

COUNTER-INTUITIVE ACOUSTO-ELASTICITY

Author:

Artur L. Gower

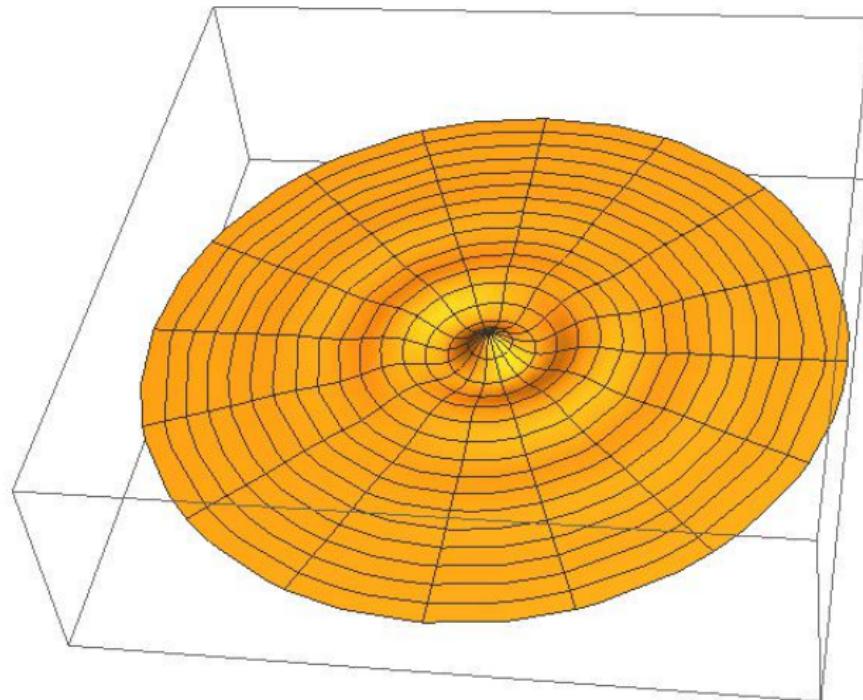
Co-Authors:

