

$$x_2(z) = \frac{1}{2j} \left\{ (1 - z^{-1}) f_{1,2} + \frac{1 - z^{-1}}{2j} \right\} e^{j(\theta - \omega_0)z} \\ = \underline{-\frac{2j}{2j+2}} \cdot \underline{(1-z^{-1})f_{1,2} + \frac{1-z^{-1}}{2j+2}e^{j(\theta-\omega_0)z}}$$

### Module-3

FIR filters are having linear phase characteristics.

FIR filters are stable, and a lot of design methods for FIR filter (direct design).

Multi filtering, i.e., same system can do multiple type of filtering (LPF, HPF)

### Design of FIR filter

An FIR filter of length  $M$  (finite impulse) with i/p  $x(n)$  and o/p  $y(n)$  is described by difference equation.

$$y(n) = b_0 x(n) + b_1 x(n-1) + \dots + b_{M-1} x(n-M+1) \quad y(n) = x(n) * h(n)$$

$$= \sum_{k=0}^{M-1} b_k x(n-k)$$

$$y(n) = \sum_{k=0}^{M-1} h(k) x(n-k)$$

$$H(z) = \sum_{k=0}^{M-1} h(k) z^{-k}$$

$$H(e^{j\omega}) = \sum_{n=0}^{M-1} h(n) e^{-j\omega n}$$

$$H(e^{j\omega}) = |H(e^{j\omega})| e^{j\theta(\omega)}$$

$$h(n) = \pm h(M-1-n) \quad n = 0, 1, 2, \dots, M-1$$

$\rightarrow$  center of symmetry.

In FIR filter;  $\alpha \rightarrow$  constant

$$\theta(\omega) = -\alpha\omega$$

(as FIR filter is Linear)



$$\frac{1}{2\pi n} \left[ e^{j\omega n} - e^{-j\omega n} + e^{j\omega n} - e^{-j\omega n} \right]$$

$$= \frac{1}{\pi n} \left[ \frac{e^{j\omega n} - e^{-j\omega n}}{2j} + \frac{e^{j\omega n} - e^{-j\omega n}}{2j} \right]$$

$$= \frac{1}{\pi n} \left[ \sin(\omega n) - \sin(-\omega n) \right] \quad n \neq 0$$

$$= \left[ \frac{\sin(\omega n)}{\pi n} - \frac{\omega n \sin(\omega n)}{\pi n^2} \right]$$

$$h(n) = 1 - \frac{\omega n}{\pi}, \quad n = 0$$

$\approx$

\* Here in Fourier Series three arises the phenomenon so we use different method called window's method.

→ FIR FILTER USING WINDOWS.

$$H(\omega) = \sum_{n=0}^{\infty} h(n) e^{-j\omega n}$$

$$h(n) = \frac{1}{2\pi} \int H(\omega) e^{j\omega n} d\omega$$

$h(n) = h(n) w(n)$ .

$$= \begin{cases} h(n), & n = 0, 1, \dots, M-1 \\ 0, & \text{otherwise.} \end{cases}$$

$$W(\omega) = \sum_{n=0}^{M-1} w(n) e^{-j\omega n}$$

$$h(n) = h(n) w(n) \xrightarrow{\text{DTF}} W(\omega) = \frac{1}{2\pi} \int [H(j\omega) * w(j\omega)] d\omega$$

$$H(\omega) = \frac{1}{2\pi} \int h(d) w(\omega - d) d\omega$$

→ Rectangular windows:

$$w(n) = \begin{cases} 1, & n = 0, 1, \dots, M-1 \\ 0, & \text{otherwise.} \end{cases}$$

Bartlett X  
Blackman X

The FT of rectangular window is

$$W(\omega) = \sum_{n=0}^{M-1} e^{j\omega n}.$$

Hanning ✓  
Kahngular ✓

Hanning :

$$0.54 - 0.46 \cos\left(\frac{2\pi n}{M-1}\right)$$

time domain

Hanning:

$$\frac{1}{2} (1 - \cos\left(\frac{2\pi n}{M-1}\right))$$

time domain

Main lobe  $\Rightarrow$  decide transmission width  
Side lobe  $\Rightarrow$  decide noise.

- Rectangular windows has highest side lobe (-13) so it has high noise.

