

COUNTER-INTUITIVE ACOUSTO-ELASTICITY

Author:

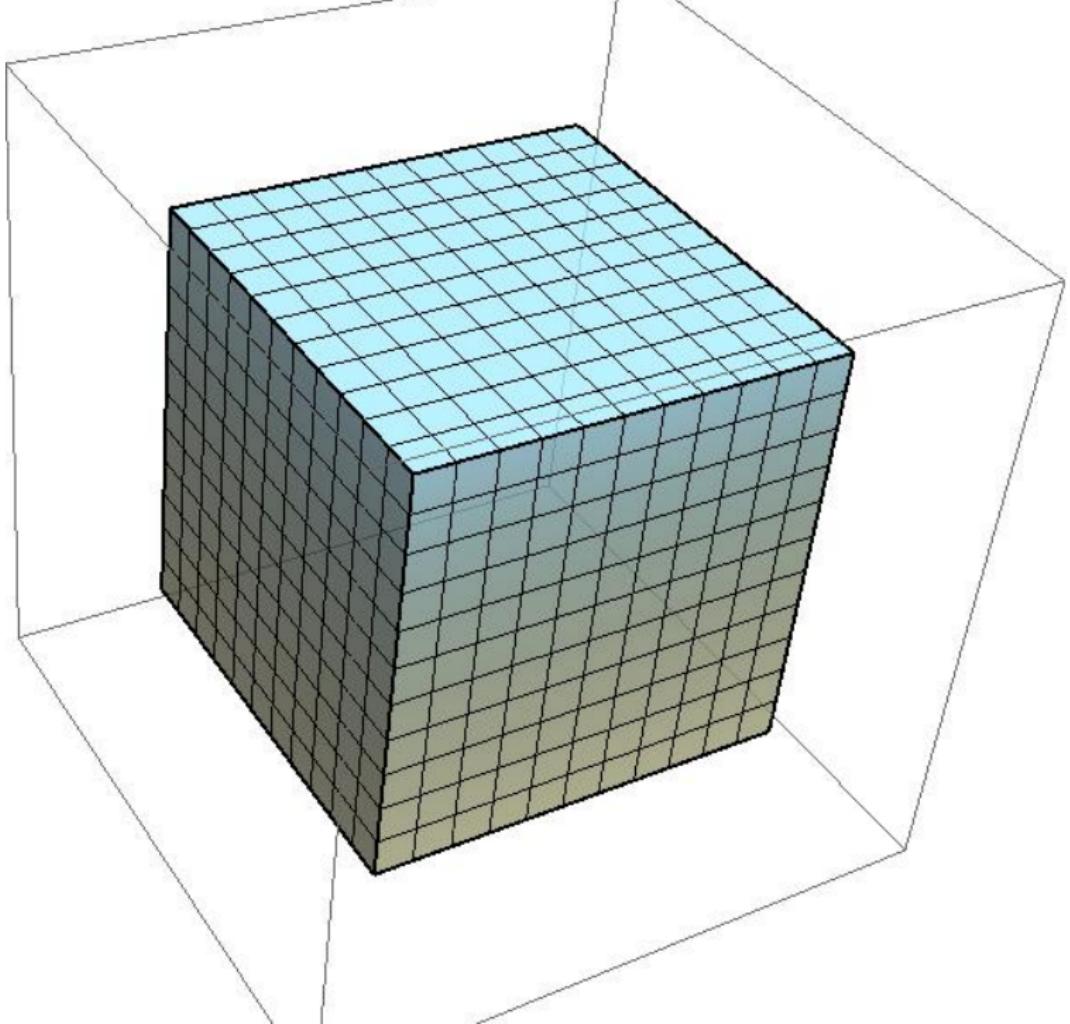
Artur L. Gower

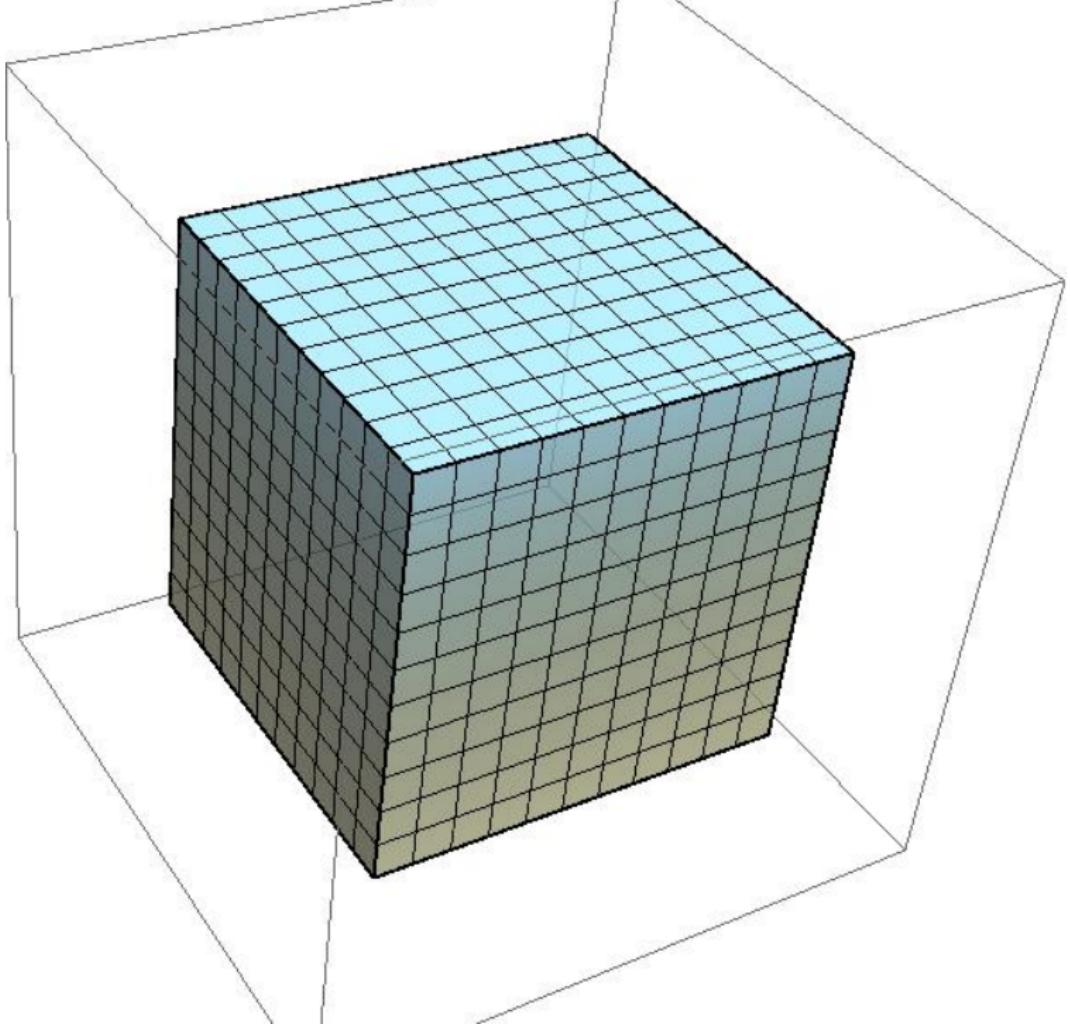
Co-Authors:

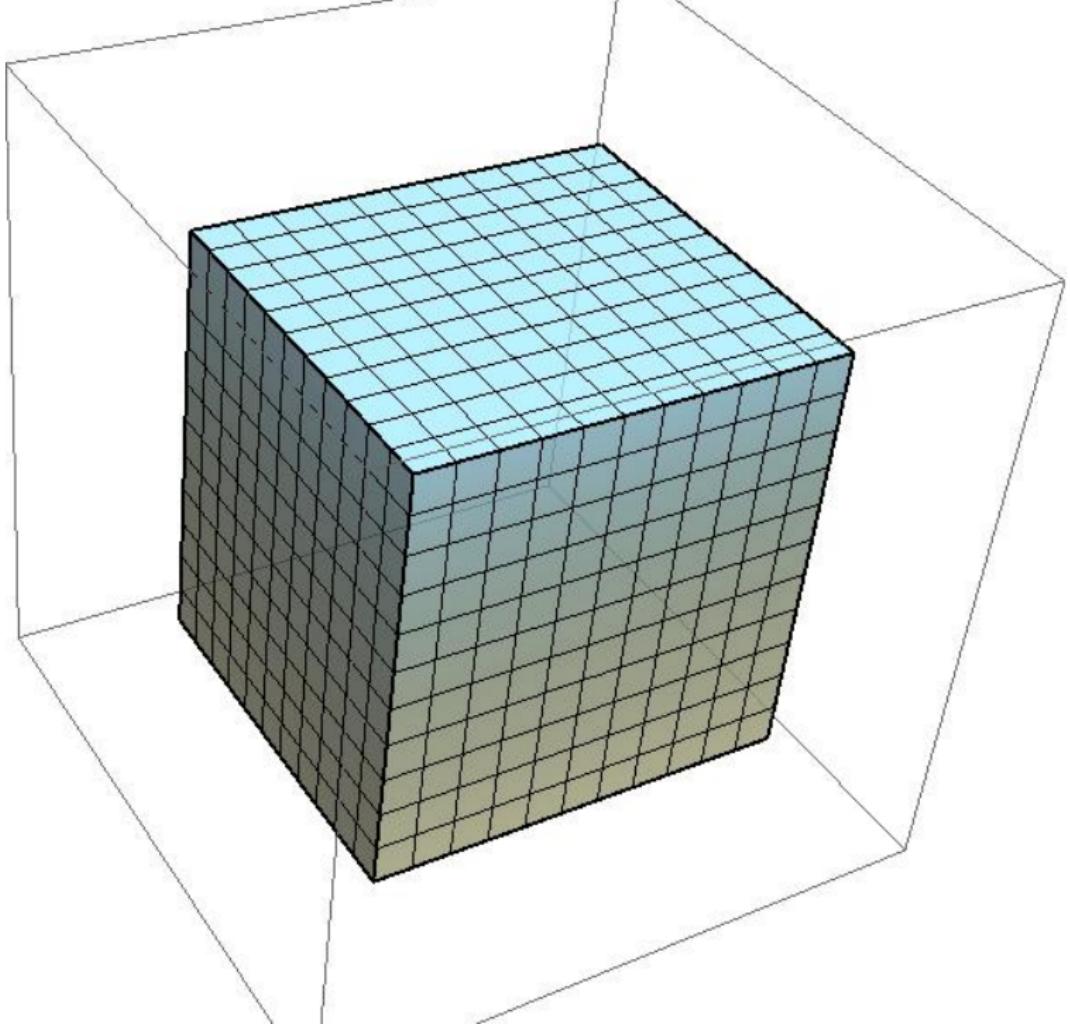
Prof. Michel Destrade
Prof. Ray Ogden

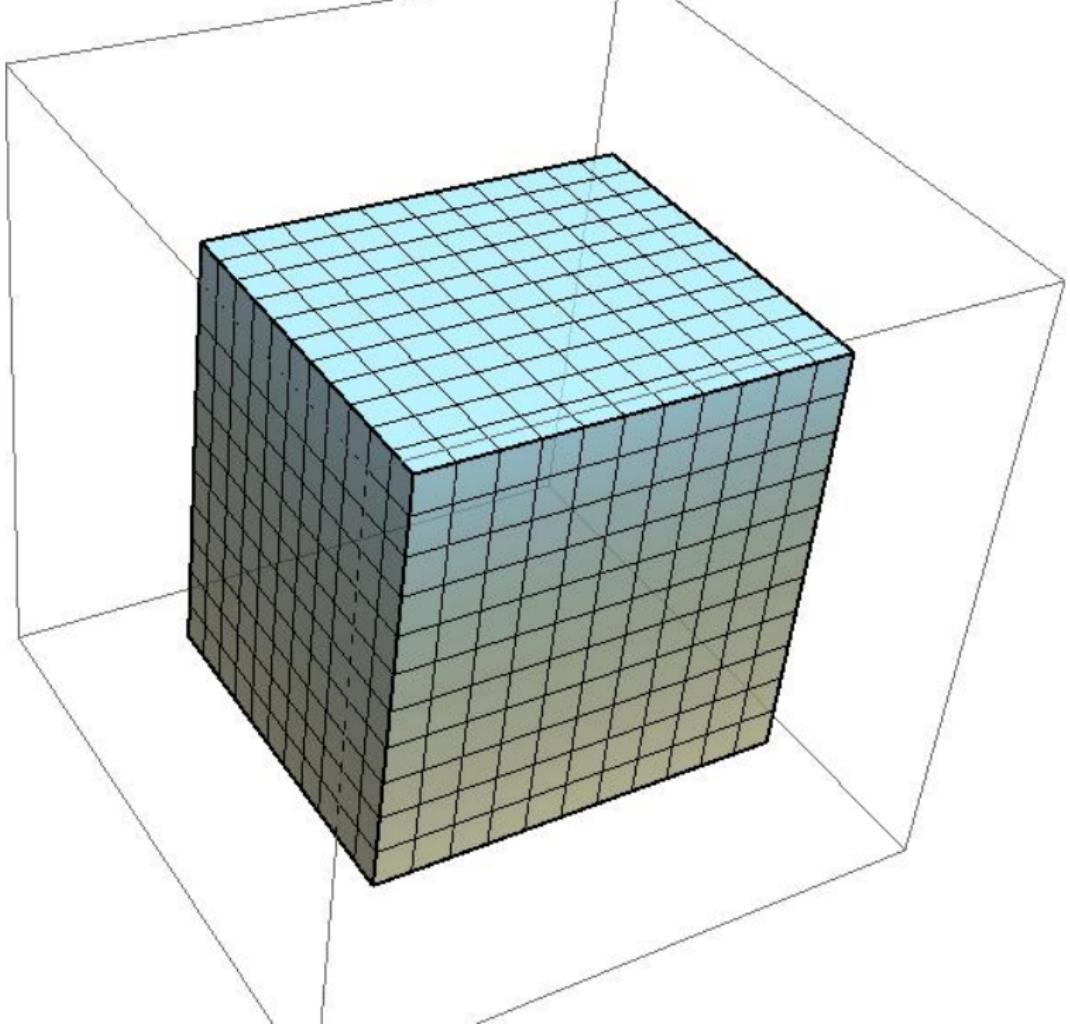
National University of Ireland Galway

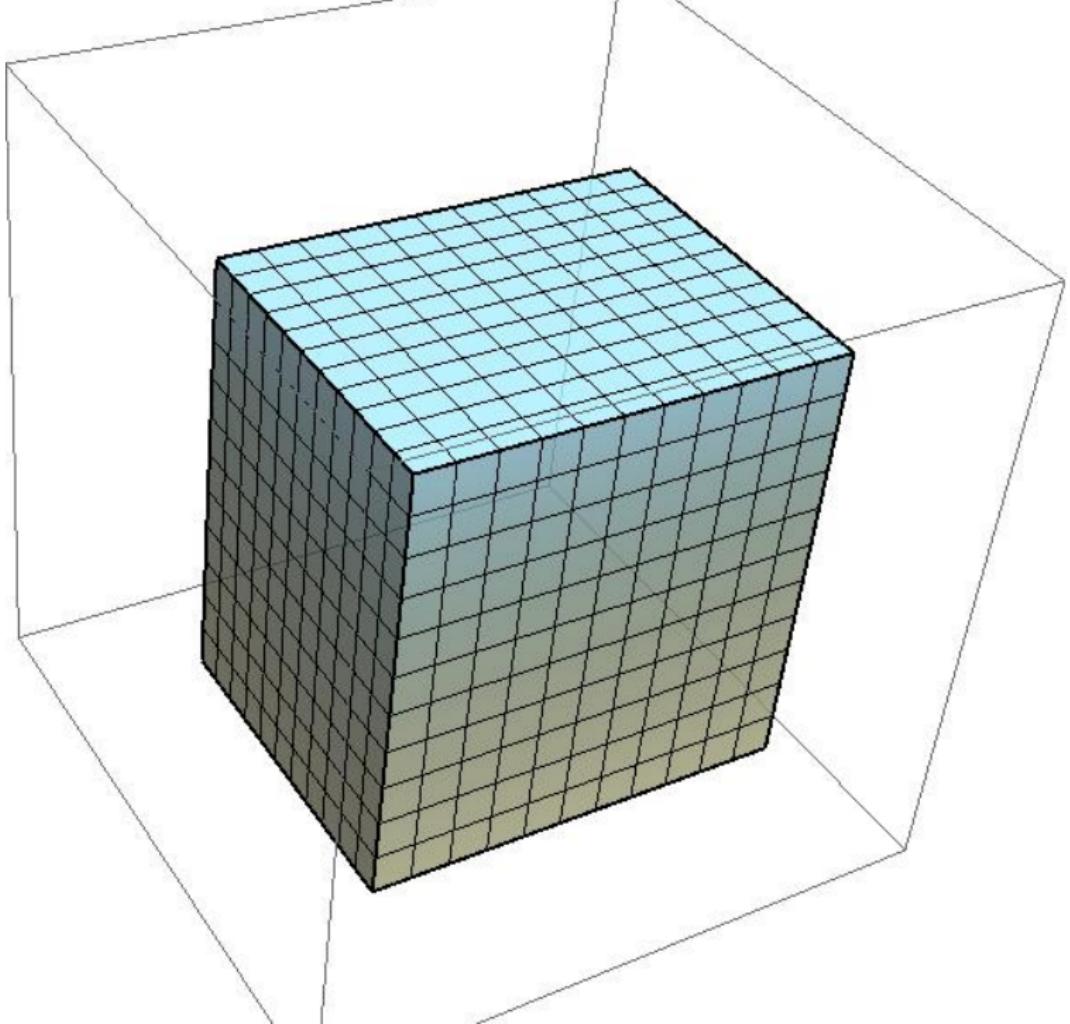


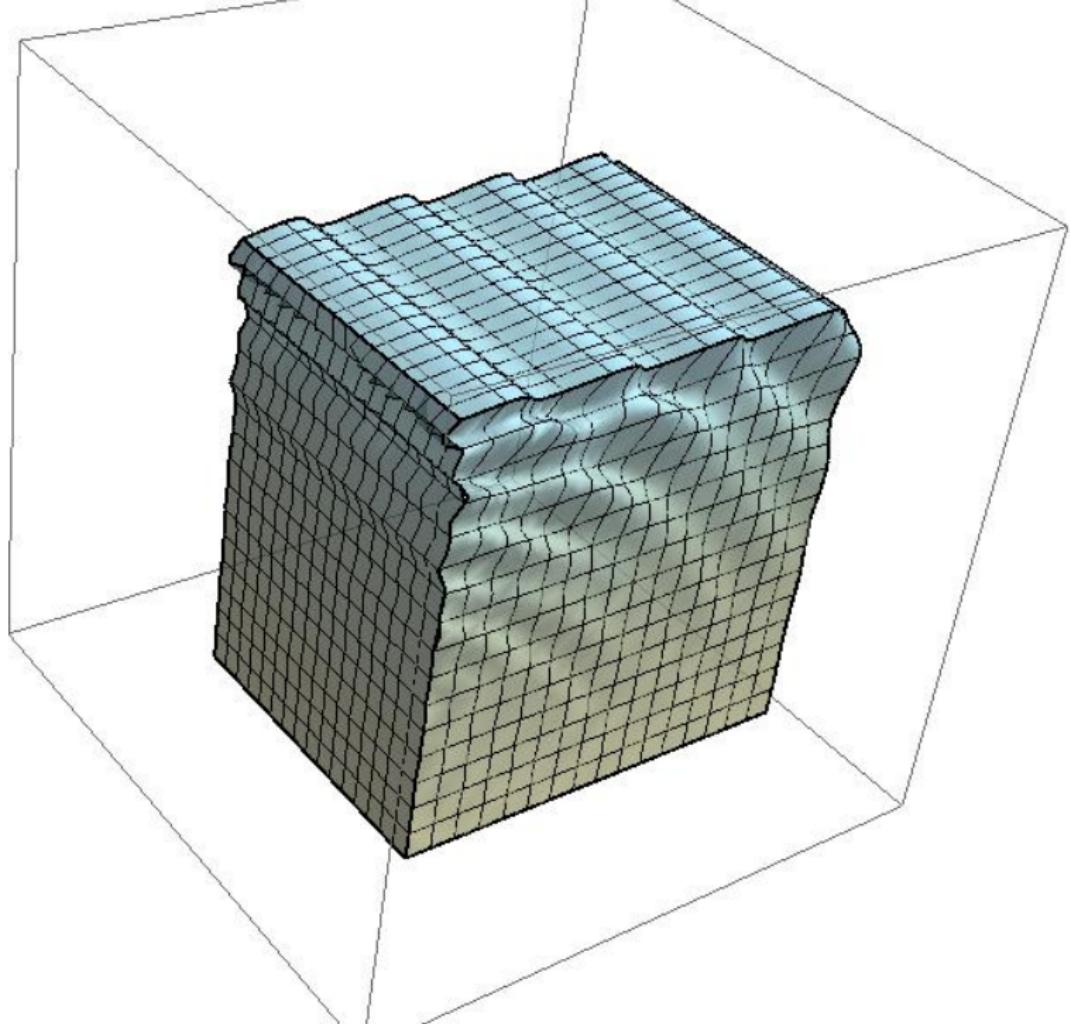


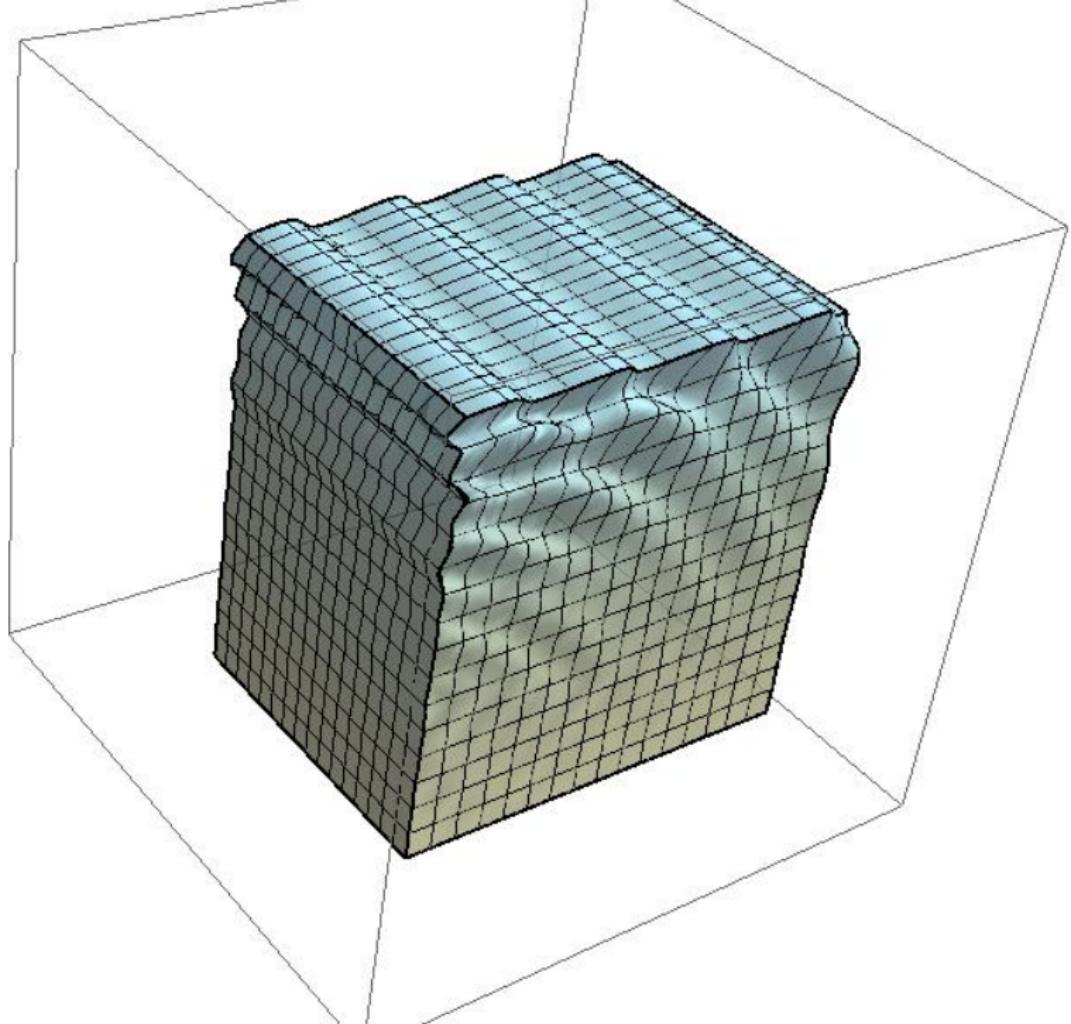