Prof. Michel Destrade
Prof. Ray Ogden

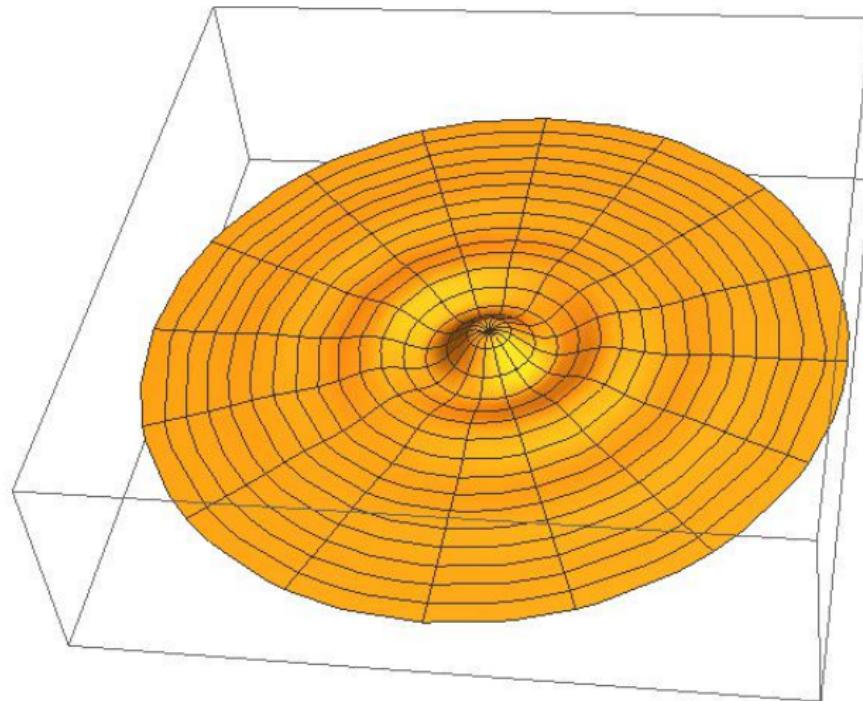
National University of Ireland Galway



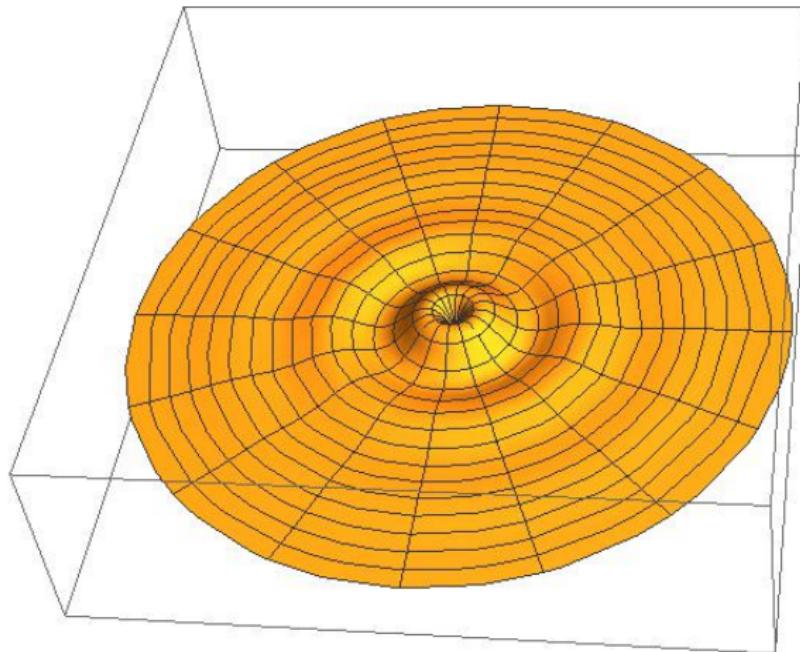
Surface waves



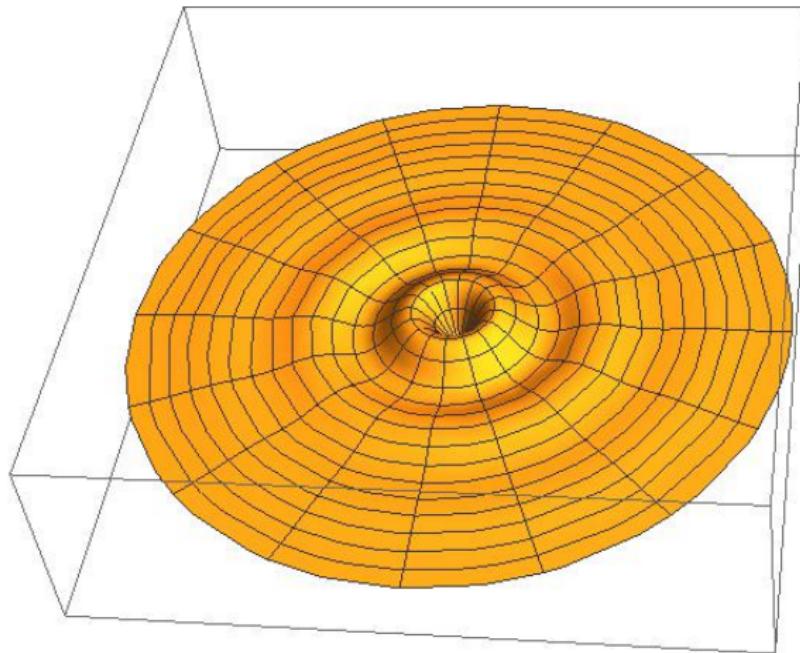
Surface waves



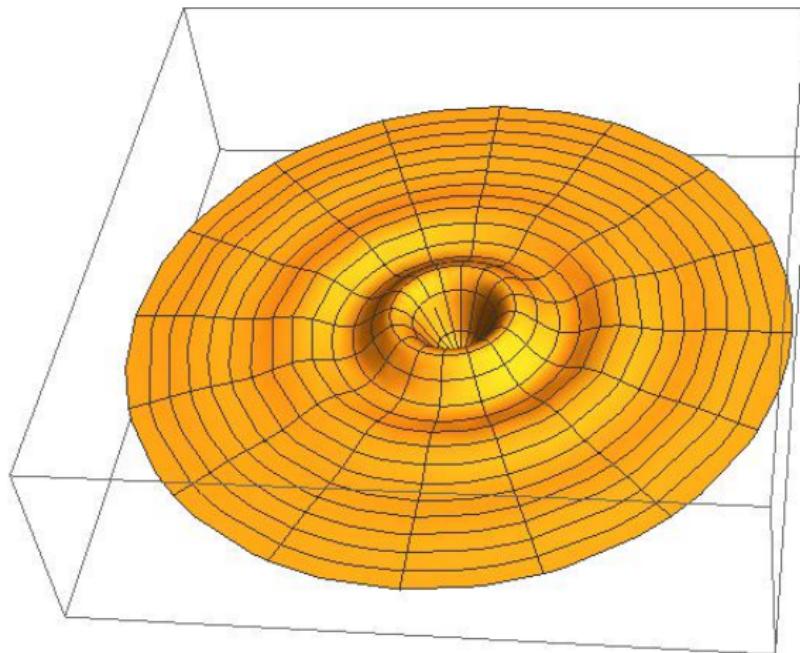
Surface waves



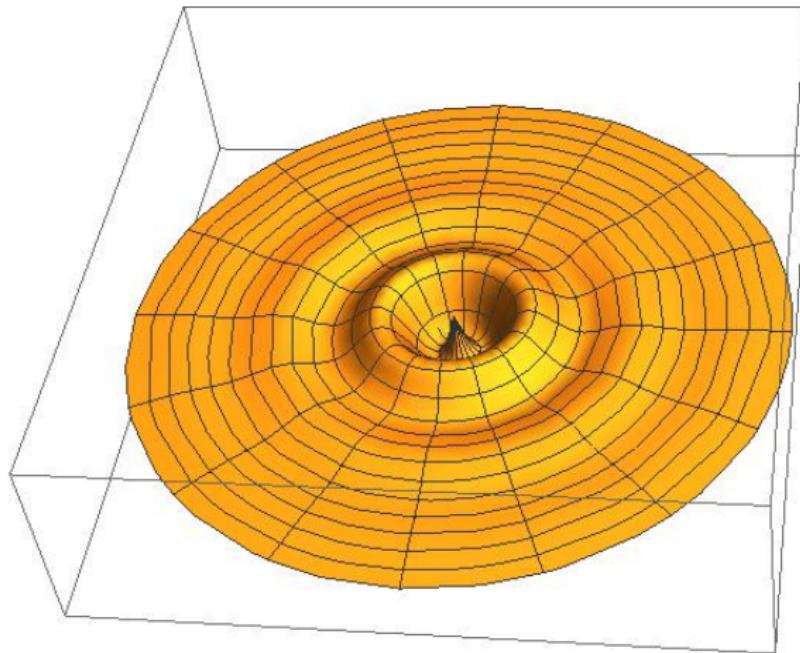
Surface waves



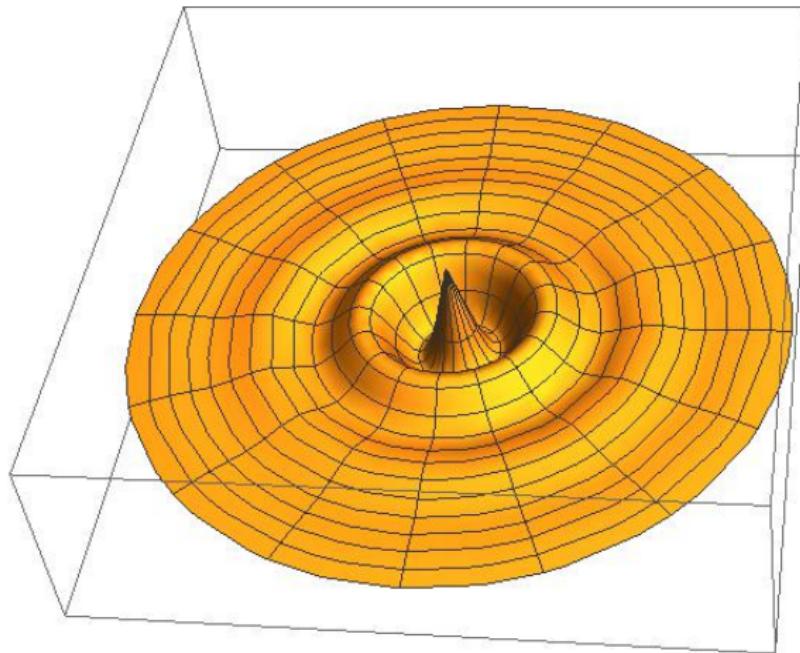
Surface waves



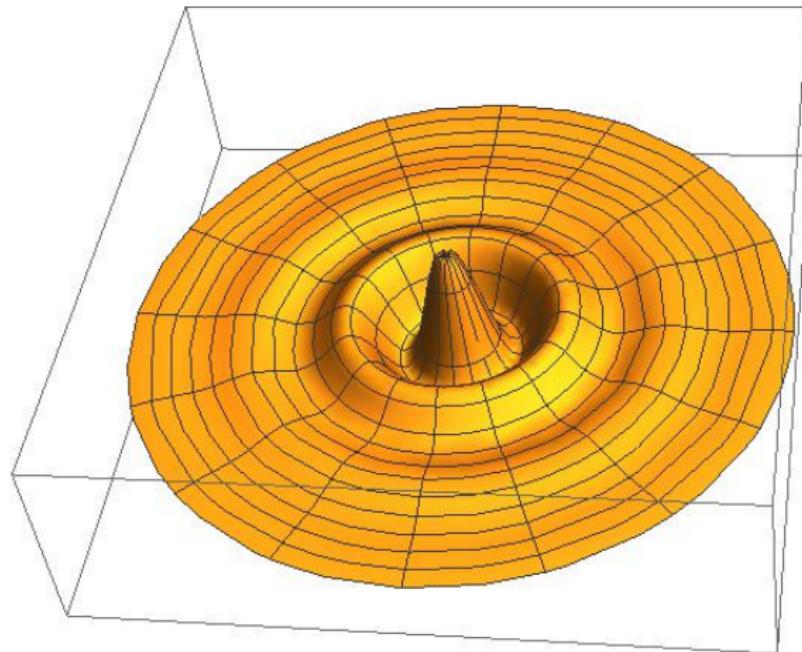
Surface waves



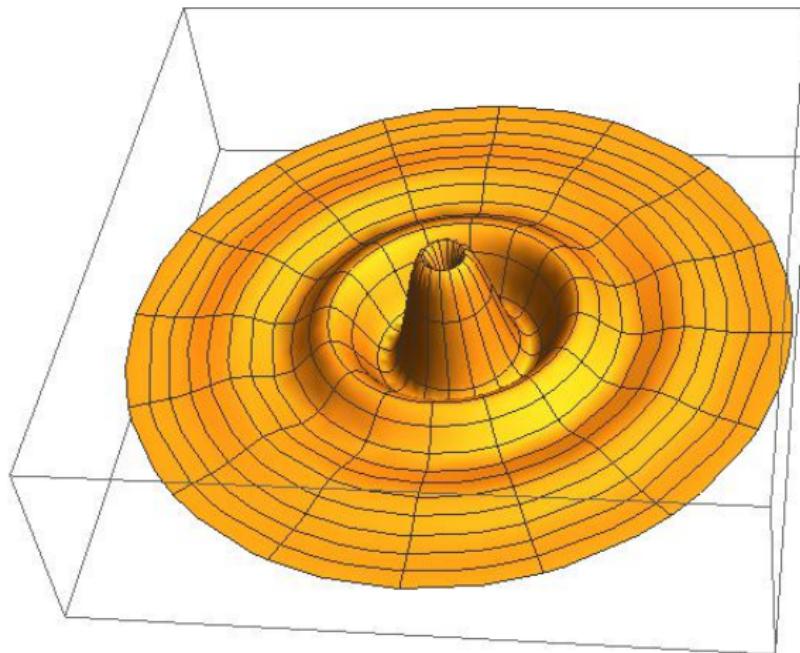
Surface waves



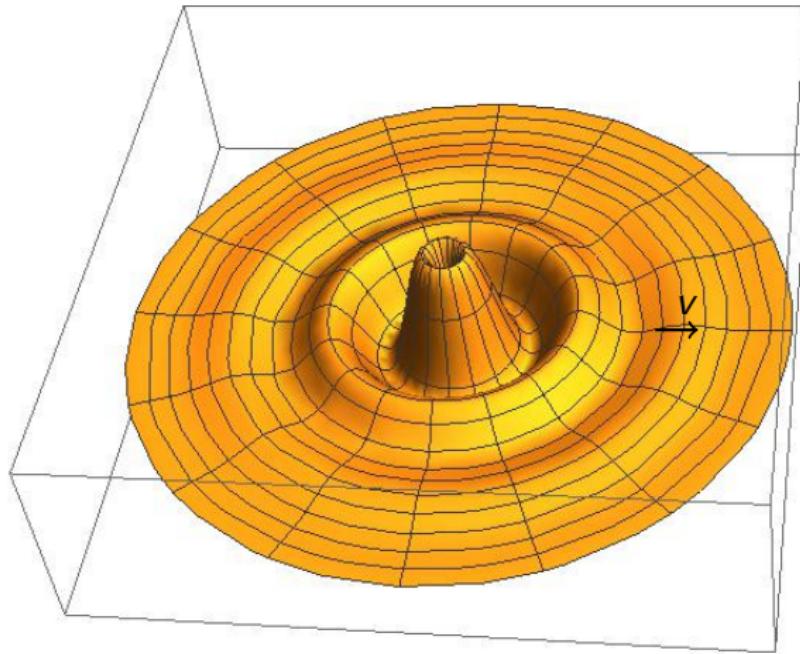
Surface waves



Surface waves



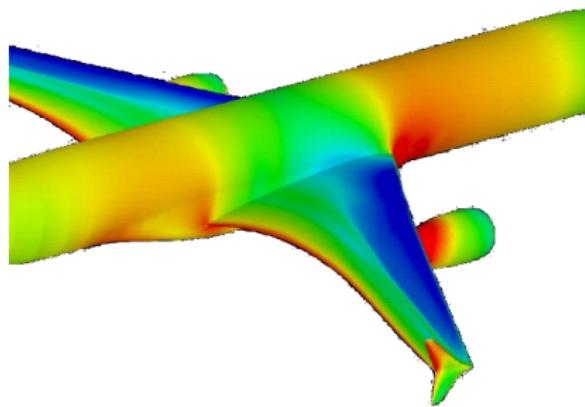
Surface waves



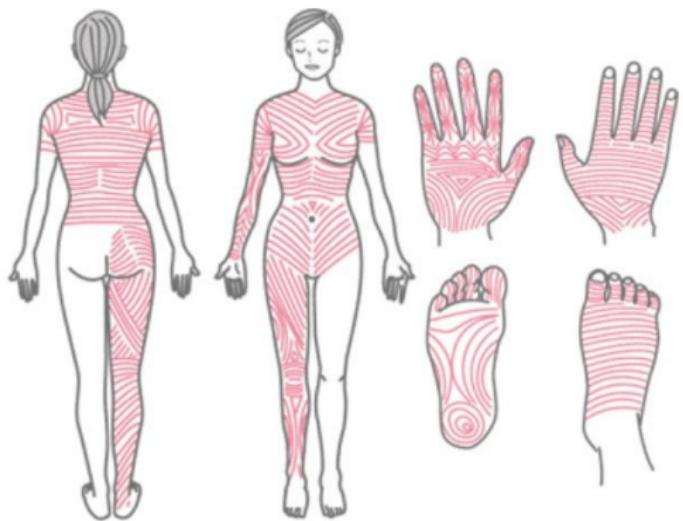
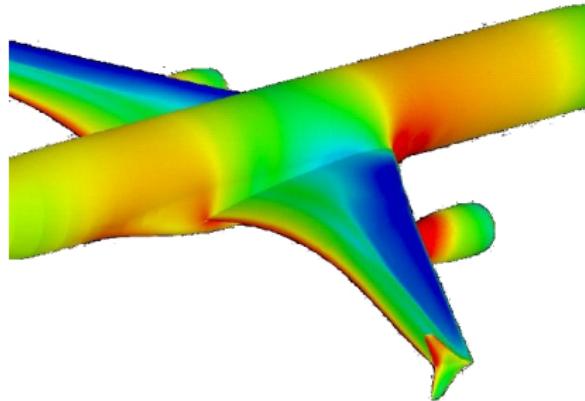
Optical Coherence Tomography (Dundee School of Medicine).
and

Lazer Vibrometers (Ultrasound Imaging Laboratory, Mayo Clinic).

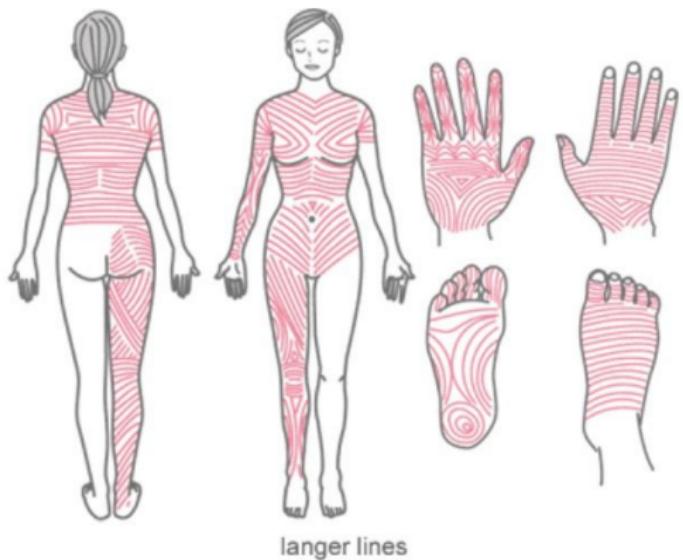
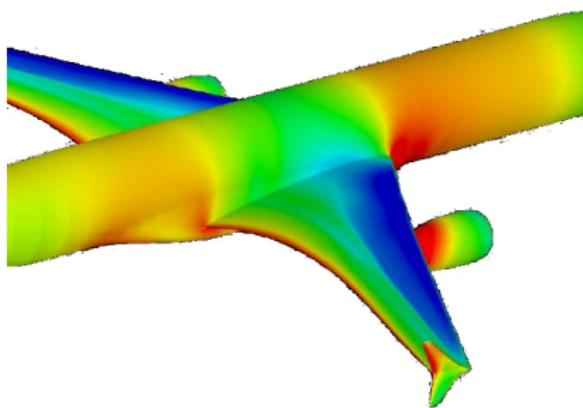
Non destructive evaluation of the surface



Non destructive evaluation of the surface



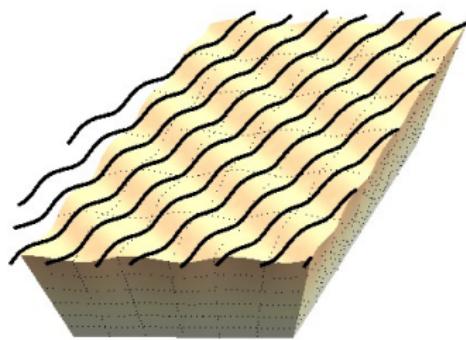
Non destructive evaluation of the surface



Langer lines

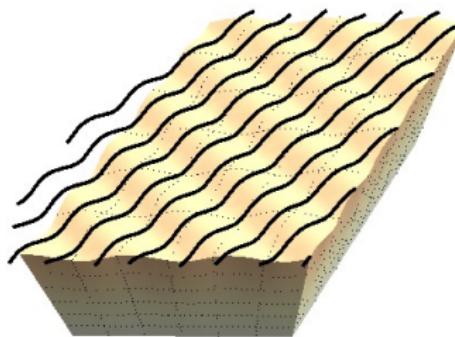
Measure stress and discover defects.

Testing ground for soft matter models



Fibre reinforced?

Testing ground for soft matter models

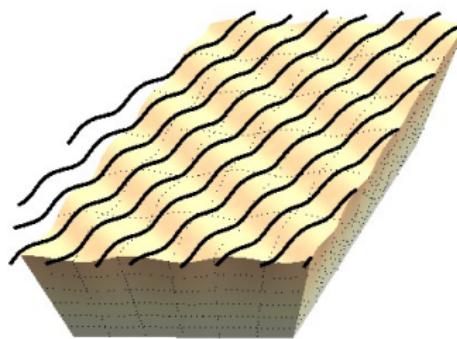


Fibre reinforced?

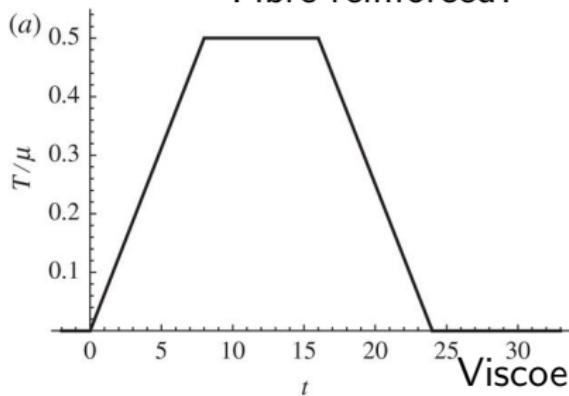


Initial and residual Stress?

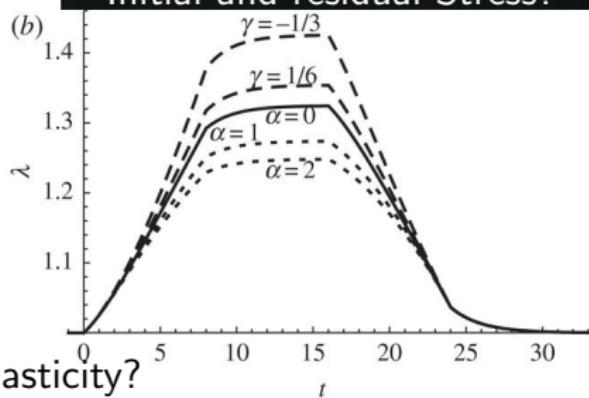
Testing ground for soft matter models

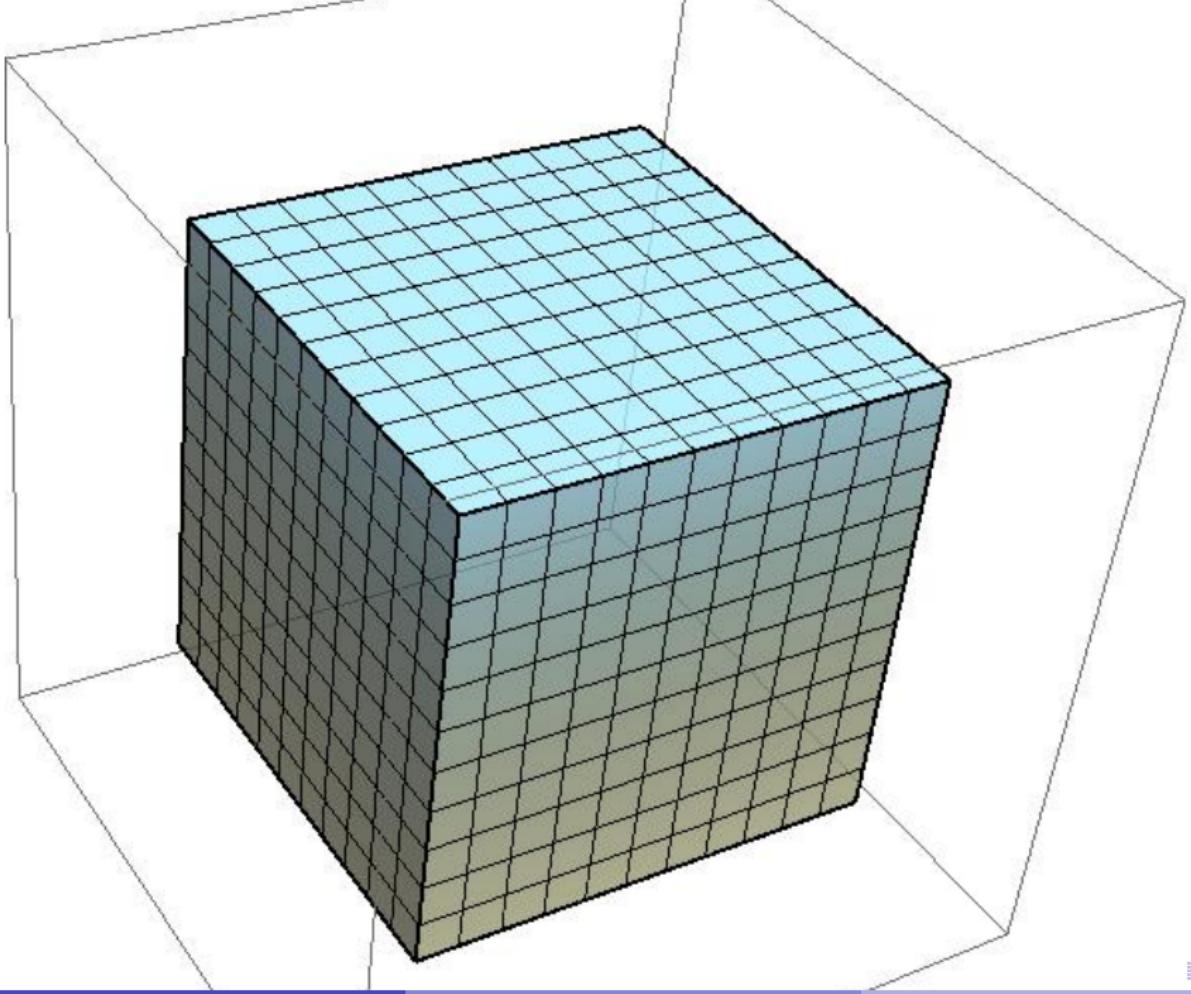


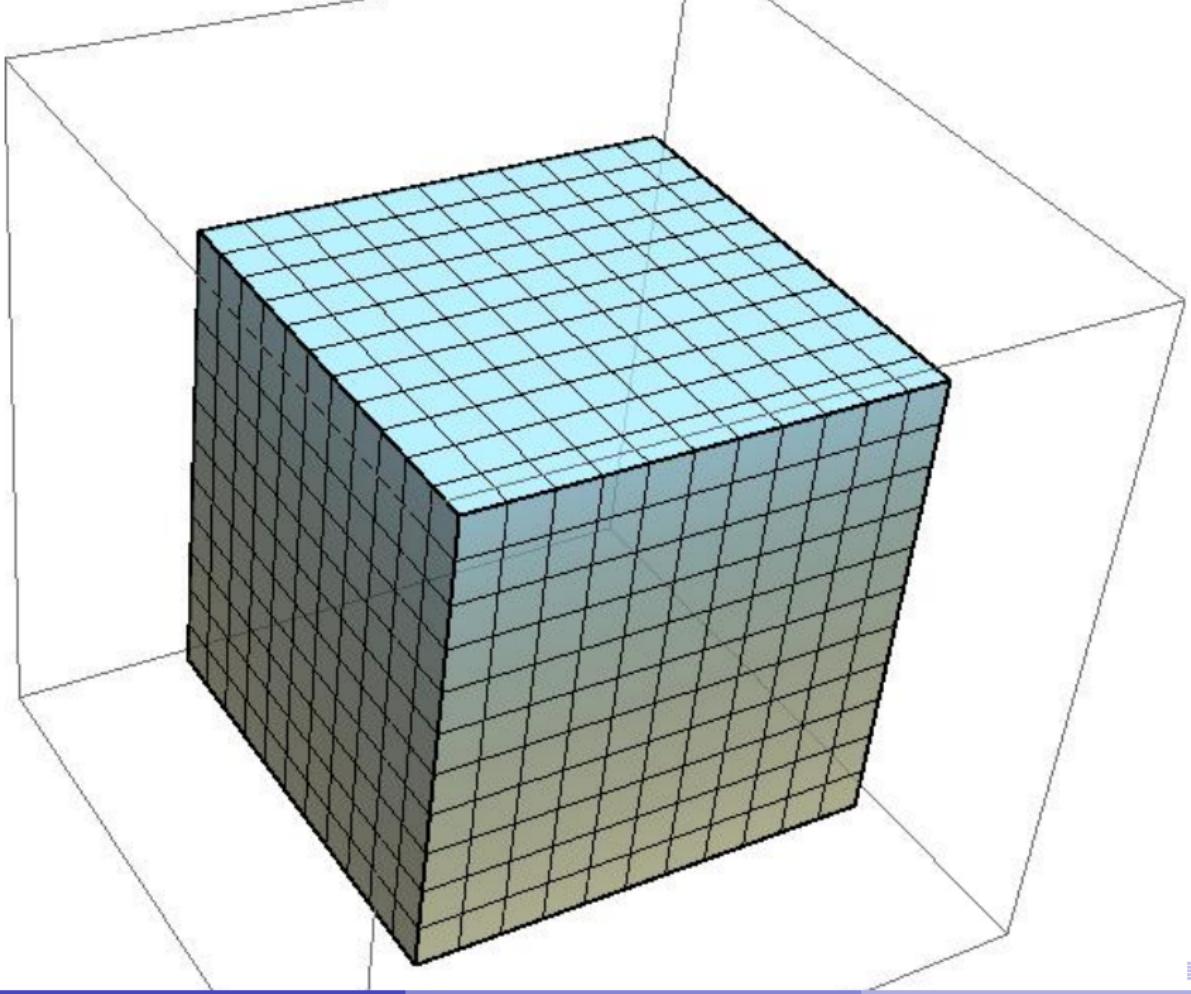
Fibre reinforced?