- Rectangular has low transmission width (main lobe  $\downarrow$ ) so sharp peak.

Symmetrical linear phase FIR LPF using windows.

$$H(\omega) = \sum_{n=0}^{M-1} w(n) e^{-j\omega n} \quad h(n) = h(n) w(n) \xrightarrow{\text{DTF}}$$

$$W(\omega) = \frac{1}{2\pi} \int [H(j\omega) * w(j\omega)] d\omega$$

$$h(n) = \frac{1}{2\pi} \int e^{-j\omega(\frac{m-1}{2})} e^{j\omega n} d\omega \cdot \frac{1}{2\pi} \int e^{j\omega(n - \frac{m-1}{2})} d\omega.$$

$$h(n) = \frac{1}{2\pi} \int e^{-j\omega(\frac{m-1}{2})} e^{j\omega n} d\omega \cdot \frac{1}{2\pi} \int e^{j\omega(n - \frac{m-1}{2})} d\omega.$$

$$\frac{1}{2\pi} \left[ \frac{e^{j\omega(n-\frac{m-1}{2})}}{j(n-\frac{m-1}{2})} \right]_{-\omega_c}$$

$$\frac{1}{2\pi j(n-\frac{m-1}{2})} \left[ e^{j(n-\frac{m-1}{2})\omega_c} - e^{-j(n-\frac{m-1}{2})\omega_c} \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ \frac{e^{j(n-\frac{m-1}{2})\omega_c} - e^{-j(n-\frac{m-1}{2})\omega_c}}{2j} \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ \sin \omega_c \left( n - \frac{m-1}{2} \right) \right]_{-\frac{\omega_c}{2} \text{ to } \frac{\omega_c}{2}}$$

①

$$h[n] = h(\omega) \omega(n)$$

②

$$H[z]$$

steps: For designing f filter:

$$h[n] \quad @ \quad w[n] \quad \text{ideal case}$$

③

$$h[n] = h(\omega) \omega(n)$$

④

$$H[z]$$

Symmetrized

? Define the desired impulse response of an FIR

filter of length  $m$ , having cut-off frequency  $\omega_c$ ,

$$h[n] = \frac{1}{\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{jn\omega} d\omega.$$

$$= \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{-j\omega(n-\frac{m-1}{2})} j\omega(n-\frac{m-1}{2}) d\omega.$$

$$= \frac{1}{2\pi} \left[ \int_{-\pi}^{\pi} e^{-j\omega(n-\frac{m-1}{2})} j\omega(n-\frac{m-1}{2}) d\omega + \int_{\pi}^{\pi} e^{-j\omega(n-\frac{m-1}{2})} j\omega(n-\frac{m-1}{2}) d\omega \right]$$

$$= \frac{1}{2\pi} \left[ \int_{-\pi}^{\pi} e^{-j\omega(n-\frac{m-1}{2})} j\omega(n-\frac{m-1}{2}) d\omega + \int_{\pi}^{\pi} e^{-j\omega(n-\frac{m-1}{2})} j\omega(n-\frac{m-1}{2}) d\omega \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ e^{-j\omega(n-\frac{m-1}{2})} - e^{j\omega(n-\frac{m-1}{2})} \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ -\sin \omega_c \left( n - \frac{m-1}{2} \right) + \sin \omega_c \left( n - \frac{m-1}{2} \right) \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ \sin \pi \left( n - \frac{m-1}{2} \right) - \sin \omega_c \left( n - \frac{m-1}{2} \right) \right]$$

$$= \frac{1}{\pi(n-\frac{m-1}{2})} \left[ \sin \pi \left( n - \frac{m-1}{2} \right) - \sin \omega_c \left( n - \frac{m-1}{2} \right) \right]$$

When  $n = \frac{m-1}{2}$ , ( $\alpha = 0 \Rightarrow$  ideal case)

$$h[n] = 1 - \frac{\omega_c}{\pi} \left( \frac{\sin \pi \left( n - \frac{m-1}{2} \right)}{\pi} - \frac{\sin \omega_c \left( n - \frac{m-1}{2} \right)}{\omega_c \left( n - \frac{m-1}{2} \right)} \right)$$

Implementation of the design.

