

# **BIASING CIRCUITS**

# BIASING CIRCUITS



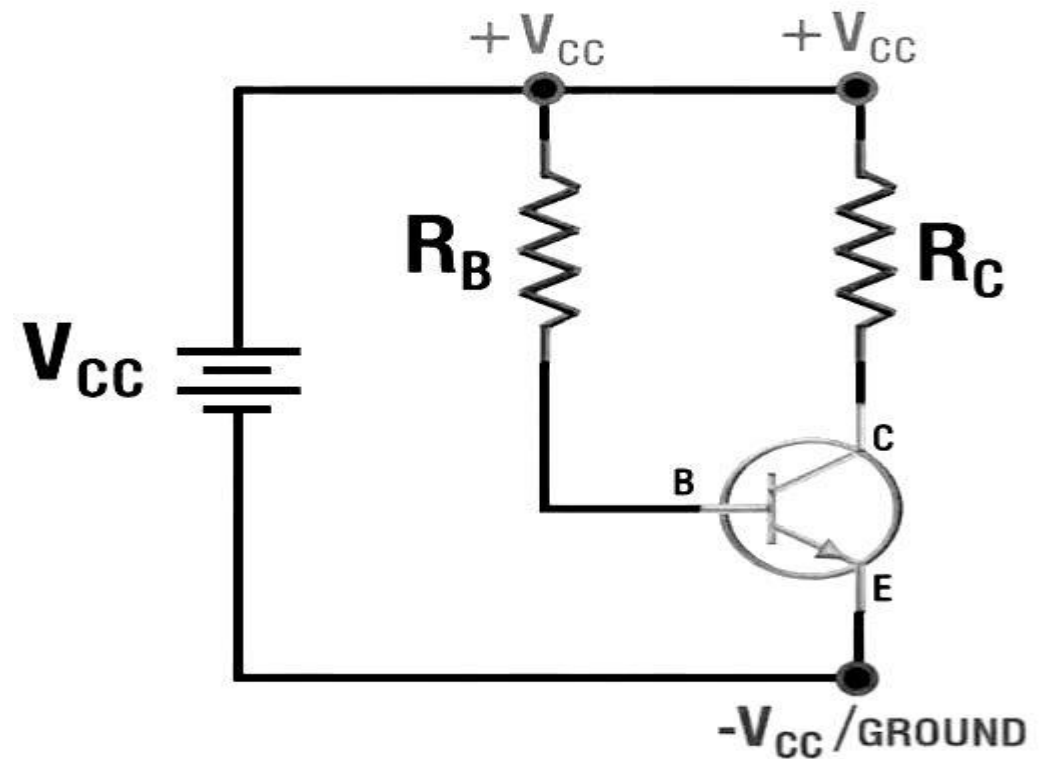
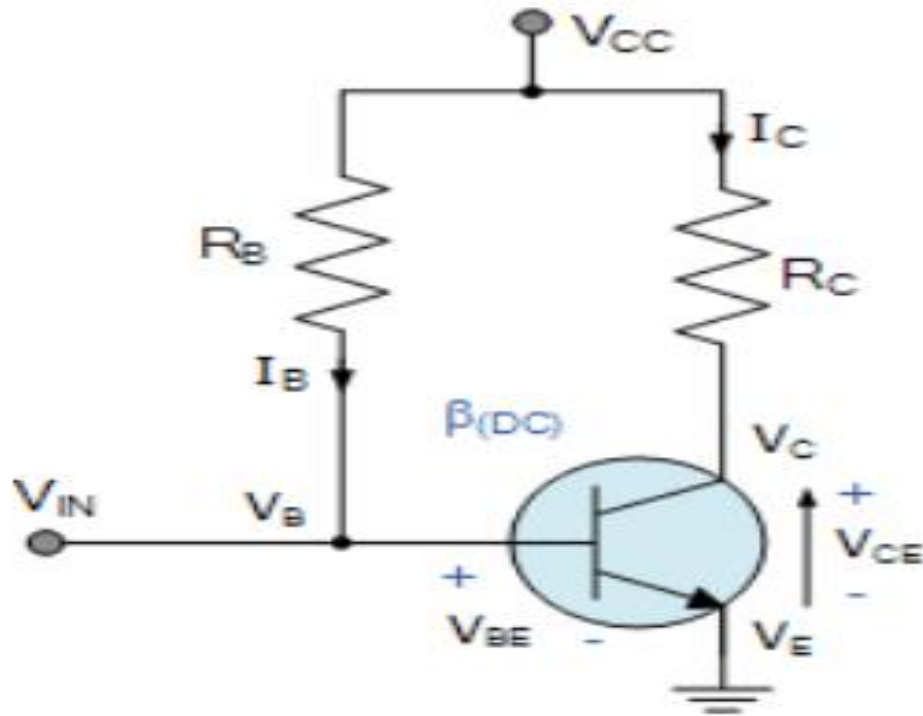
**FIXED BIAS CIRCUIT**

**COLLECTOR TO BASE BIAS CIRCUIT**

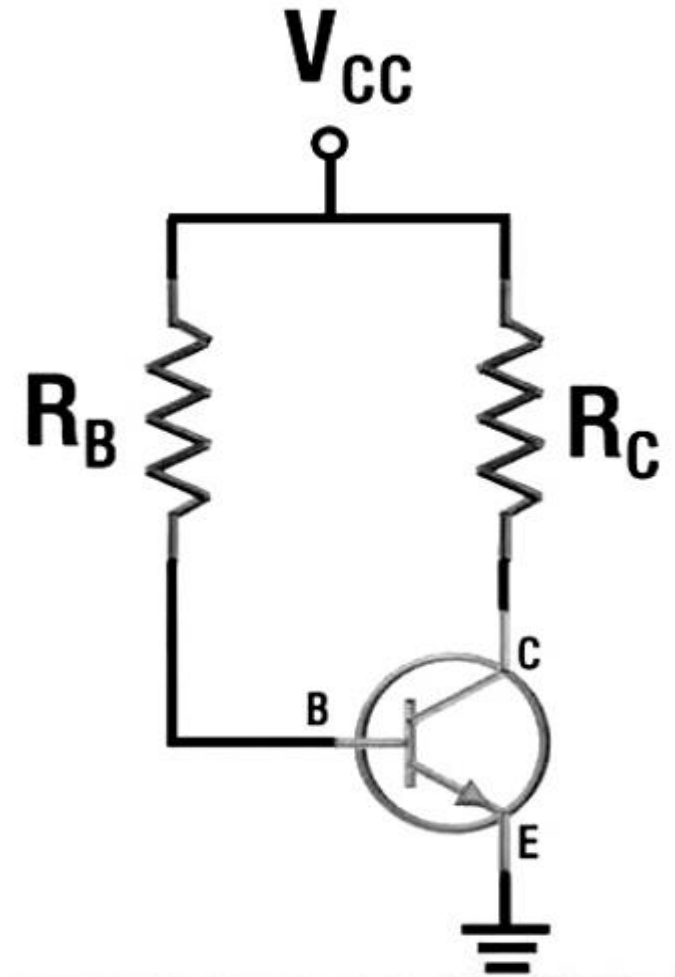
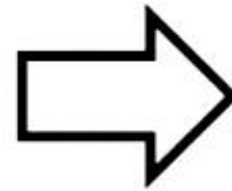
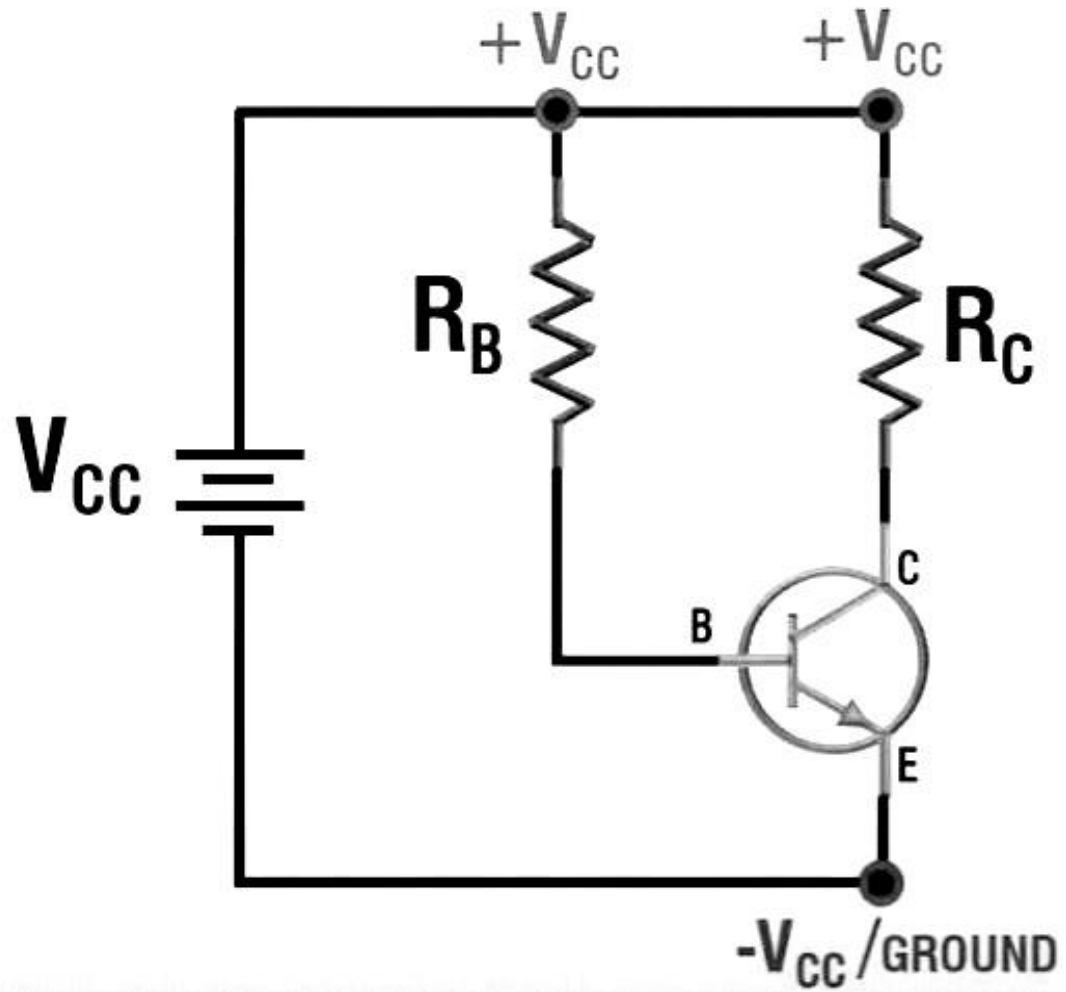
**VOLTAGE DIVIDER BIAS CIRCUIT**

# FIXED BIAS CIRCUIT

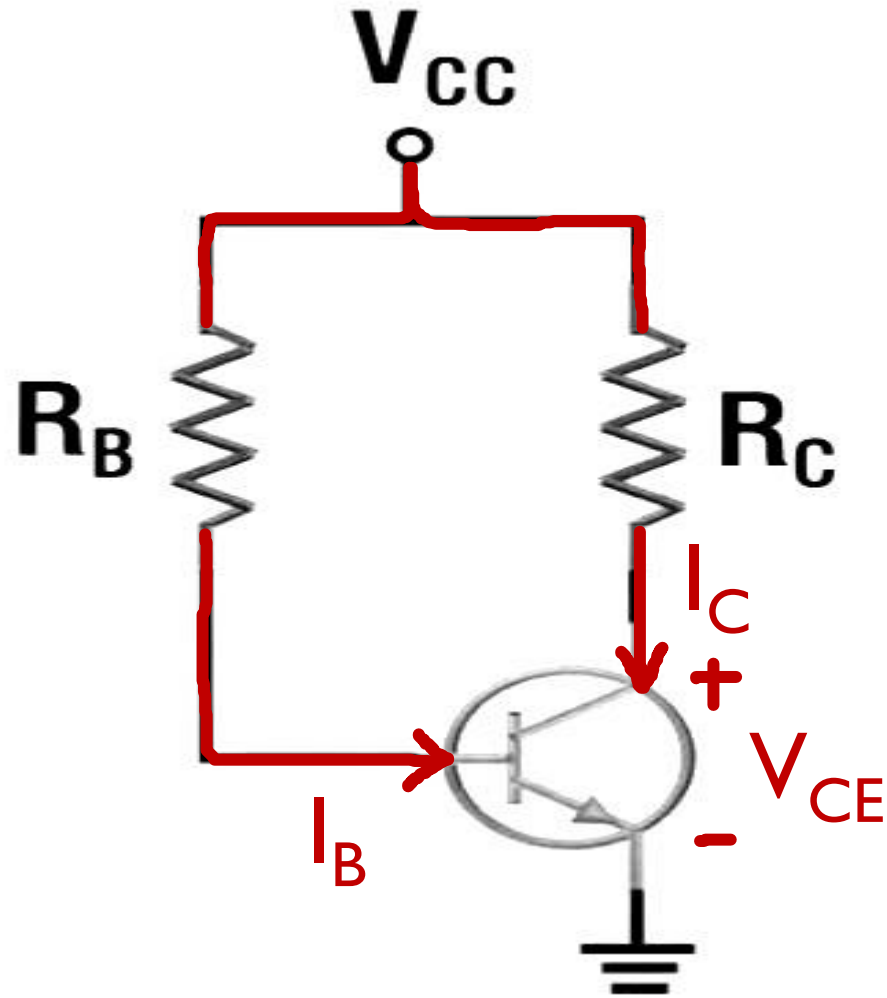
- Simplest DC bias configuration.
- Transistors base current,  $I_B$  remains constant for given values of  $V_{CC}$ , and therefore the transistors operating point must also remain fixed.
- Positive terminal of Battery is connected to Collector and Base Resistor.