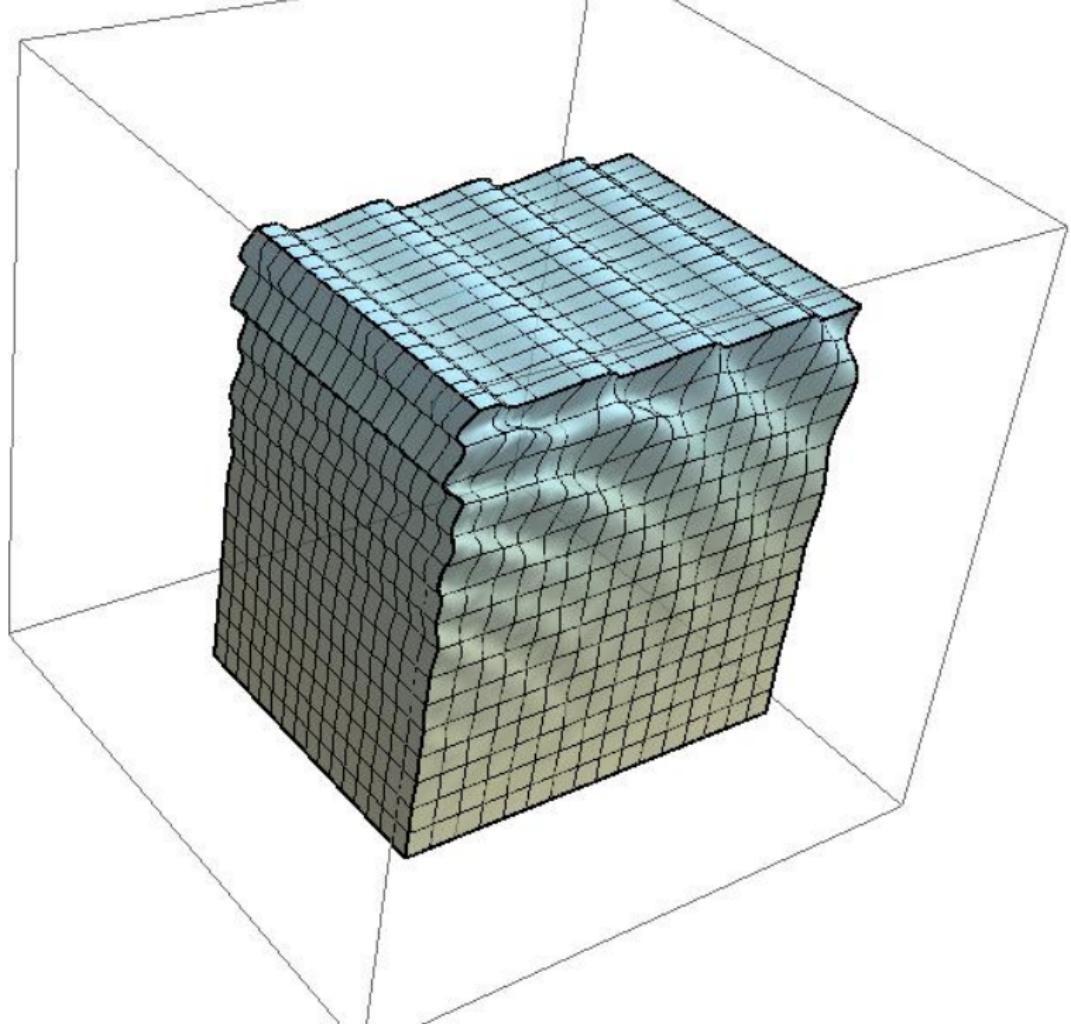


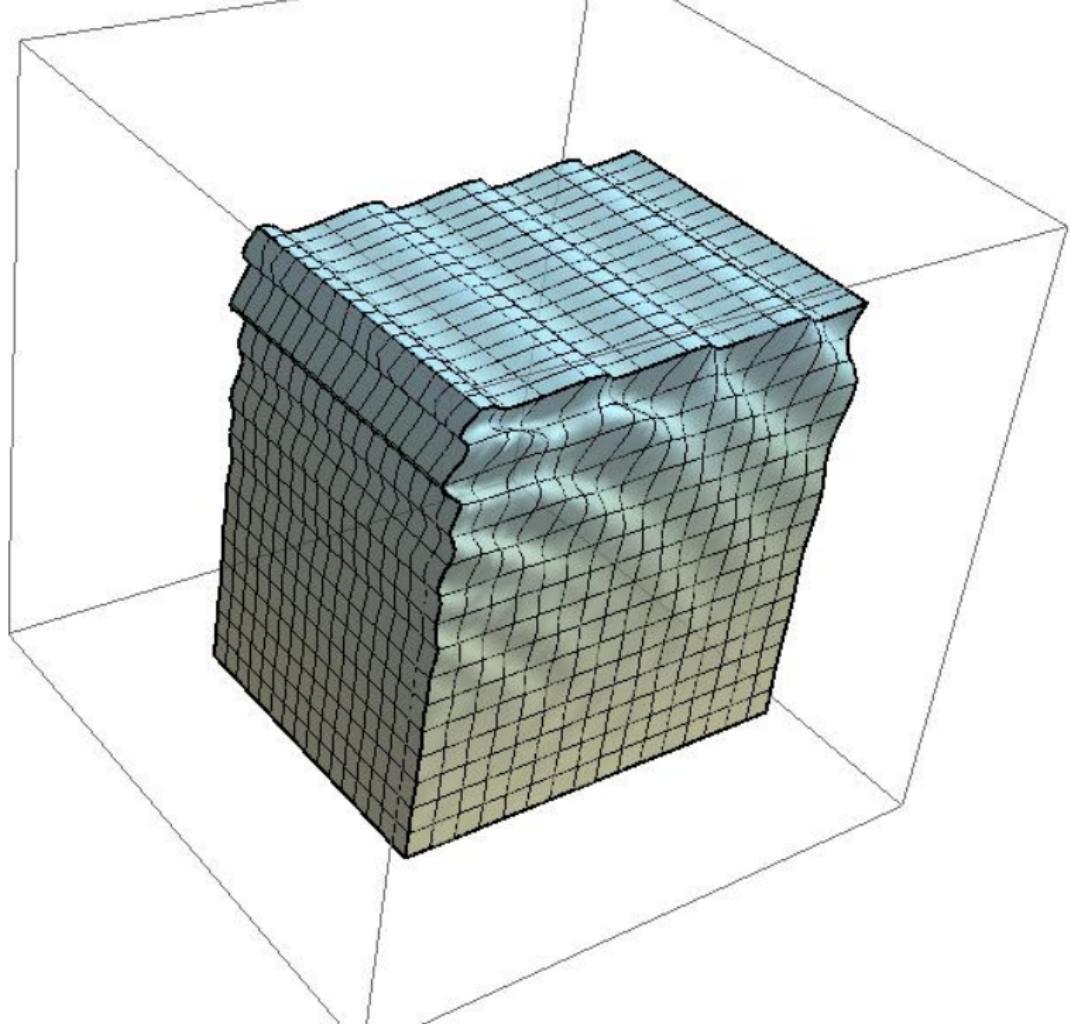


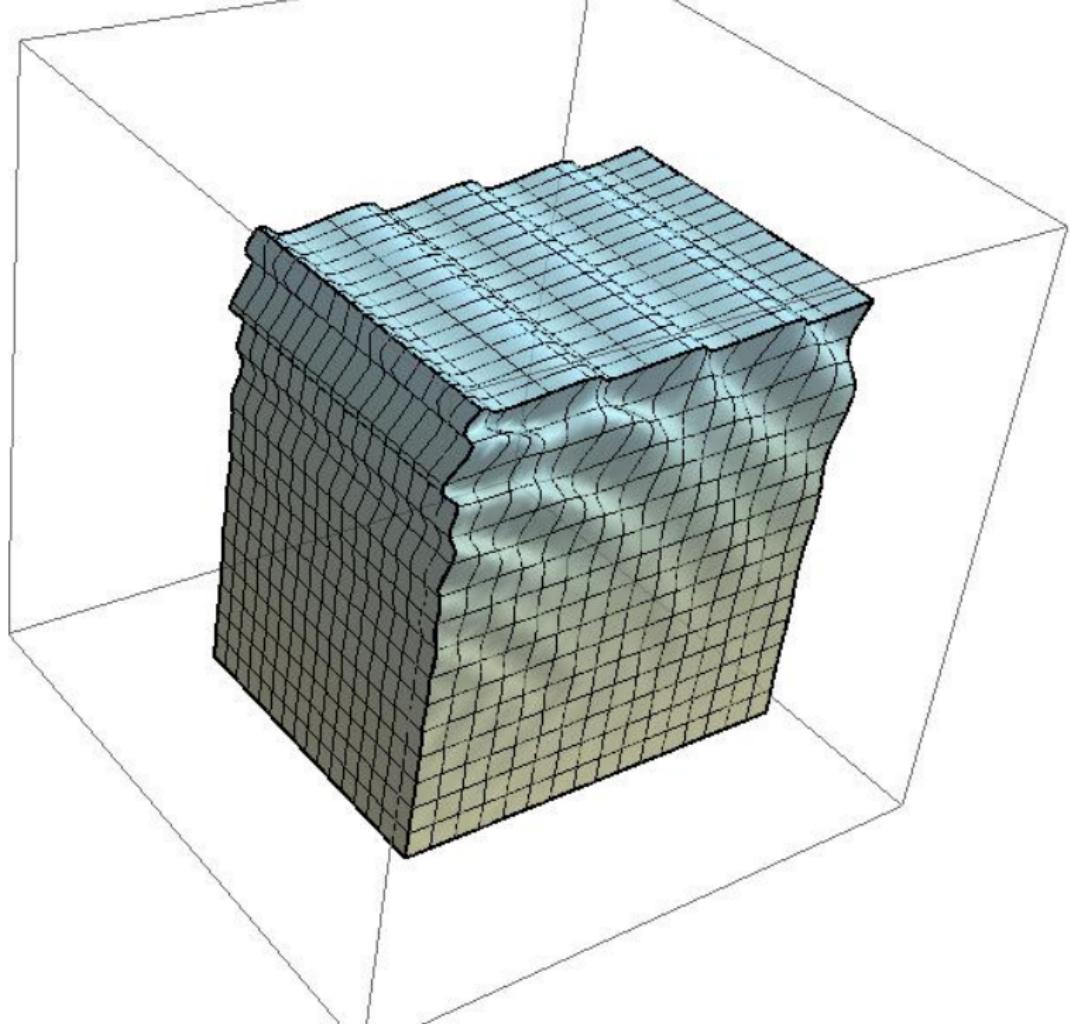


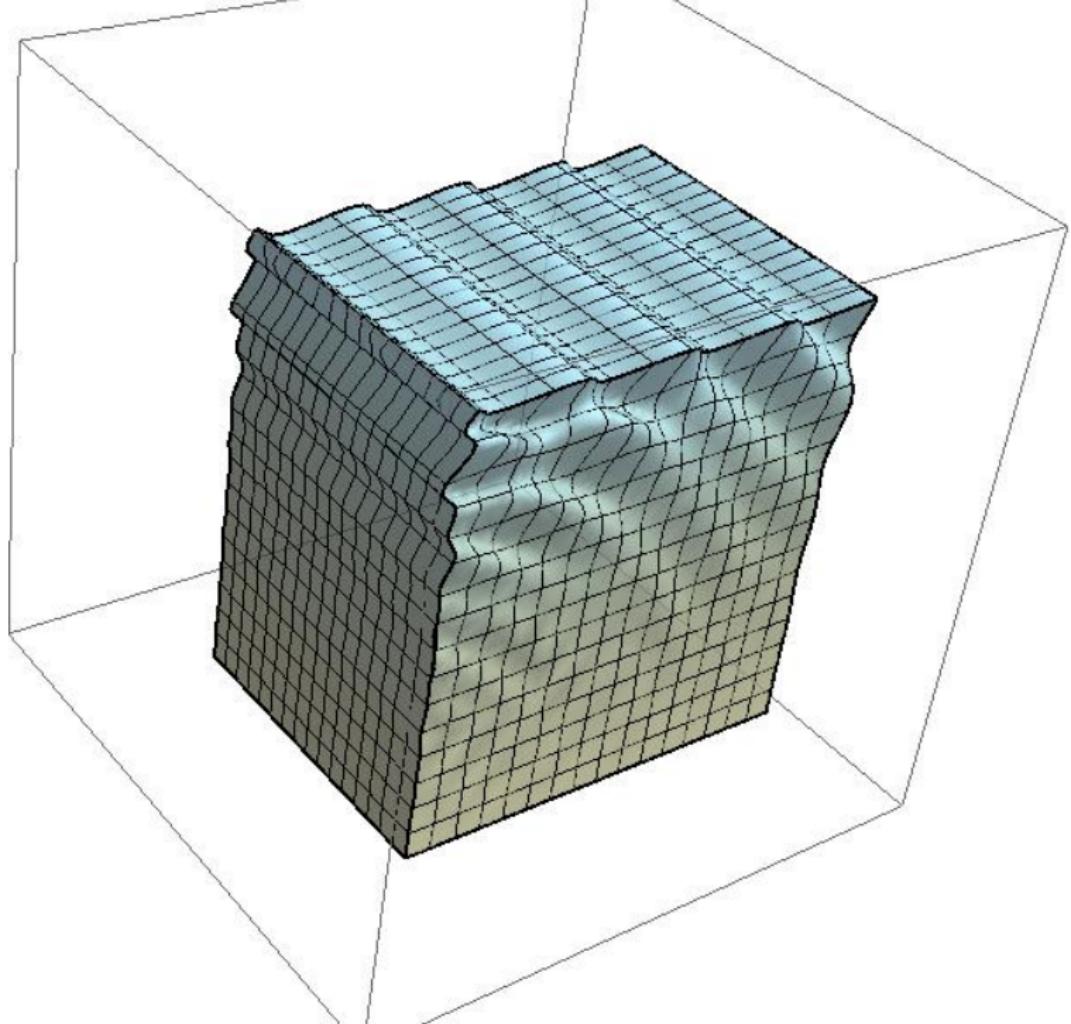


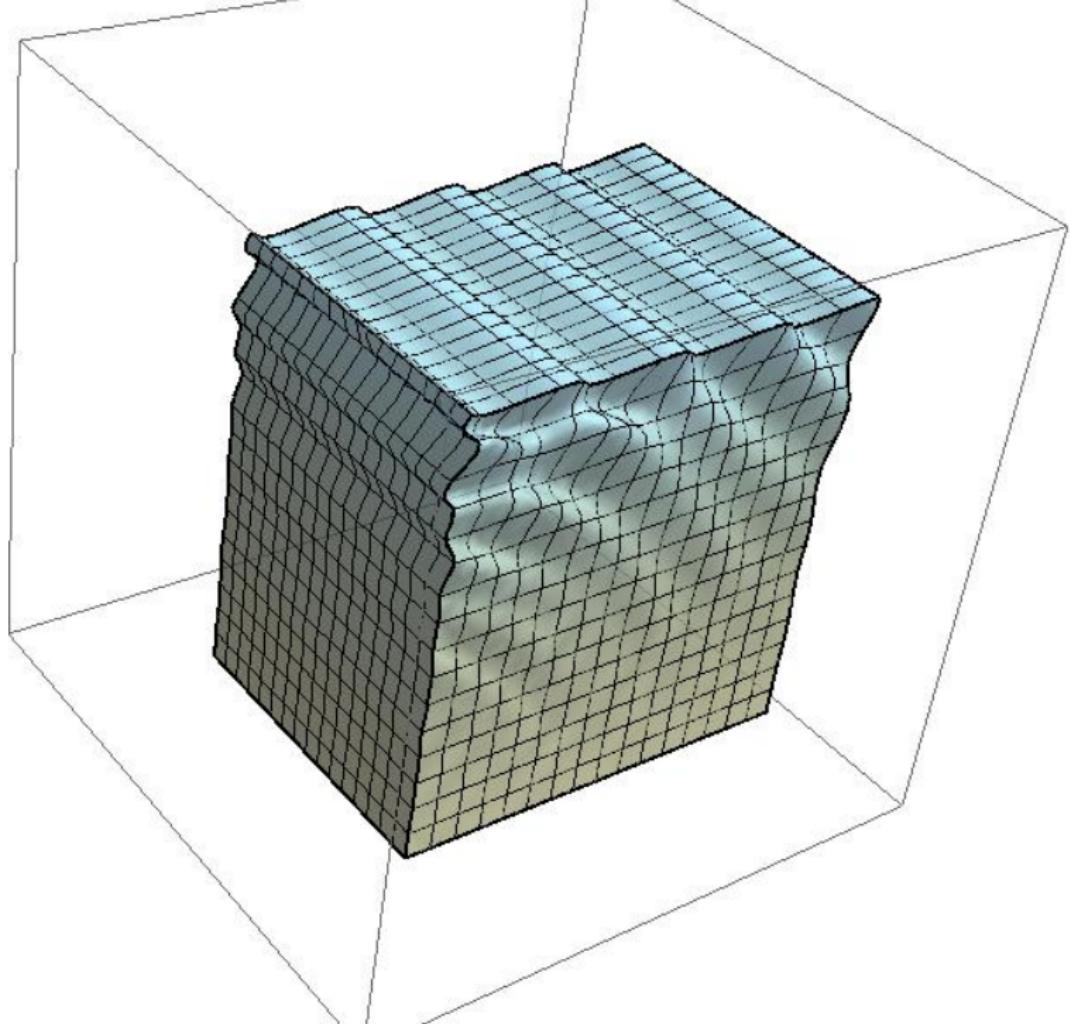


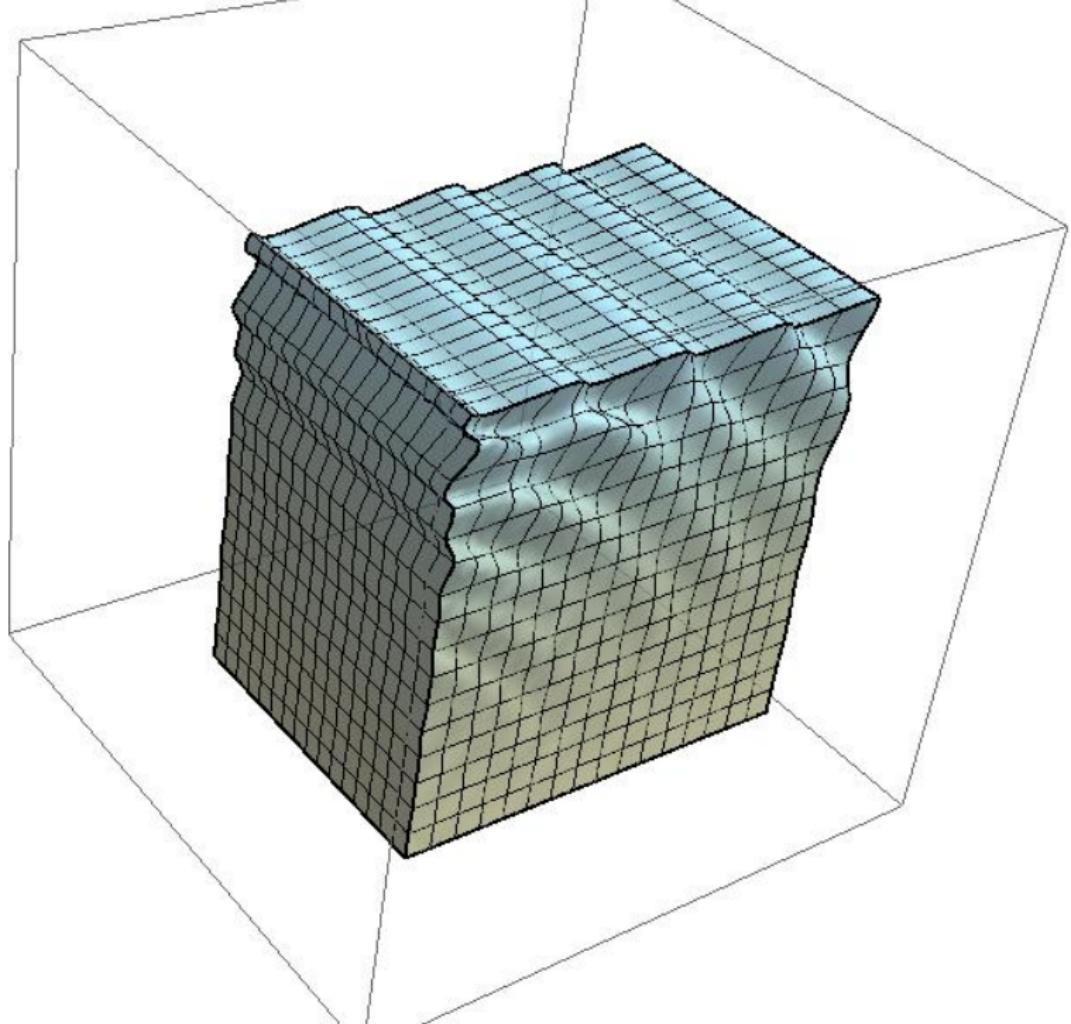