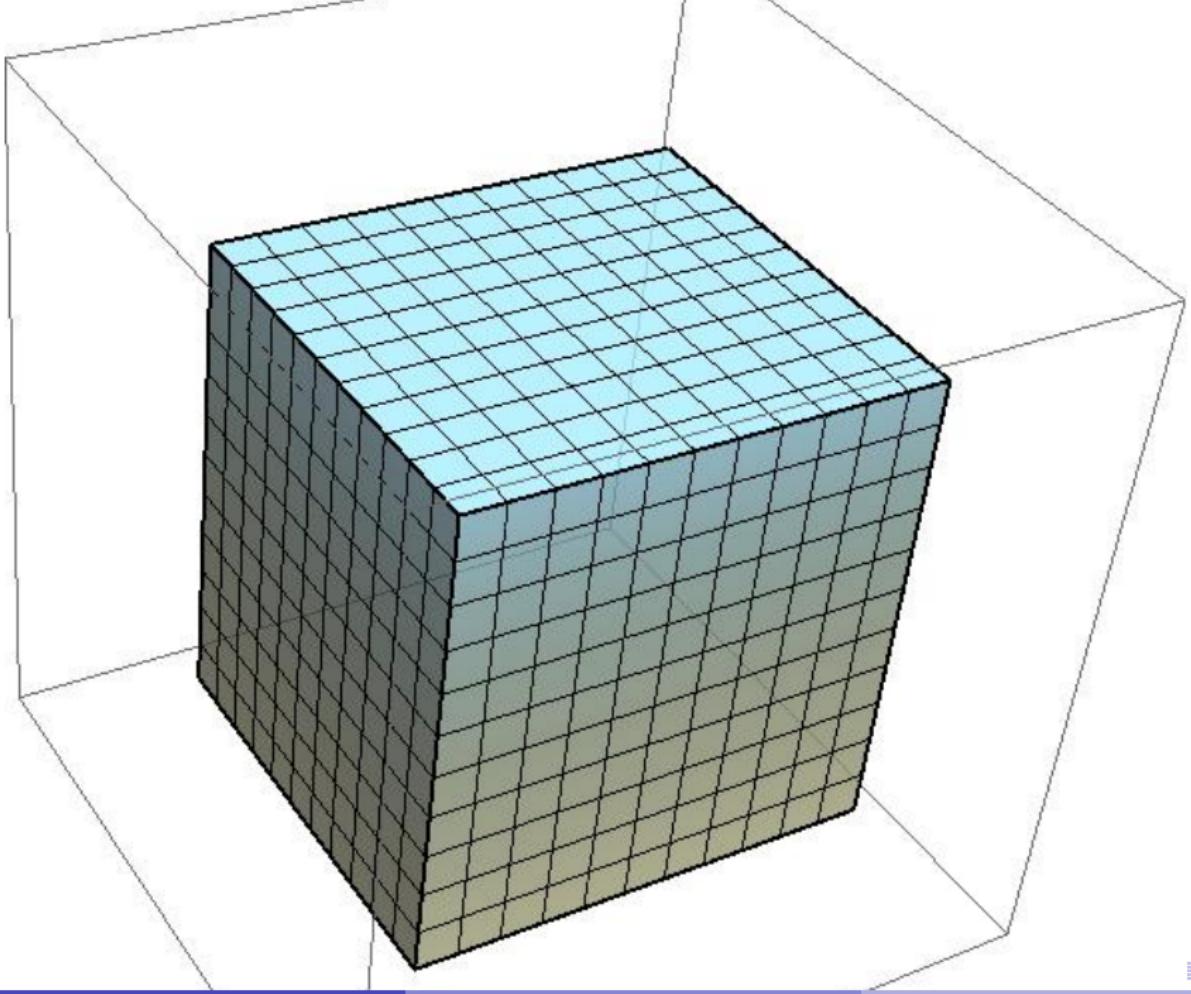


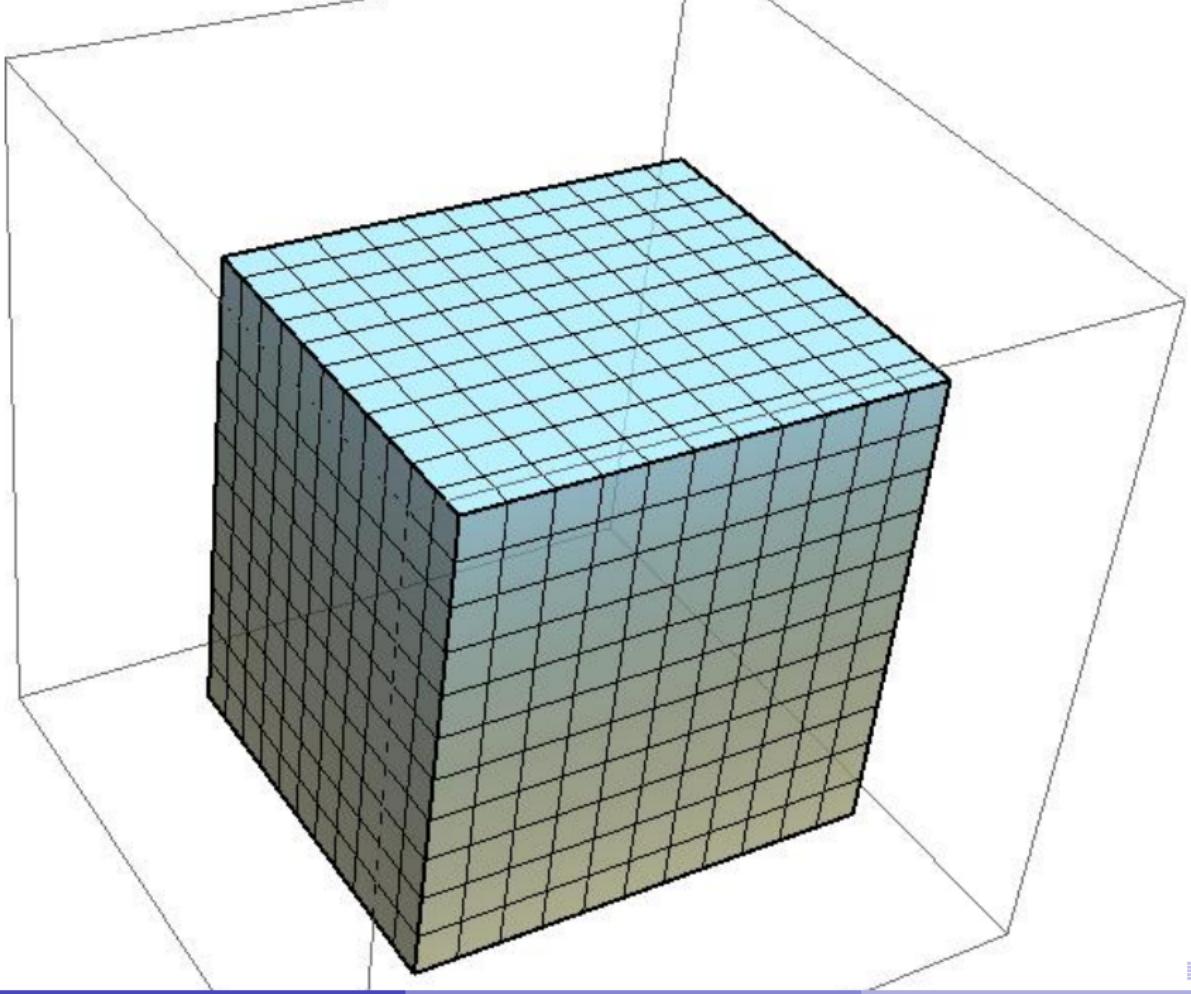
Initial and residual Stress?