$$H[z] = \bar{z}^{-(m-1)} \left[ h(0) + \sum_{n=1}^{m-1} h(n) \left[ \frac{1}{z^n} + \frac{1}{\bar{z}^n} \right] \right]$$

$$= \bar{z}^{-(m-1)} \left[ \sum_{n=0}^{m-1} h(n) (\bar{z})^{-n} \right] = 0$$

$\Rightarrow$  In FIR filter general equation:

$$H(z) = \sum_{n=0}^{m-1} h(n) z^{-n} \quad \text{--- (1)}$$

Location of zeros of FIR filter on  $z$ -plane:

- In FIR filter for a zero there always exist its inverse

FIR is called non-causal filter because

equation output depends on the present ip and past ip not past ip.

$$h(z_0) = \sum_{n=0}^{m-1} h(n) \bar{z}_0^{-n} = 0 \quad \text{--- (2)}$$

$$= h(0) \bar{z}_0^0 + h(1) \bar{z}_0^{-1} + h(2) \bar{z}_0^{-2} + \dots + h(m-1) \bar{z}_0^{-(m-1)} = 0$$

Sufficient condition:

$$h(0) = h(m-1) = 0 \quad \text{--- (3)}$$

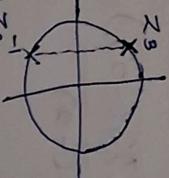
$$\begin{aligned} \text{in (3), } & \bar{z}_0^{m-1} = 1 \\ H(z_0) &= h(m-1) \bar{z}_0^{-(m-1)} + h(m-2) \bar{z}_0^{-(m-2)} + \dots \\ &+ h(0) = 0 \end{aligned}$$

$$= \bar{z}_0^{-(m-1)} \left[ h_0 \bar{z}_0^{m-1} + h_1 \bar{z}_0^{m-2} + \dots + h(m-1) \bar{z}_0^0 \right]$$

Case III:

$$|z_3| = 1$$

Here  $z_3$  will not be on any axis but on the circle.  $z_3^* = z_3$

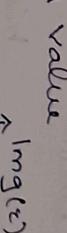


$$z_3^{-1} = \text{conjugate of } z_3.$$

If there exist a zero and its inverse exist for an FIR filter.

We can locate zeros of FIR filter for 4 cases:

Case I:  $z$  is a real value



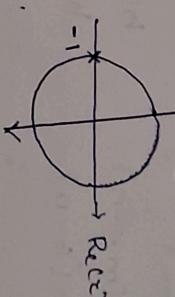
$\Rightarrow$   $|z| = 1$  [for eg].

Inverse and original value will be same value.

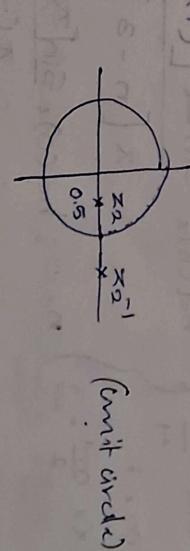
Here  $\bar{z}_1 = -1, \bar{z}_1^{-1} = 1$

# Filter. Case II:  $z_2$  is real zero.

$$|z| < 1, [z_2 = \alpha]$$



(unit circle)



Final output for implementation of the design:

$$H[z] = \bar{z}^{-(\frac{m-1}{2})} \left[ h(0) + \sum_{n=1}^{\frac{m-1}{2}} \bar{z}^{-n} h(n) \left[ \bar{z}^{-1} + \bar{z}^0 \right] \right]$$

$\Rightarrow$  In FIR filter general equation;

$$H(z) = \sum_{n=0}^{m-1} h(n) \bar{z}^{-n} \quad \text{--- (1)}$$

\* Location of zeros of FIR filter on z-plane:

- In FIR filter for a zero there always exist its inverse.

$$\bar{z}_0 \Rightarrow \bar{z}_0^{-1}$$

Proof:

$$H[z_0] = \sum_{n=0}^{m-1} h(n) \bar{z}_0^{-n} = 0 \quad \text{--- (2)}$$

$$= h(0) \bar{z}_0^0 + h(1) \bar{z}_0^{-1} + h(2) \bar{z}_0^{-2} + \dots + h(m-1) \bar{z}_0^{-(m-1)} = 0$$