# FIXED BIAS CIRCUIT



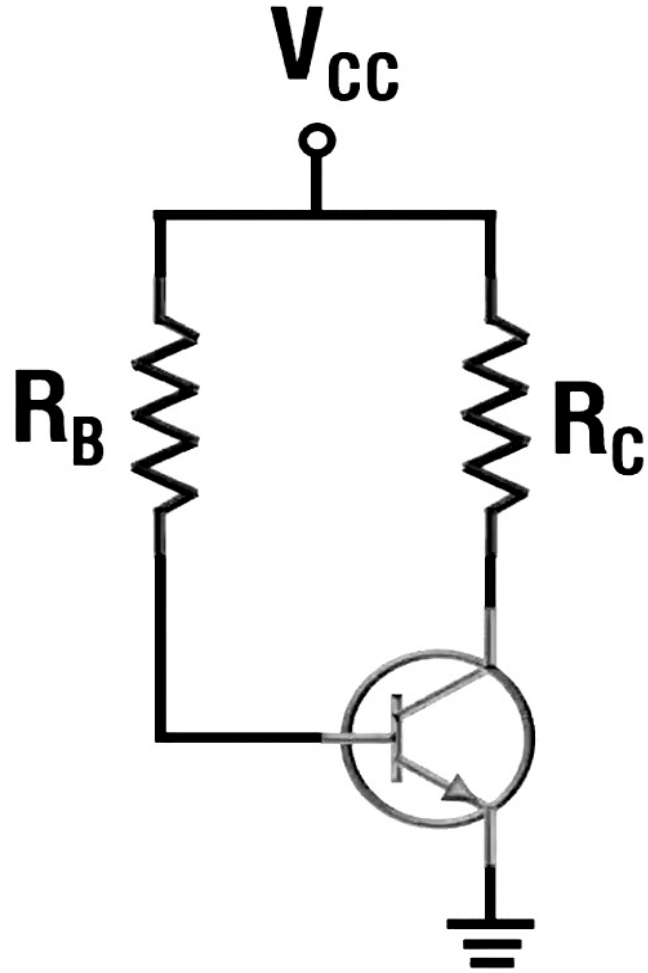
# FIXED BIAS CIRCUIT - ANALYSIS



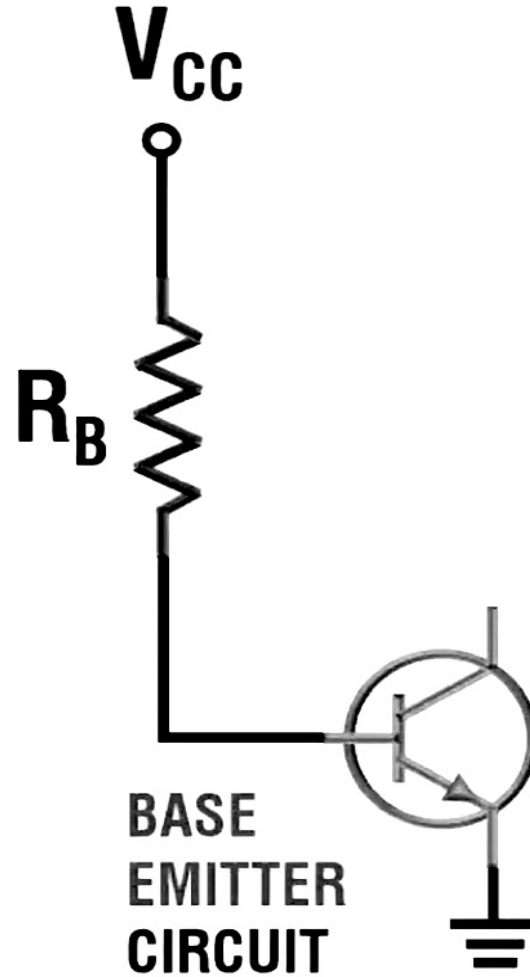
- $I_B$
- $I_C$
- $V_{CE}$

# FIXED BIAS CIRCUIT - ANALYSIS

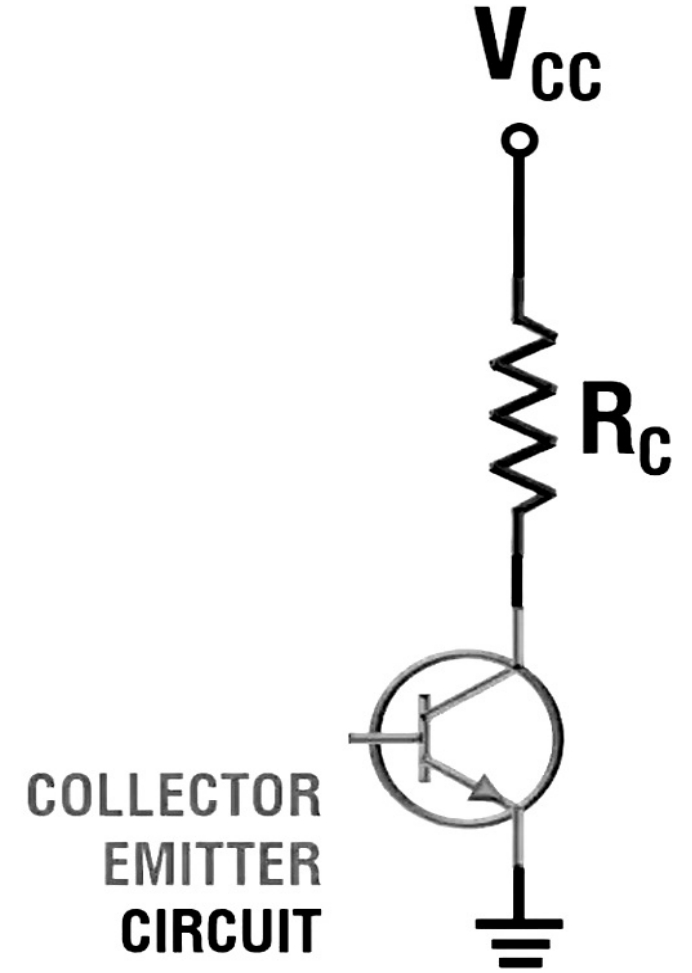
## ANALYSIS



## INPUT CIRCUIT

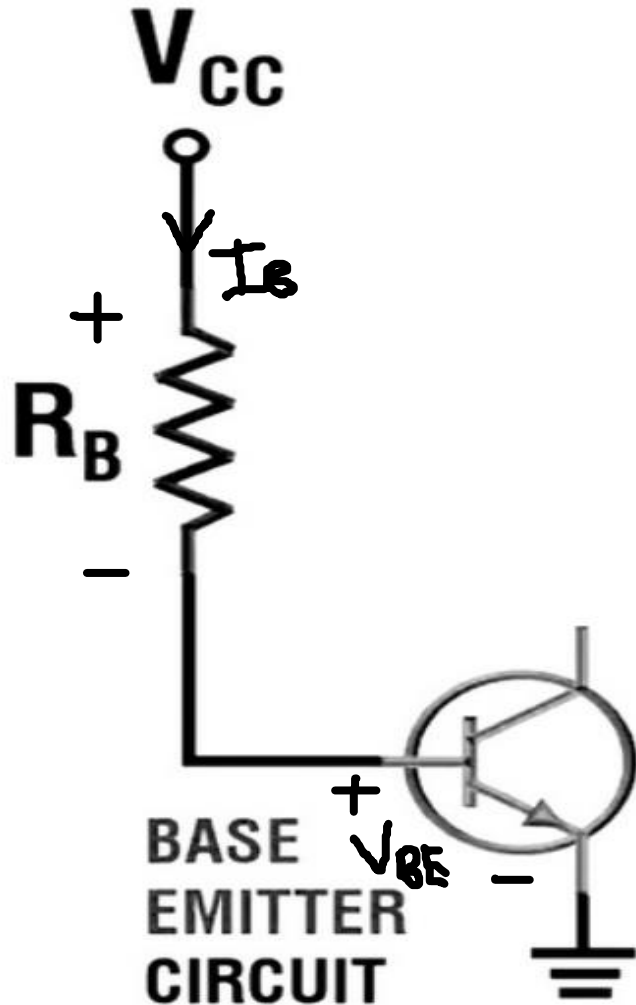


## OUTPUT CIRCUIT



# FIXED BIAS CIRCUIT - ANALYSIS

## INPUT CIRCUIT



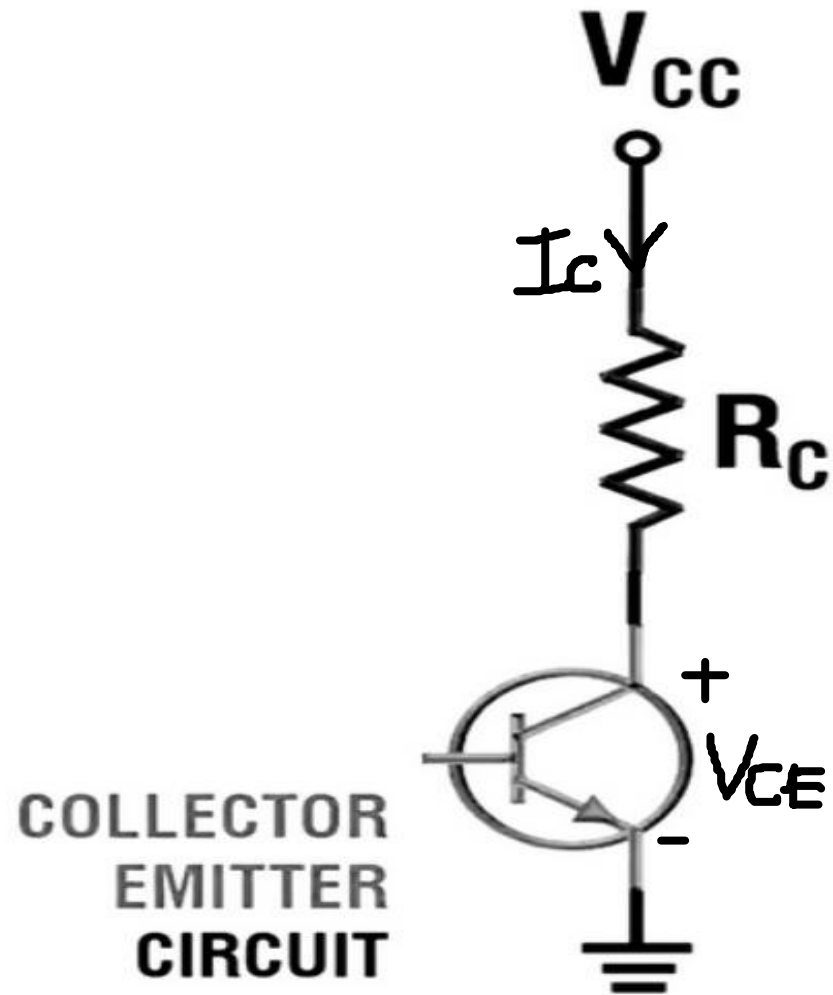
$$V_{CC} - I_B R_B - V_{BE} = 0$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

$$I_B \approx \frac{V_{CC}}{R_B}$$

# FIXED BIAS CIRCUIT - ANALYSIS

## OUTPUT CIRCUIT



$$V_{cc} - I_C R_C - V_{CE} = 0$$

$$V_{CE} = V_{cc} - I_C R_C$$

$$I_C = \beta I_B$$

$$I_C = \frac{V_{cc} - V_{CE}}{R_C}$$

$$I_{C(sat)} = \frac{V_{cc}}{R_C}$$





**Given the fixed bias circuit with  $V_{CC} = 12V$ ,  $R_B = 240\text{ k}\Omega$ ,  $R_C = 2.2\text{ k}\Omega$  and  $\beta = 75$ . Determine the values of operating point.**

Equation for the input loop is:

$$I_B = [V_{CC} - V_{BE}] / R_B \text{ where } V_{BE} = 0.7V$$

$$I_B = [12 - 0.7] / [240 * 10^3]$$

$$I_B = 47.08\mu A$$

$$I_C = \beta I_B = 75 * 47.08\mu A = 3.53\text{mA}$$

$$V_{CE} = V_{CC} - I_C R_C = 12 - ((3.53 * 10^{-3}) * (2.2 * 10^3)) = 4.23V$$

**Determine the Q-point values of  $I_C$  and  $V_{CE}$  for the circuit. Assume  $V_{CE} = 8\text{ V}$ ,  $R_B = 360\text{ k}\Omega$  and  $R_C = 2\text{ k}\Omega$ .  $\beta = 100$**   
**Construct the dc load line and plot the Q-point.**