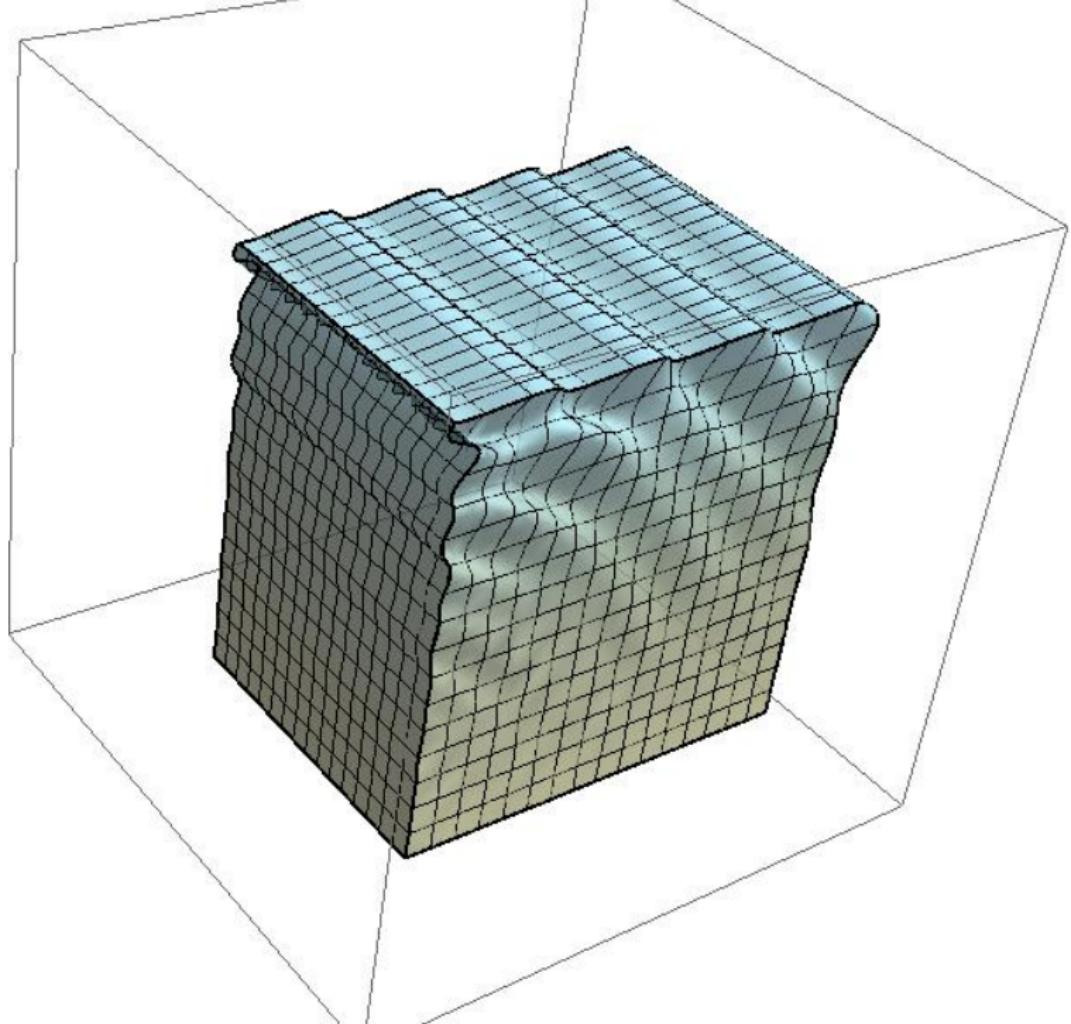






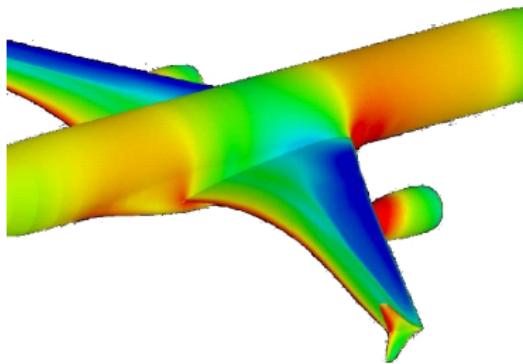






Waves tell us about stress

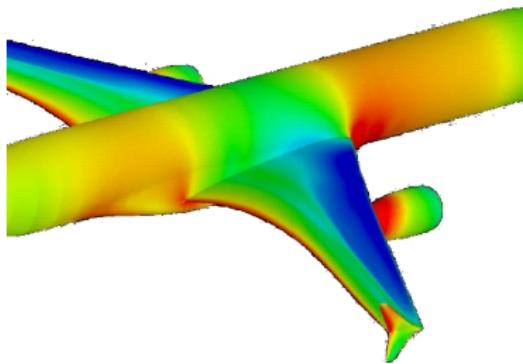
Measure wave velocity to uncover
stress field →



← Predict wave velocity from a
known stress field

