

OP-AMP OSCILLATORS AND MULTIVIBRATORS

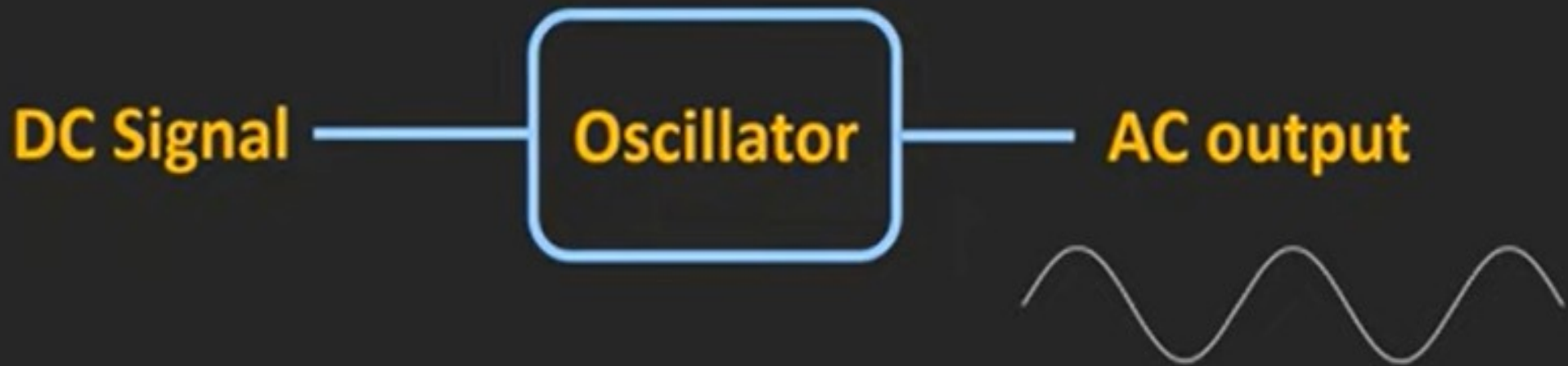
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Oscillators uses:

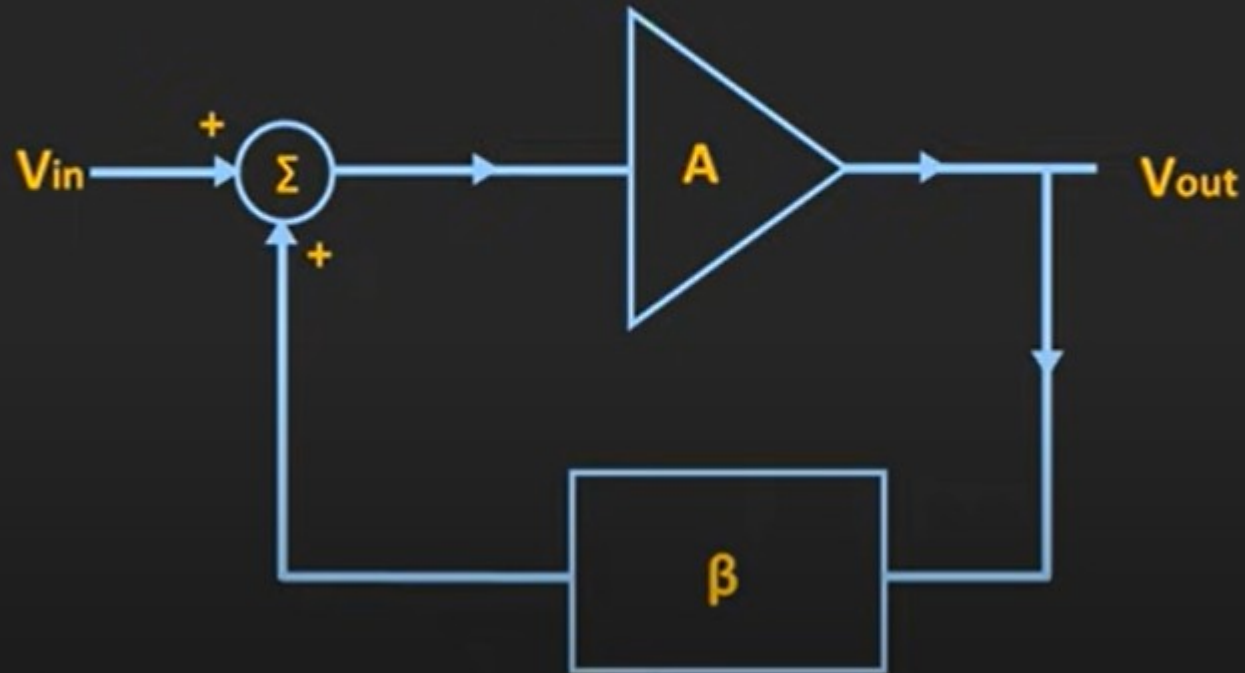
- Used in laptop and smartphone processors for generating the clock signals.
- Used in radio & mobile receivers for generating the local carrier frequency.
- Used in signal generators used in lab.

OSCILLATOR

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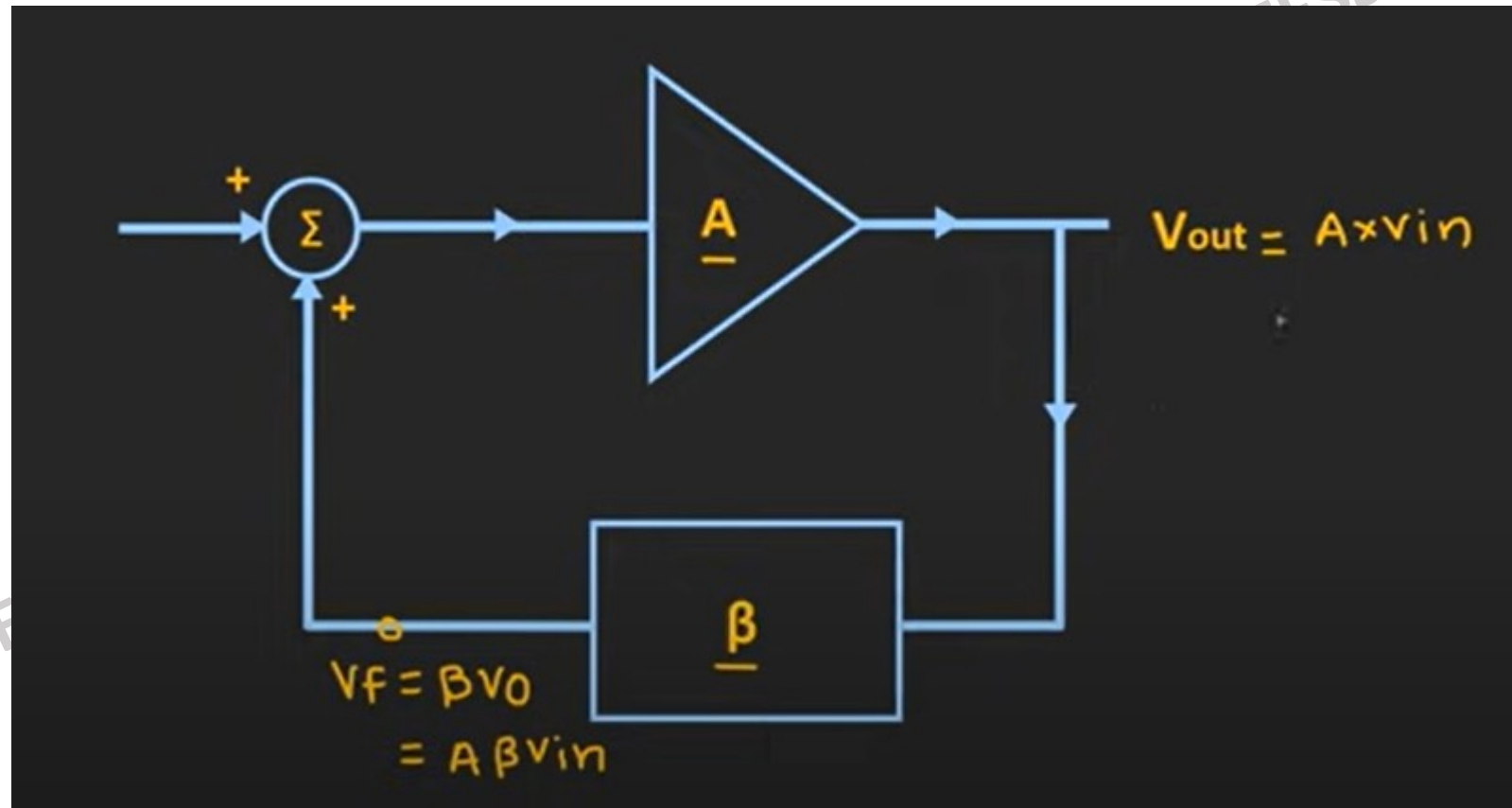