Equation for the input loop is:

$$I_B = [V_{CC} - V_{BE}] / R_B \text{ where } V_{BE} = 0.7\text{V}$$

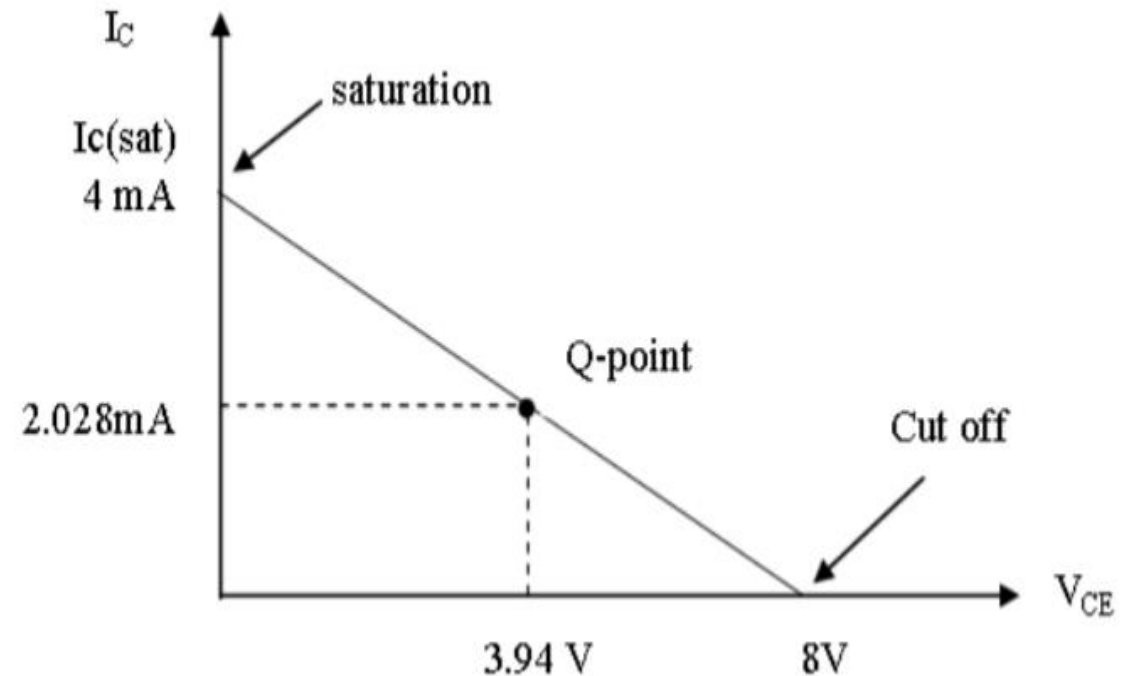
$$I_B = [8\text{V} - 0.7\text{V}] / [360 * 10^3] = 20.28\mu\text{A}$$

$$I_C = \beta I_B = 100 * 20.28\mu\text{A} = 2.028\text{mA}$$

$$V_{CE} = V_{CC} - I_C R_C = 8\text{V} - (2.028\text{mA} * (2 * 10^3)) = 3.94\text{V}$$

$$V_{CE(\text{sat})} = 0 ; I_C = \frac{V_{CC} - V_{CE}}{R_C} = \frac{V_{CC} - 0}{R_C} ; I_{C(\text{sat})} = \frac{V_{CC}}{R_C} = \frac{8\text{V}}{2\text{ k}\Omega} = 4\text{mA}$$

$$I_{C(\text{cutoff})} = 0 ; V_{CE(\text{cutoff})} = V_{CC} = 8\text{V}$$



# FIXED BIAS CIRCUIT

## ADVANTAGES

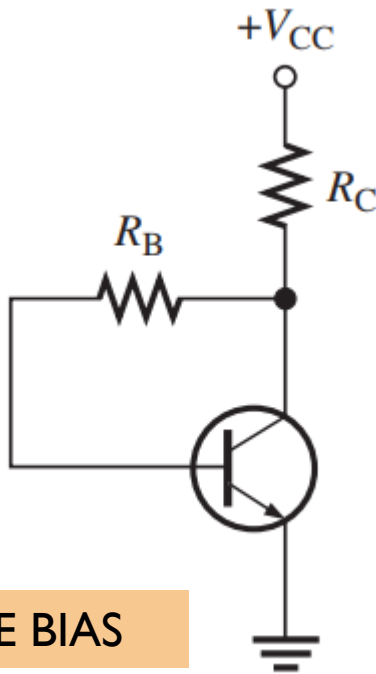
- Simple circuit, uses very few components.
- The operating point can be selected anywhere in the active region, by simply changing the value of  $R_B$ . Thus it provides maximum flexibility in the design.

## DISADVANTAGES

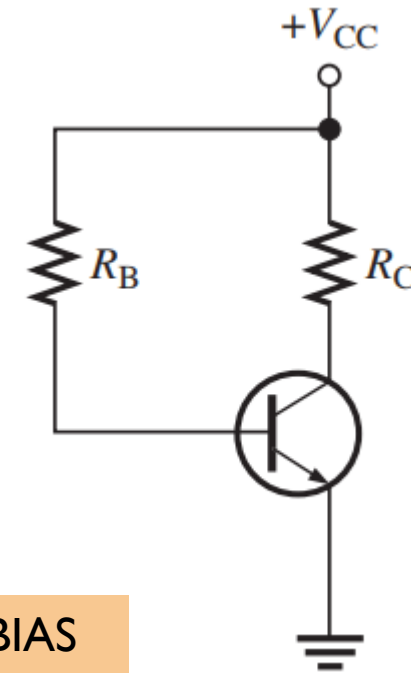
- Thermal stability is not provided in the circuit. Thus Q-point is not maintained.
- Since  $I_B$  is already fixed,  $I_C$  depends on  $\beta$  which changes unit to unit and shifts the Q-point. Thus stability is very poor.

# COLLECTOR TO BASE BIAS CIRCUIT

- Also called Collector-feedback bias.
- The base resistor,  $R_B$ , is connected to the collector rather than to  $V_{CC}$ , as in the base bias arrangement.
- Collector gives a negative feedback to achieve stability.

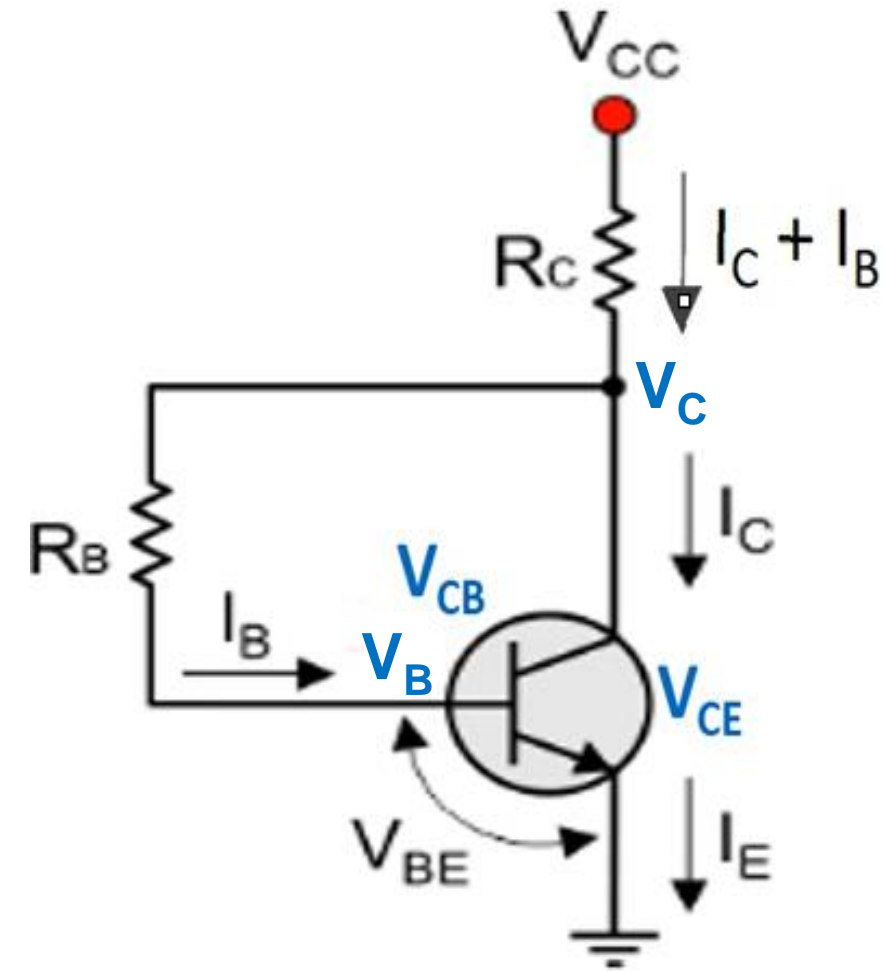


COLLECTOR TO BASE BIAS



FIXED BIAS

# COLLECTOR TO BASE BIAS CIRCUIT



- Improved version of Fixed Bias Circuit.
- The negative feedback creates a compensating effect that tends to keep the Q-point stable.
- Assume a temperature Increase, it will increase  $I_C$ , which cause more voltage drop across  $R_C$ .
- With more voltage drop across  $R_C$ ,  $V_C$  will decrease
- The decrease in  $V_C$  causes,  $V_{CB}$  to decrease, which reduces  $I_B$ .
- As  $I_B$  is decreased  $I_C$  will decrease
- Thus, the original increase in temperature is compensated by a smaller bias current by negative feedback

# COLLECTOR TO BASE BIAS CIRCUIT

## INPUT ANALYSIS

$$V_{CC} - (I_C + I_B)R_C - I_B R_B - V_{BE} = 0$$

$$V_{CC} = I_C R_C + I_B (R_B + R_C) + V_{BE}$$

$$I_C = \beta I_B$$

$$V_{CC} = \beta R_C I_B + I_B (R_B + R_C) + V_{BE}$$

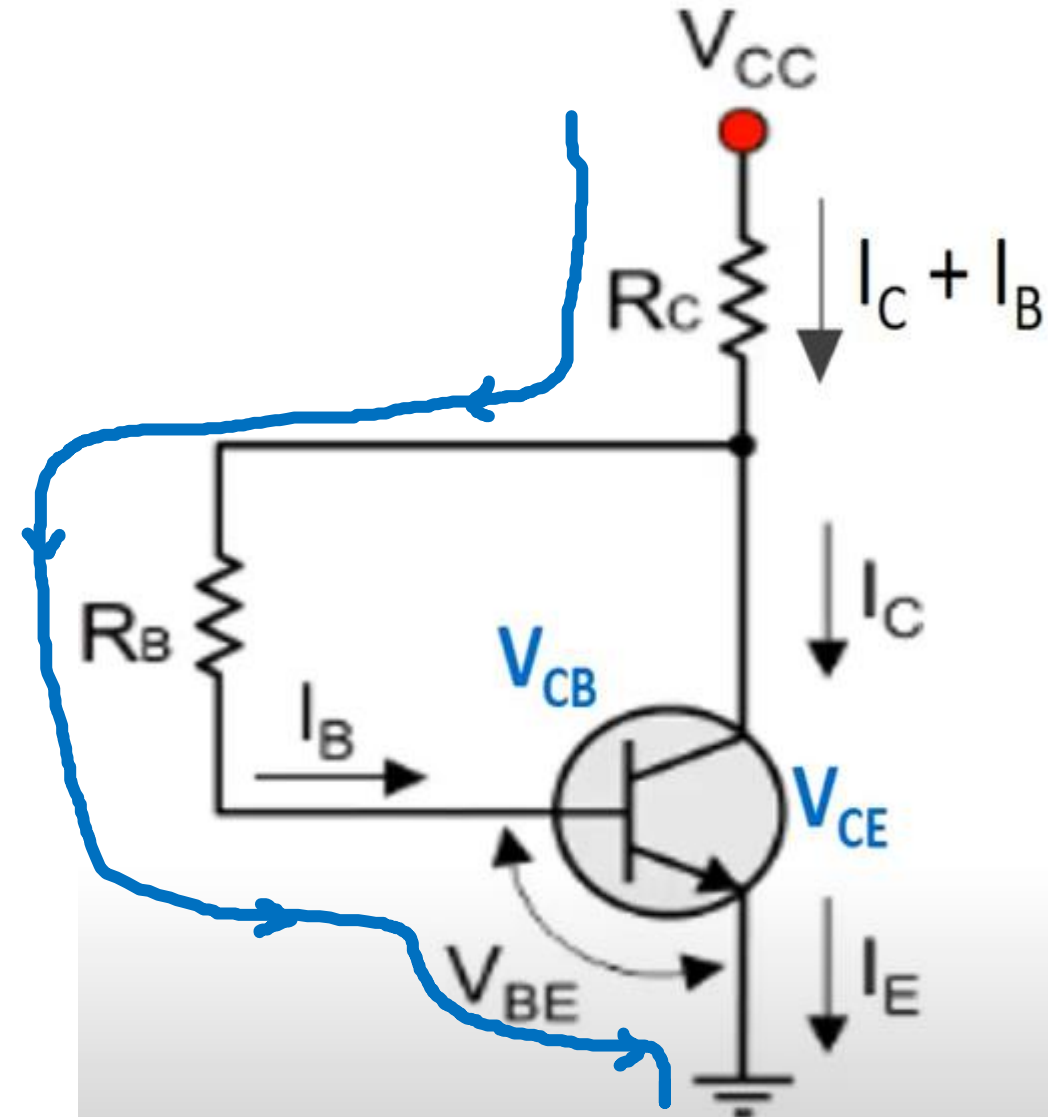
$$V_{CC} = (\beta R_C + R_C + R_B) I_B + V_{BE}$$