Sufficient condition:  
 $b(0), b(m-1-n) = 0$

(4) in (3);

$$H[z_0]^2 = b(m-1) \bar{z}_0^{-(m-1)} + b(m-2) \bar{z}_0^{-(m-2)} + \dots + b(0) \bar{z}_0^0$$

$$+ b(0) = 0$$

$$= \bar{z}_0^{-(m-1)} \left[ b_0 \bar{z}_0^{m-1} + b(1) \bar{z}_0^{m-2} + \dots + b(m-1) \bar{z}_0^0 \right]$$

$$H[z_0] = \bar{z}_0^{-(m-1)} \left[ \sum_{n=0}^{m-1} b(n) \bar{z}_0^n \right] = 0$$

$$= \bar{z}_0^{-(m-1)} \left[ \sum_{n=0}^{m-1} b(n) (\bar{z}_0^{-1})^{-n} \right] = 0 \quad \text{--- (3)}$$

Comparing (2) and (3).

If there exist a zero and its inverse exist for an FIR filter.

We can locate zeros of FIR filter for 4 cases:

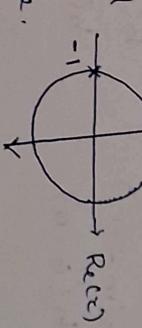
# Case I:  $z$  is a real value

$$z_1 = -1$$

[For eg.]

$z_1 = -1$  [For eg].  
 because differential  
 value will be same  
 value.

$$H(z) = 1, z_1 = -1$$



# Case II:  $z_2$  is real zero.

$$|z_2| \leq 1$$

[For eg.]

$$z_2 = 1$$

[For eg.]

~~#~~ Case IV: Magnitude not 1.5-1

二十一

二  
四

$z_4^{-1}$  outside the

Both are different values.

? Design an FIR LPF of length  $N$  having cut-off frequency  $\omega_c$ .

(iii) Hammer windows.

11

$$\left. \begin{aligned} h(n) &= h(m-1-n) \\ &= h(6-n) \end{aligned} \right\} \begin{aligned} h(1) &= h(5) \\ h(2) &= h(4) \end{aligned} \quad \begin{array}{l} \text{should be} \\ \text{same value.} \end{array}$$

二〇

$$\frac{\sin \omega_c}{\pi} \left[ C_0 - \frac{B_{11}}{\omega} \right]$$

$$\omega_n = \sin \frac{\pi}{n} [(n-3)]$$

$$\begin{aligned} \text{; } h(-3) &= \frac{\sin[\pi/4 \times (-3)]}{\pi(-3)} = \frac{\sin(3\pi/4)}{-3\pi} \\ &\approx 0.045 \end{aligned}$$

$$\text{Ans: } \sin(\gamma_4(-2)) = \frac{\sin(2\pi/4)}{2\pi} = 0.15\%$$

$$hdc(0) = \frac{\sin(\frac{\pi}{4})}{\pi} = 0.242$$

$$hdc(1) = \frac{\sin \frac{\pi}{4}}{\pi} = 0.242$$

$$hdc(2) = \frac{\sin \frac{3\pi}{4}}{\pi} = 0.245$$

$$hdc(5) = \frac{\sin \frac{2\pi}{4}}{\pi} = 0.159$$

$$hdc(0) = \frac{\sin \frac{3\pi}{4}}{3\pi} = 0.045$$

$$hdc(3) = \frac{\sin \frac{\pi}{4}}{3\pi}$$

Next calculates the win

Final suspension =  $\text{h}_{\text{ext}}(n) \times w(n)$

$$h(0) = 0, \quad h(1) = 0.159, \quad h(2) = 0.25, \quad h(3) = \frac{1}{3}$$

(ii) → Desired impulse response.

→ Calculate the window; set  $hd(0), hd(1), hd(2), hd(3), hd(4), hd(5), hd(6)$

$$w(t) = 0.54 - 0.46 \cos\left(\frac{2\pi t}{H-1}\right)$$

$$w_2 = 0.54 - 0.46 \left( \frac{v}{c} \right) = 0.4$$

$$w_3(3), \quad 0.54 = 0.46 \cos\left(\frac{8\pi}{3}\right) = 0.377$$

$$w(\alpha) = 0.54 - 0.46 \cos\left(\frac{12\pi}{\alpha}\right), \quad 0.08 \leq w(\alpha) \leq 0.54$$

