2,056.00         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           100         65.00         208.00         395.90         758.20         1,983.70         160.20         276.30         1,179.10         2,155.50         4,981.50           150         151.70         356.80         1,970.20         4,837.30         4,149.50         7,612.00         14,338.20         34,916.60		150	223.40	196.90	1,448.70	3,019.10	7,749.50	323.80	1,360.10	2,561.50	5,367.50	11,886.10	13,686.90
50         18.00         53.70         103.60         190.80         487.40         32.80         113.30         218.20         453.50         1,105.60           100         68.30         229.50         433.30         846.80         1,993.60         154.30         656.70         1,255.30         2,261.20         5,893.50           150         153.10         547.60         1,164.10         2,190.90         5,292.60         413.90         1,894.10         3,777.40         7,156.60         17,704.60           200         270.00         976.90         2,056.00         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           50         18.60         60.40         119.30         220.30         528.50         29.50         109.00         200.90         406.60         919.30           100         65.00         208.00         395.90         758.20         1,983.70         1,964.40         3,815.50         8,109.50         17,854.20           150         156.80         1,004.90         1,964.40         3,815.50         8,109.50         17,854.20           200         296.80         1,004.90         3,471.70         9,174.80         896.00		200	401.90	1,555.60	2,820.30	5,229.50	12,899.70	624.40	2,523.20	4,943.60	9,218.90	23,577.80	27,697.11
100         68.30         229.50         433.30         846.80         1,993.60         154.30         656.70         1,255.30         2,261.20         5,893.50           150         153.10         547.60         1,164.10         2,190.90         5,292.60         413.90         1,894.10         3,777.40         7,156.60         17,704.60           200         270.00         976.90         2,056.00         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           50         18.60         60.40         119.30         220.30         528.50         109.00         200.90         406.60         919.30           100         65.00         208.00         395.90         758.20         1,983.70         160.20         576.30         1,179.10         2,155.50         4,981.50           150         151.70         516.30         1,970.20         4,837.30         433.10         1,964.40         3,815.50         8,109.50         17,854.20           200         296.80         1,004.90         1,835.80         3,471.70         9,174.80         896.00         4,149.50         7,612.00         14,338.20         34,916.60	7	20	18.00	53.70	103.60	190.80	487.40	32.80	113.30	218.20	453.50	1,105.60	2,586.50
150         153.10         547.60         1,164.10         2,190.90         5,292.60         413.90         1,894.10         3,777.40         7,156.60         17,704.60           200         270.00         976.90         2,056.00         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           50         18.60         60.40         119.30         220.30         528.50         29.50         109.00         406.60         919.30           100         65.00         208.00         395.90         758.20         1,983.70         160.20         576.30         1,179.10         2,155.50         4,981.50           150         151.70         516.30         1,970.20         4,837.30         433.10         1,964.40         3,815.50         8,109.50         17,854.20           200         296.80         1,004.90         1,835.80         3,471.70         9,174.80         896.00         4,149.50         7,612.00         14,338.20         34,916.60		100	68.30	229.50	433.30	846.80	1,993.60	154.30	656.70	1,255.30	2,261.20	5,893.50	10,669.31
200         270.00         976.90         2,056.00         3,804.10         10,078.00         808.70         4,513.50         7,854.10         14,518.60         32,642.10           50         18.60         60.40         119.30         220.30         528.50         29.50         109.00         200.90         406.60         919.30           100         65.00         208.00         395.90         758.20         1,983.70         160.20         576.30         1,179.10         2,155.50         4,981.50           150         151.70         516.30         937.80         1,970.20         4,837.30         433.10         1,964.40         3,815.50         8,109.50         17,854.20           200         296.80         1,004.90         1,835.80         3,471.70         9,174.80         896.00         4,149.50         7,612.00         14,338.20         34,916.60		150	153.10	547.60	1,164.10	2,190.90	5,292.60	413.90	1,894.10	3,777.40	7,156.60	17,704.60	24,571.75
5018.6060.40119.30220.30528.5029.50109.00200.90406.60919.3010065.00208.00395.90758.201,983.70160.20576.301,179.102,155.504,981.50150151.70516.30937.801,970.204,837.30433.101,964.403,815.508,109.5017,854.20200296.801,004.901,835.803,471.709,174.80896.004,149.507,612.0014,338.2034,916.60		200	270.00	06.926	2,056.00	3,804.10	10,078.00	808.70	4,513.50	7,854.10	14,518.60	32,642.10	46,125.92
65.00208.00395.90758.201,983.70160.20576.301,179.102,155.504,981.50151.70516.30937.801,970.204,837.30433.101,964.403,815.508,109.5017,854.20296.801,004.901,835.803,471.709,174.80896.004,149.507,612.0014,338.2034,916.60	$\infty$	20	18.60	60.40	119.30	220.30	528.50	29.50	109.00	200.90	406.60	919.30	2,909.81
151.70         516.30         937.80         1,970.20         4,837.30         433.10         1,964.40         3,815.50         8,109.50         17,854.20           296.80         1,004.90         1,835.80         3,471.70         9,174.80         896.00         4,149.50         7,612.00         14,338.20         34,916.60		100	65.00	208.00	395.90	758.20	1,983.70	160.20	576.30	1,179.10	2,155.50	4,981.50	13,148.04
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		150	151.70	516.30	937.80	1,970.20	4,837.30	433.10	1,964.40	3,815.50	8,109.50	17,854.20	25,002.84
		200	296.80	1,004.90	1,835.80	3,471.70	9,174.80	896.00	4,149.50	7,612.00	14,338.20	34,916.60	48,604.65