$$V_{CC} = ((\beta + 1)R_C + R_B) I_B + V_{BE}$$

$$I_B = \frac{V_{CC} - V_{BE}}{(\beta + 1)R_C + R_B}$$

When  $V_{BE} \approx 0$

$$I_B \approx \frac{V_{CC}}{(\beta + 1)R_C + R_B}$$



# COLLECTOR TO BASE BIAS CIRCUIT

## INPUT ANALYSIS

$$V_{CE} = V_{CB} - V_{BE}$$

$$I_B = V_{CB} / R_B$$

When temperature  $\uparrow$

$$I_C \uparrow$$

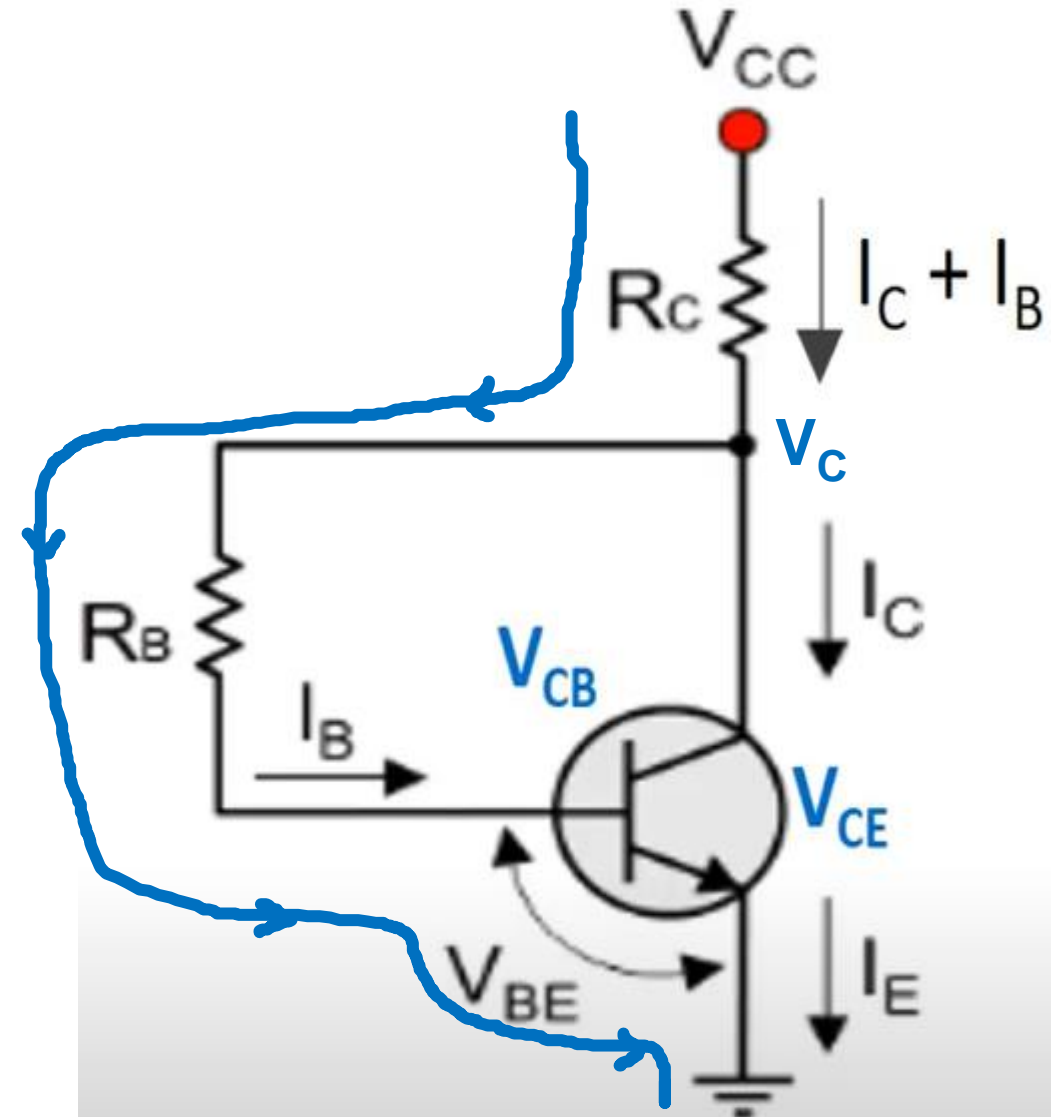
voltage drop across  $R_C \uparrow$

$$V_C \downarrow$$

$$V_{CB} \downarrow$$

$$I_B \downarrow$$

$$I_C \downarrow$$



# COLLECTOR TO BASE BIAS CIRCUIT

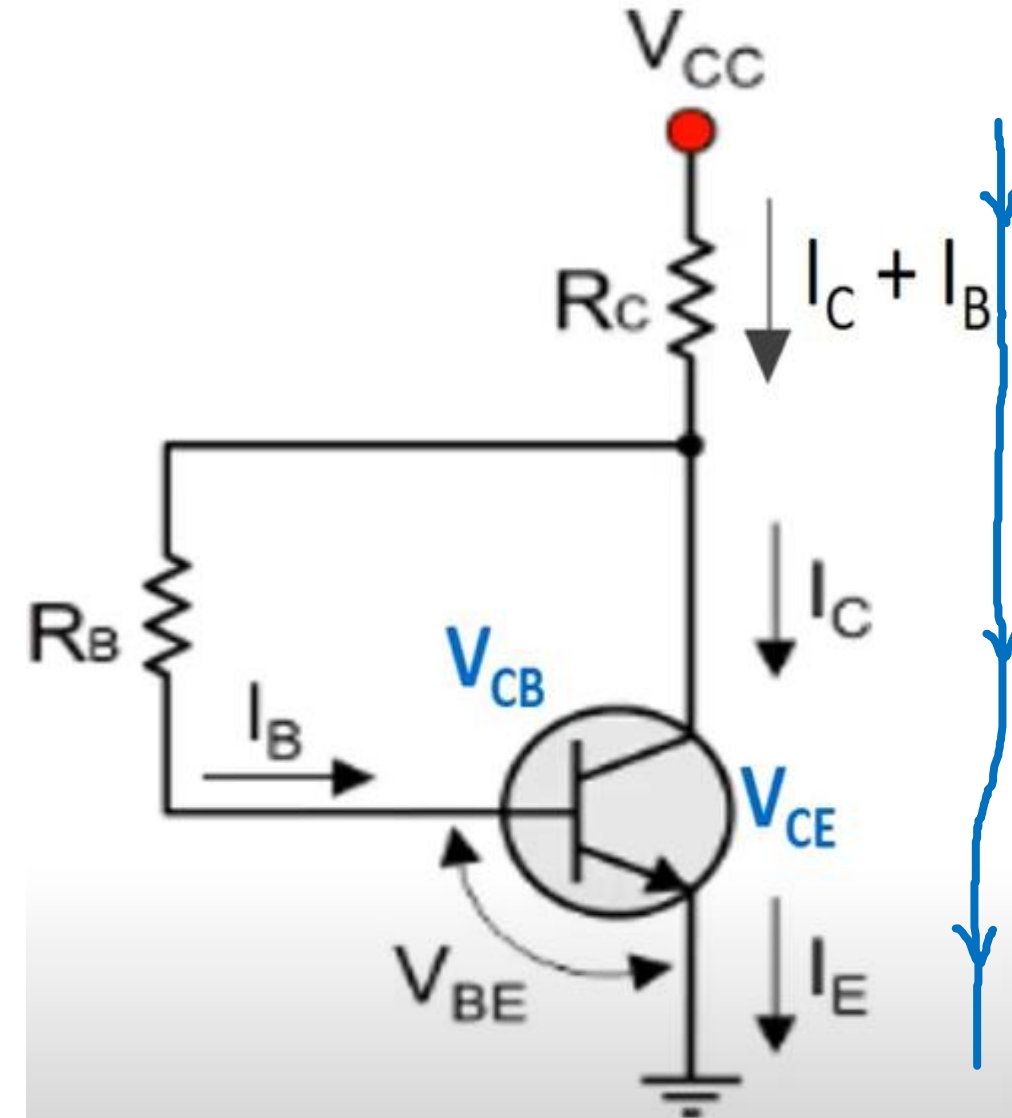
## OUTPUT ANALYSIS

$$V_{CC} - (I_C + I_B)R_C - V_{CE} = 0$$

$$V_{CE} = V_{CC} - (I_C + I_B)R_C$$

If  $I_C \gg I_B$ ,

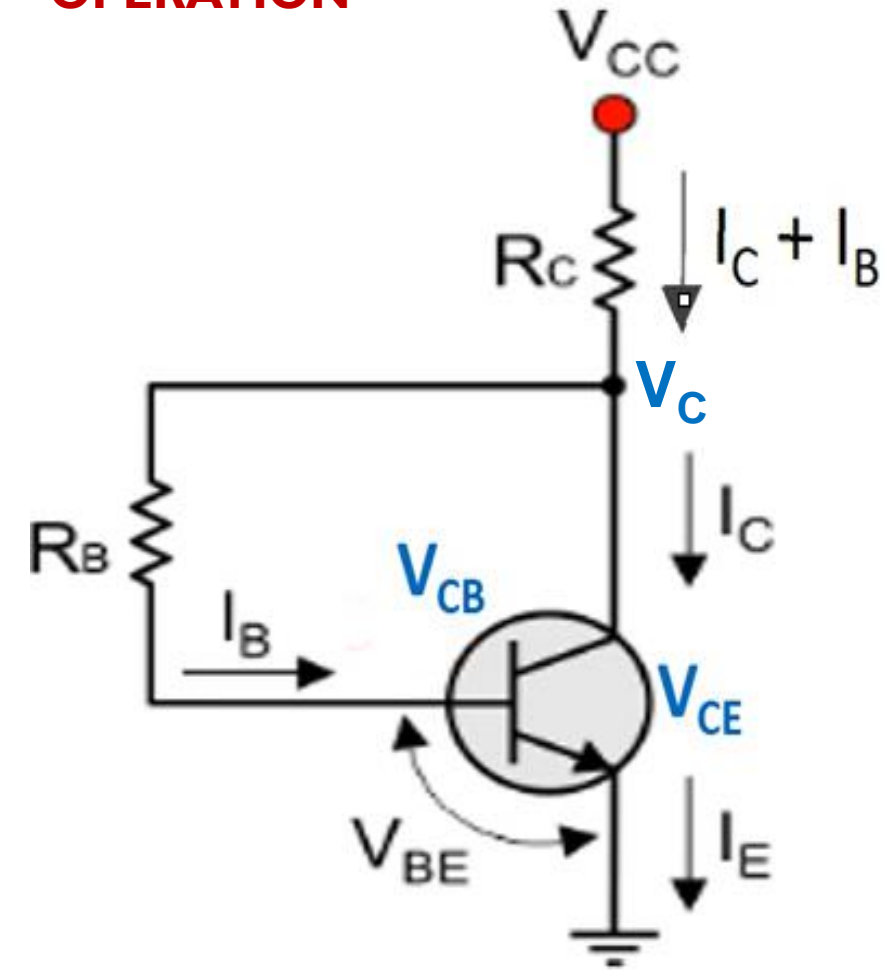
$$V_{CE} \approx V_{CC} - I_C R_C$$





# COLLECTOR TO BASE BIAS CIRCUIT

## OPERATION



- If there is change in  $\beta$  due to transistor replacement or change in  $I_{CEO}$  increase due to change in increase in temperature then  $I_C$  increases
- $I_C = \beta I_B + I_{CEO}$
- Since,  $V_{CE} = V_{CC} - (I_C + I_B)R_C$  then if  $I_C$  increases,  $V_{CE}$  decreases
- Since,  $V_{CB} = V_{CE} + V_{BE}$
- With decrease in  $V_{CE}$ ,  $V_{CB}$  decreases
- $I_B = V_{CB} / R_B$  base current  $I_B$ , decreases
- Thus, the with the decrease in base current the circuit tends to maintain stable value collector current, keeping Q point fixed.

# COLLECTOR TO BASE BIAS CIRCUIT

## ADVANTAGES

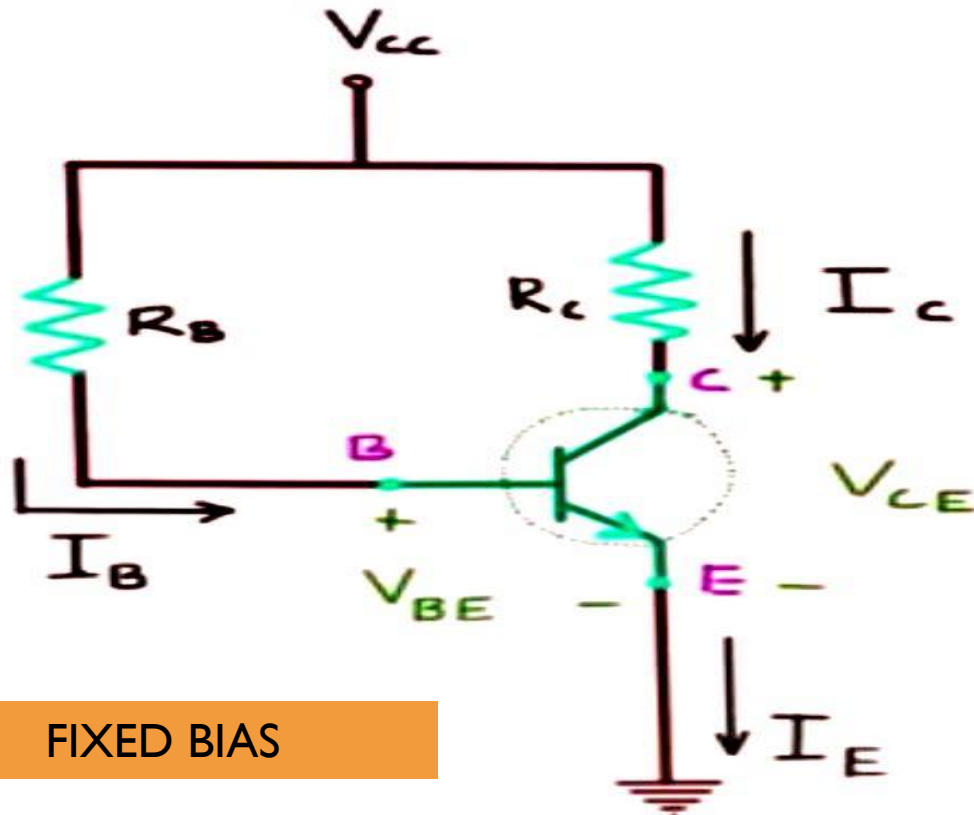
- Simple circuit, as it uses very few components.
- Better stabilization than fixed bias circuit.