$$\rightarrow h(n) = h_d(n) w(n)$$

$$h(0) = 0.045 \times 0.08 = \underline{\underline{0.036}}$$

$$h(1) = 0.159 \times 0.31 = \underline{\underline{0.049}}$$

$$h(2) = 0.225 \times 0.44 = \underline{\underline{0.143}}$$

$$h(3) = 0.225 \times 0.31 = \underline{\underline{0.143}}$$

(iii)  $\rightarrow$  Direct

$$\rightarrow w(n) = \frac{1}{2} (1 - \cos(\frac{2\pi n}{N-1})) \quad w(1) = \frac{1}{2} (1 - \cos \frac{2\pi}{6})$$

$$w(0) = \frac{1}{2} (1 - \cos(0)) = \underline{\underline{0}}. \quad \approx 0.25.$$

$$w(2) = \frac{1}{2} (1 - \cos(\frac{4\pi}{6})) = \underline{\underline{0.45}}.$$

$$w(3) = \frac{1}{2} (1 - \cos(\pi)) = \underline{\underline{1}}.$$

$$w(4) = \frac{1}{2} (1 - \cos(\frac{8\pi}{6})) = 0.45$$

$$w(5) = \frac{1}{2} (1 - \cos(\frac{10\pi}{6})) = \underline{\underline{0.25}}.$$

$$w(6) = \frac{1}{2} (1 - \cos(\frac{12\pi}{6})) = \underline{\underline{0}}.$$

$\rightarrow h(n) = h_d(n) w(n)$

$$h(0) = 0.045 \times 0 = \underline{\underline{0}} \quad h(1) = 0.159 \times 0.25$$

$$h(2) = \underline{\underline{0}}.$$

$$h(3) = 0.039$$

$$h(4) = \underline{\underline{0.039}}$$

$$h(5) = 0.168$$

$$h(6) = 0.225 \times 0.75 = \underline{\underline{0.168}}$$

$$h(7) = 0.075$$

$$h(8) = \underline{\underline{0}}.$$

Design an FIR HPF of cut off frequency  $\frac{\pi}{4}$  rad/s.

and having the desired impulse response

$h_d(e^{j\omega}) = e^{j4\omega}$ , we know  $\omega_0 = \pi$  using

(a) Rectangular (b) Hamming (c) Hanning.

$$e^{-j\alpha\omega} = h_d(e^{j\omega}).$$

$$\alpha = 4, \quad \alpha = \frac{m-1}{2}, \quad \alpha = \frac{m-1}{2}.$$

$$h_d(n) = \frac{1}{\pi(n-\frac{m-1}{2})} \left[ \sin \pi \left( n - \frac{m-1}{2} \right) - \sin \frac{\pi}{4} \left( n - \frac{m-1}{2} \right) \right]$$

$$h_d(n) = \frac{1}{\pi(n-4)} (\sin(n-4\pi) - \sin \frac{\pi}{4} (n-4))$$

$$h_d(0) = \frac{1}{\pi(-4)} (\sin(-4\pi) - \sin(-\frac{4\pi}{4}))$$

$$= \frac{1}{-4\pi} (-\sin 4\pi + \sin \pi) = \underline{\underline{0}}.$$

$$h_d(1) = \frac{1}{\pi(-3)} \left[ \sin(-3\pi) - \sin(-\frac{3\pi}{4}) \right]$$

$$= -\underline{\underline{0.045}},$$

$$h_d(2) = \frac{1}{-2\pi} \left( -\sin 2\pi + \sin \frac{2\pi}{4} \right) = -\underline{\underline{0.159}}$$

$$h_d(3) = \frac{1}{-\pi} \left( -\sin(\pi) + \sin(\pi/4) \right) = -\underline{\underline{0.225}}.$$

$$h_d(4) = 1 - \frac{\omega_0}{\pi} = 1 - \frac{\pi/4}{\pi} = \underline{\underline{-0.25}},$$

$$h_d(5) = \frac{1}{\pi} \left( \sin(\pi) - \sin(\pi/4) \right) = \underline{\underline{0.225}}$$

$$h_d(6) = \frac{1}{2\pi} \left( \sin(2\pi) - \sin \frac{2\pi}{4} \right) = \underline{\underline{0.159}}.$$