Amplifier with Positive Feedback



- Accepts DC voltage and it generates periodic AC s/g of the desired freq.
- Can generate freqs from few Hz to even GHz.
- o/p of oscr can be sinusoidal or non sinusoidal s/gs (like square and triangular wave)
- **Oscr – amplifier with a positive feedback.**

BASIC PRINCIPLE OF SINE WAVE OSCILLATORS

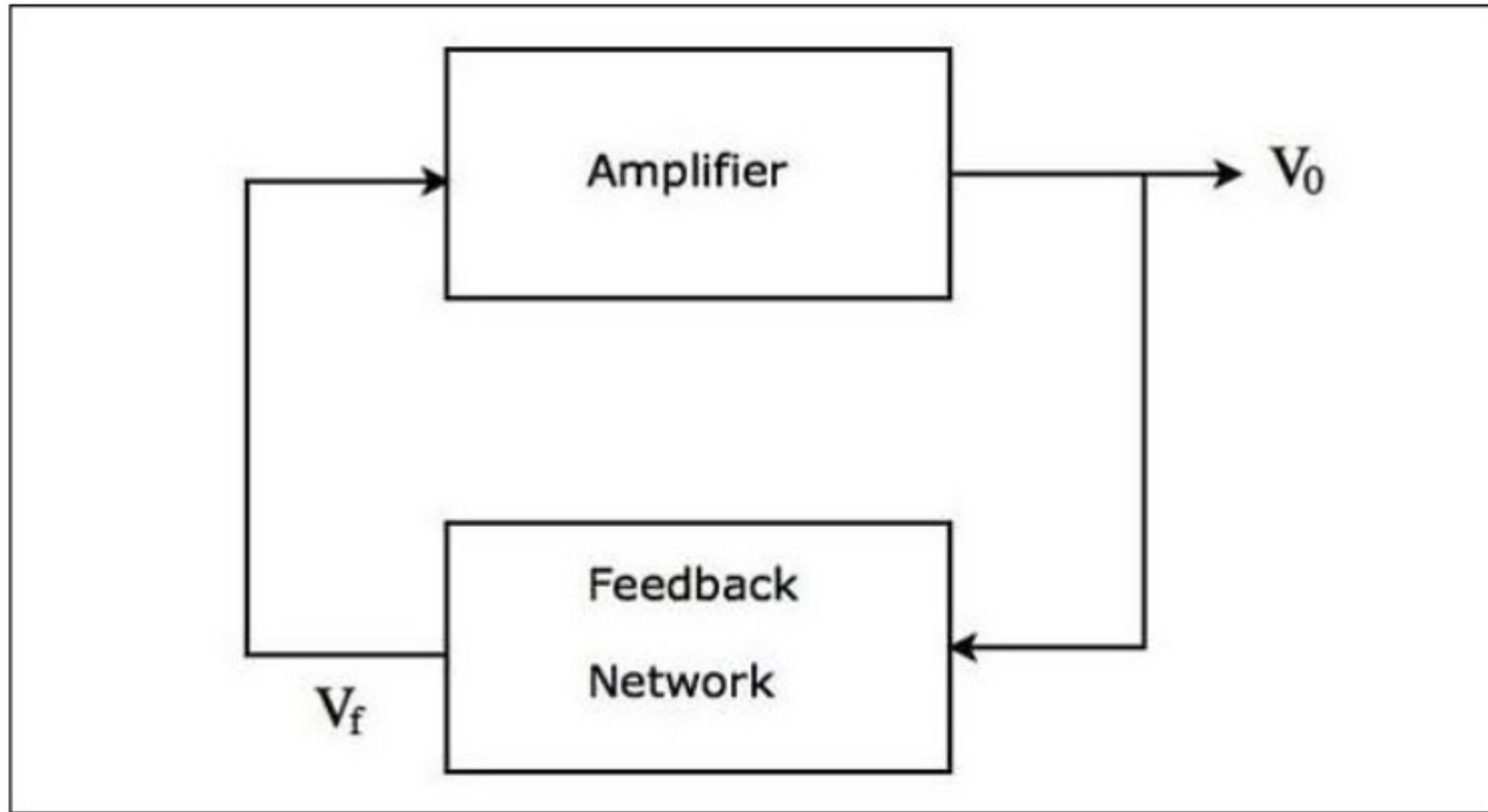


- If the oscillator produces sinusoidal oscillations, it is called as a **sinusoidal oscillator**.
- Let's say some input sinusoidal s/g is applied to this amplifier.
- At o/p, we get i/p multiplied by gain of this ampr.

$$V_{\text{out}} = AV_{\text{in}}$$

- This o/p s/g is given as i/p to f/b ckt with gain β .
- A freq selective f/b n/w (having inductive or capacitive components) with transfer ratio β .
- o/p of f/b ckt $V_f = \beta V_{\text{out}} = A\beta V_{\text{in}}$
- $A\beta$ is known as **loop gain**

- If the values of A and β are adjusted so that $A\beta = 1$, then $V_f = V_{in}$.
- Now if the original external s/g V_{in} is removed and only this f/b is connected, then the ckt will continue to provide o/p as the ampr cannot distinguish whether input V_{in} is coming from ext source or f/b ckt.
- Thus o/p can be continuously obtained w/o any i/p s/g if we can satisfy the condition on the loop gain $A\beta = 1$.
- This is called as **Barkhausen criterion for oscillations**.
- The condition $A\beta = 1$ can be satisfied only at one specific freq f_0 for the given component values.