## DISADVANTAGES

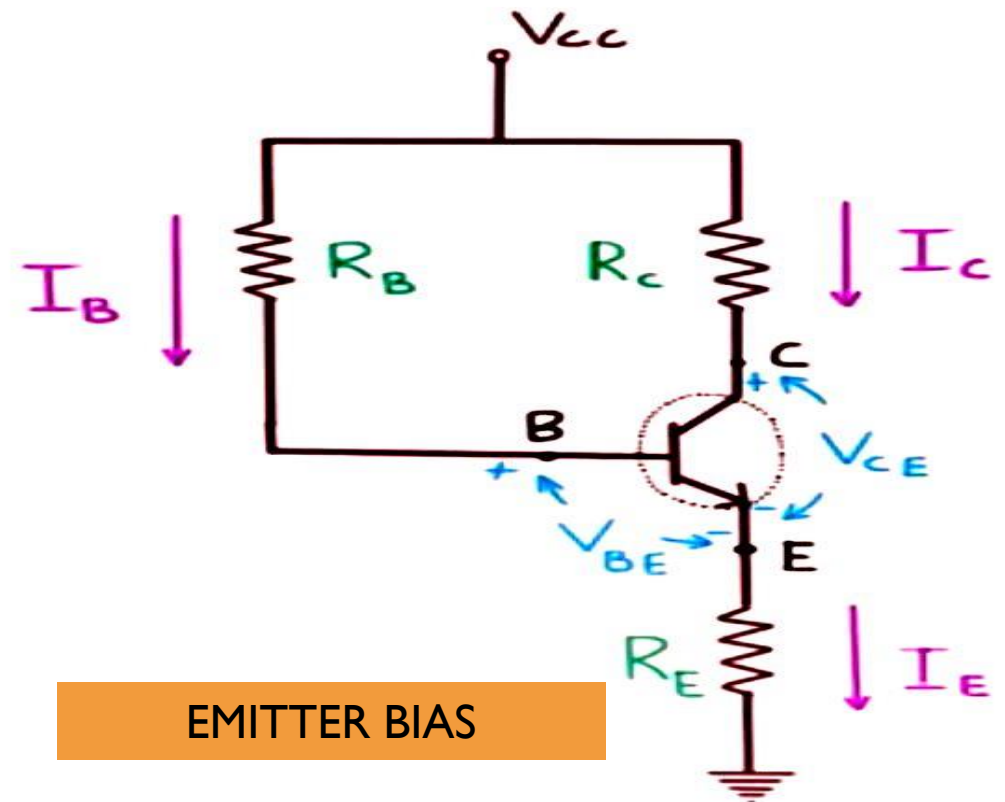
- Poor stability, as Stability factor ( $S$ ) is high.
- Since it provides negative feedback through  $R_B$ , the gain of the amplifier is reduced.

# EMITTER BIAS CIRCUIT

- Modification of Fixed Bias or Collector to Base bias circuit by adding a Emitter Resistor  $R_E$
- Emitter Resistance provide more stability.



FIXED BIAS



EMITTER BIAS

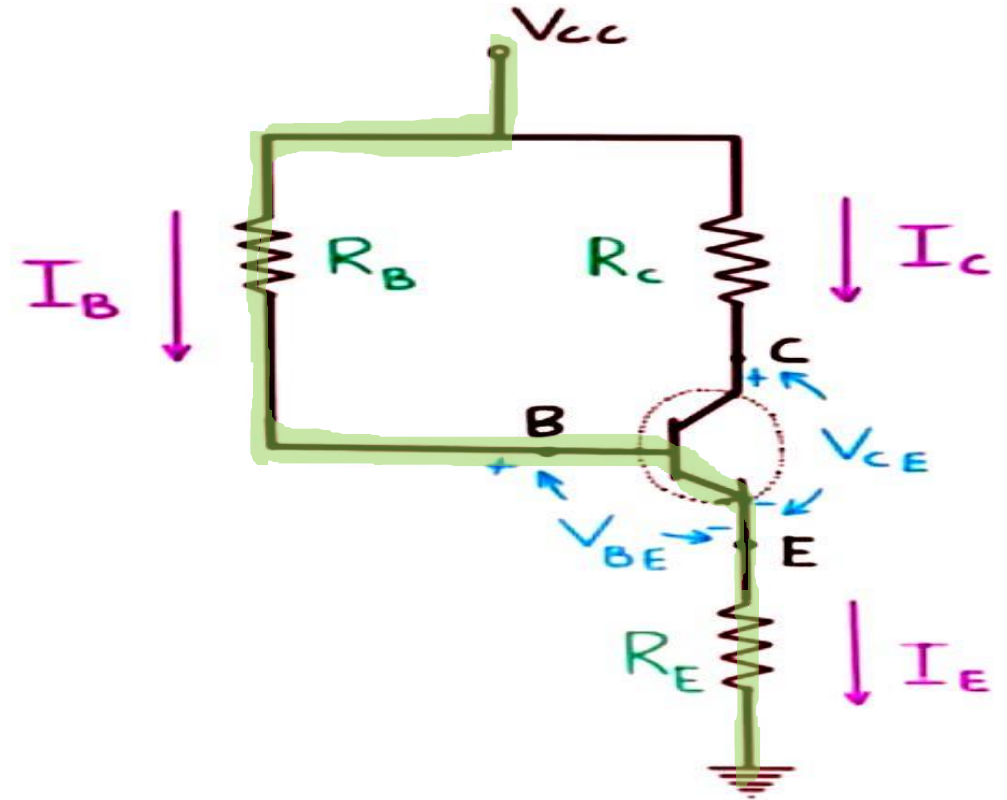
# EMITTER BIAS CIRCUIT

## INPUT ANALYSIS

$$V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0$$

$$V_{CC} = I_B R_B + V_{BE} + I_E R_E$$

$$I_B = \frac{V_{CC} - V_{BE} - I_E R_E}{R_B}$$



# EMITTER BIAS CIRCUIT

## OUTPUT ANALYSIS

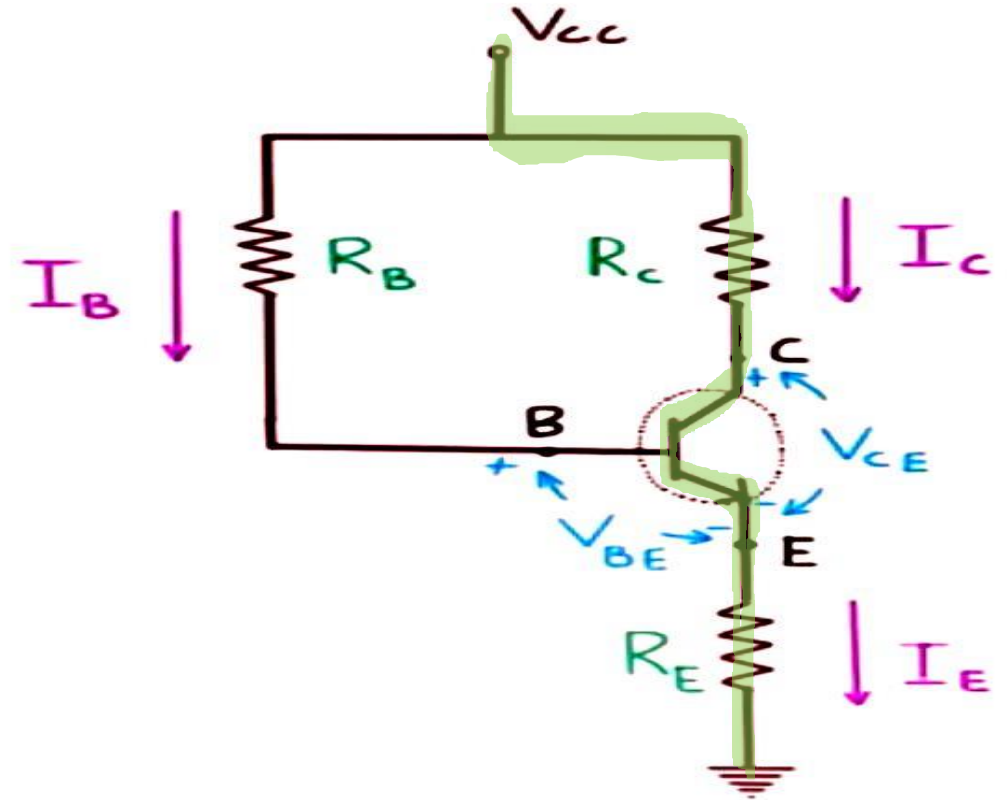
$$V_{CC} - I_C R_C - V_{CE} - I_E R_E = 0$$