Waves tell us about stress

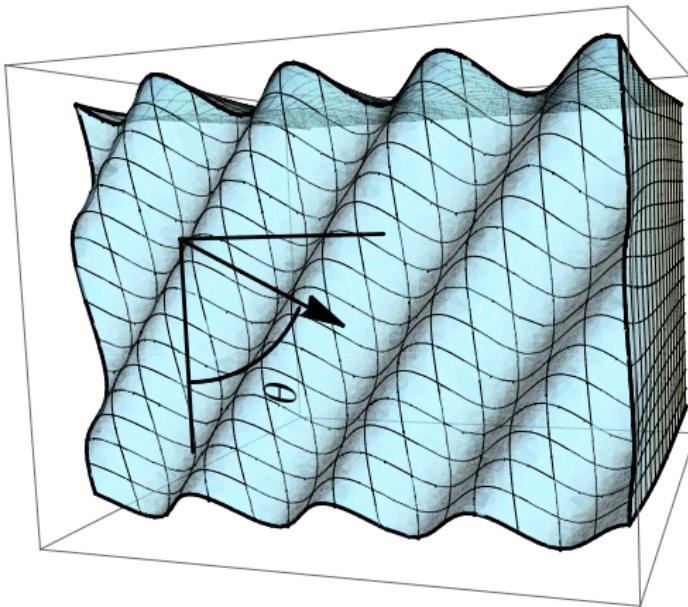
Measure wave velocity to uncover
stress field →



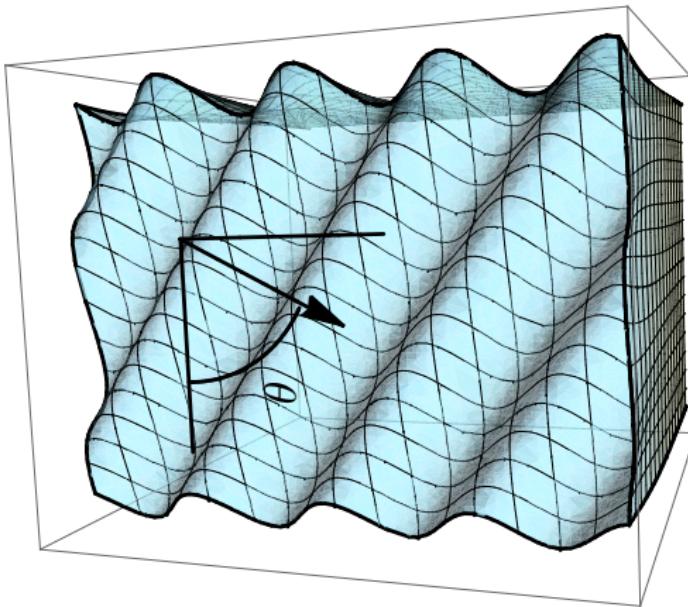
← Predict wave velocity from a
known stress field

Because rocks behave approximately like a big rubber ball.