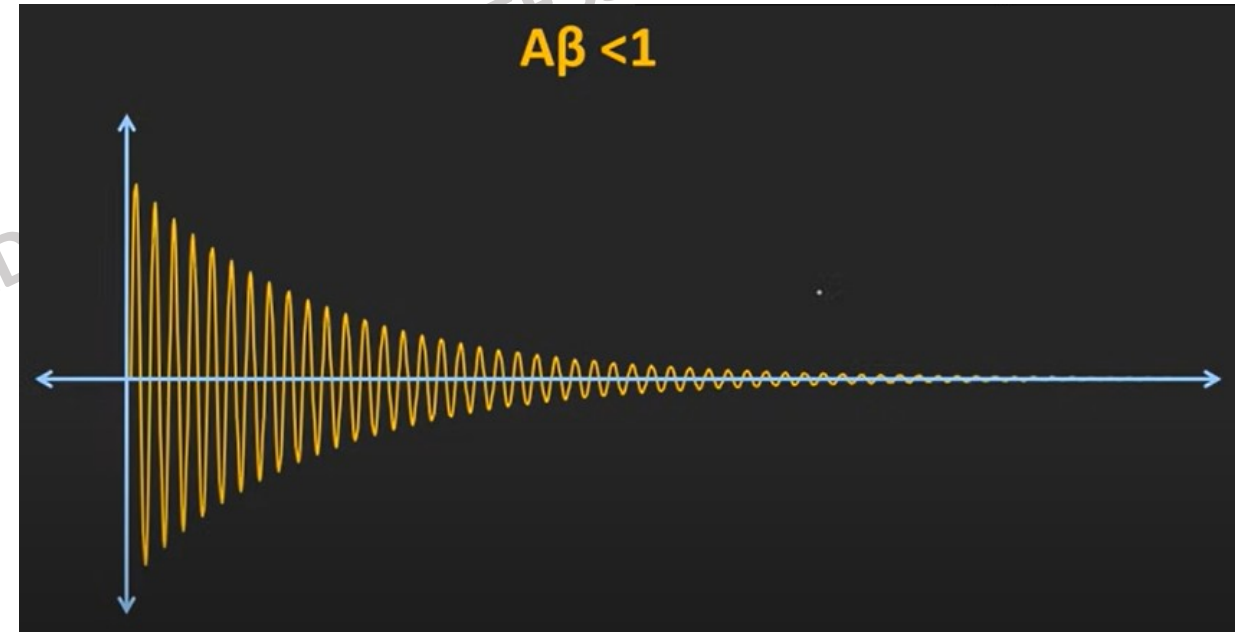


- Ckt thus provides o/p at freq f_0 where the ckt components meets the condition $A\beta = 1$.
- We can rewrite eqn as $A(j\omega_0) \beta(j\omega_0) = 1$ °
- There are 2 conditions (one on phase and other on magnitude) of the loop gain which needs to be satisfied simultaneously to achieve oscillations.
- Total phase shift of the loop gain should be 0 or multiples of 2π
- The magnitude of the loop gain should be equal to unity.

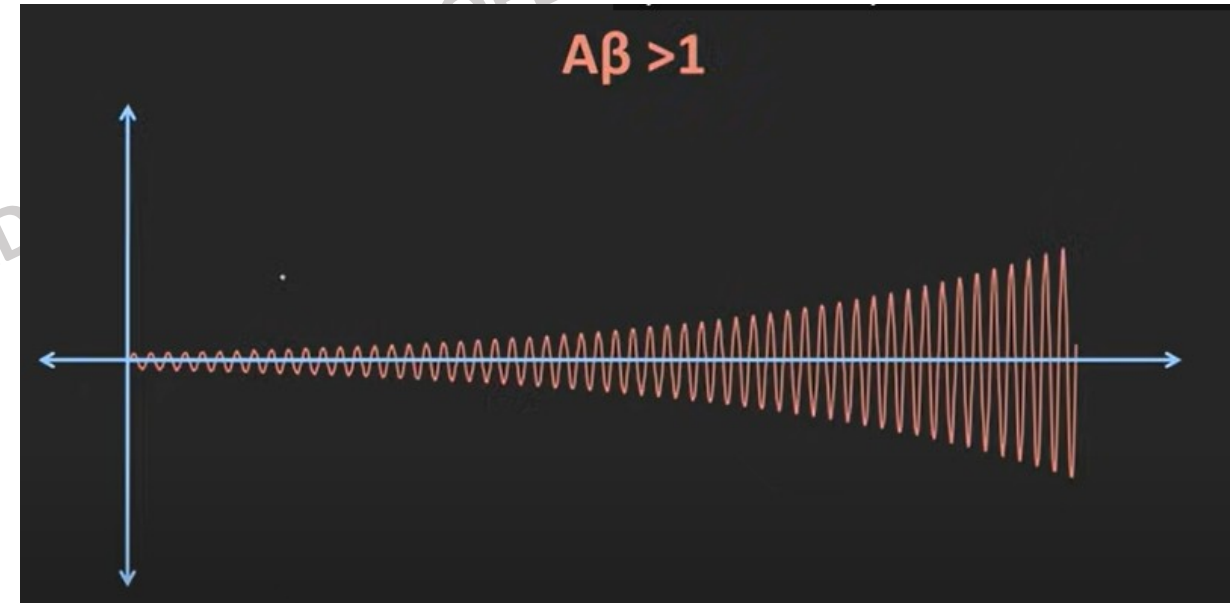
$$|A\beta| = 1$$

$$\angle A\beta = 0^\circ \text{ or multiples of } 2\pi$$

- The condition $|A\beta|=1$ is usually difficult to maintain in the ckt as the values of A and β vary due to temp variations, aging of components, change of supply voltage, etc.
- if $|A\beta|<1$, f/b s/g V_f goes on reducing in each f/b cycle and the oscns will die down eventually.

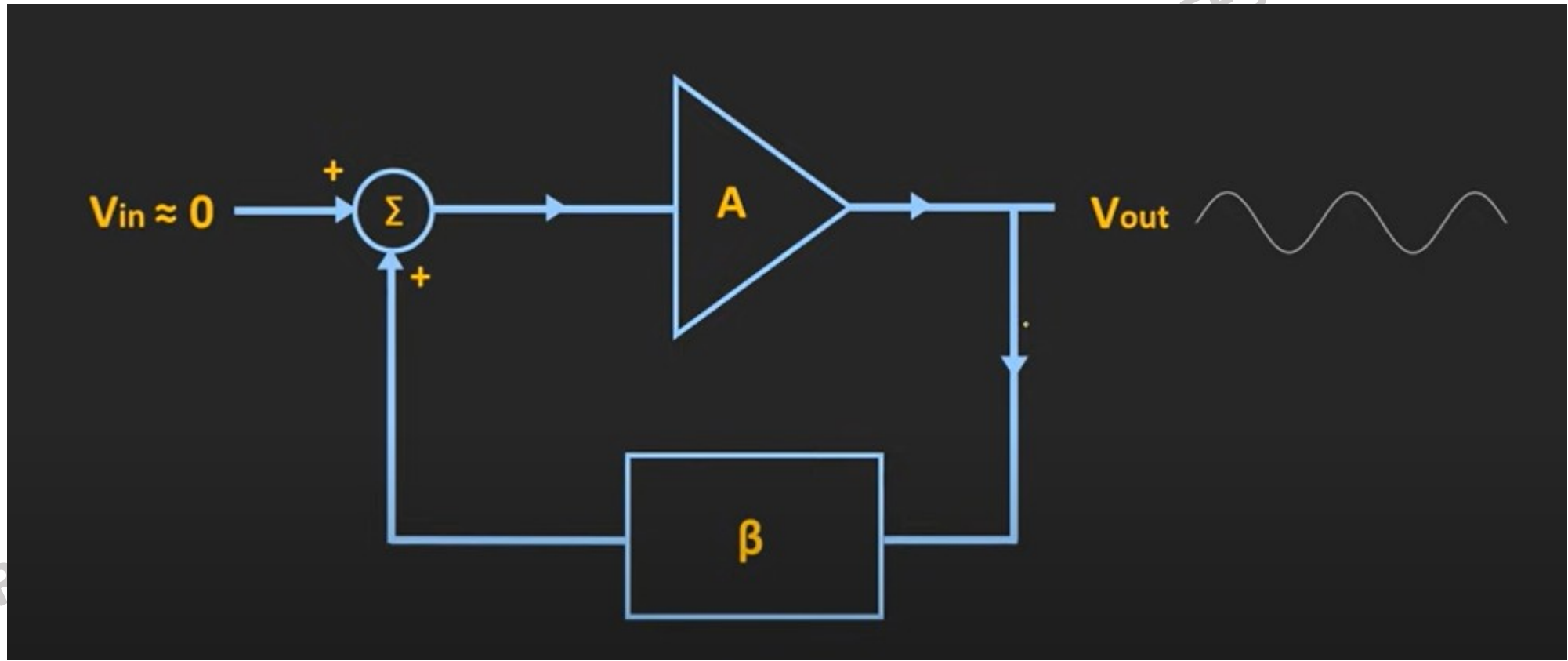


- When $|A\beta| > 1$, oscn in the ckt will build up.
- So in both cases we are not getting sustained oscns.