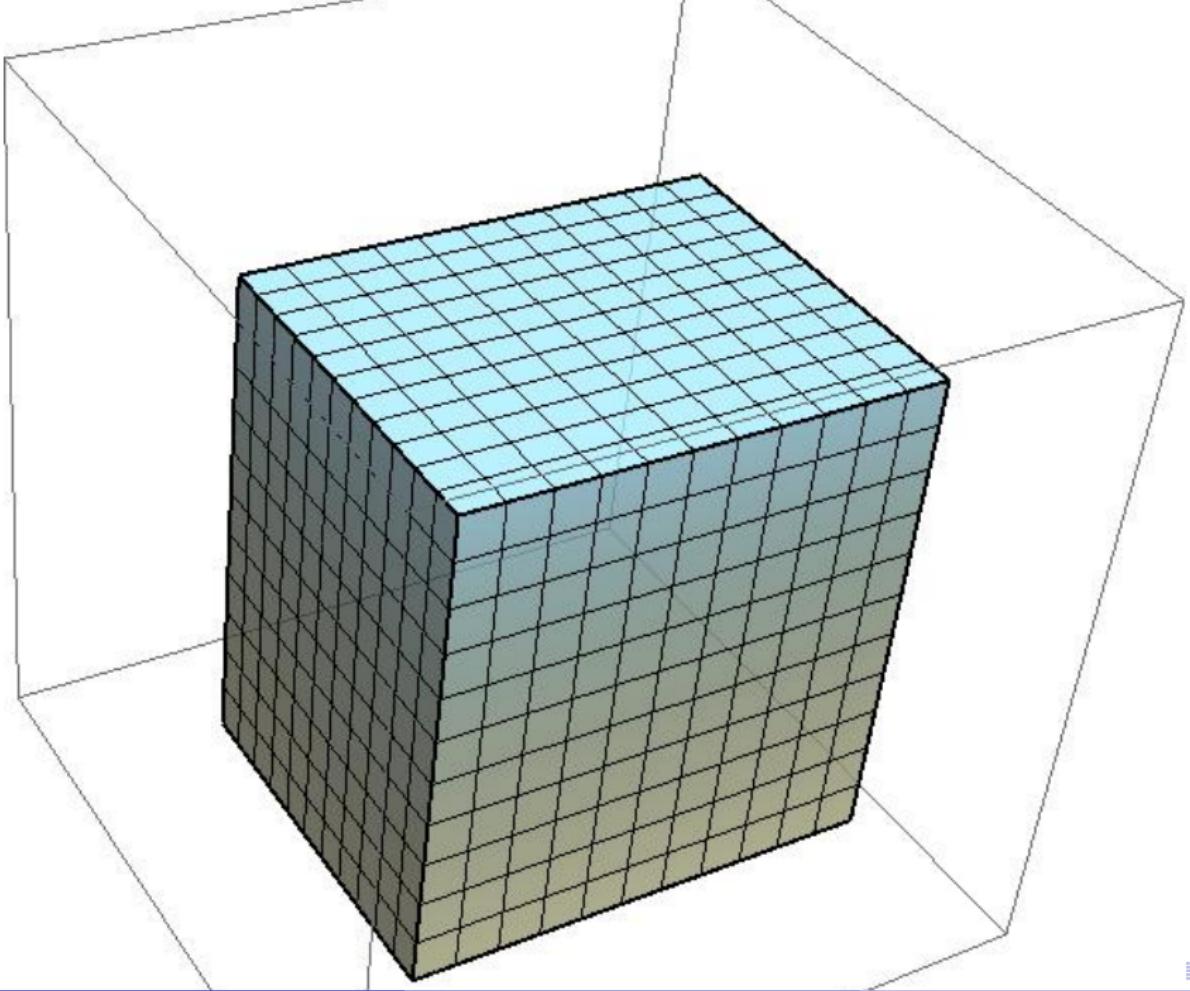


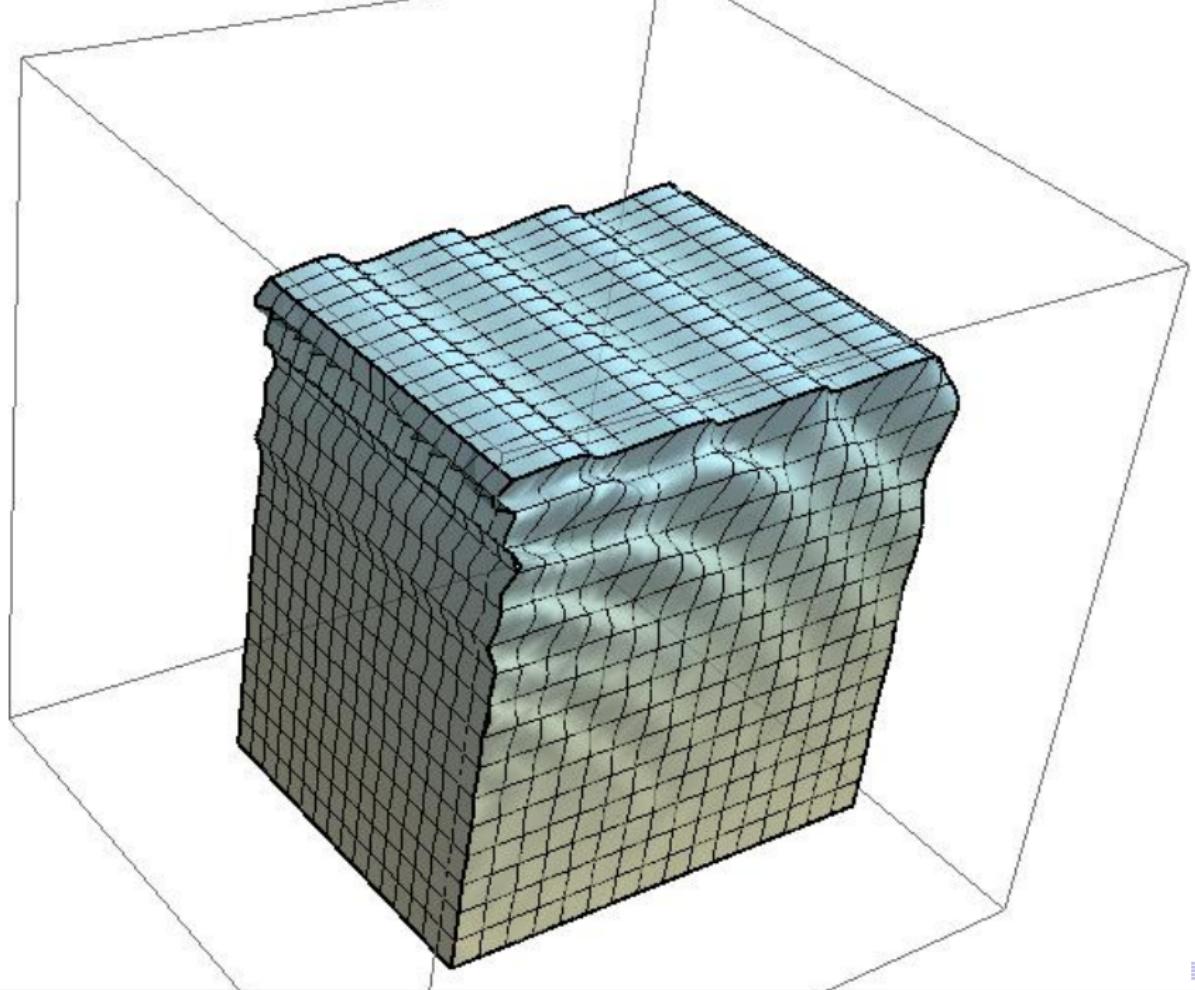


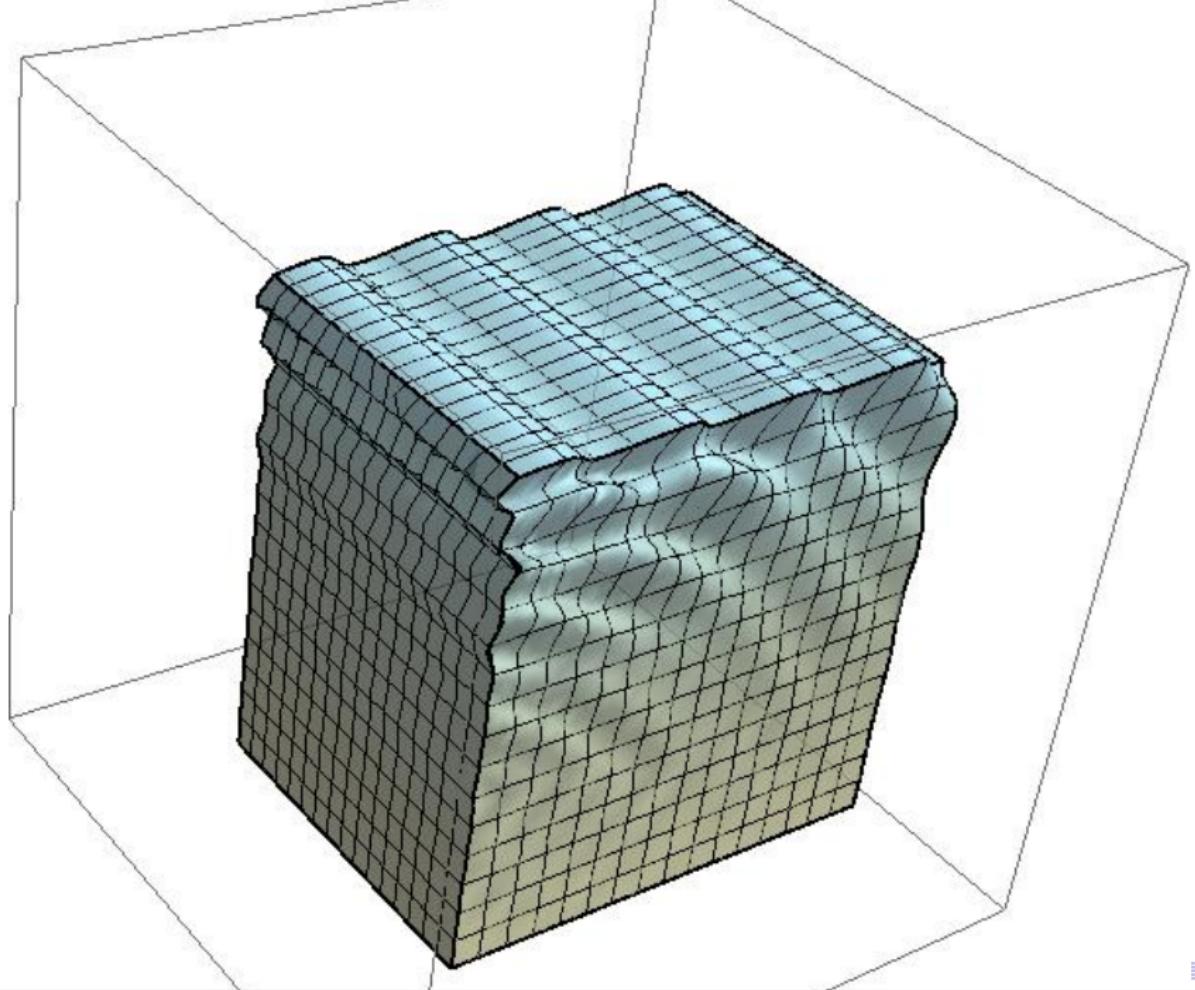


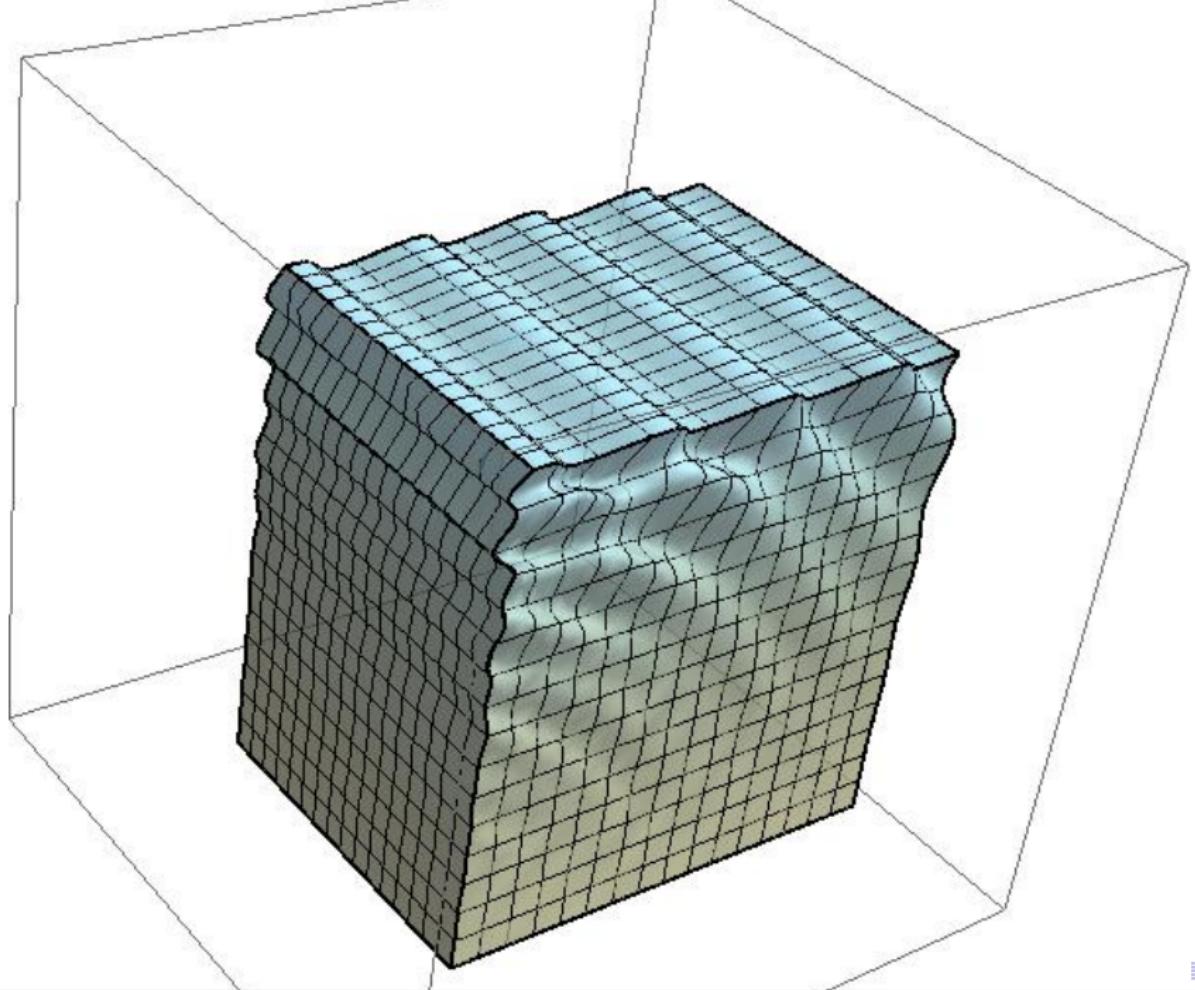


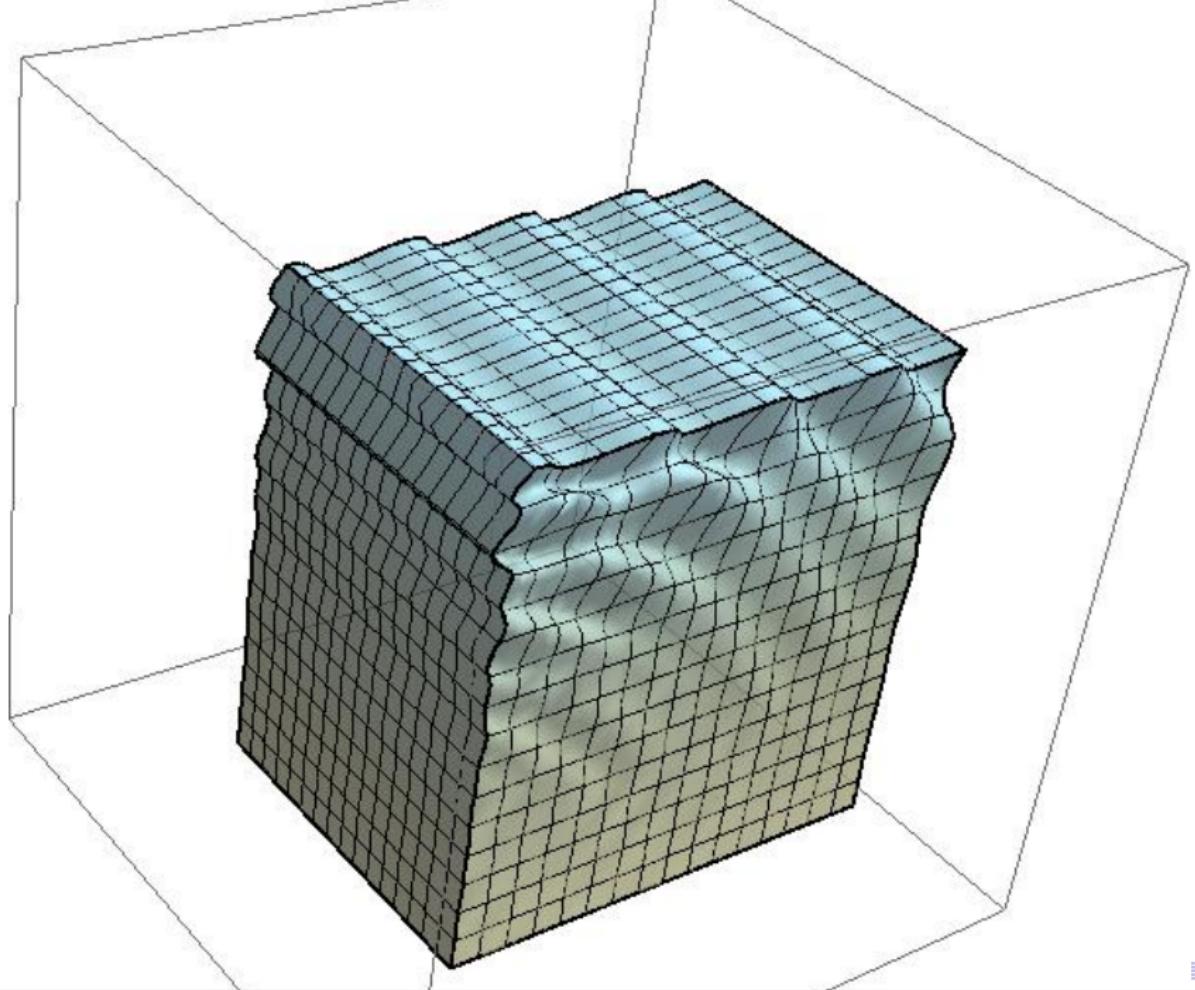


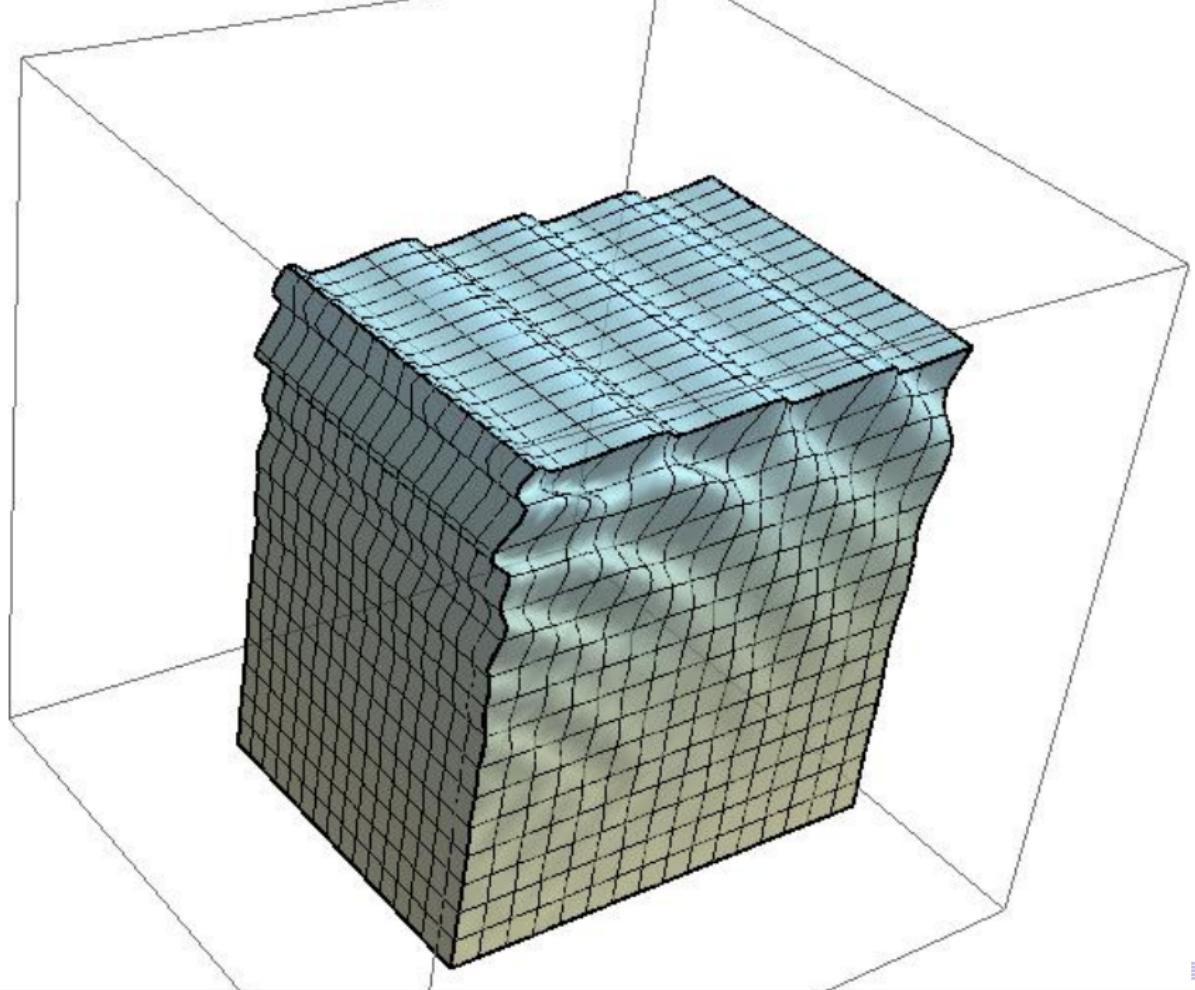


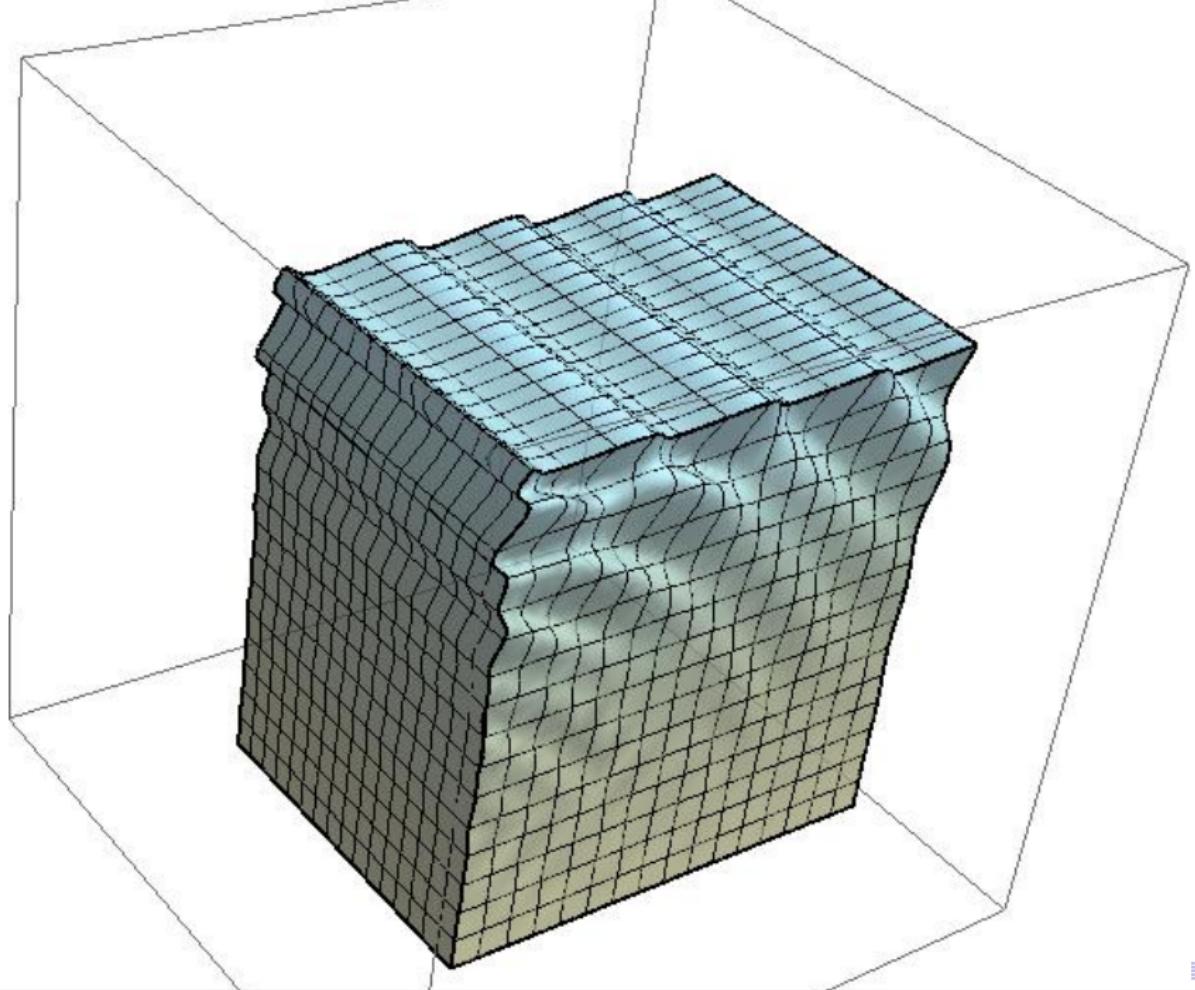


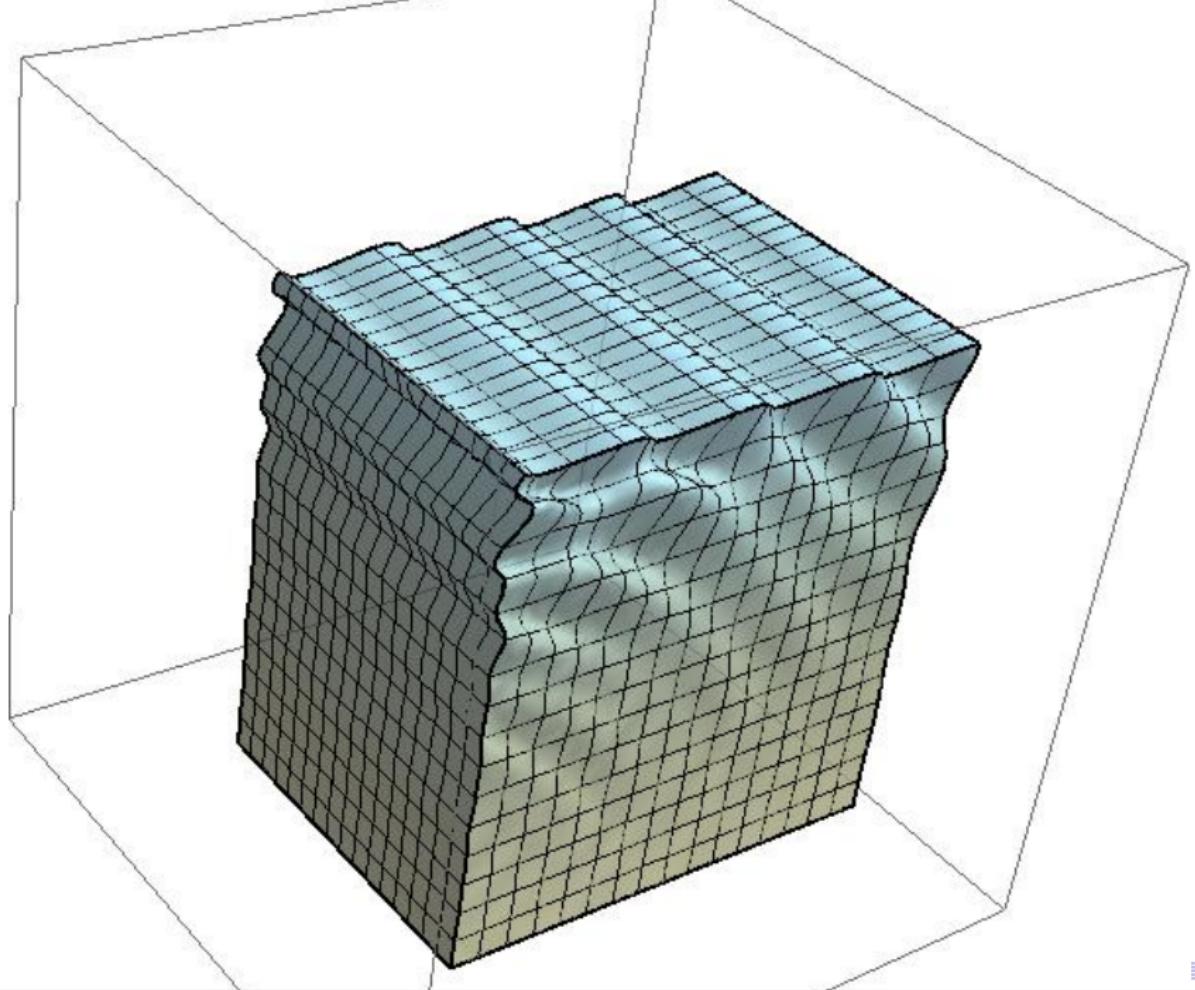


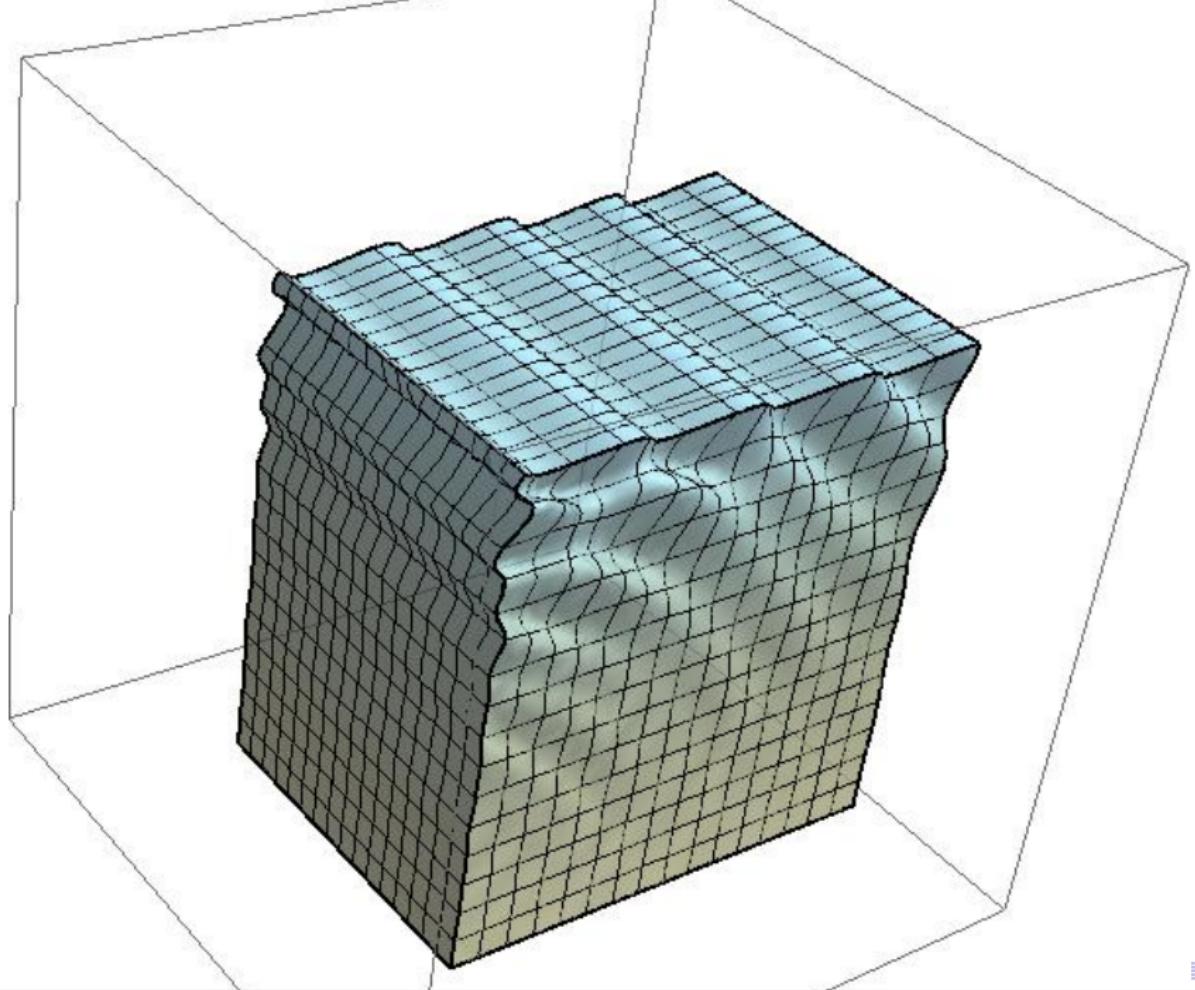


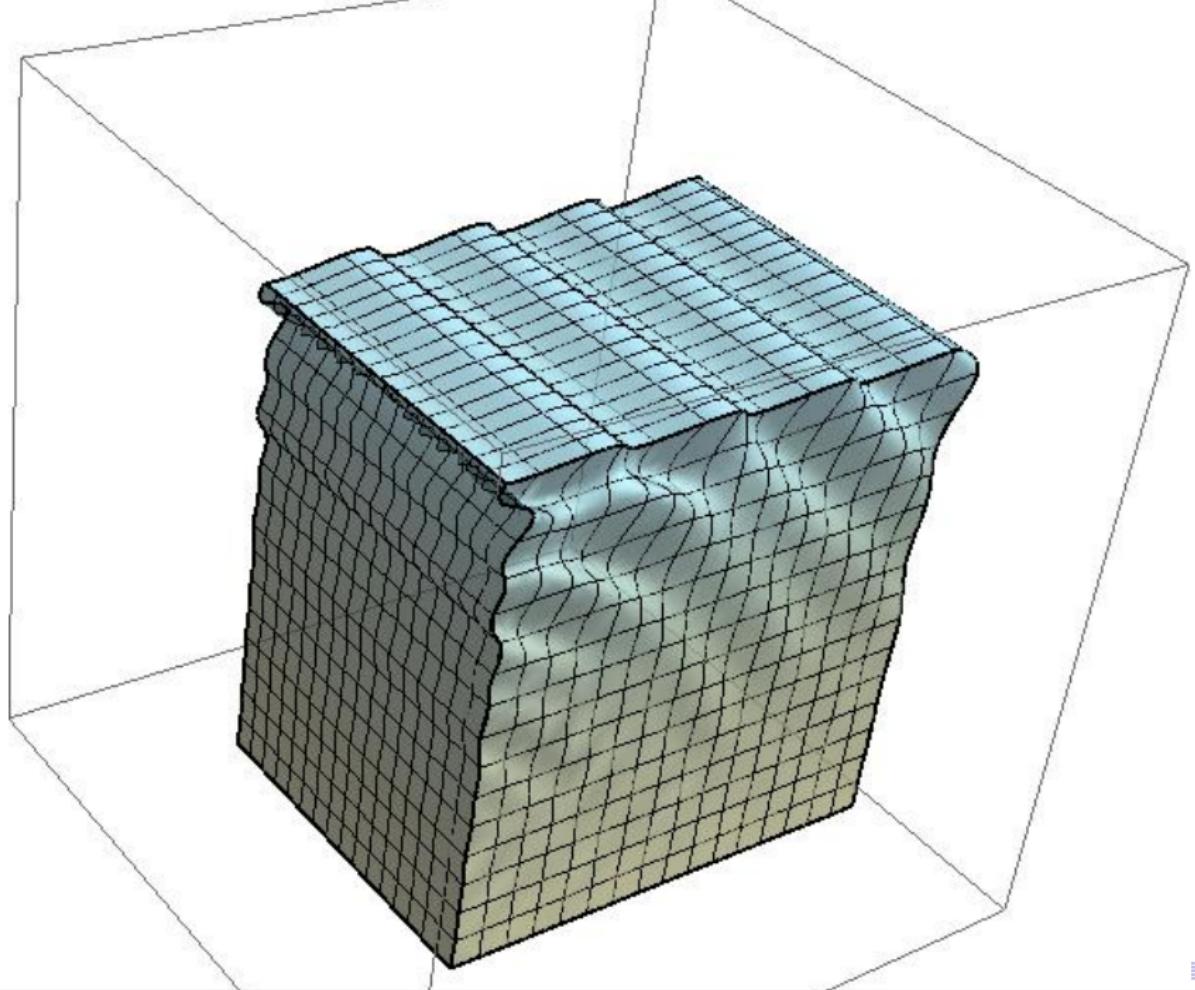




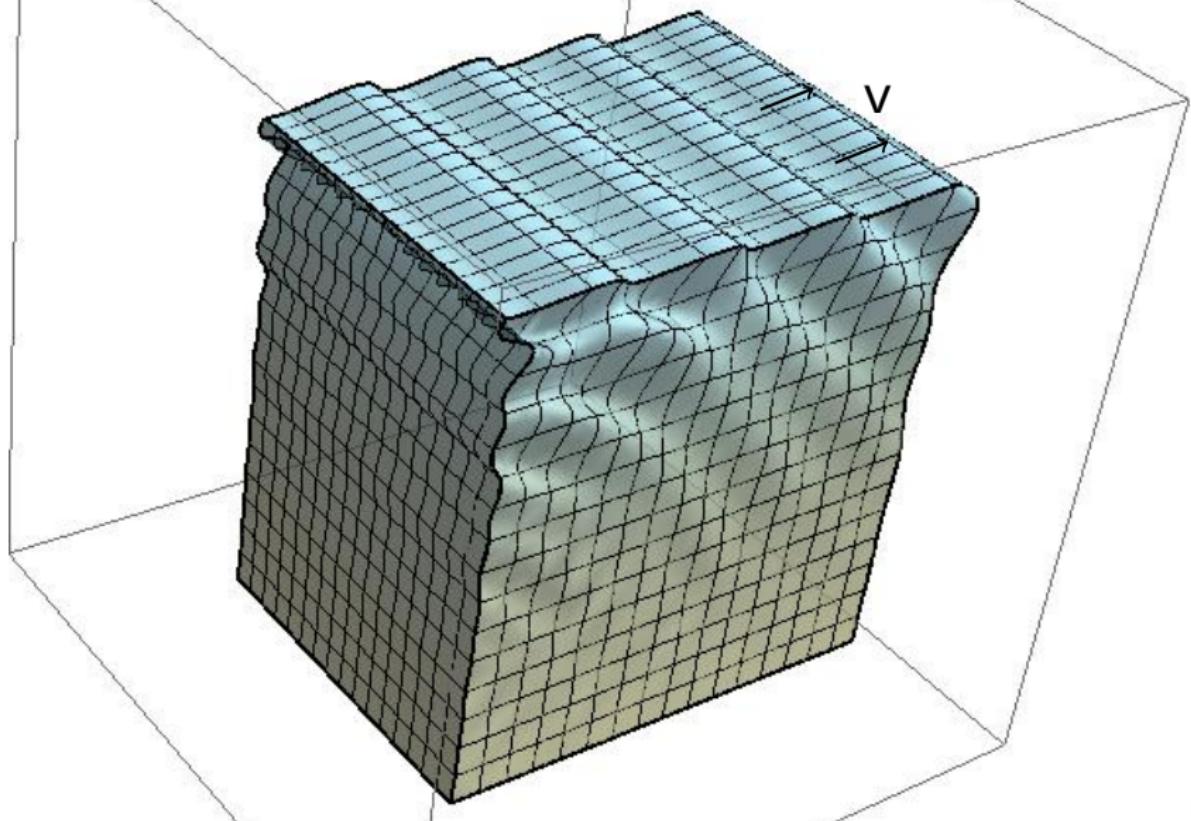




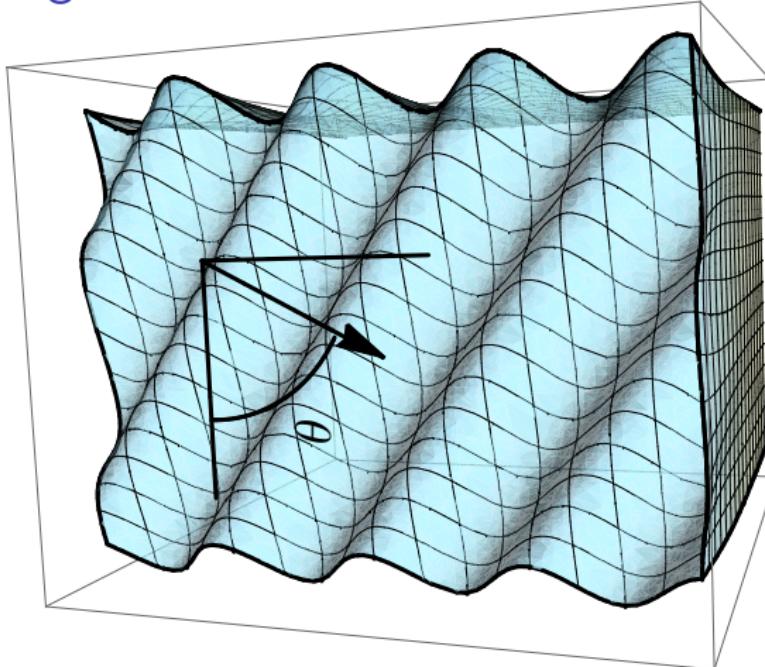




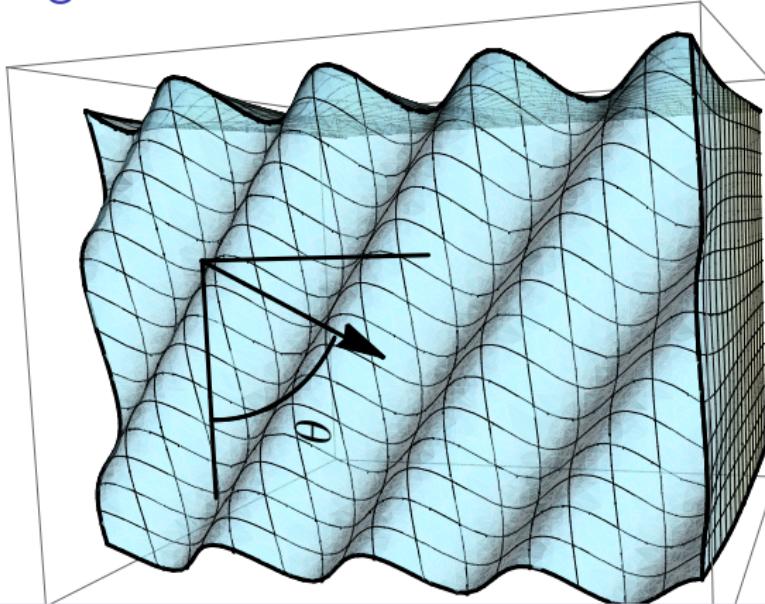
Incremental surface wave on top of large deformation



Wavefront Angle from direction of Greatest Compression



Wavefront Angle from direction of Greatest Compression



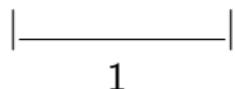
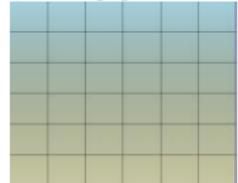
Incremental

$$\mathbf{u}(x, y, z) = \mathbf{U}(y) e^{ik(x \cos \theta + z \sin \theta - vt)} \quad (\text{Displacement})$$

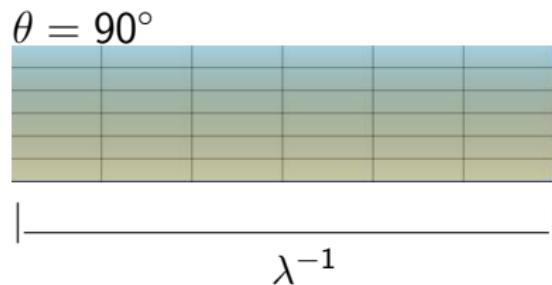
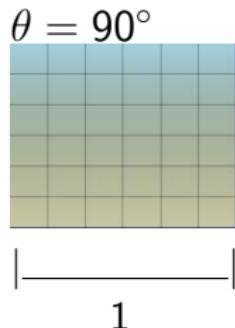
$$\lim_{y \rightarrow \infty} \mathbf{U}(y) = \mathbf{0} \quad \text{and} \quad \boldsymbol{\sigma} \cdot \mathbf{e}_y = \mathbf{0} \quad \text{on } y = 0 \quad (\text{Boundary conditions})$$