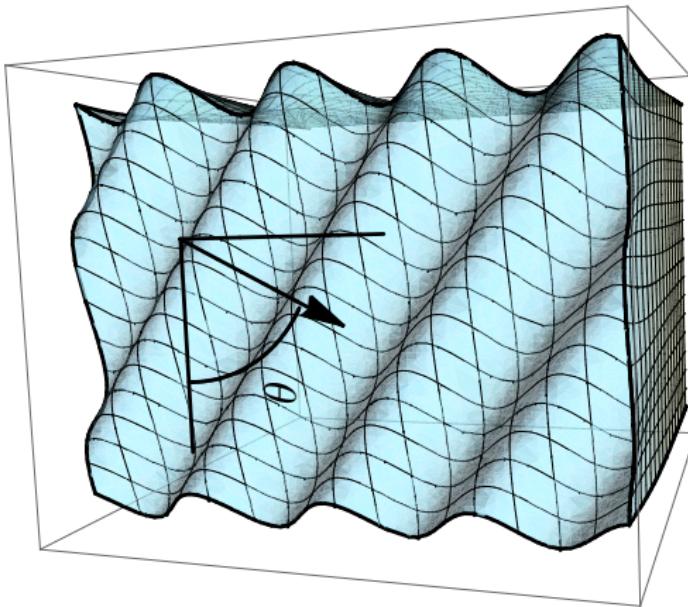
Wavefront Angle from direction of Greatest Compression



Wavefront Angle from direction of Greatest Compression



Wavefront Angle from direction of Greatest Compression

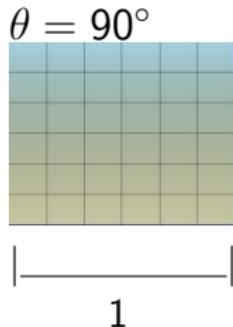


$$\mathbf{u}(x, y, z) = \mathcal{U}(y) e^{ik(x \cos \theta + z \sin \theta - vt)} \quad (\text{Incremental displacement})$$

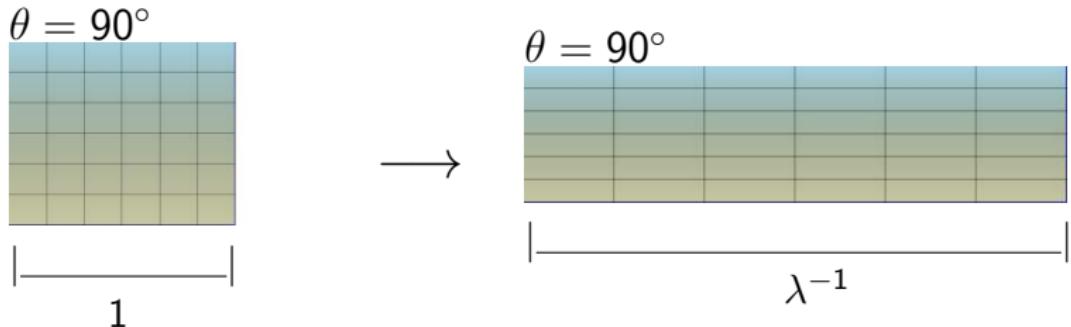
$$\lim_{y \rightarrow \infty} \mathcal{U}(y) = 0 \text{ and } \mathcal{V}(0) = \mathbf{0} \quad (\text{Boundary conditions})$$

(CORRECT DECAY & ZERO SURFACE TRACTION)

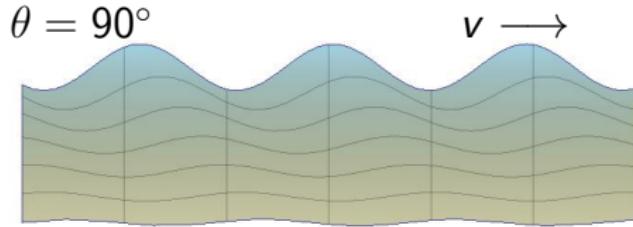
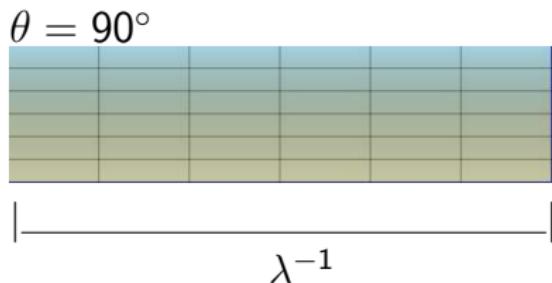
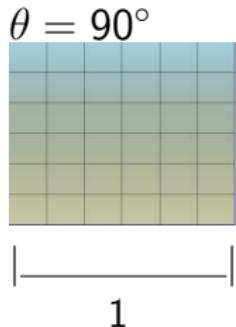
What is intuitive about a deformed isotropic material?



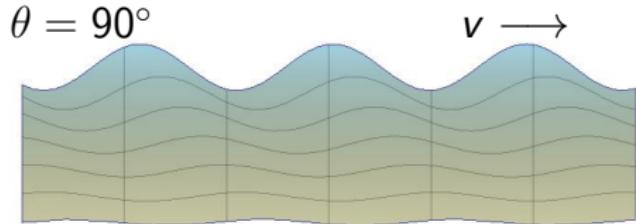
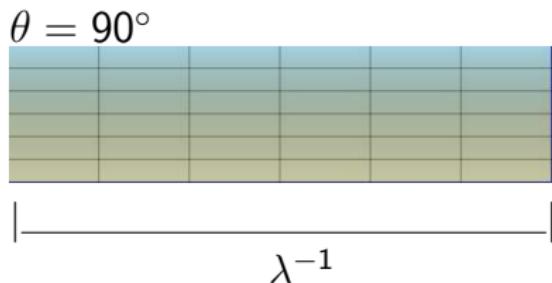
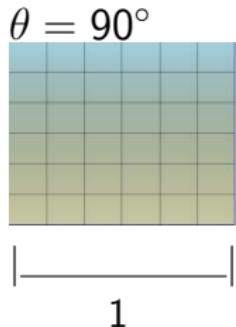
What is intuitive about a deformed isotropic material?



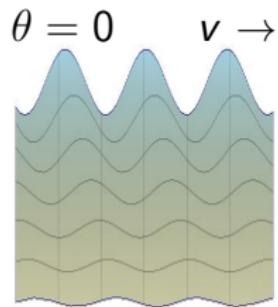
What is intuitive about a deformed isotropic material?



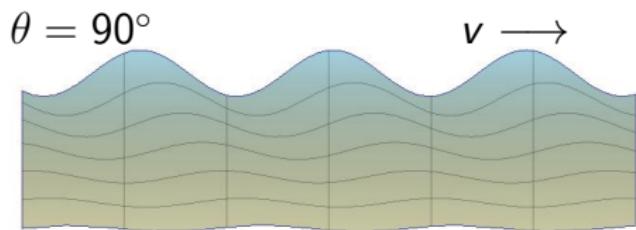
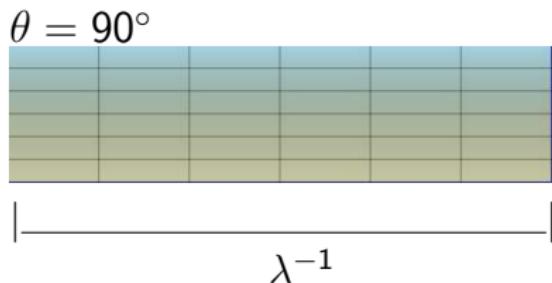
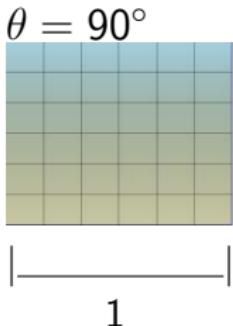
What is intuitive about a deformed isotropic material?



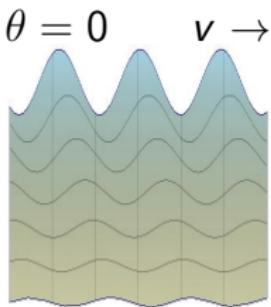
Faster
than



What is intuitive about a deformed isotropic material?



Faster
than



ISOTROPIC:

Direction of greatest stress = Direction of greatest strain

Inuitive Infinitesimal Prestress

- ▶ K.Y. Kim, W. Sachse, (2001):
“The principal stress direction is found where the variations of the SAW speeds show symmetry about the direction”.

Inuitive Infinitesimal Prestress

- ▶ K.Y. Kim, W. Sachse, (2001):
“The principal stress direction is found where the variations of the SAW speeds show symmetry about the direction”.
- ▶ K. Tanuma, C.-S. Man, W. Du., (2013):

$$v_R(\theta) = v_R^0 + C_1(\sigma_1 + \sigma_2) - C_2(\sigma_1 - \sigma_2) \cos 2\theta ,$$

Inuitive Infinitesimal Prestress

- ▶ K.Y. Kim, W. Sachse, (2001):
“The principal stress direction is found where the variations of the SAW speeds show symmetry about the direction”.
- ▶ K. Tanuma, C.-S. Man, W. Du., (2013):

$$v_R(\theta) = v_R^0 + C_1(\sigma_1 + \sigma_2) - C_2(\sigma_1 - \sigma_2) \cos 2\theta ,$$

$$v_R(0) = v_R^0 + C_1(\sigma_1 + \sigma_3) - C_2(\sigma_1 - \sigma_3) \quad \leftarrow \text{Min Velocity}$$

$$v_R(\pi/2) = v_R^0 + C_1(\sigma_1 + \sigma_3) + C_2(\sigma_1 - \sigma_3) \quad \leftarrow \text{Max Velocity}$$

If the principal pre-stresses along the surface σ_1 and σ_3 satisfy $\sigma_1 > \sigma_2$. Where C_1 and C_2 are complicated constants.

Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

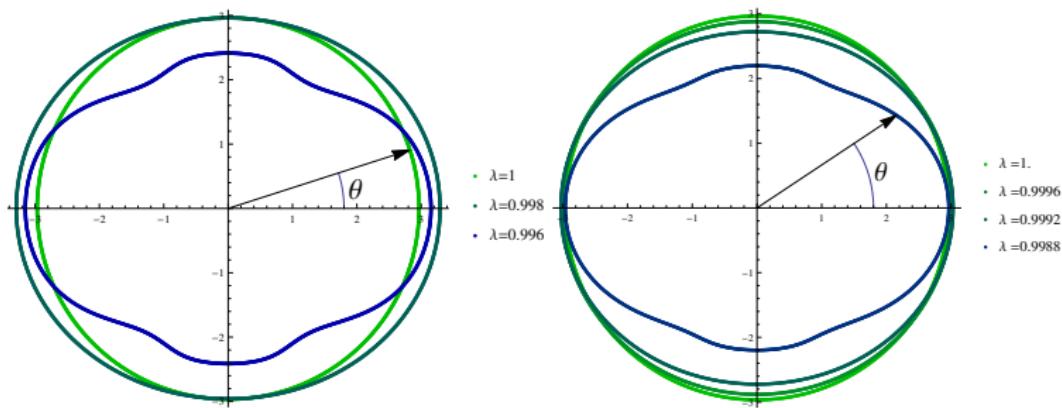


Figure: Speed profiles for surface waves (plotted as $v\sqrt{\rho}$) in Concrete subject to Uniaxial stress (left) and to Shear Stress (right).

Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

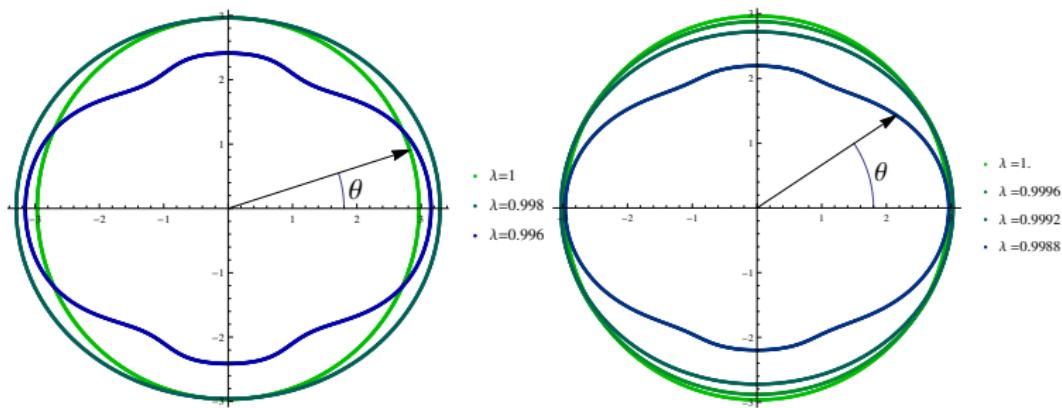
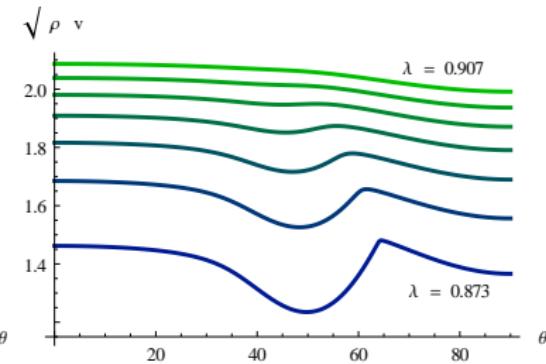
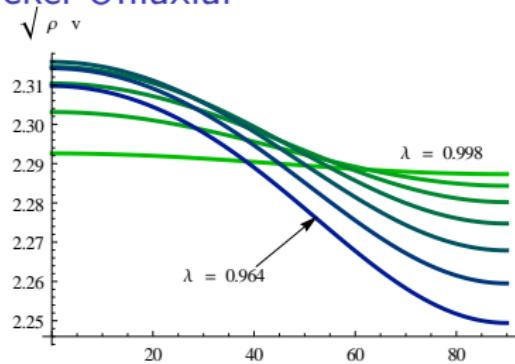


Figure: Speed profiles for surface waves (plotted as $v\sqrt{\rho}$) in Concrete subject to Uniaxial stress (left) and to Shear Stress (right).

- The sinusoidal regularity was lost early, for strains less than 1% (though the stress is reasonable.)

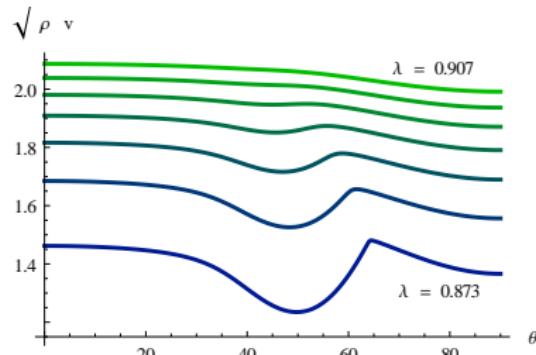
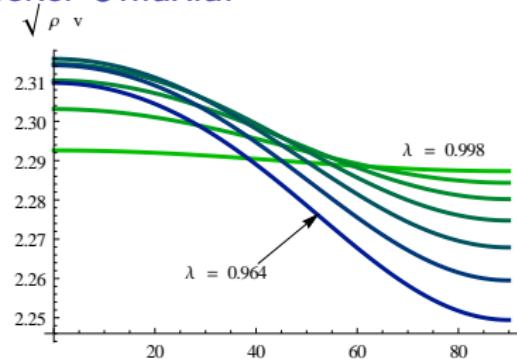
Nonlinear Elastic Results

Nickel Uniaxial

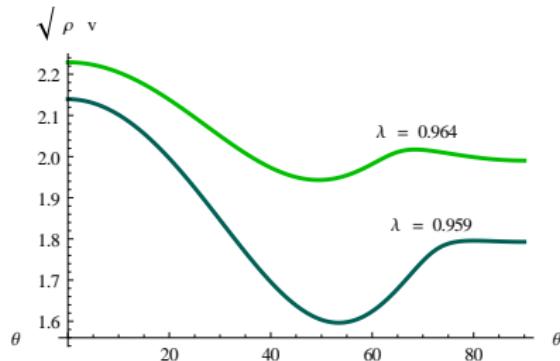
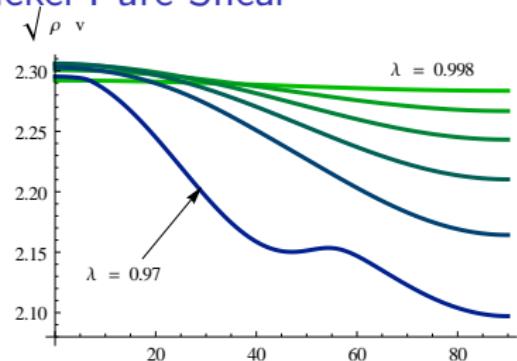


Nonlinear Elastic Results

Nickel Uniaxial



Nickel Pure Shear



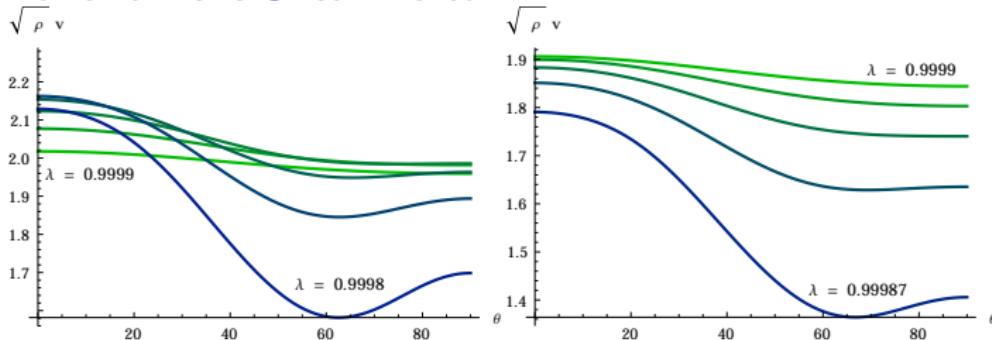
Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

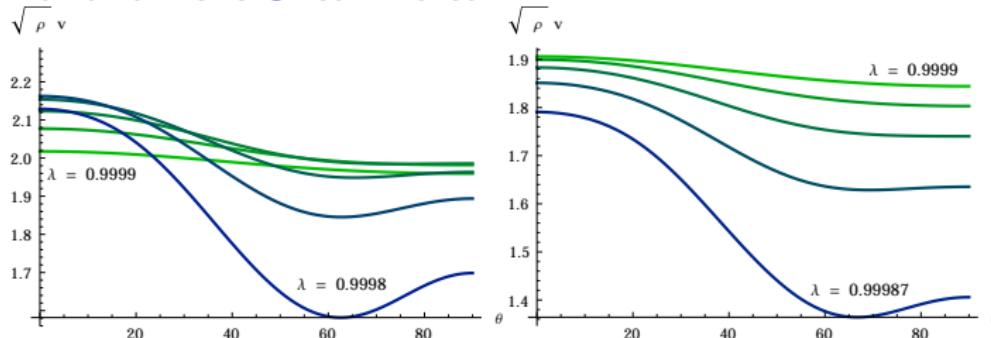
Uniaxial and Pure Shear Berea



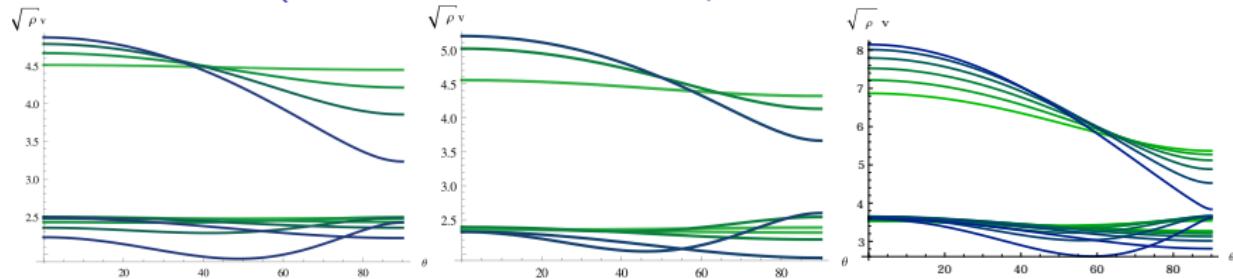
Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

Uniaxial and Pure Shear Berea



Bulk Waves (Nickel, Steel and Concrete)



Matrix Impedance Method

Incremental quantities:

$$\mathbf{u}(x, y, t) = \underbrace{\mathcal{U}(y) e^{ikx - i\omega t}}_{Displacement}$$

$$\mathbf{v}(x, y, t) = \underbrace{-i\mathcal{V}(y) e^{ikx - i\omega t}}_{Normal Traction}$$

Matrix Impedance Method

Incremental quantities:

$$\mathbf{u}(x, y, t) = \underbrace{\mathcal{U}(y) e^{ikx - i\omega t}}_{Displacement}$$

$$\mathbf{v}(x, y, t) = \underbrace{-i\mathcal{V}(y) e^{ikx - i\omega t}}_{Normal Traction}$$

Surface Waves:

$$\lim_{y \rightarrow \infty} \mathcal{U}(y) = 0$$

Matrix Impedance Method

Incremental quantities:

$$\mathbf{u}(x, y, t) = \underbrace{\mathcal{U}(y)e^{ikx - i\omega t}}_{Displacement} \quad \mathbf{v}(x, y, t) = \underbrace{-i\mathcal{V}(y)e^{ikx - i\omega t}}_{Normal Traction}$$