$$V_{CE} = V_{CC} - I_C R_C - I_E R_E$$

$$I_B = \frac{V_{CC} - V_{BE} - I_E R_E}{R_B}$$

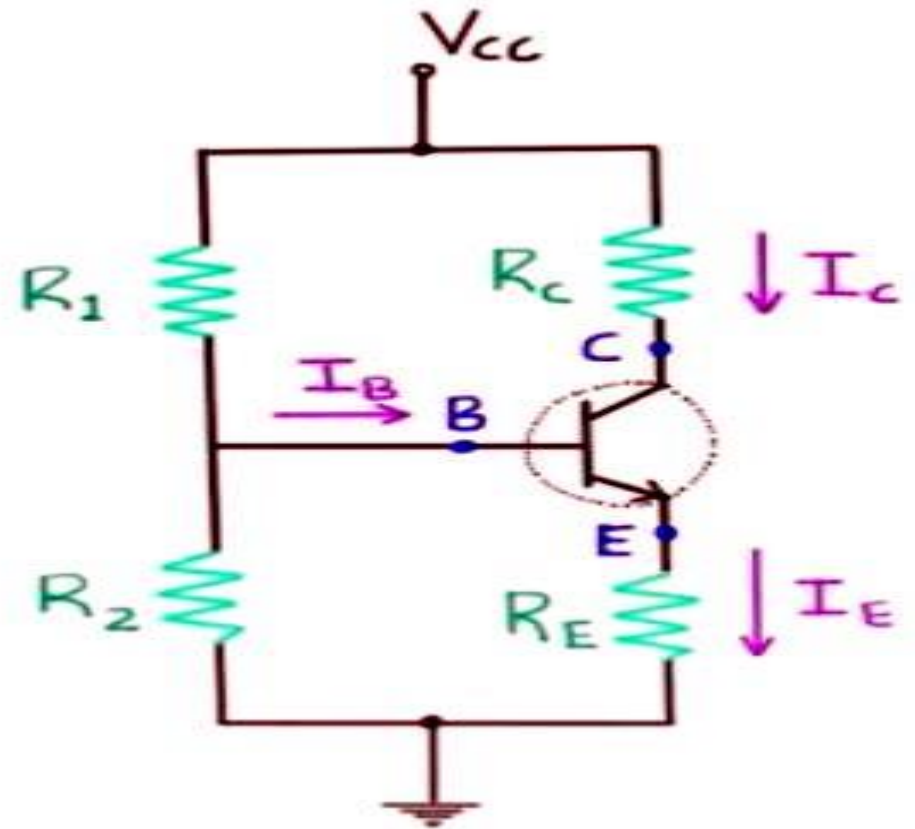
$$I_C = \beta I_B$$

$$I_C = \beta \frac{(V_{CC} - V_{BE} - I_E R_E)}{R_B}$$

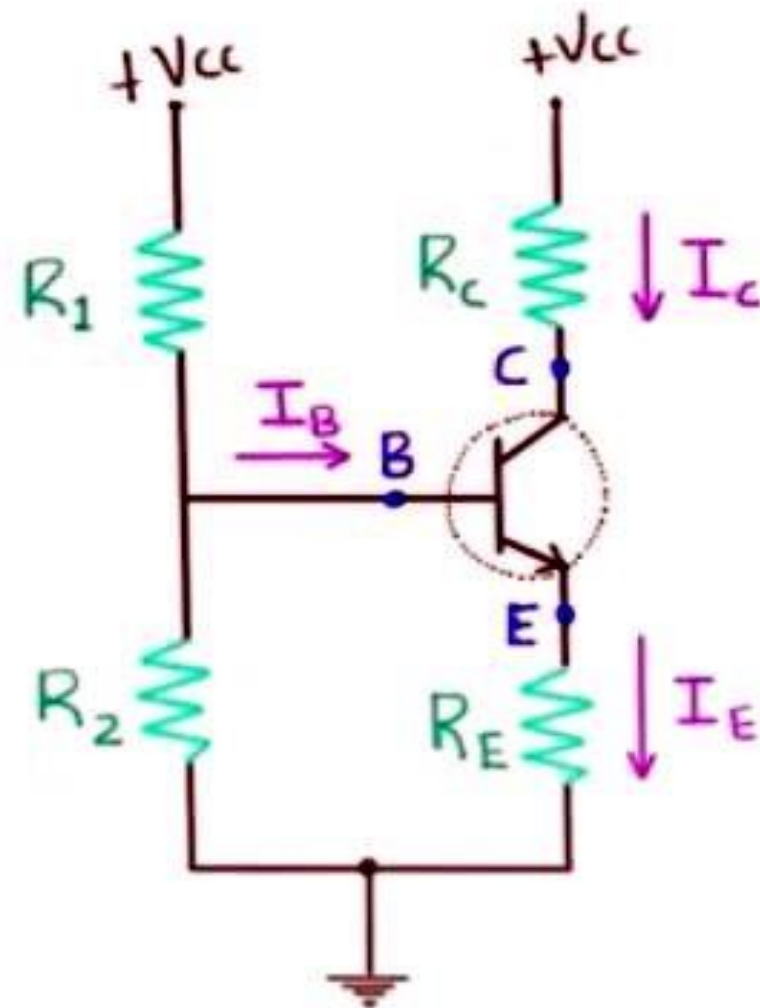
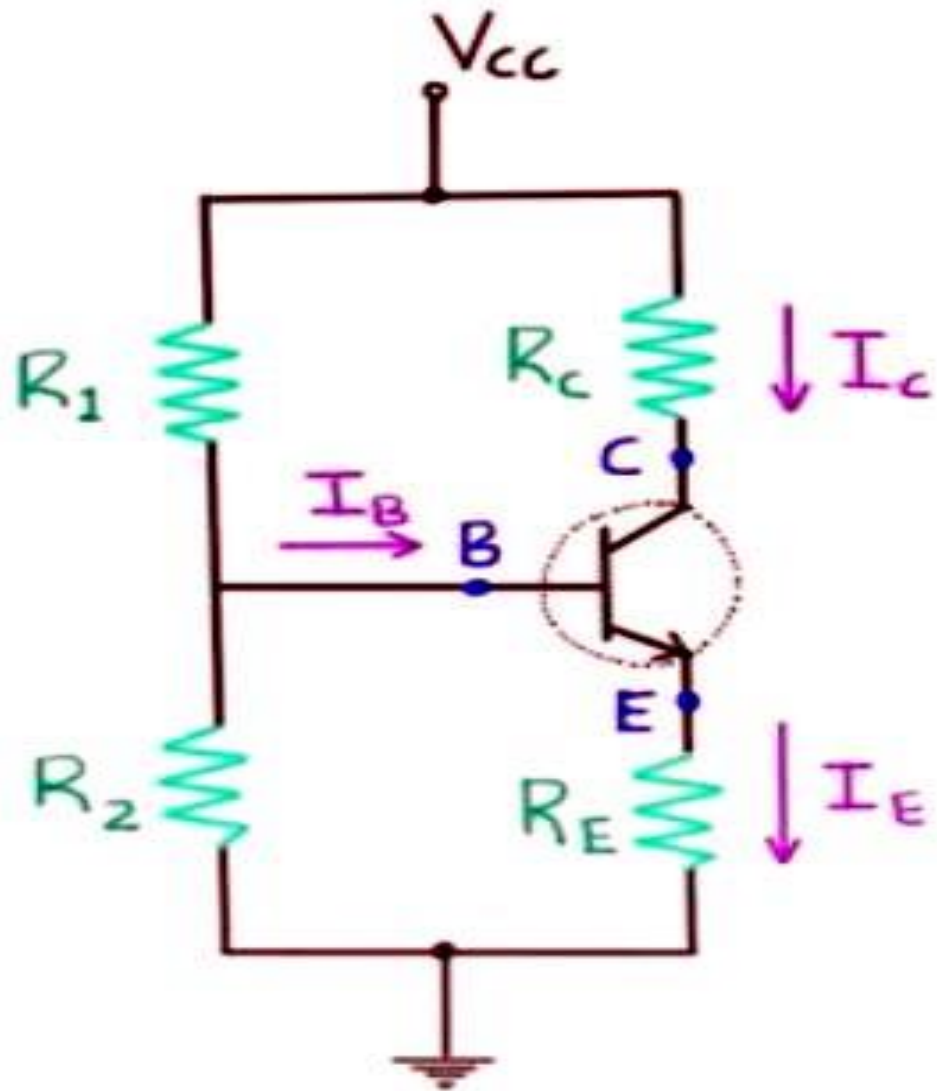


# VOLTAGE DIVIDER BIAS CIRCUIT

- Voltage Divider Bias Circuit is the most stable circuit of the basic transistor bias circuits.
- Two resistors  $R_1$  and  $R_2$  are connected to  $V_{CC}$  to provide biasing.
- Resistors  $R_1$  and  $R_2$  constitute a voltage divider that divides the supply voltage to produce the base bias voltage ( $V_B$ ).
- Collector resistor ( $R_C$ ) and an emitter resistor ( $R_E$ ) connected in series with the transistor.
- The emitter resistance  $R_E$  provides Stabilization.
- Voltage drop across  $R_2$ , make Base emitter junction Forward biased, and the base current produced make collector current to flow in the zero signal conditions.

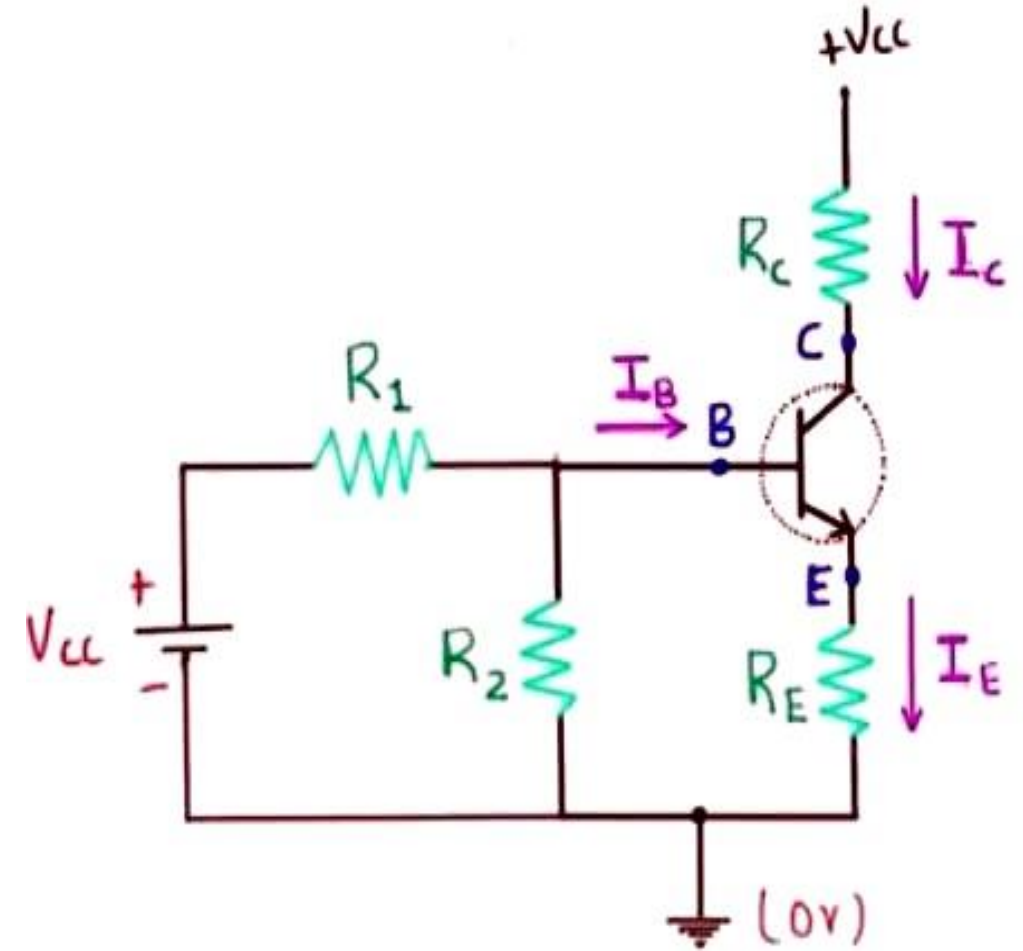
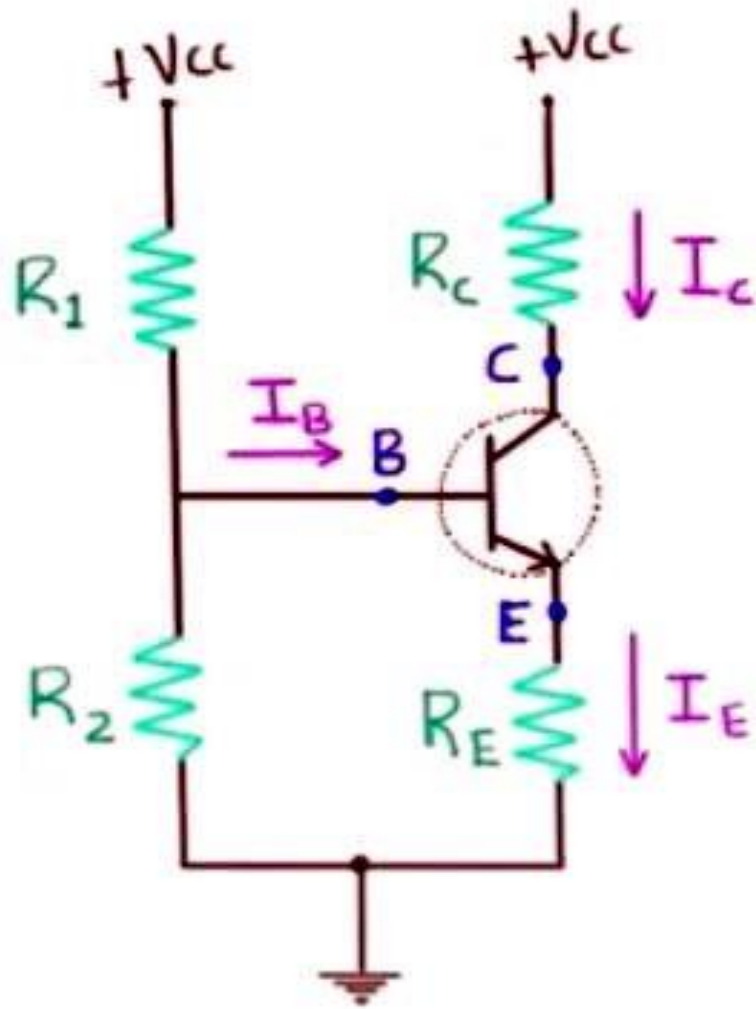


# VOLTAGE DIVIDER BIAS CIRCUIT



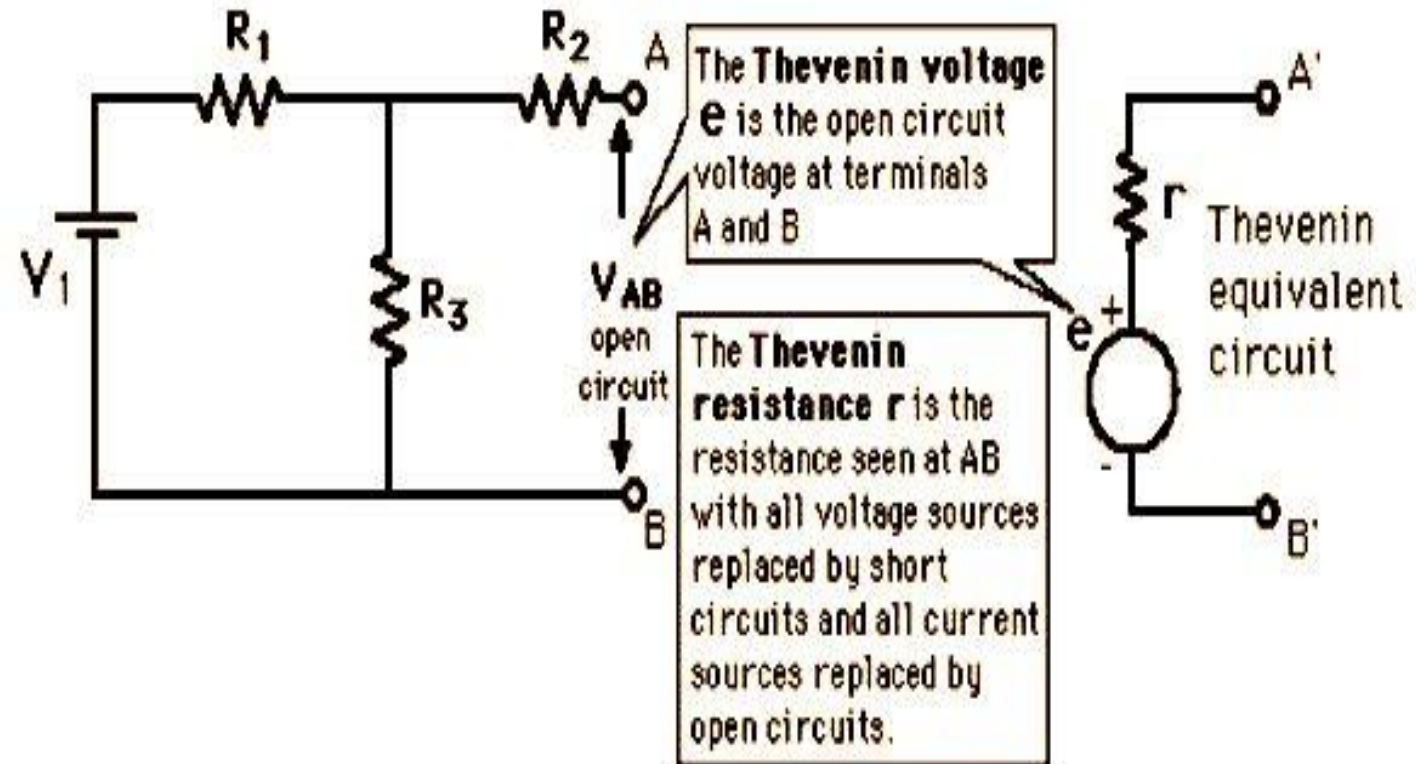
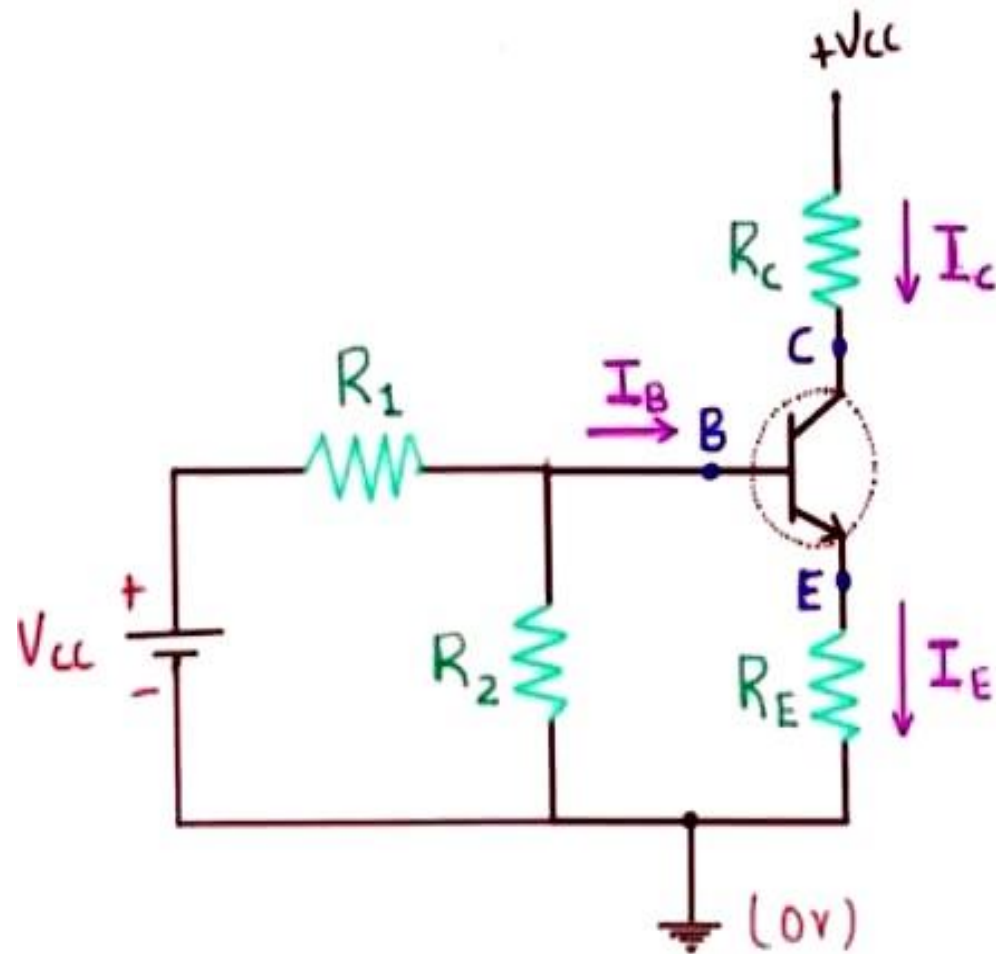