- In order to ensure sustained oscns inspite of variations, the ckt is designed so that $|A\beta|$ is slightly >1 .
- Now the o/p amp will go on increasing with every f/b cycle.

- The s/g however cannot go on increasing & gets limited due to the non linearity of the device (ie, as transistor enters into saturation).
- It is the non linearity of the transistor bcoz of which the sustained oscns can be achieved.
- The value of $|A\beta|$ is usually kept greater by abt 1 to 5% to ensure that $|A\beta|$ does not fall below unity.
- Till now, we had assumed that we first connect a s/g source to start the oscn and later remove it.
- In **practical oscr**, it is not done so.



- o/p waveform is obtained as soon as power is turned ON.
- Actually there is noise signal always present at input (ie, base) of the transistor due to temp (called Johnson's noise) or variation in the carrier conc(Schottky noise).
- Thermal noise contains all freqs(few Hz to even hundreds of GHz).
- So initially when this oscr is turned on, all the freq components of this noise will get amplified by the ampr.
- The noise s/g at the freq at which the ckt satisfies the condition $|A\beta|=1$ is picked up and amplified.

SINE WAVE OSCILLATORS

1. RC phase shift oscillator
2. Wein Bridge oscillator

Both are audio frequency oscillators.

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RC PHASE SHIFT OSCILLATOR

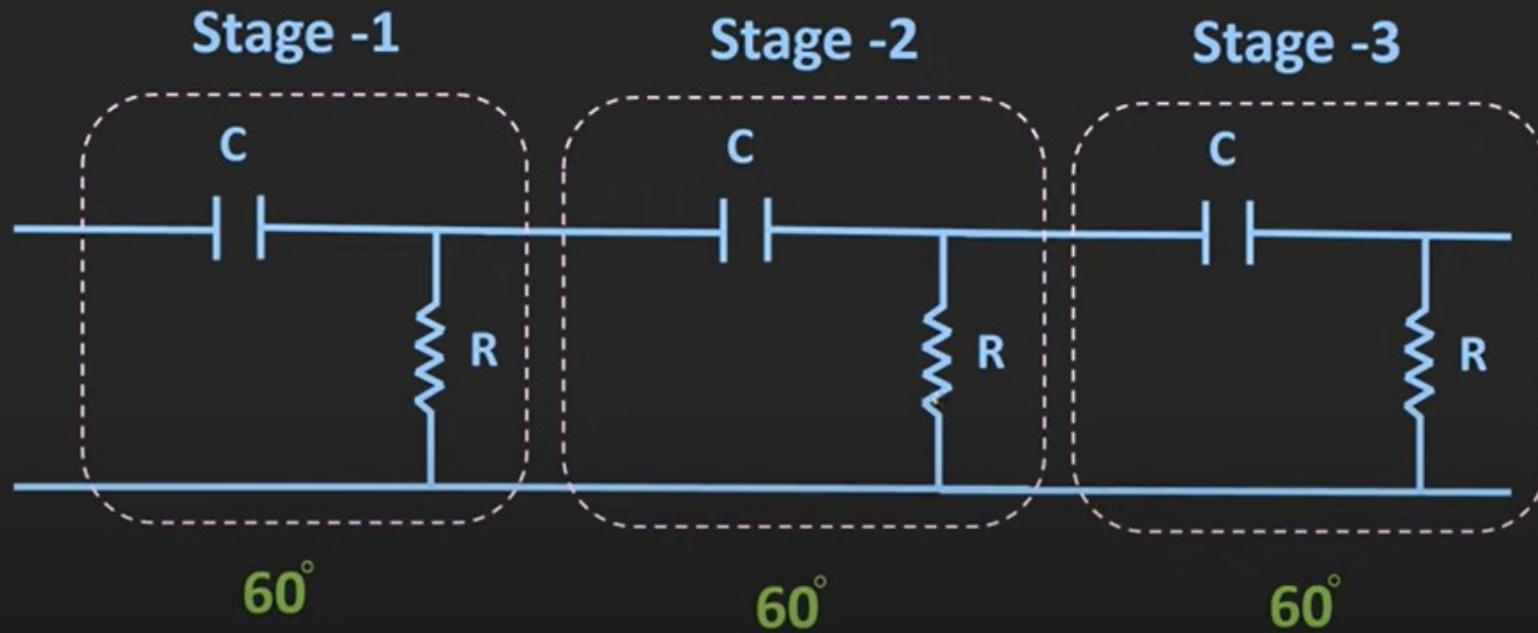
- RC ckt is used in the f/b path.
- Generates stable sine wave.
- Usually used in the low freq generations. Typically in the AF range.
- The op amp is used in inverting mode and hence provides 180° phase shift.
- The additional 180° phase shift is provided by RC n/w.