Surface Waves:

$$\lim_{y \rightarrow \infty} \mathcal{U}(y) = 0 \quad \text{and} \quad \mathcal{V}(0) = 0,$$

Matrix Impedance Method

Incremental quantities:

$$\mathbf{u}(x, y, t) = \underbrace{\mathcal{U}(y) e^{ikx - i\omega t}}_{Displacement} \quad \mathbf{v}(x, y, t) = \underbrace{-i\mathcal{V}(y) e^{ikx - i\omega t}}_{Normal Traction}$$

Surface Waves:

$$\lim_{y \rightarrow \infty} \mathcal{U}(y) = 0 \quad \text{and} \quad \mathcal{V}(0) = 0,$$

the decay condition and zero-traction lead to

$$\mathcal{V}(y) = -iZ(\nu)\mathcal{U}(y) \quad \text{and} \quad \det Z(\nu) = 0.$$

Matrix Impedance Method

Incremental quantities:

$$\mathbf{u}(x, y, t) = \underbrace{\mathcal{U}(y)e^{ikx - i\omega t}}_{Displacement} \quad \mathbf{v}(x, y, t) = \underbrace{-i\mathcal{V}(y)e^{ikx - i\omega t}}_{Normal Traction}$$

Surface Waves:

$$\lim_{y \rightarrow \infty} \mathcal{U}(y) = 0 \quad \text{and} \quad \mathcal{V}(0) = 0,$$

the decay condition and zero-traction lead to

$$\mathcal{V}(y) = -iZ(\nu)\mathcal{U}(y) \quad \text{and} \quad \det Z(\nu) = 0.$$

We've identified the object of study $Z(\nu)$, now for some *magic*.

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy - v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0)}_{\text{Surface Stress Power}} = \frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy - v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy}_{\text{Potential Energy}} - v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy}_{\text{Kinetic Energy}}$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy}_{\text{Kinetic Energy}}$$

Meaning,

$$\mathcal{U}^*(0) \cdot Z(0) \mathcal{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy,$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathcal{U}^*(0) \cdot Z(v) \mathcal{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy}_{\text{Kinetic Energy}}$$

Meaning,

$$\mathcal{U}^*(0) \cdot Z(0) \mathcal{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathcal{U}(y)) dy,$$

$$\mathcal{U}^*(0) \cdot \frac{\partial Z(v)}{\partial v} \mathcal{U}(0) = -2v \int_0^\infty \rho \mathcal{U}^*(y) \cdot \mathcal{U}(y) dy,$$

positive definite $Z(0)$ with monotone decreasing Eigenvalues!

Analytic Solution

from balance of momentum we get an algebraic Riccati equation,

$$H^\dagger(v)H(v) = Q - \rho v^2 I \quad \text{and} \quad Z(v) = T^{1/2}H(v) - iR,$$

Analytic Solution

from balance of momentum we get an algebraic Riccati equation,

$$H^\dagger(v)H(v) = Q - \rho v^2 I \quad \text{and} \quad Z(v) = T^{1/2}H(v) - iR,$$

where T , R and Q depend on the instantaneous (incremental) moduli \mathcal{A}_{ijkl} .

Analytic Solution

from balance of momentum we get an algebraic Riccati equation,

$$H^\dagger(v)H(v) = Q - \rho v^2 I \quad \text{and} \quad Z(v) = T^{1/2}H(v) - iR,$$

where T , R and Q depend on the instantaneous (incremental) moduli \mathcal{A}_{ijkl} .

The restriction

$$Z(v) > 0$$

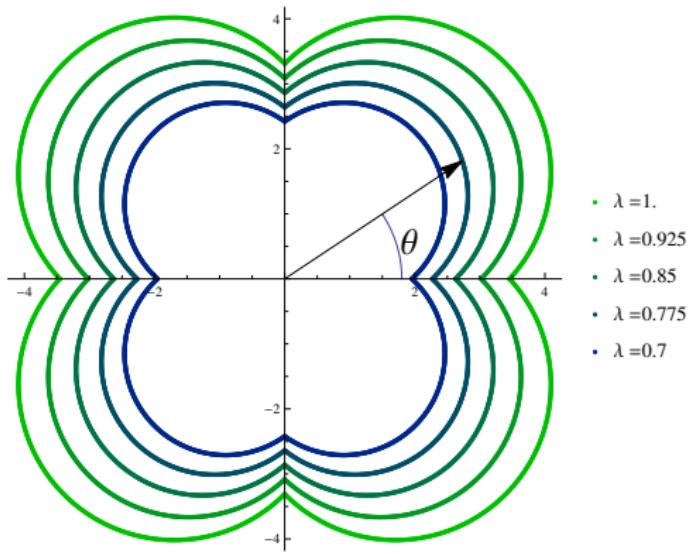
uniquely defines $Z(v)$, which is then easy to find numerically for each v .

More results

This procedure works for any elastic strain-energy function, for example...

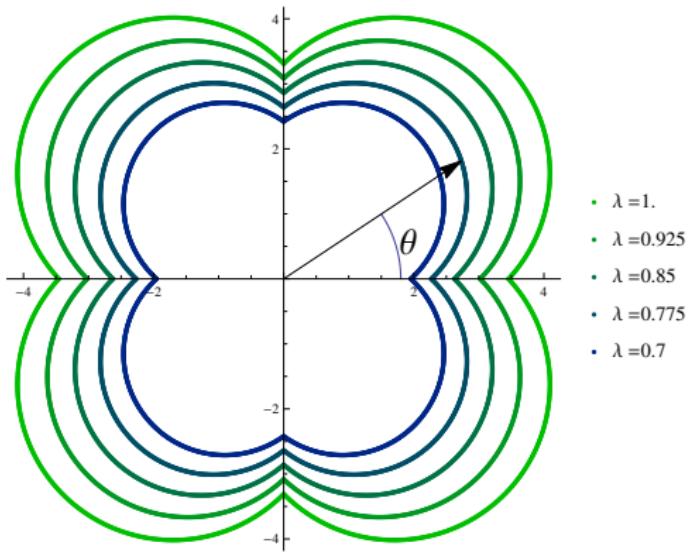
More results

This procedure works for any elastic strain-energy function, for example...



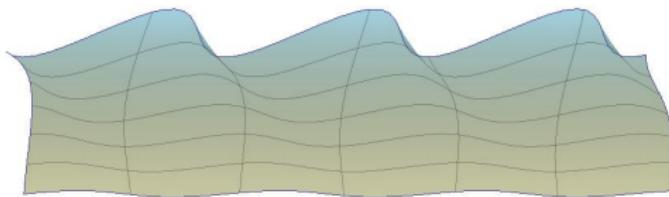
More results

This procedure works for any elastic strain-energy function, for example...

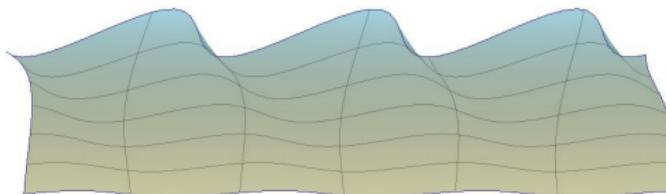


A model for skin, that has a neo-hookean matrix with fibers. This is an example of shear against the skin fibers.

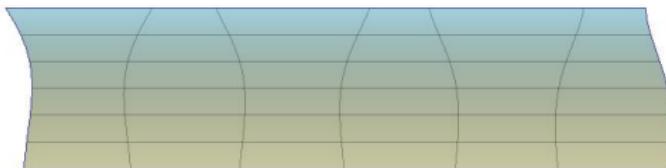
What happened to our intuition?



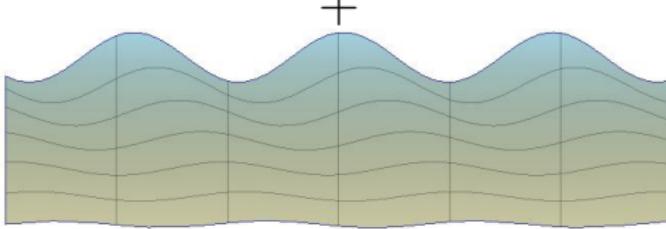
What happened to our intuition?



||

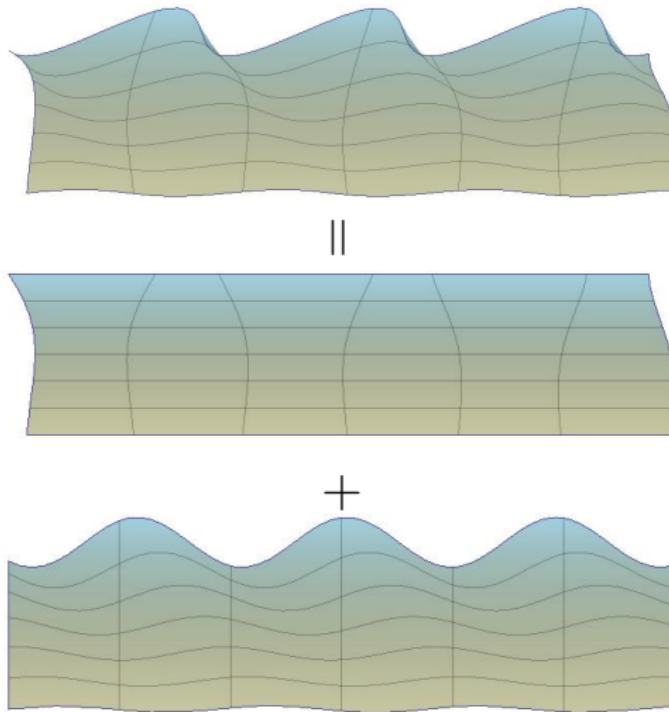


+



Any questions?

What happened to our intuition?



Any questions?

Thanks for listening and hope you enjoyed the talk!

-  A.L. Gower, M. Destrade and R.W. Ogden Counter-intuitive results in acousto-elasticity, *Wave Motion*, (2013) doi:10.1016/j.wavemoti.2013.03.007 (In Press)
-  A. Mielke, Y.B. Fu. A proof of uniqueness of surface waves that is independent of the Stroh Formalism, *Math. Mech. Solids* **9** (2003), 5–15.
-  K.Y. Kim, W. Sachse. Acoustoelasticity of elastic solids, in *Handbook of Elastic Properties of Solids, Liquids, and Gases*, **1**, 441–468. Academic Press, New York (2001).
-  K. Tanuma, C.-S. Man, W. Du. Perturbation of phase velocity of Rayleigh waves in pre-stressed anisotropic media with orthorhombic principal part, *Math. Mech. Solids*, DOI:10.1177/1081286512438882 (In Press)