# VOLTAGE DIVIDER BIAS CIRCUIT

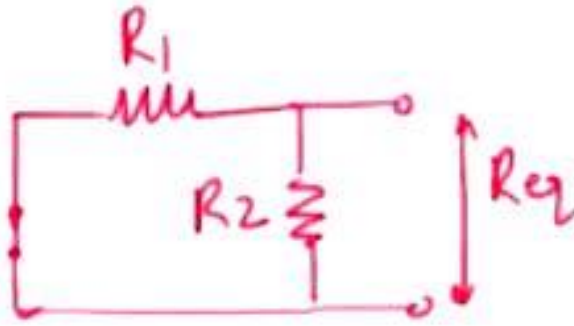
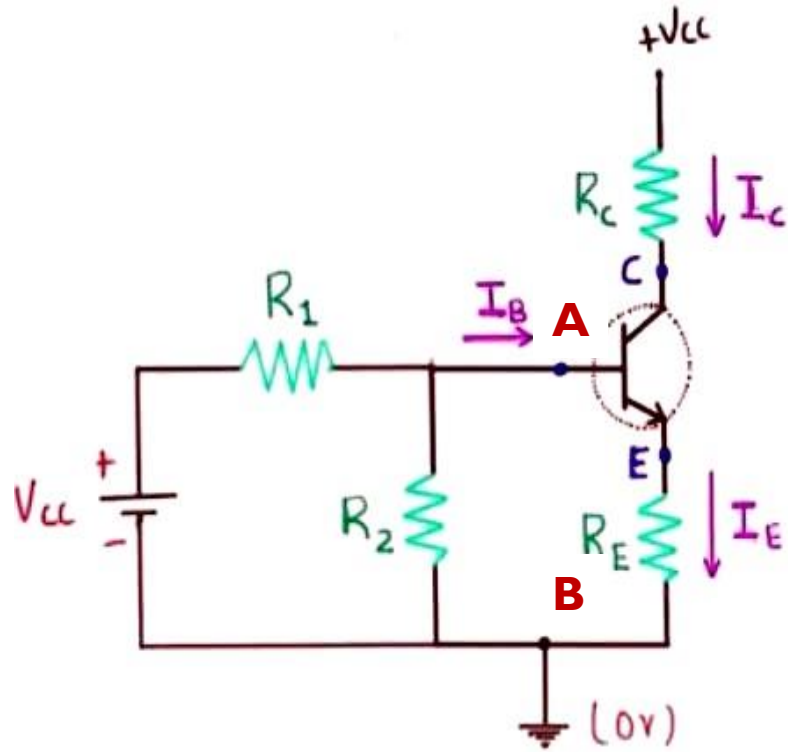