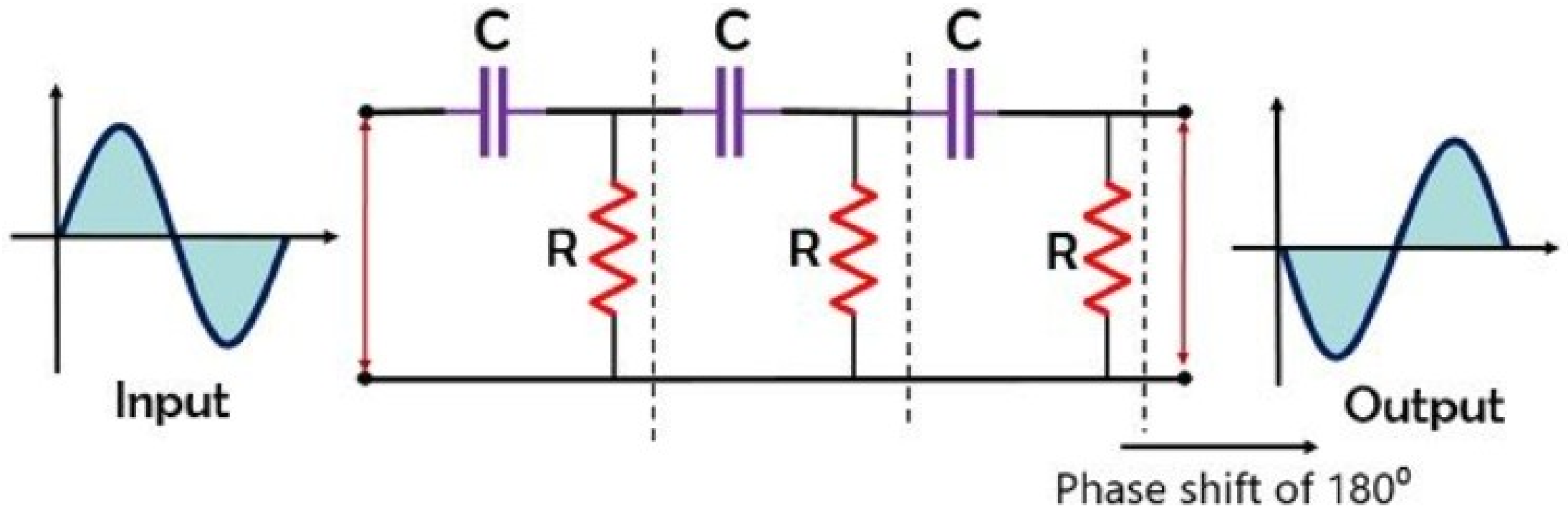
$$|A\beta| = 1$$

$$\angle A\beta = 0$$

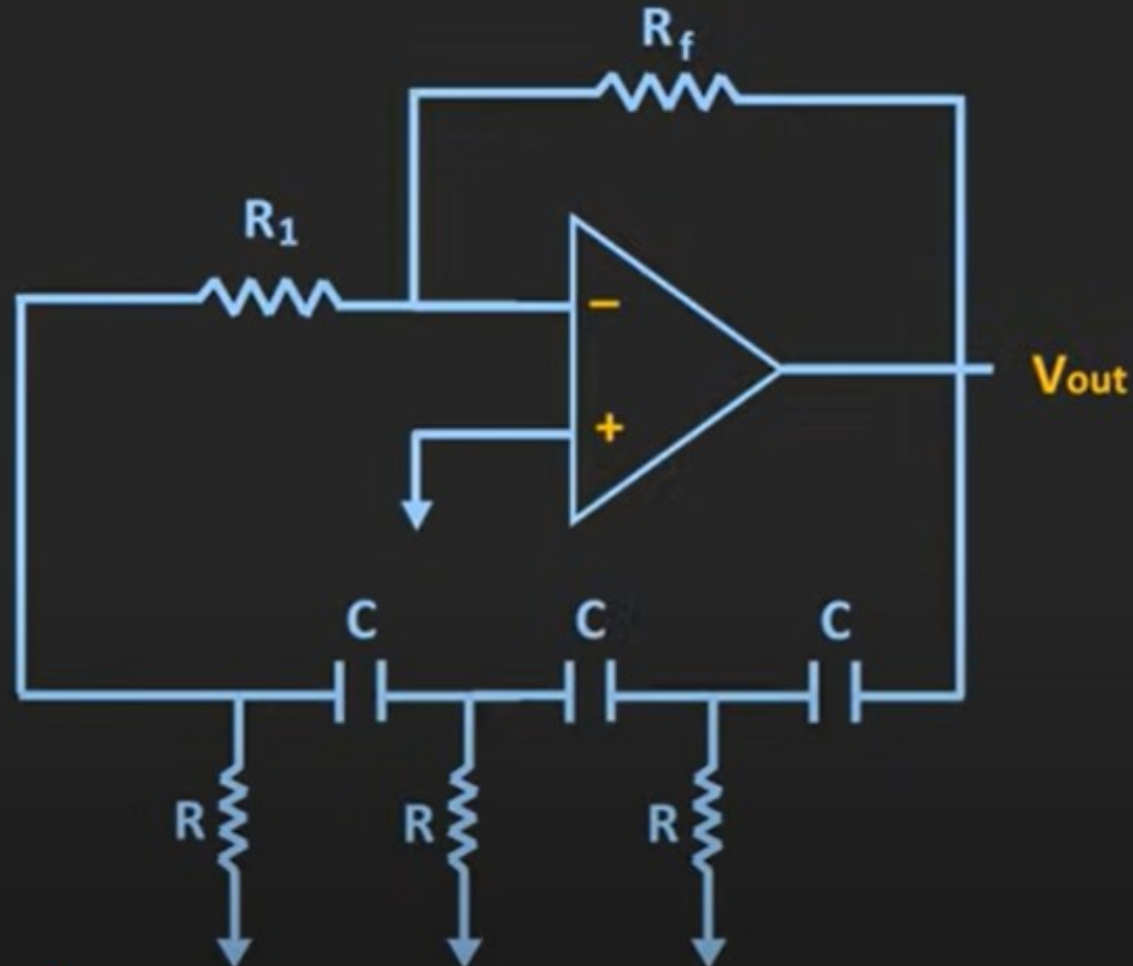
- To satisfy Barkhausen criterion, phase shift introduced by ampr & f/b ckt should be 0 or multiples of 2π .
- So to get sustained oscn, f/b ckt shud also provide 180° phase shift.
- So overall phase shift = 360°
- By tuning the gain of ampr and f/b ckt, we can achieve loop gain $|A\beta|=1$.

Cascade Connection of RC Stages

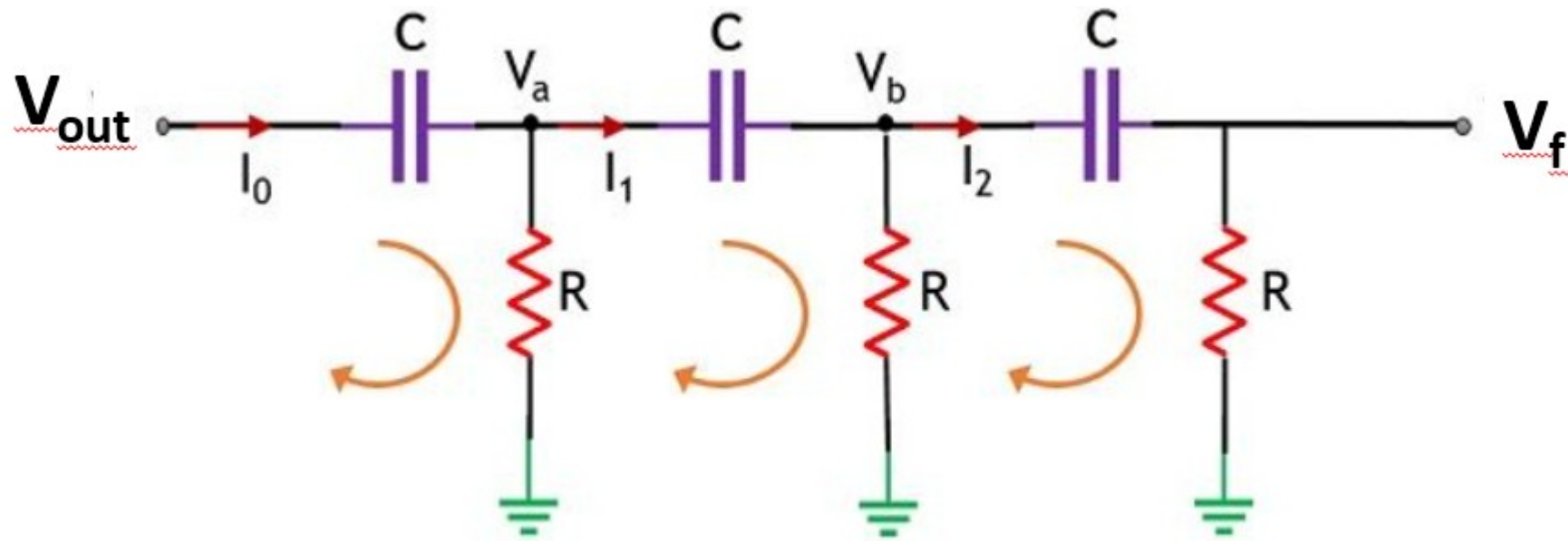




RC Phase Shift Oscillator using op-amp



Feedback network



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- At node V_b , the overall voltage will be equal to the sum of output voltage V_{out} and drop across the capacitor.