(i) Rectangular :  $\omega_m = 1, m \in \mathbb{Z}^+$

$$h(0) = h(8) = 0$$

$$h(2) = h(6) = -0.159 \quad h(3) = h(5) = -0.225$$

$$h(4) = 0.45.$$

(ii) Hamming  $\omega_m = 0.54 - 0.46 \cos\left(\frac{2m\pi}{m-1}\right)$

$$\omega(0) = 0.54 - 0.46 \cos\left(\frac{0\pi}{8}\right) = 0.08$$

$$\omega(1) = 0.54 - 0.46 \cos\left(\frac{\pi}{8}\right) = 0.814$$

$$\omega(2) = 0.54 - 0.46 \cos\left(\frac{2\pi}{8}\right) = 0.54$$

$$\omega(3) = 0.54 - 0.46 \cos\left(\frac{3\pi}{8}\right) = 0.86$$

$$\omega(4) = 0.54 - 0.46 \cos\left(\frac{4\pi}{8}\right) = 1.$$

$$\omega(5) = 0.54 - 0.46 \cos\left(\frac{5\pi}{8}\right) = 0.86$$

$$\omega(6) = 0.54$$

$$\omega(7) = 0.214$$

$$\omega(8) = 0.08.$$

$$h(0), h(1) \times \omega_m)$$

$$h(0) = h(8) = 0. \quad h(1) = h(7) = -0.045 \times 0.146$$

$$= -0.0193$$

$$h(2) = h(6) = -0.159 \times 0.54$$

$$= -0.085$$

$$h(3) = h(5) = -0.225 \times 0.86 = -0.193$$

$$h(4) = 0.45.$$

(iii) Hanning.  $\omega_m = \frac{1}{2}(1 - \cos\left(\frac{2m\pi}{m-1}\right))$

$$\omega(0) = \frac{1}{2}(1 - \cos(0)) = 0.$$

$$\omega(1) = \frac{1}{2}(1 - \cos\left(\frac{2\pi}{7}\right)) = 0.146.$$

$$\omega(2) = \frac{1}{2}(1 - \cos\left(\frac{4\pi}{7}\right)) = 0.5.$$

$$\omega(3) = \frac{1}{2}(1 - \cos\left(\frac{6\pi}{7}\right)) = 0.853.$$

$$\omega(4) = \frac{1}{2}(1 - \cos \pi) = 1.$$

$$\omega(5) = \frac{1}{2}(1 - \cos\left(\frac{10\pi}{7}\right)) = 0.853$$

$$\omega(6) = 0.5 \quad \omega(7) = 0.146 \quad \omega(8) = 0.$$

$$h(0) = h(8) = 0 \quad h(1) = h(7) = -0.045 \times 0.146$$

$$= -0.0193$$

$$h(2) = h(6) = -0.159 \times 0.54$$

$$= -0.085$$

$$h(3) = h(5) = -0.225 \times 0.86 = -0.193$$

$$h(4) = 0.45.$$

$$h(5) = -0.085$$

$$h(6) = 0.146$$

$$h(7) = 0.853$$

$$h(8) = 1$$

$$h(9) = 0$$

$$h(10) = -0.045$$

$$h(11) = 0.146$$

$$h(12) = -0.853$$

$$h(13) = 0$$

\* Design of IIR filter from Analog filters.

$$H_a(s) = \frac{B(s)}{A(s)} = \frac{\sum_{k=0}^N B_k s^k}{\sum_{k=0}^N A_k s^k}$$

(Design of  
indirect)

IIR filter first  
we have to

design the  
analog counter-

impulse response.

$P_k, \alpha_k \rightarrow$  Filter coefficient.

Analog filter having the natural sys function  $H_0$  can be described by the linear constant coeff differential equation:

$$\sum_{k=0}^N \alpha_k \frac{d^k g(t)}{dt^k} < \sum_{k=0}^M \beta_k \frac{d^k x(t)}{dt^k}$$

Taking Laplace:

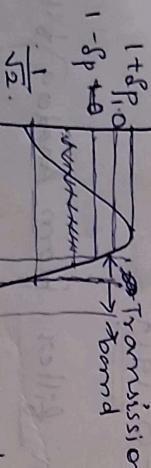
$$\sum_{k=0}^N \alpha_k s^k = \sum_{k=0}^M \beta_k s^k$$

→ Indirect Design:  
Step: ① Map the digital specification to those of analog filter specification.