What is intuitive about a deformed isotropic material?

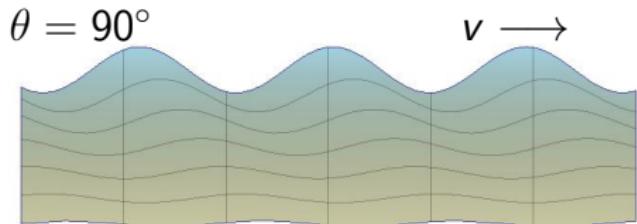
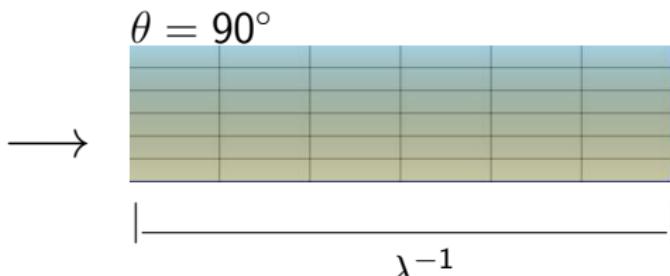
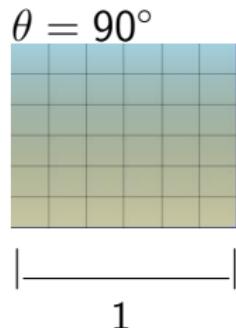
$$\theta = 90^\circ$$



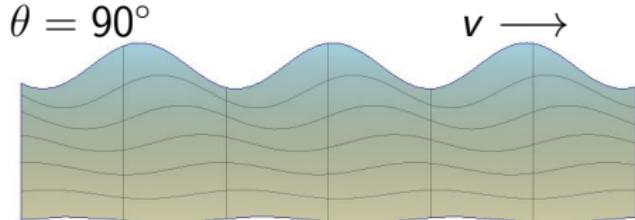
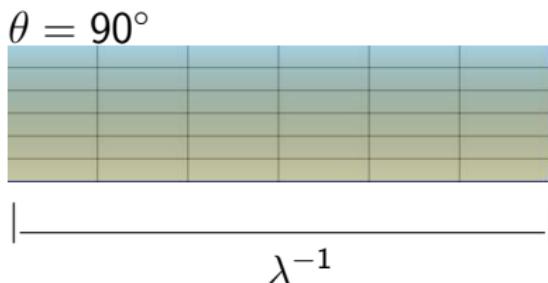
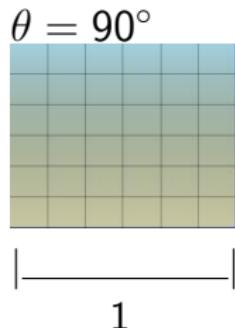
What is intuitive about a deformed isotropic material?



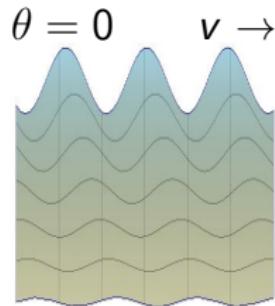
What is intuitive about a deformed isotropic material?



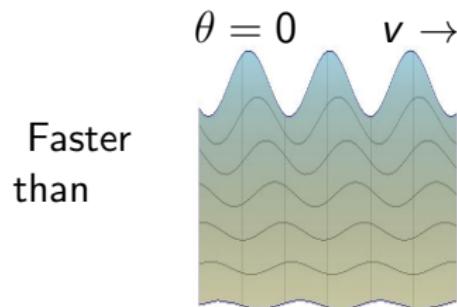
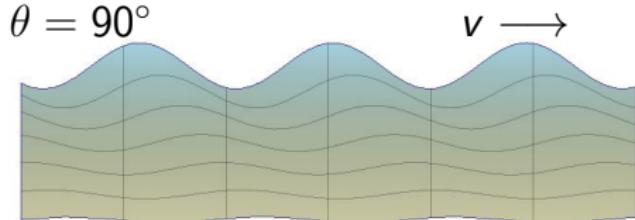
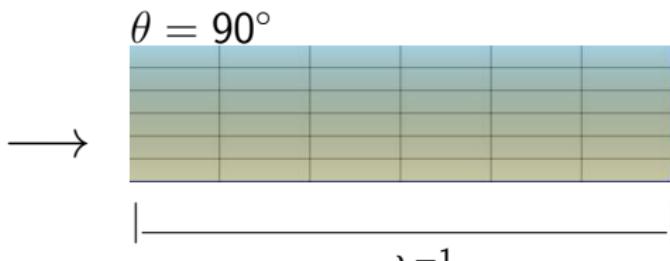
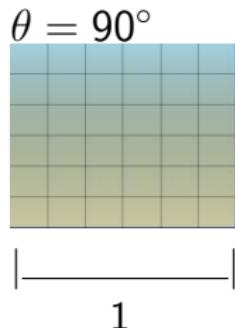
What is intuitive about a deformed isotropic material?



Faster
than



What is intuitive about a deformed isotropic material?



ISOTROPIC: Direction of greatest stress = Direction of greatest strain

Intuitive Infinitesimal Prestress

- K. Tanuma, C.-S. Man, W. Du., (2013), perturbation of phase velocity of Rayleigh waves :

$$v(\theta) = v^0 + C_1(\sigma_1 + \sigma_2) - C_2(\sigma_1 - \sigma_2) \cos 2\theta,$$

Intuitive Infinitesimal Prestress

- K. Tanuma, C.-S. Man, W. Du., (2013), perturbation of phase velocity of Rayleigh waves :