$$V_b = I_2 * R + V_f$$

$$V_f = I_2 R \text{ ----- } I_2 = V_f / R$$

- $V_b = V_{out} + V_f \text{ ----- } V_b = V_f [1 + \frac{R}{R}]$

Applying KCL

$$I_1 = I_2 + I_3 \text{ ----- } I_1 = I_2 [2 + \frac{R}{R}]$$

- $V_a = V_b + I_1 \cdot R_f$ ----- $V_a = V_f [1 + \frac{R_f}{R_1}]$

KCL at V_a

$$I_0 = I_1 + I_2 \text{ ----- } I_0 = [3 + \frac{R_f}{R_1}] I_1$$

Now $V_{out} = V_a + I_0 \cdot R_2$

$$\text{--- } V_{out} = V_f [1 + \frac{R_f}{R_1} + \frac{R_2}{R_1}]$$

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- Equating imaginary part, we get

$$- = 0$$

$$\omega = \quad f =$$

Equating real part,

$$V_{\text{out}} = V_f [1 -]$$

Substitute $\omega =$ in the above eqn, we get

$$V_{\text{out}} = -29 V_f$$

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- Gain of f/b n/w, $\beta = -$
- the negative sign indicates that f/b n/w produces a phase shift of 180° .
- Since $|A\beta| \beta| =$
- Therefore for sustained oscn, $|A| \geq 29$.
- That is gain of inv op amp should be atleast 29 or $R_f = 29 R_1$.

- Gain A_v is kept greater than 29 to ensure that the variations in ckt parameters will not make $|A_v \beta| < 1$, otherwise oscns will die out.

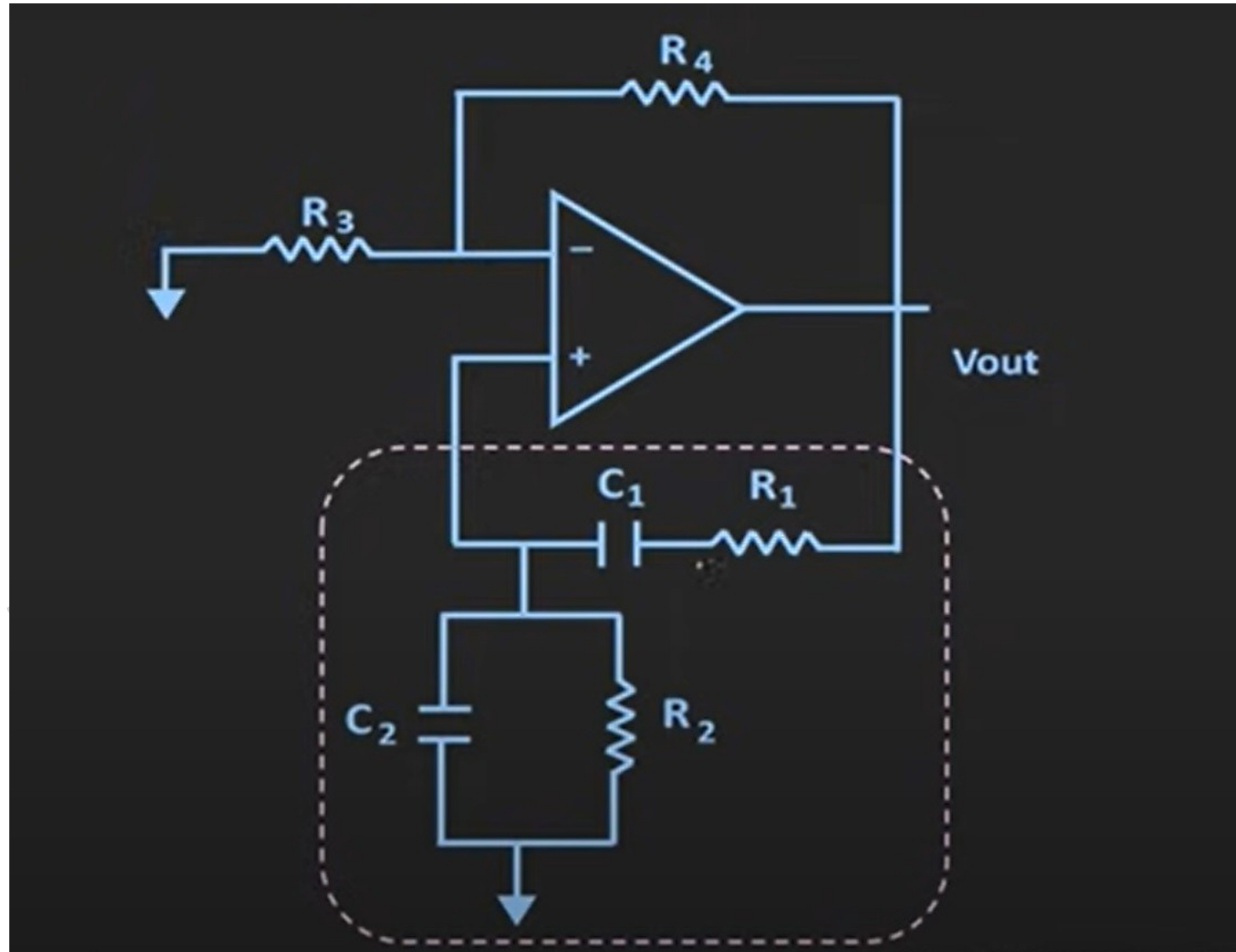
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WIEN BRIDGE OSCILLATOR

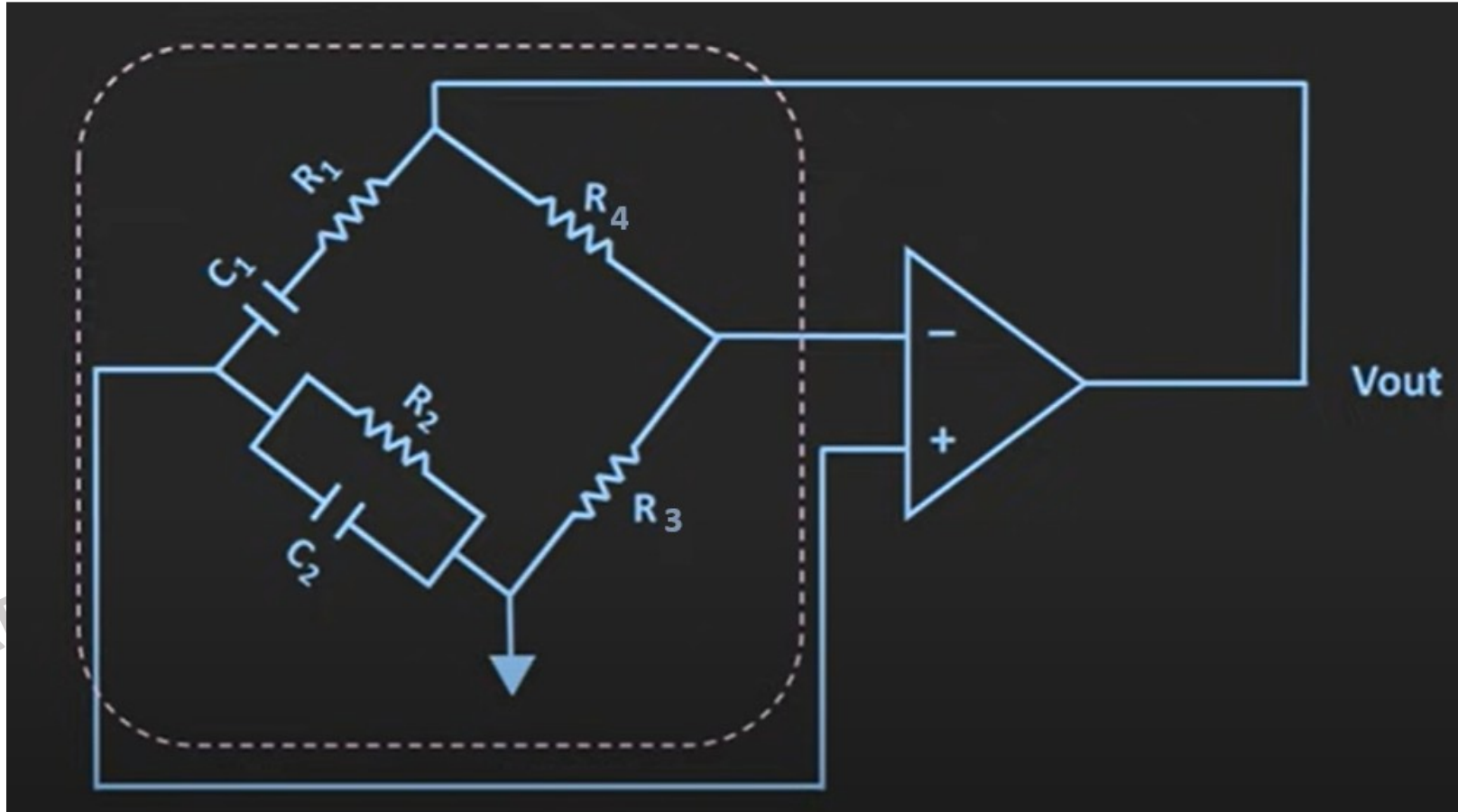
- Harmonic oscr – o/p of oscr is sinusoidal s/g.
- AF oscr – generates sine wave typically in the range of AF.