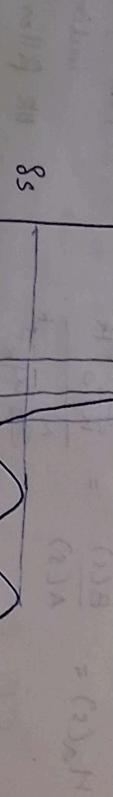
- ② Derive the TF of analog LP prototype  
③ Design. Convert this analog LP prototype to given filter. (LP, HP, BP) type.

④ Final digital transformation using number of methods. (Bilinear transfer etc.)  $\{H(s) \rightarrow H(z)\}$

$$|H(e^{j\omega})|$$



stop band.



and  $\omega_s$

Instead of:  $1 - \delta_p = \frac{1}{\sqrt{1 + \epsilon^2}}$   $\omega_s = \text{stopband frequency}$ .

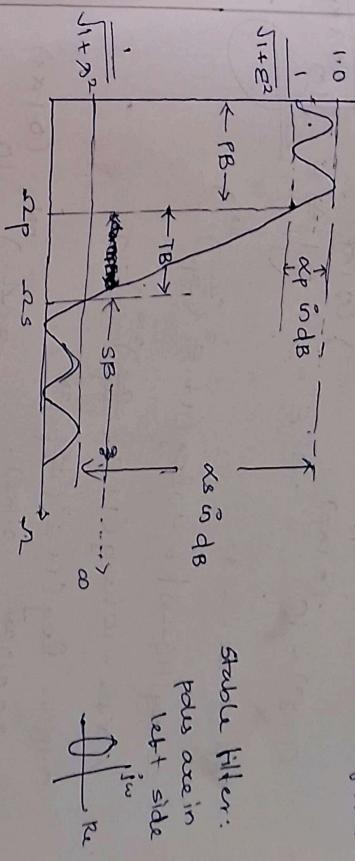
$$\delta_s = \frac{1}{\sqrt{1 + \epsilon^2}}$$

$$H(s) = \frac{\prod_{k=0}^N \beta_k s^k}{\prod_{k=0}^M \alpha_k s^k} = \frac{N(s)}{D(s)}$$

(N ≥ M)

Denominator mostly  $N=M$

N → order of filter.



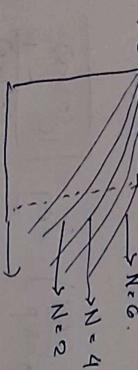
Butterworth: Flat passband and flat stopband

All pole filter ( $H(s) = \frac{1}{D(s)}$ )

For Butterworth:

$$|H(j\omega)|^2 = \frac{1}{1 + \left(\frac{\omega}{\omega_c}\right)^{2N}} = \frac{1}{1 + \epsilon^2 \left(\frac{\omega}{\omega_p}\right)^{2N}} \quad ①$$

For diff values of N:



Normalized  $\omega_c, \omega_p$

Steps: ①  $\# N$  ②  $H_N(s) | \omega_c, \text{rad/sec}$  ③ Apply the diff of analog freq. transformation (TF)

Butterworth LP  $\rightarrow$  LP  $\rightarrow$  HP  $\rightarrow$  BP  $\rightarrow$  BR.

Always first we have to find LP analog prototype

$$\left( \frac{2 \times 10^{10} \log |H(j\omega)|}{20 \log |H(j\omega)|} \right)^N = -10 \log \left[ 1 + \epsilon^2 \left( \frac{\omega_p}{\omega_p} \right)^{2N} \right] \quad \text{--- (2)}$$

when  $\omega = \omega_p$ ;  $\Rightarrow 20 \log |H(j\omega)| = -10 \log [1 + \epsilon^2]$

$$\omega \alpha_p = -10 \log [1 + \epsilon^2] \Rightarrow \alpha_p = 10 \log (1 + \epsilon^2)$$

$$\otimes \quad 0.1 \alpha_p = \log (1 + \epsilon^2).$$

$$(1 + \epsilon^2) = 10^{(0.1 \alpha_p)} \Rightarrow \epsilon^2 = 10 - 1 \Rightarrow \epsilon = \sqrt{\frac{(0.1 \alpha_p)}{10 - 1}}.$$