68 A Appendix A

Table A.23: Cage ratio of literature tests

Class	5			$\mathbf{PM}$					PS		
Instance	n	k = 1	k=5	k = 10	k = 20	k = 50	k = 1	k = 5	k = 10	k = 20	k = 50
1	50	69.36	69.84	69.66	69.74	71.73	70.09	70.5	70.45	70.06	72.36
	100	73.01	73.62	73.37	73.44	74.78	74.56	74.25	74.26	74.17	74.56
	150	75.66	75.53	75.61	75.91	76.07	75.93	75.93	76.04	76.31	76.9
	200	75.33	75.28	75.56	75.62	75.78	75.71	75.8	75.99	75.9	75.93
2	50	69.6	69.5	69.48	69.79	69.31	67.92	68.71	68.09	68.32	68.78
	100	73.05	72.76	73.09	72.7	72.7	71.37	71.74	71.74	72.22	72.54
	150	72.95	73.15	73.28	73.11	73.04	71.51	71.28	71.5	71.38	71.66
	200	73.21	73.29	73.34	73.24	73.42	72.23	72.36	72.12	72.43	72.55
3	50	71.61	71.81	73.08	72.94	72.87	72.38	71.9	72.63	71.88	73.4
	100	73.52	73.62	73.7	74.37	73.73	73.99	74.28	74.97	74.79	74.83
	150	74.94	75.1	75.04	75.04	75.78	75.6	75.98	76.04	75.83	75.94
	200	76.09	76.01	76.21	76.43	76.08	76.58	76.74	76.82	77.01	77.03
4	50	61.49	61.49	61.62	61.8	61.79	61.49	61.6	61.7	61.73	61.78
	100	63.48	63.46	63.53	63.53	63.58	63.49	63.5	63.52	63.53	63.57
	150	61.91	61.96	61.92	61.95	61.98	61.94	61.84	61.94	61.95	61.96
	200	61.83	61.84	61.82	61.84	61.8	61.81	61.83	61.83	61.82	61.83
5	50	69.08	68.72	69.03	69.44	70.5	69.45	69.54	70.35	70.18	70.69
	100	73.49	73.66	73.8	74.1	73.71	74.52	74.94	74.85	75.02	75.01
	150	76.38	76.48	76.5	76.14	76.43	77.32	77.28	77.33	77.23	77.01
	200	77.12	77.19	77.11	77.06	76.99	77.88	78.46	78.14	77.99	77.8
6	50	77.26	78.65	79.52	79.09	80.12	75.65	77.23	77.44	79.06	78.44
	100	84.63	84.59	84.17	85.74	85.03	84.2	84.69	84.34	84.62	84.91
	150	84.66	85.17	85.33	85.45	85.4	84.97	85.32	85.2	86.48	85.93
	200	86.35	86.35	86.36	87.17	86.83	85.99	87.1	86.9	87.27	87.53
7	50	64.49	66.32	65.35	66.5	66.69	66.8	65.44	65.53	66.87	68.5
	100	71.22	72.94	71.64	72.64	73.37	71.48	71.63	71.8	72.03	73.12
	150	76.65	76.63	76.31	76.69	76.05	75.11	77.25	76.11	76.73	76.76
	200	77.48	77.95	77.97	77.08	78.06	77.66	79	78.04	78.16	78.44
8	50	69.61	69.48	70.75	70.81	70.62	70.7	71.38	71.38	71.83	71.14
	100	74.38	74.51	74.38	74.44	74.28	73.16	73.68	73.43	73.13	73.3
	150	77.07	77.52	77.19	77.07	77.22	75.89	76.73	76.81	76.4	76.61
	200	79.5	79.51	79.24	79.86	79.36	78.47	78.59	78.61	78.99	79.76

Bold values are the best average values

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## List of Symbols

Variable	Description	SI unit
u	solid displacement	m
$\boldsymbol{u}_f$	fluid displacement	m



## Acknowledgements

Here you might want to acknowledge someone.