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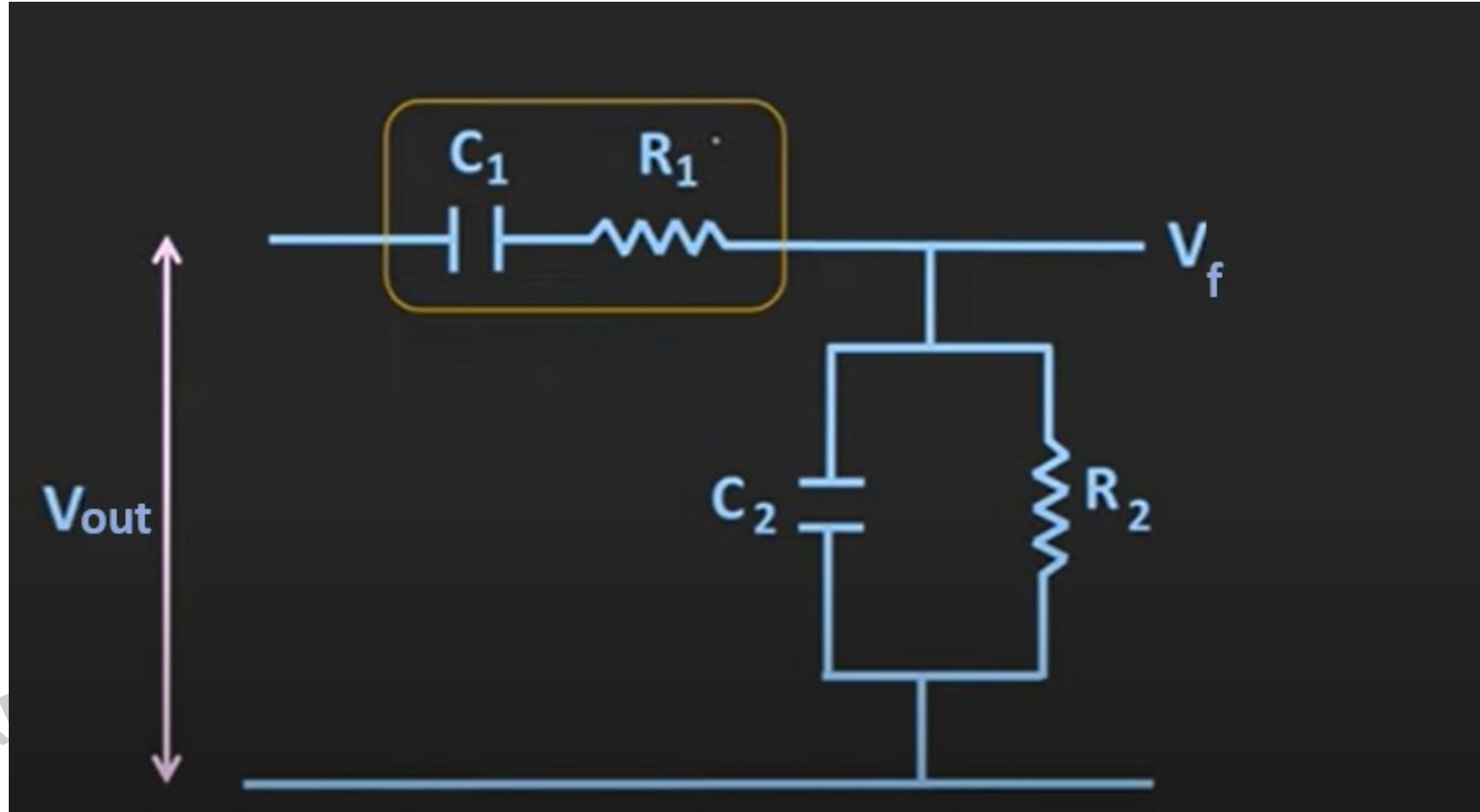
WIEN BRIDGE OSCILLATOR



Wien Bridge Oscillator Showing The Bridge Network



- Feedback RC n/w is connected to non inv terminal. So op amp – non inv ampr.
- Therefore f/b n/w need not provide any phase shift.
- Ckt can be viewed as a Wien bridge with a **series RC n/w** in one arm and a **parallel RC n/w** in the adjoining arm.
- Condition of zero phase shift around the ckt is achieved by **balancing the bridge**.



Series RC n/w acts like HPF .

- At low freq, $1/jX_c$ is high. So capr C1 acts like OC. So it doesnot pass low freq s/gs.
- At high freq, impedance provided by capacitor is low. So easily allows HF.