At (2)  $\omega_c = \omega_s$ ,

$$20 \log |H(j\omega_s)| = -10 \log (1 + \epsilon^2 \left( \frac{\omega_s}{\omega_p} \right)^{2N})$$

$$\omega_s = 10 \log (1 + \epsilon^2 \left( \frac{\omega_s}{\omega_p} \right)^{2N})$$

$$0.1 \omega_s = \log (1 + \epsilon^2 \left( \frac{\omega_s}{\omega_p} \right)^{2N}).$$

$$1 + \epsilon^2 \left( \frac{\omega_s}{\omega_p} \right)^{2N} = 10^{(0.1 \omega_s)} \Rightarrow \epsilon^2 \left( \frac{\omega_s}{\omega_p} \right)^{2N} = 10 - 1.$$

$$2 \quad \omega_c = \frac{10^{(0.1 \omega_s)}}{\left( \frac{\omega_s}{\omega_p} \right)^{2N}} = \frac{10^{(0.1 \alpha_s)}}{10 - 1} = \frac{\epsilon^2}{\epsilon^2 - 1}.$$

$$\omega_c = \frac{\omega_p}{\epsilon^2}.$$

$$N \geq$$

$$\left( \frac{\omega_s}{\omega_p} \right)^{2N} = \frac{10^{(0.1 \omega_s)}}{10 - 1} \Rightarrow \left( \frac{\omega_s}{\omega_p} \right)^N = \sqrt[N]{\frac{10^{(0.1 \omega_s)}}{10 - 1}}.$$

$$\left( \frac{\omega_s}{\omega_p} \right)^N = \frac{10^{(0.1 \omega_s)}}{10 - 1}.$$

$$\left( \frac{\omega_s}{\omega_p} \right)^N = \sqrt[N]{\frac{0.1 \omega_s}{10 - 1}}.$$

$$\omega_c = \frac{\omega_p}{\epsilon^2}.$$

$$\log_{10} \left( \frac{\omega_s}{\omega_p} \right) = \log \sqrt{\frac{10^{(0.1 \omega_s)}}{10 - 1}}$$

$$N \geq \log \sqrt{\frac{10^{(0.1 \omega_s)}}{10 - 1}} = \frac{1}{2} \log \frac{10^{(0.1 \omega_s)}}{10 - 1}$$

$$\log \left( \frac{\omega_s}{\omega_p} \right)$$

$$\omega_c = \frac{\omega_p}{\epsilon^2} = \frac{\omega_s}{\lambda^{1/N}} \quad \omega_c \rightarrow \text{cut off frequency}$$

$$\omega_c = \frac{\omega_p}{\epsilon^2} = \frac{\omega_s}{\lambda^{1/N}}.$$

$$\left| H(j\omega_c) \right|^2 = \frac{1}{1 + \left( \frac{\omega_c}{\omega_p} \right)^{2N}} = \frac{1}{1 + \epsilon^2 \left( \frac{\omega_c}{\omega_p} \right)^{2N}}$$

$$\left( \frac{\omega_c}{\omega_p} \right)^{2N} = \epsilon^2 \left( \frac{\omega_c}{\omega_p} \right)^{2N}$$

$$\left( \frac{\omega_c}{\omega_p} \right)^{2N} = \frac{1}{\epsilon^2}.$$

$$(\omega_c)^{\frac{2N}{2N}} = \frac{(\omega_p)^{\frac{2N}{2N}}}{\epsilon^2} = \frac{(\omega_p)^{\frac{2N}{2N}}}{\epsilon^2}.$$

$$\omega_c = \frac{\omega_p}{\epsilon^2}.$$

$$\omega_c = \frac{\omega_p}{\epsilon^2}.$$

$$(\omega_s)^N = (\omega_p)^{\frac{N}{2}} \cdot \frac{\lambda}{\epsilon^2}.$$

$$(\omega_s)^N = (\omega_c \epsilon^{1/N})^{\frac{N}{2}} \cdot \frac{\lambda}{\epsilon^2} \Rightarrow (\omega_s)^N = (\omega_c)^N \cdot \frac{\lambda}{\epsilon^2}$$

$$\omega_s = \omega_c \lambda^{1/N}$$

$$\omega_c = \frac{\omega_s}{\lambda^{1/N}}$$