$$v(\theta) = v^0 + C_1(\sigma_1 + \sigma_2) - C_2(\sigma_1 - \sigma_2) \cos 2\theta,$$

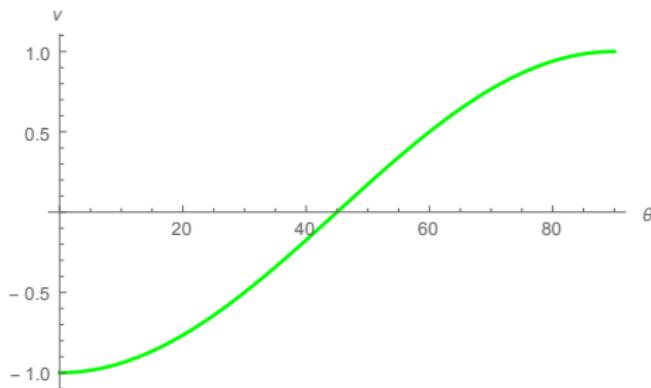
Where σ_1 and σ_2 are the principal pre-stresses along the surface, and v^0 , C_1 and C_2 are complicated constants.

Intuitive Infinitesimal Prestress

- K. Tanuma, C.-S. Man, W. Du., (2013), perturbation of phase velocity of Rayleigh waves :

$$v(\theta) = v^0 + C_1(\sigma_1 + \sigma_2) - C_2(\sigma_1 - \sigma_2) \cos 2\theta,$$

Where σ_1 and σ_2 are the principal pre-stresses along the surface, and v^0 , C_1 and C_2 are complicated constants.



Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

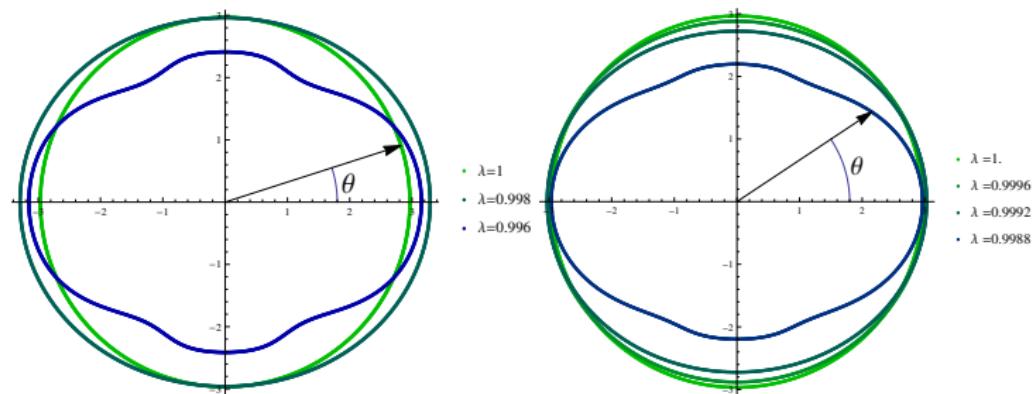


Figure: Speed profiles for surface waves (plotted as $v\sqrt{\rho}$) in Concrete subject to Uniaxial stress (left) and to Shear Stress (right).

Nonlinear Elastic Results

$$W = \frac{\lambda_0}{2} i_1^2 + \mu_0 i_2 + \frac{A}{3} i_3 + Bi_1 i_2 + \frac{C}{3} i_1^3 \quad (\text{Landau coefficients})$$

For nonlinear elasticity, all bets are off...

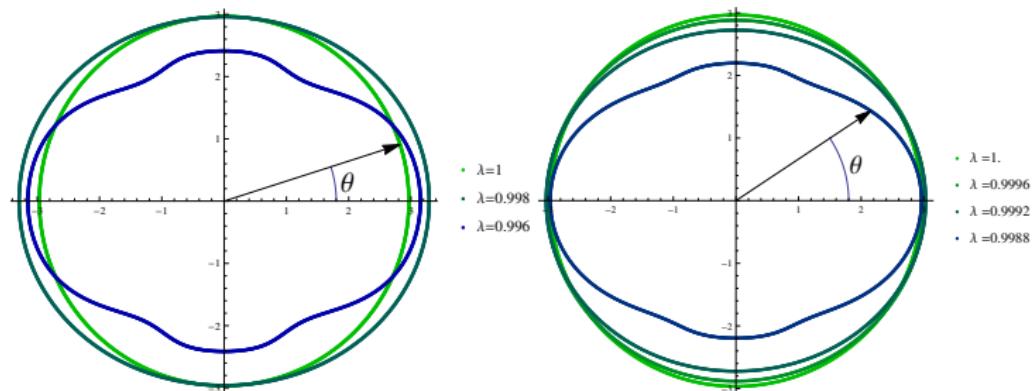


Figure: Speed profiles for surface waves (plotted as $v\sqrt{\rho}$) in Concrete subject to Uniaxial stress (left) and to Shear Stress (right).