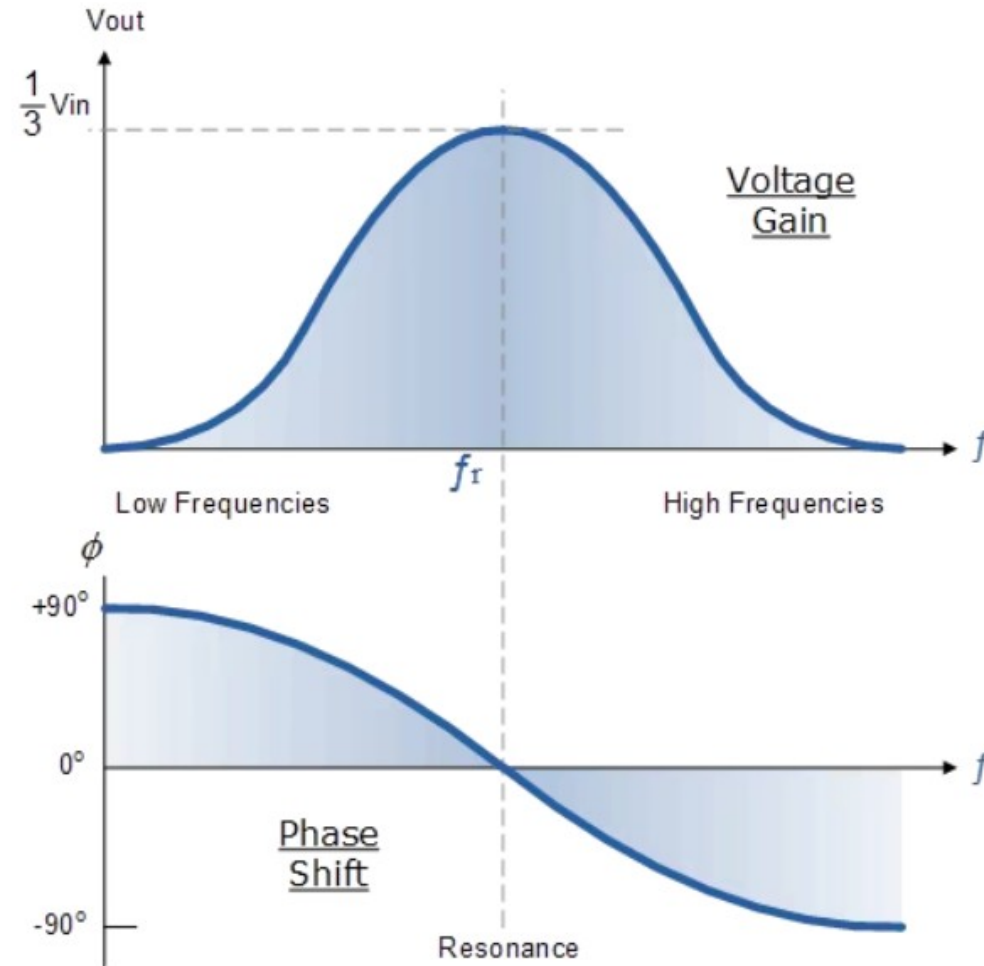
Parallel RC n/w acts like LPF

- At low freq, $1/jX_c$ is high. So capr C2 acts like OC. So o/p is taken across R2.
- At high freq, impedance provided by capacitor is very low. So o/p gets short cktd to grnd terminal.

- So this RC n/w doesnot allow low as well as high freqs.
- So there must be a frequency point between these two extremes of C1 being open-circuited and C2 being short-circuited where the output voltage, V_{OUT} reaches its maximum value.
- The frequency value of the input waveform at which this happens is called the oscillator's **Resonant Frequency (fr)**.

- At this resonant frequency, the phase difference between the input and output equals 0 deg.
- The magnitude of the output voltage of f/b n/w is therefore at its max and is equal to one third ($1/3$) of the input voltage as shown.
- $\beta = 1/3$

Oscillator o/p gain and phase shift



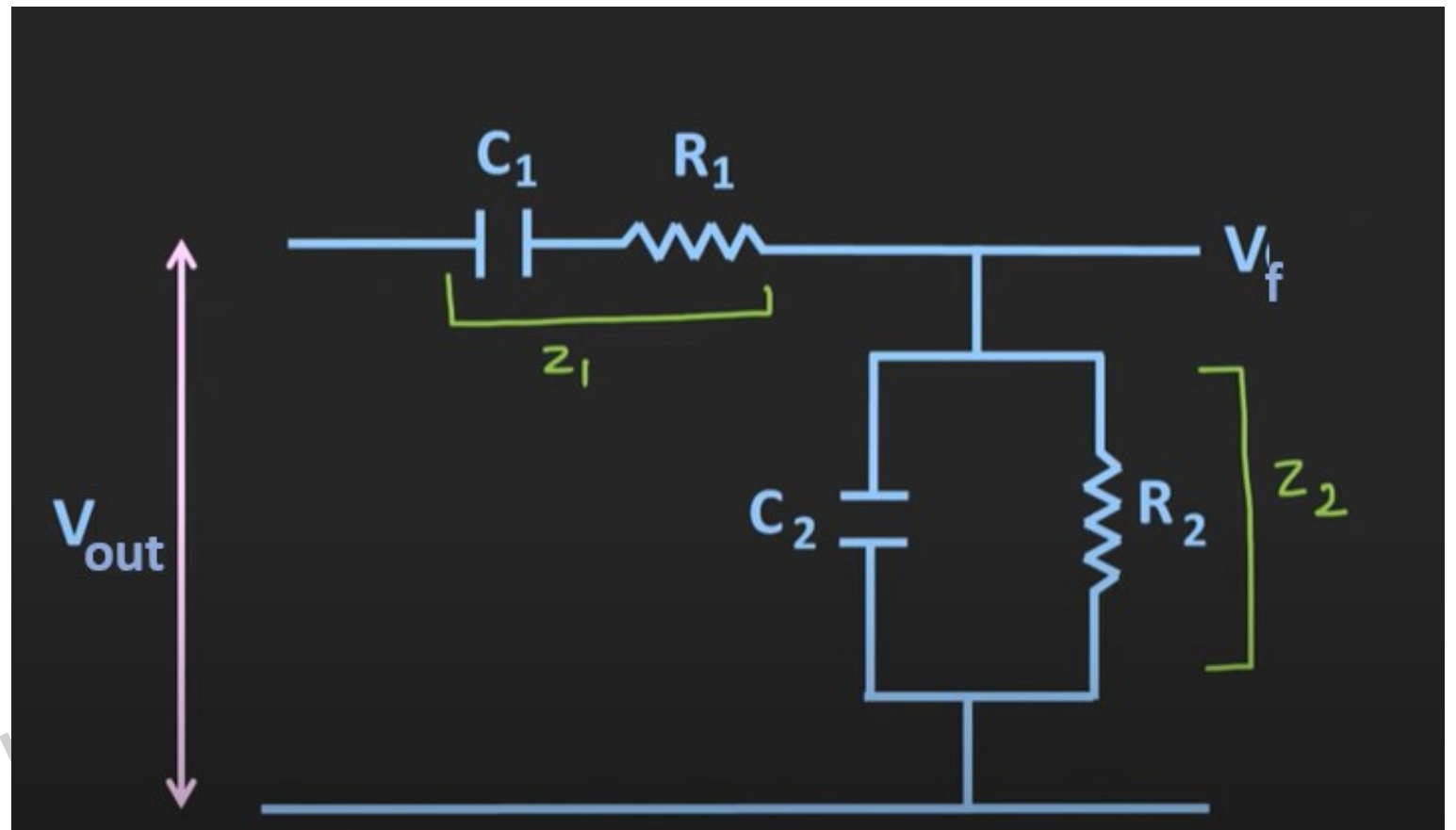
- =

- $Z_1 = R_1 + (1/j\omega C_1)$

- $Z_2 = R_2 \parallel (1/j\omega C_2)$
=

Substituting ,

$=\beta =$



- At resonant freq, phase shift offered by f/b n/w = 0.
- = 0 (so that $j\omega$ term cancel out)
- = 1

$$\omega =$$

- At resonance, the phase angle and mag condition for oscillation is satisfied.
- This condition occurs only when **bridge is balanced**.
- The freq of oscn f_o = resonant freq f_r of balanced Wien Bridge

$$f_o = f_r =$$

$$f_o = f_r =$$

$$\beta = 1/3$$

A=3 (to satisfy Barkhausen criterion)

At resonance, $\beta = 1/3$

$=\beta =$

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- $A\beta = 1$
- $A_v = +1 = 3$
- Here op amp is configured in non inverting configuration, so gain
- $A = 1 + R_4 / R_3 = 3$ **$R_4 = 2R_3$**
- $1 + \frac{R_4}{R_3} = 3$
- If $R_1 = R_2$ and $C_1 = C_2$, then $A_v = 2$ ----- **$R_4 = 2R_3$**

Q: Design a Wien bridge oscr of freq of 10KHz.

$C = 0.01\mu\text{F}$ $R = 1.59\text{K}$ $R_3 = 10\text{K}$ $R_4 = 20\text{K}$

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