- The sinusoidal regularity was lost early, for strains less than 1% (though the stress is reasonable.)

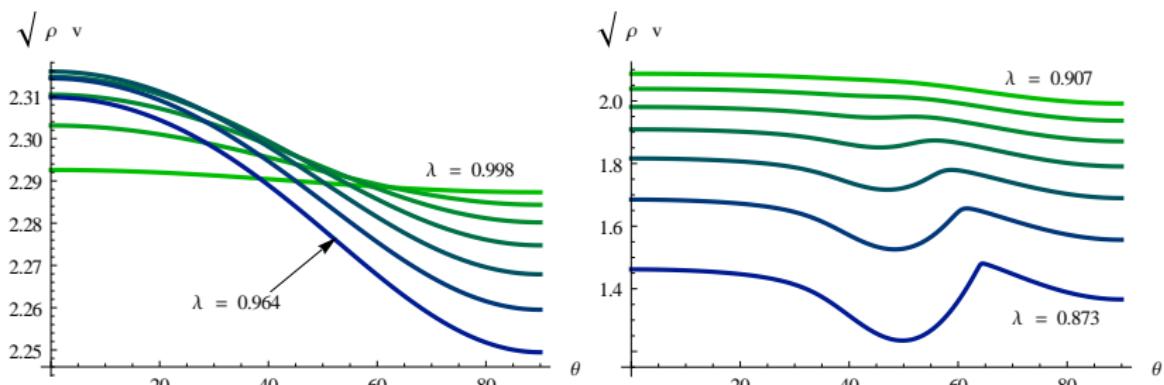


Figure: Nickel Uniaxial for varying strains λ .

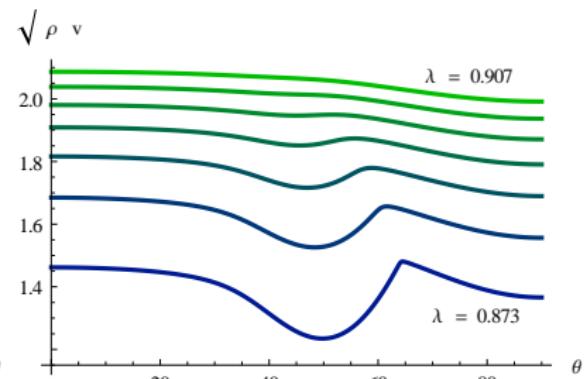
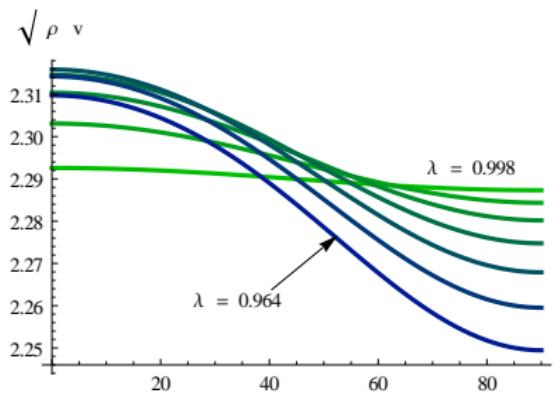


Figure: Nickel Uniaxial for varying strains λ .

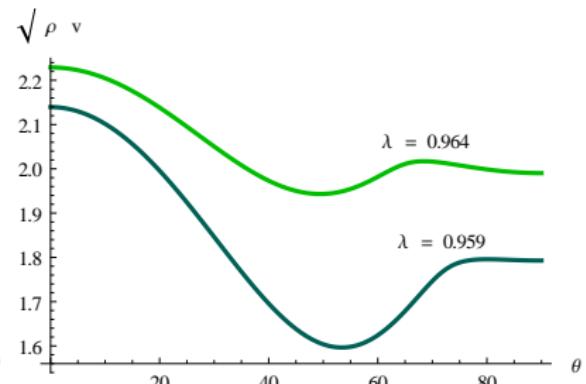
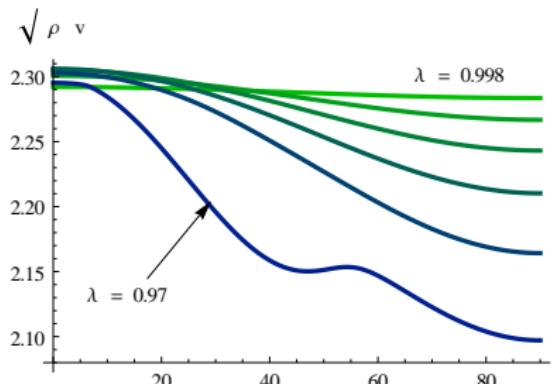


Figure: Nickel Pure Shear for varying strains λ

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

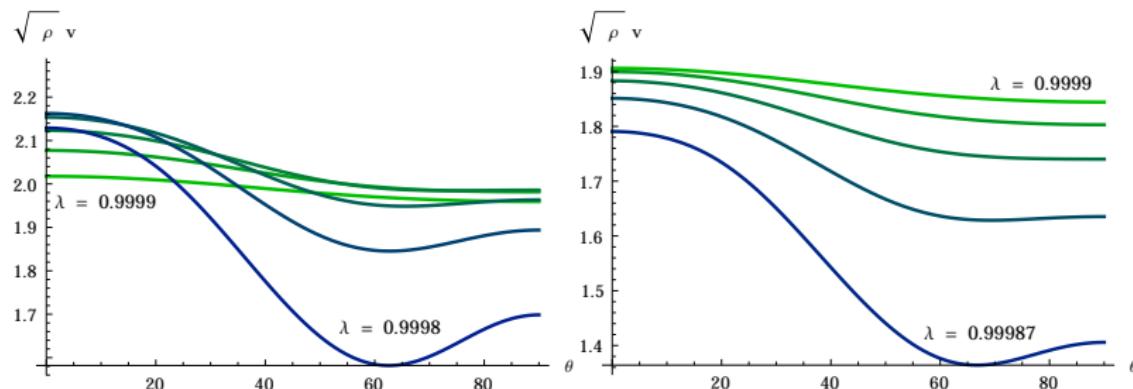


Figure: Uniaxial and Pure Shear Berea for varying strains λ

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

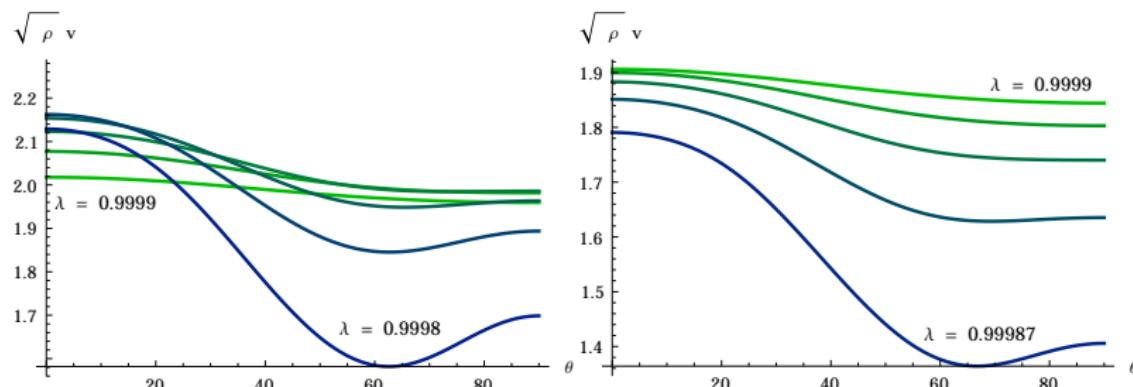


Figure: Uniaxial and Pure Shear Berea for varying strains λ
[A.L. Gower et al, Wave Motion, (2013)]

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

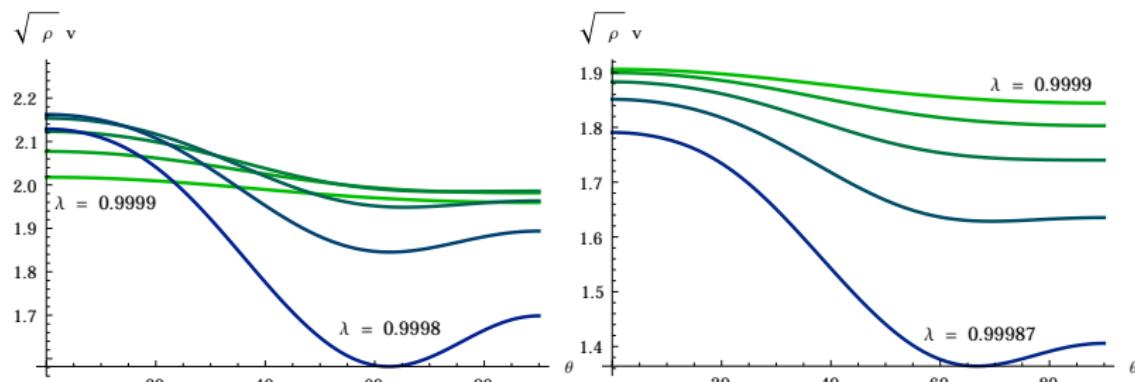


Figure: Uniaxial and Pure Shear Berea for varying strains λ
[A.L. Gower et al, Wave Motion, (2013)]

- These results complicate protocols for finding the directions of greatest and least stress.

Nonlinear Elastic Results

The higher the third-order constants (Landau/Murnaghan) the earlier the onset of nonlinear effects.

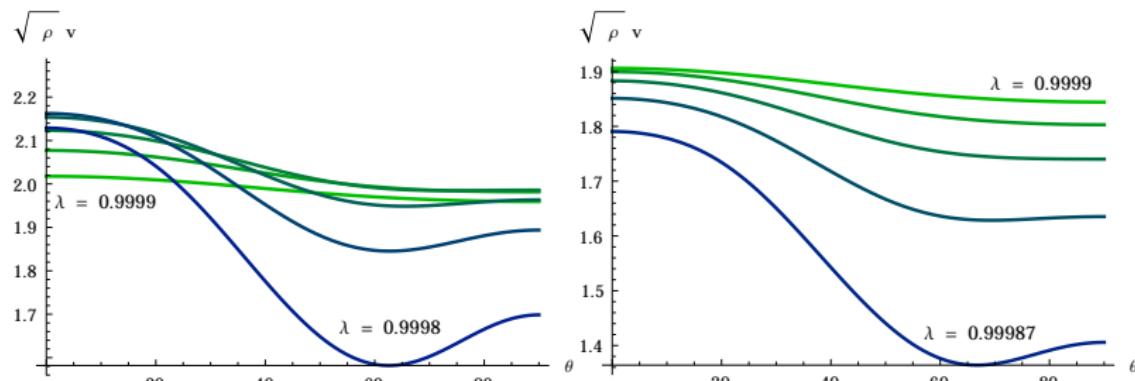


Figure: Uniaxial and Pure Shear Berea for varying strains λ
[A.L. Gower et al, Wave Motion, (2013)]

- These results complicate protocols for finding the directions of greatest and least stress.
- K.Y. Kim, W. Sachse, (2001):
“The principal stress direction is found where the variations of the SAW speeds show symmetry about the direction”.

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with}$$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ik\mathbf{E}y} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}\mathbf{E}^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$,

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{Displacement} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{Balance\ of\ Momentum}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ik\mathbf{E}y} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}\mathbf{E}^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj,q} u_{j,q}$$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow s = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow s = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

To exist a solution $s = \mathbf{0}$ on $x_2 = 0$ we need

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow s = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

To exist a solution $s = \mathbf{0}$ on $x_2 = 0$ we need $\det(\mathbf{R} + \mathbf{T}\mathbf{E}) = 0$.

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow \mathbf{s} = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

To exist a solution $\mathbf{s} = \mathbf{0}$ on $x_2 = 0$ we need $\det(\mathbf{R} + \mathbf{T}\mathbf{E}) = 0$.

Let $\mathbf{Z} = -i(\mathbf{R} + \mathbf{T}\mathbf{E})$ then

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}E^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow \mathbf{s} = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

To exist a solution $\mathbf{s} = \mathbf{0}$ on $x_2 = 0$ we need $\det(\mathbf{R} + \mathbf{T}\mathbf{E}) = 0$.

Let $\mathbf{Z} = -i(\mathbf{R} + \mathbf{T}\mathbf{E})$ then

$$\boxed{\mathbf{H}^\dagger(v)\mathbf{H}(v) = \mathbf{Q} - \rho v^2 \mathbf{I} \quad \text{and} \quad \mathbf{Z}(v) = \mathbf{T}^{1/2}\mathbf{H}(v) - i\mathbf{R},}$$

Matrix Impedance Method

take:

$$\mathbf{u}(x, y, t) = \underbrace{\mathbf{U}(y) e^{ikx - i\omega t}}_{\text{Displacement}} \rightarrow \underbrace{\rho u_{i,tt} = \mathcal{C}_{ipjq} u_{j,pq}}_{\text{Balance of Momentum}}$$

together with $\lim_{y \rightarrow \infty} \mathbf{U}(y) = 0$ results in

$$\mathbf{U}(y) = e^{ikEy} \mathbf{U}_0 \quad \text{with} \quad \mathbf{T}\mathbf{E}^2 + (\mathbf{R} + \mathbf{R}^T)\mathbf{E} - \rho v^2 \mathbf{I} + \mathbf{Q} = 0,$$

and $\operatorname{Im} \operatorname{Spec} \mathbf{E} > 0$, where \mathbf{R} , \mathbf{T} and \mathbf{Q} are given in terms of \mathcal{C}_{ipjq} .

Not the best way to solve yet.

Stress for boundary condition:

$$s_p := \sigma_{2p} = \mathcal{C}_{2pj} u_{j,q} \rightarrow \mathbf{s} = ik(\mathbf{R} + \mathbf{T}\mathbf{E})\mathbf{u}$$

To exist a solution $\mathbf{s} = \mathbf{0}$ on $x_2 = 0$ we need $\det(\mathbf{R} + \mathbf{T}\mathbf{E}) = 0$.

Let $\mathbf{Z} = -i(\mathbf{R} + \mathbf{T}\mathbf{E})$ then

$$\boxed{\mathbf{H}^\dagger(v)\mathbf{H}(v) = \mathbf{Q} - \rho v^2 \mathbf{I} \quad \text{and} \quad \mathbf{Z}(v) = \mathbf{T}^{1/2}\mathbf{H}(v) - i\mathbf{R},}$$

with the restriction $\boxed{\mathbf{Z}(v) > 0}$.

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\mathbf{U}^*(0) \cdot \mathbf{Z}(v) \mathbf{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy - v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathbf{U}^*(0) \cdot \mathbf{Z}(v) \mathbf{U}(0)}_{\text{Surface Stress Power}} = \frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy - v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathbf{U}^*(0) \cdot \mathbf{Z}(v) \mathbf{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy}_{\text{Potential Energy}} - v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathbf{U}^*(0) \cdot \mathcal{Z}(v) \mathbf{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy}_{\text{Kinetic Energy}}$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathbf{U}^*(0) \cdot \mathcal{Z}(v) \mathbf{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy}_{\text{Kinetic Energy}}$$

Meaning,

$$\mathbf{U}^*(0) \cdot \mathcal{Z}(0) \mathbf{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy,$$

Matrix Impedance Magic

$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = \operatorname{div} \boldsymbol{\sigma} \implies -v^2 \rho \mathbf{u}^* \cdot \mathbf{u} = \mathbf{u}^* \cdot \operatorname{div} \boldsymbol{\sigma},$$

resulting in

$$\underbrace{\mathbf{U}^*(0) \cdot \mathbf{Z}(v) \mathbf{U}(0)}_{\text{Surface Stress Power}} = \underbrace{\frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy}_{\text{Potential Energy}} - \underbrace{v^2 \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy}_{\text{Kinetic Energy}}$$

Meaning,

$$\mathbf{U}^*(0) \cdot \mathbf{Z}(0) \mathbf{U}(0) = \frac{1}{k} \int_0^\infty \delta W(\mathbf{U}(y)) dy,$$

$$\mathbf{U}^*(0) \cdot \frac{\partial \mathbf{Z}(v)}{\partial v} \mathbf{U}(0) = -2v \int_0^\infty \rho \mathbf{U}^*(y) \cdot \mathbf{U}(y) dy,$$

positive definite $\mathbf{Z}(0)$ with monotone decreasing Eigenvalues!

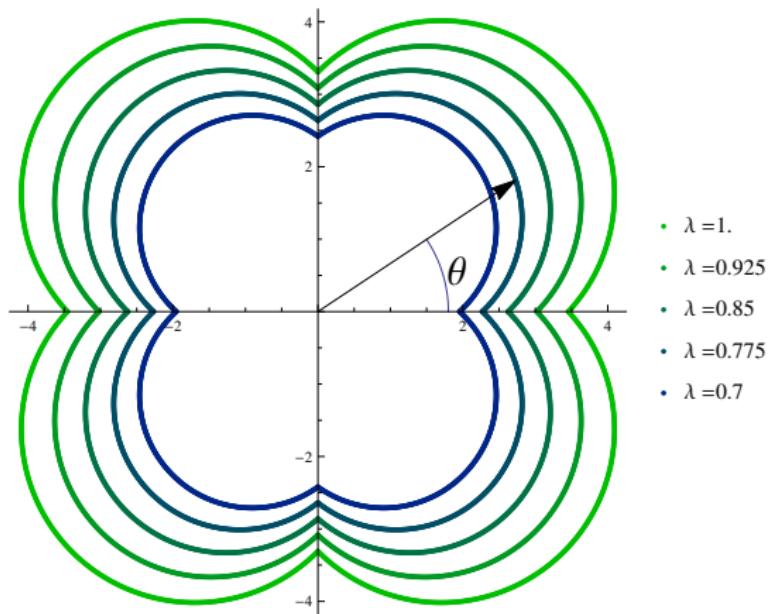
Fu, Y. B. and Mielke, A. (2002). In: Proc. R. Soc. A **458**, 25232543.

More results

This procedure works for any elastic strain-energy function, for example...

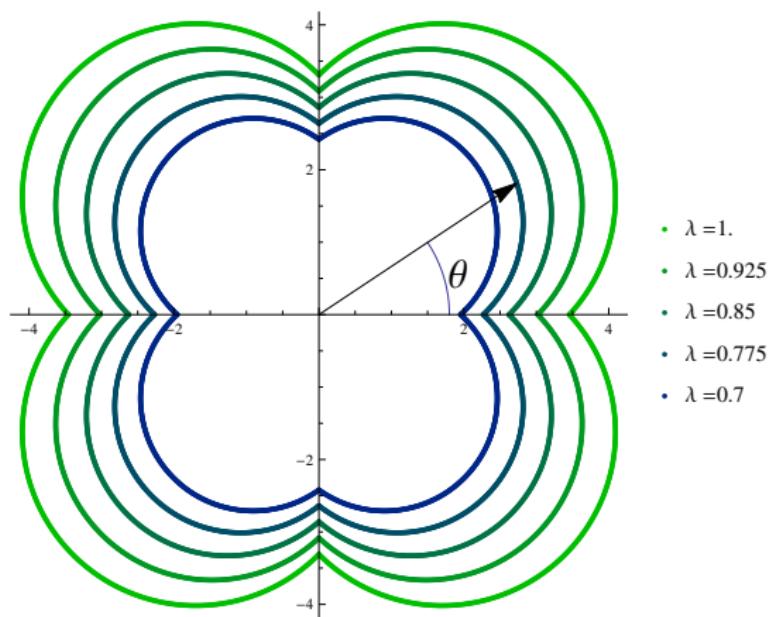
More results

This procedure works for any elastic strain-energy function, for example...



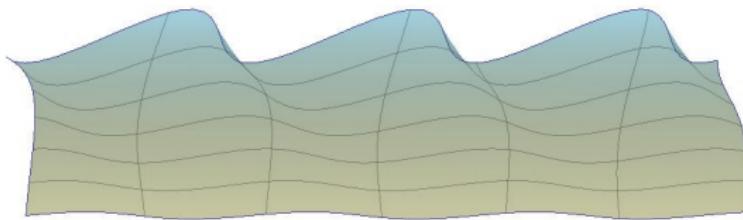
More results

This procedure works for any elastic strain-energy function, for example...

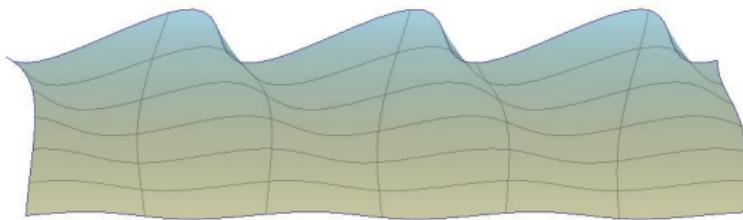


A model for skin, that has a neo-hookean matrix with fibers. This is an example of shear against the skin fibers.

What happened to our intuition?

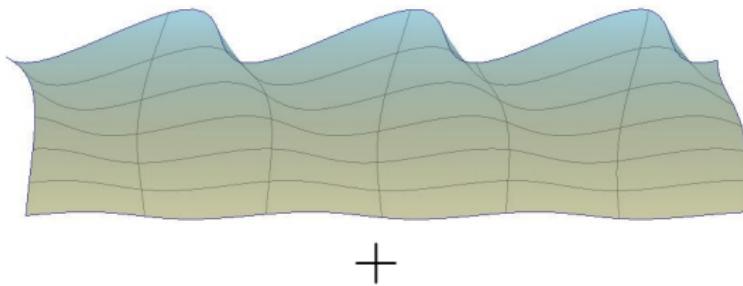


What happened to our intuition?



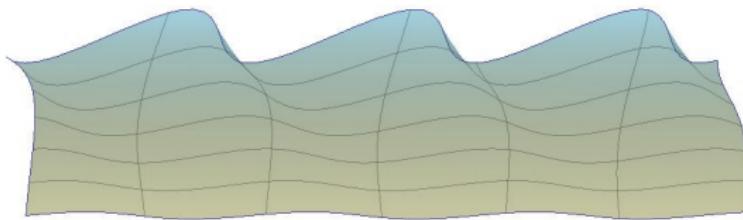
← Stretches Surface

What happened to our intuition?



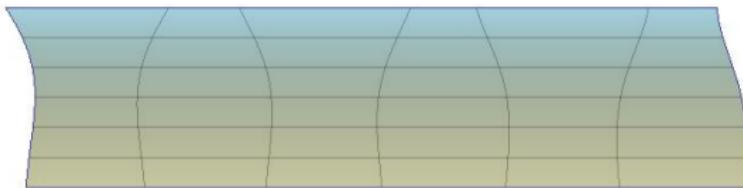
← Stretches Surface

What happened to our intuition?

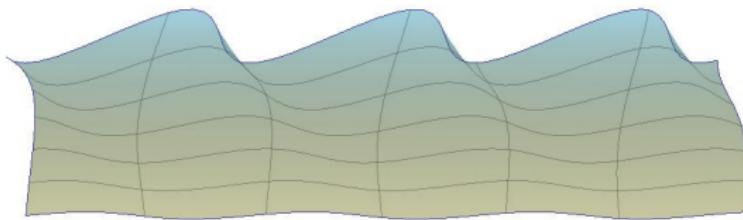


← Stretches Surface

+

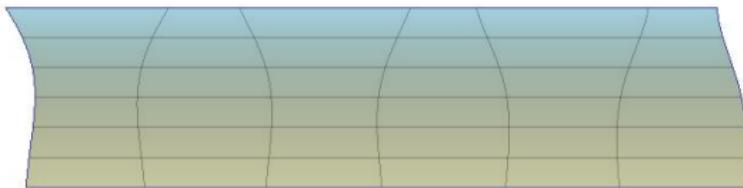


What happened to our intuition?



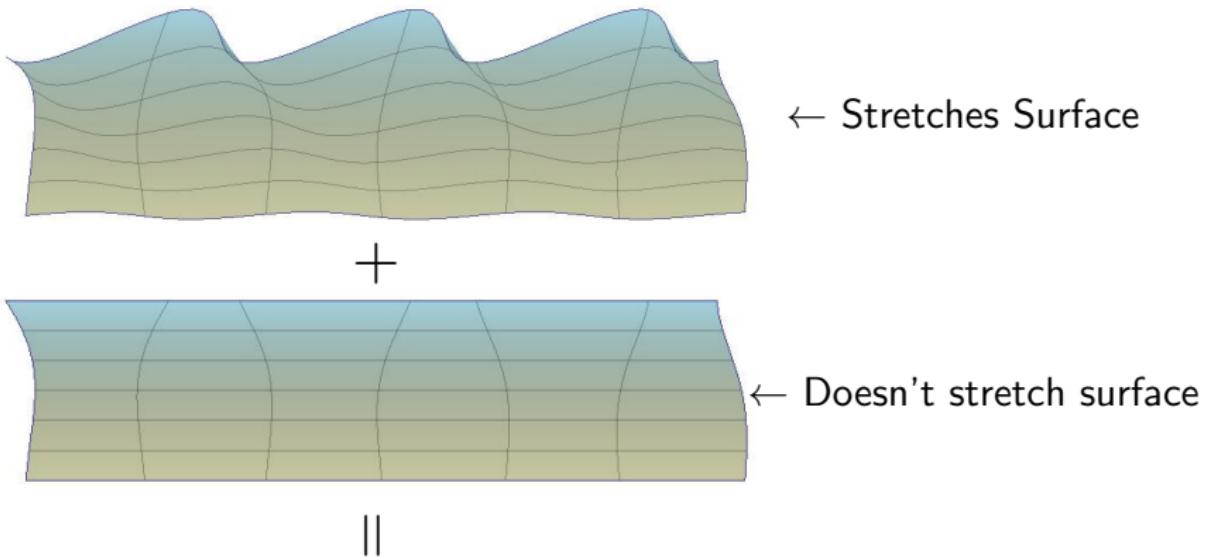
← Stretches Surface

+

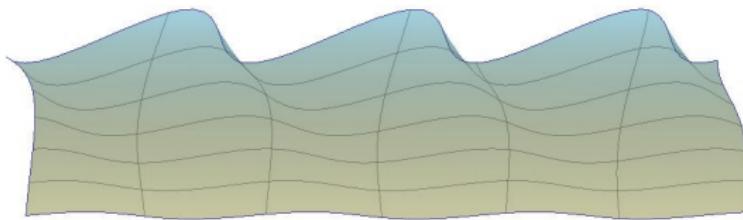


← Doesn't stretch surface

What happened to our intuition?

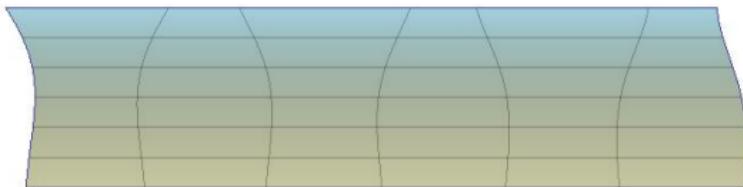


What happened to our intuition?



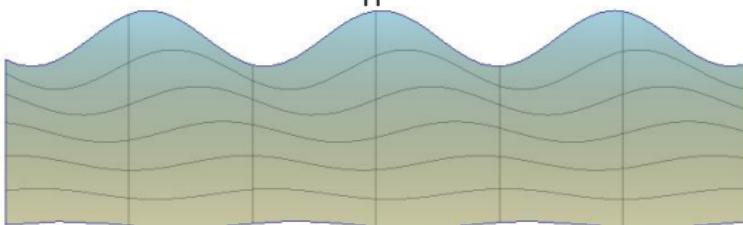
← Stretches Surface

+

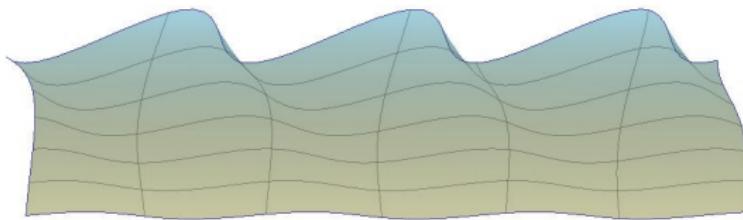


← Doesn't stretch surface

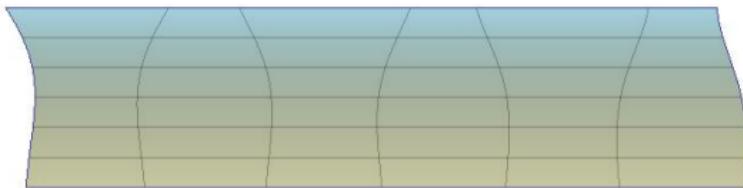
||



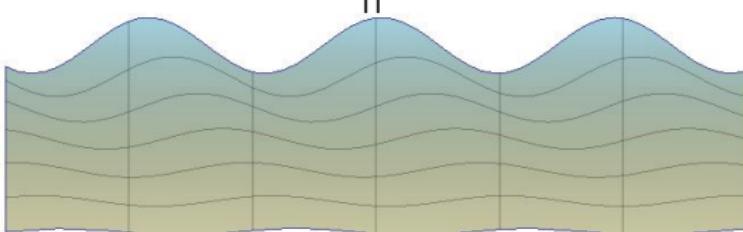
What happened to our intuition?



+

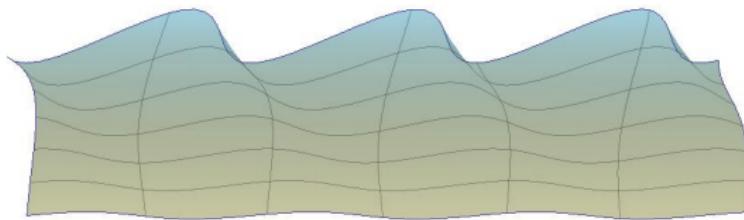


||



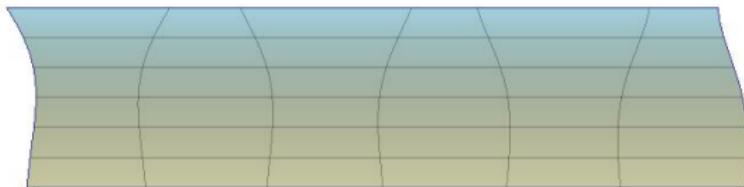
Any questions?

What happened to our intuition?

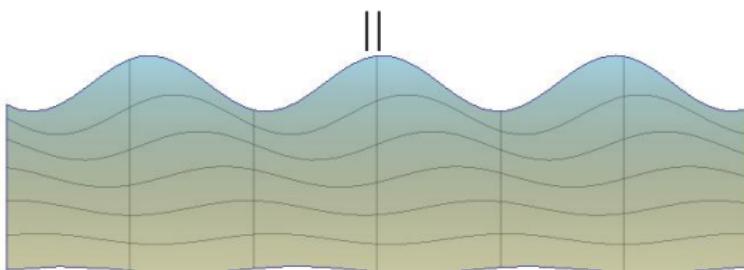


← Stretches Surface

+



← Doesn't stretch surface



Thanks for listening

Hope you enjoyed the talk!

Any questions?

 A.L. Gower, M. Destrade and R.W. Ogden Counter-intuitive results in acousto-elasticity, Wave Motion, (2013)
doi:10.1016/j.wavemoti.2013.03.007 (In Press)

-  A. Mielke, Y.B. Fu. A proof of uniqueness of surface waves that is independent of the Stroh Formalism, Math. Mech. Solids **9** (2003), 5–15.
-  K.Y. Kim, W. Sachse. Acoustoelasticity of elastic solids, in *Handbook of Elastic Properties of Solids, Liquids, and Gases*, **1**, 441–468. Academic Press, New York (2001).
-  K. Tanuma, C.-S. Man, W. Du. Perturbation of phase velocity of Rayleigh waves in pre-stressed anisotropic media with orthorhombic principal part, Math. Mech. Solids, DOI:10.1177/1081286512438882 (In Press).
-  R. De Pascalis, I. D. Abrahams and W. J. Parnell, On nonlinear viscoelastic deformations: a reappraisal of Fung's quasi-linear viscoelastic model, Proc. R. Soc. A **470** (2014).