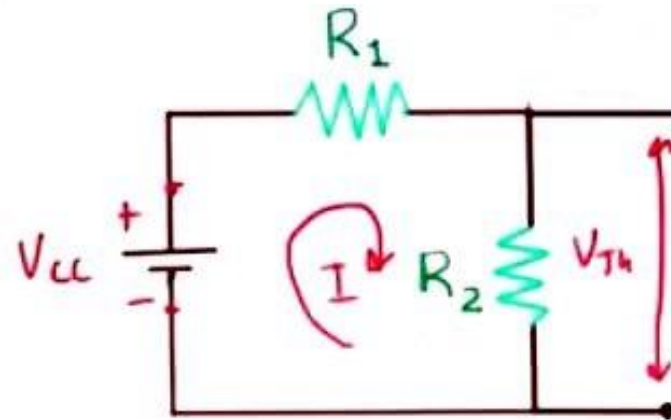
# VOLTAGE DIVIDER BIAS CIRCUIT



# VOLTAGE DIVIDER BIAS CIRCUIT



$$R_{eq} = R_{TH} = \frac{R_1 R_2}{R_1 + R_2}$$

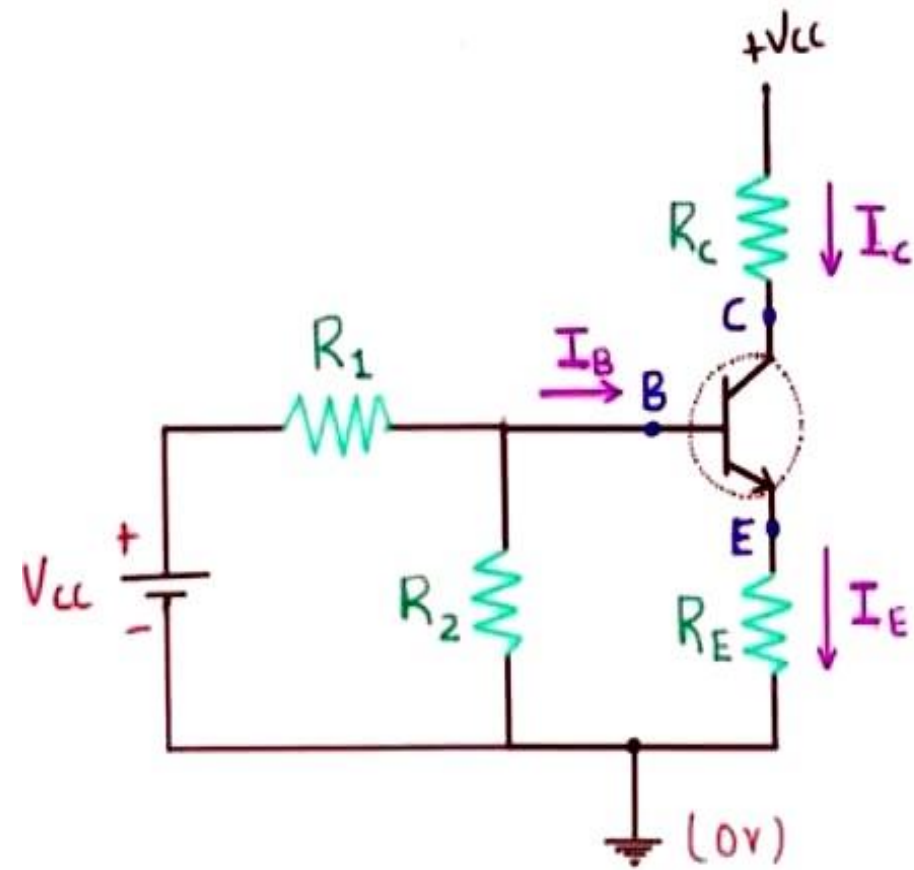


$$I = \frac{V_{CC}}{R_1 + R_2}$$

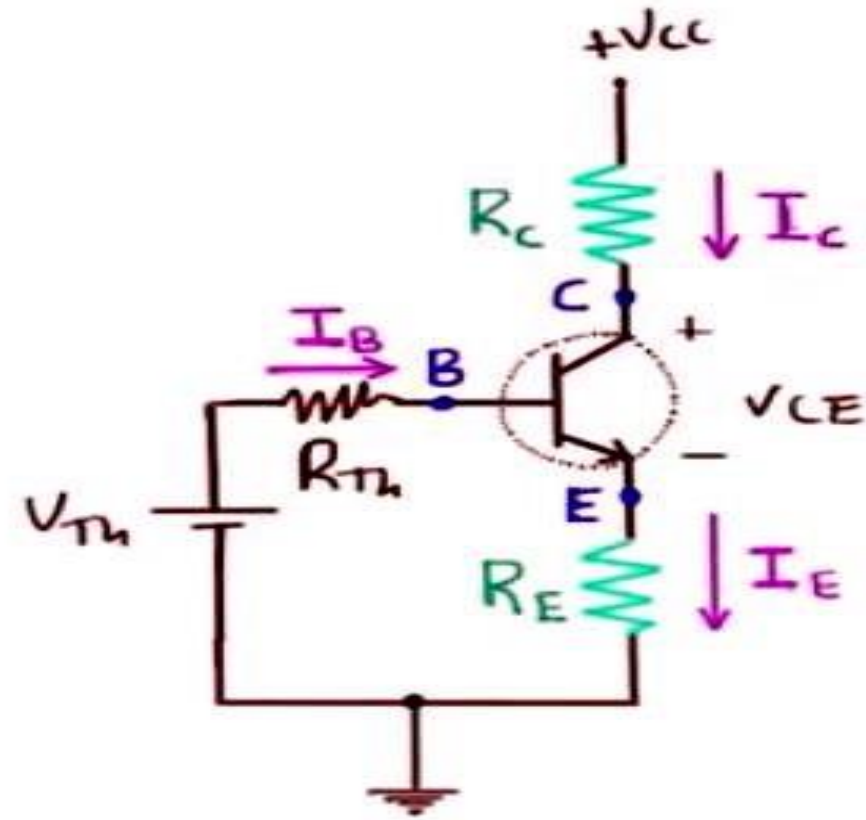
$$V_{TH} = R_2 \times I$$

$$V_{TH} = \frac{V_{CC} R_2}{R_1 + R_2}$$

# VOLTAGE DIVIDER BIAS CIRCUIT



$$R_{TH} = \frac{R_1 R_2}{R_1 + R_2}$$

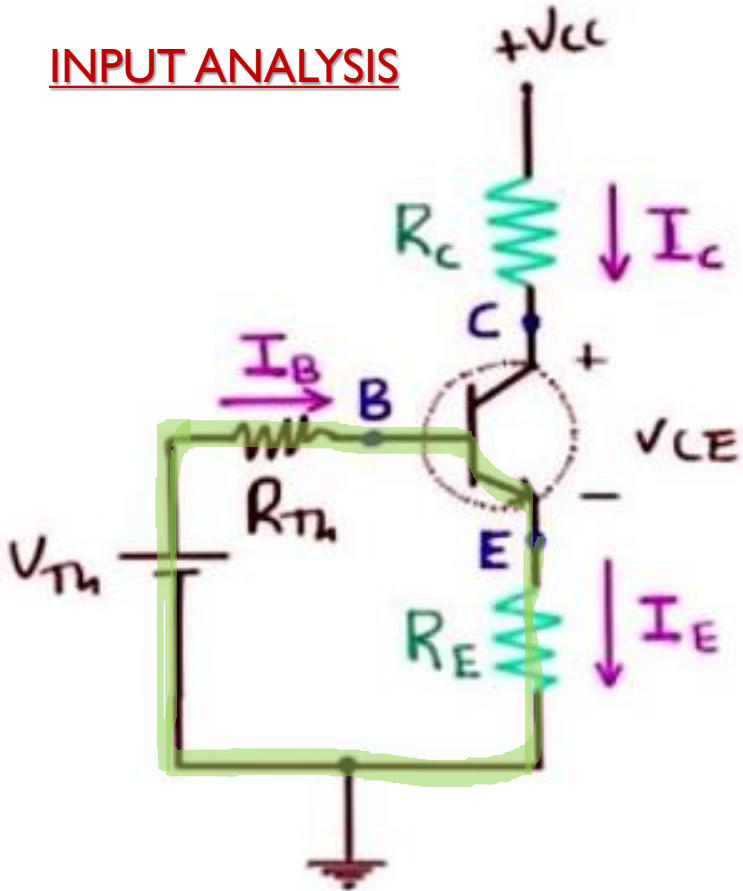


$$V_{TH} = \frac{V_{CC} R_2}{R_1 + R_2}$$



# VOLTAGE DIVIDER BIAS CIRCUIT - ANALYSIS

## INPUT ANALYSIS



$$V_{TH} - I_B R_{TH} - V_{BE} - I_E R_E = 0$$

$$V_{TH} = I_B R_{TH} + V_{BE} + I_E R_E$$

$$I_E = I_C + I_B; I_C = \beta I_B$$

$$I_E = (\beta + 1) I_B$$

$$V_{TH} = I_B R_{TH} + V_{BE} + (\beta + 1) I_B R_E$$

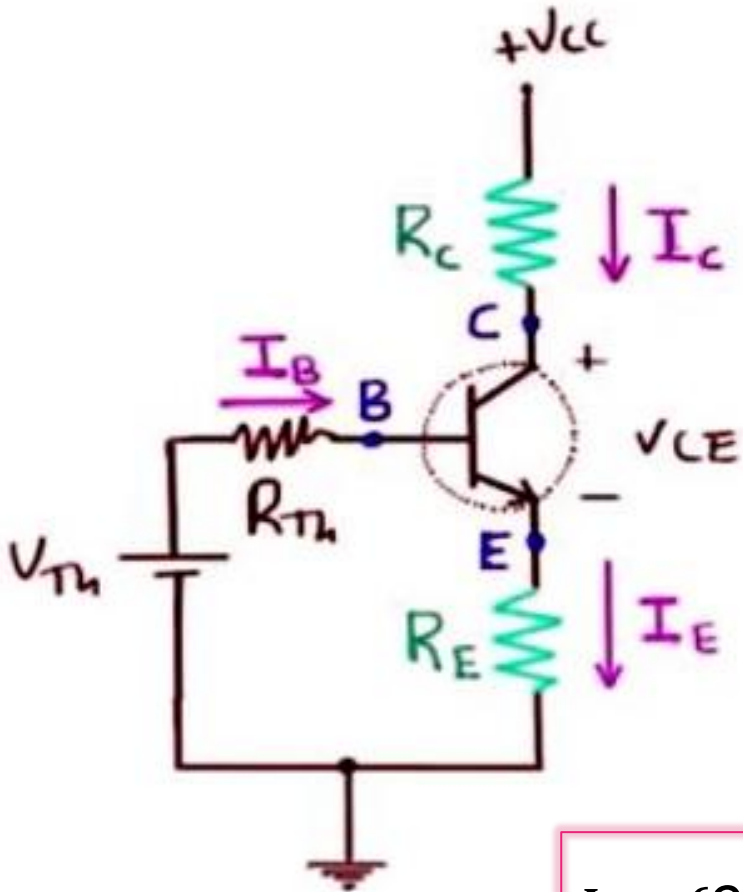
$$V_{TH} = I_B (R_{TH} + (\beta + 1) R_E) + V_{BE}$$

$$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1) R_E}$$

If,  $V_{BE} \approx 0$ , and  $R_E$  is very small

$$I_B \approx \frac{V_{TH}}{R_{TH} + \beta R_E}$$

# VOLTAGE DIVIDER BIAS CIRCUIT - ANALYSIS



$$I_C = \beta I_B$$

$$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E}$$

$$I_C = \beta \left( \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E} \right)$$

$$I_E = (\beta + 1) \left( \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E} \right)$$

$$R_{TH} = \frac{R_1 R_2}{R_1 + R_2}$$

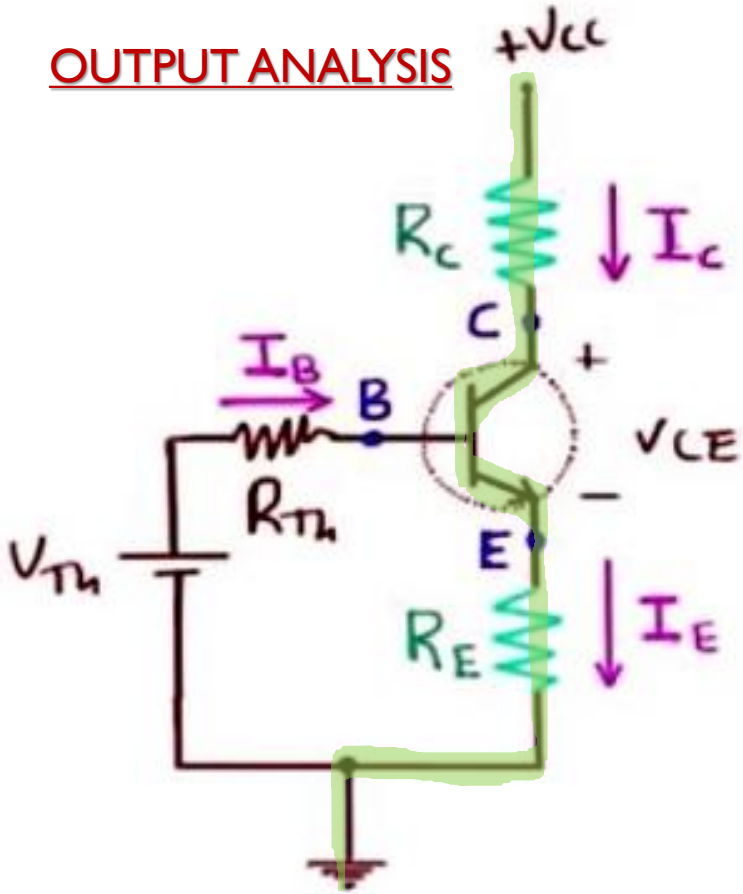
$$V_{TH} = \frac{V_{CC} R_2}{R_1 + R_2}$$

If,  $V_{BE} \approx 0$ , and  $R_E$  is very small

$$I_C \approx \beta \left( \frac{V_{TH}}{R_{TH} + \beta R_E} \right)$$

# VOLTAGE DIVIDER BIAS CIRCUIT - ANALYSIS

## OUTPUT ANALYSIS



$$V_{CC} - I_C R_C - V_{CE} - I_E R_E = 0$$

$$V_{CC} = I_C R_C + V_{CE} + I_E R_E$$

$$V_{CE} = V_{CC} - I_C R_C - I_E R_E$$

$$\text{If, } I_E \approx I_C$$

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$

# VOLTAGE DIVIDER BIAS CIRCUIT

## ADVANTAGES

- Stability factor is Independent of  $\beta$
- Voltage divider biasing is thermally stable.

## DISADVANTAGES

- Input resistance affected by parallel combination of  $R_1$  and  $R_2$ . It can overcome by using 2 power supplies.

# **STABILITY FACTOR**



# Need For Bias Stabilization?

- Transistor parameters are temperature dependent
- Parameters like  $\beta$  for transistor changes from one unit to the other.
- The process of making operating point independent of temperature, parameter variations or transistor replacement is called **Bias Stabilization**.



# Need For Bias Stabilization?

## Temperature Dependence of $I_C$

$$I_C = \beta I_B + I_{CE0} \qquad I_{CE0} = (1 + \beta) I_{CBO}$$

- Reverse saturation current  $I_{CBO}$  doubles for every **10 degree** rise in temperature.
- So  $I_{CE0}$  increases  $\beta + 1$  times of  $I_{CBO}$ .
- $I_C$  dependent on  $I_{CE0}$  , so  $I_C$  also increases  $\beta + 1$  times of  $I_{CBO}$ .
- Power dissipation of transistor,  $P = V_C I_C$ .
- So power dissipation at the junction Increases with collector current, which further increases temperature.
- The process repeats and excess heat may even burn or destroy transistor, and the situation is described as **Thermal Runaway**.

# Requirements of Biasing Circuits

- Operating point is to be fixed in the middle of the Active region to protect the signal from distortion.
- Stabilize the collector current against the variations of temperature.
- Making the operating point independent of transistor parameters.

# STABILITY FACTOR

- The **stability factor S**, is the change of collector current with respect to the reverse saturation current, keeping  $\beta$  and  $V_{BE}$  constant.

$$S = \frac{\delta I_C}{\delta I_{CO}} = \frac{\Delta I_C}{\Delta I_{CO}}$$

Where  $I_{CO}$  – Reverse Saturation Current



# STABILITY FACTOR

- The **stability factor  $S'$** , is the variation of collector current with respect to  $V_{BE}$ , keeping  $\beta$  and reverse saturation current constant.

$$S' = \frac{\delta I_C}{\delta V_{BE}} = \frac{\Delta I_C}{\Delta V_{BE}}$$

Where  $V_{BE}$  – Base emitter voltage

# STABILITY FACTOR

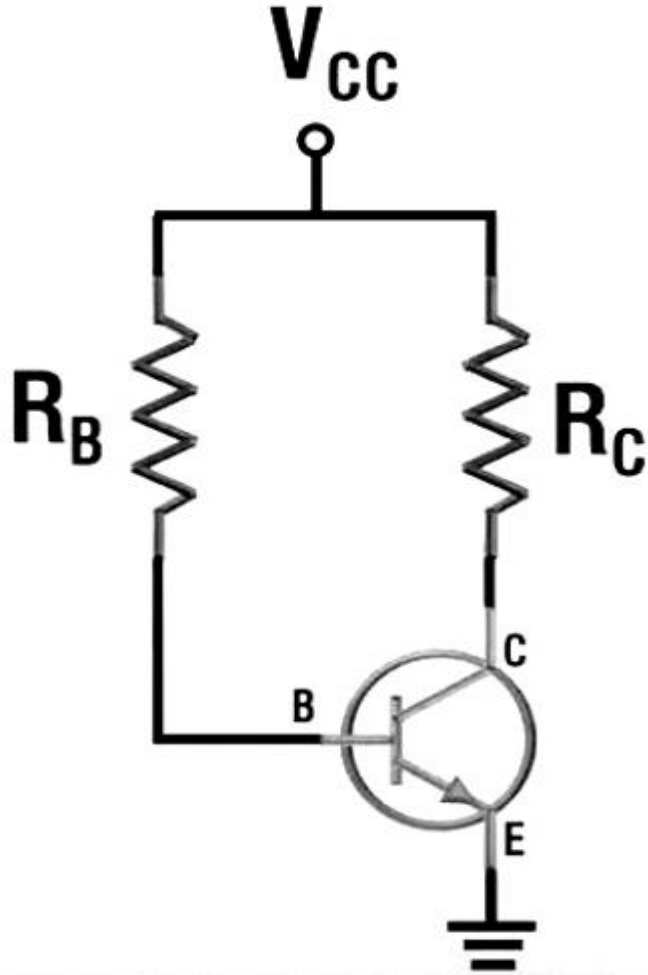
- The **stability factor  $S''$** , is the variation of collector current with respect to  $\beta$ , keeping  $V_{BE}$  and reverse saturation current constant.

$$S'' = \frac{\delta I_c}{\delta \beta} = \frac{\Delta I_c}{\Delta \beta}$$

Where  $\beta$  – Current amplification factor

$$\Delta I_c = (S * \Delta I_{c0}) + (S' * \Delta V_{BE}) + (S'' * \Delta \beta)$$

# Stability factor for Fixed Bias Circuit



$$I_C = \beta I_B + (\beta + 1)I_{CO}$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

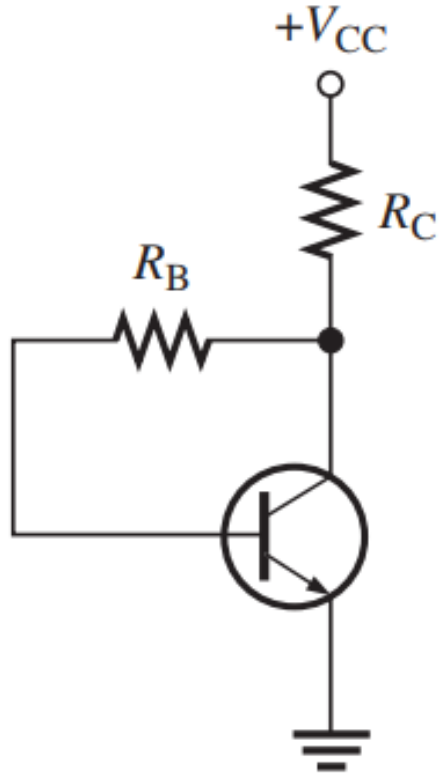
$$I_C = \beta \left( \frac{V_{CC} - V_{BE}}{R_B} \right) + (\beta + 1)I_{CO}$$

$$1 = 0 + (\beta + 1) (1/S)$$

$$S = (\beta + 1)$$



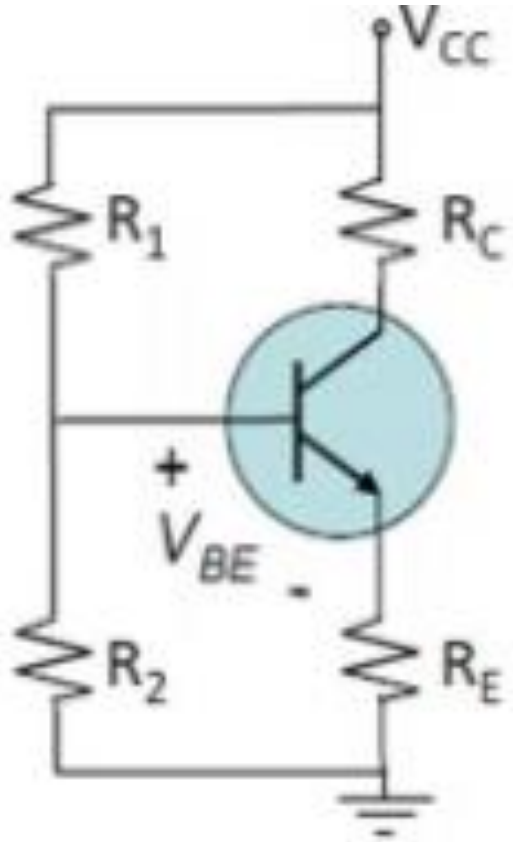
# Stability factor for Collector Bias Circuit



$$S = \frac{\beta + 1}{1 + \beta \left( \frac{R_C}{R_C + R_B} \right)}$$



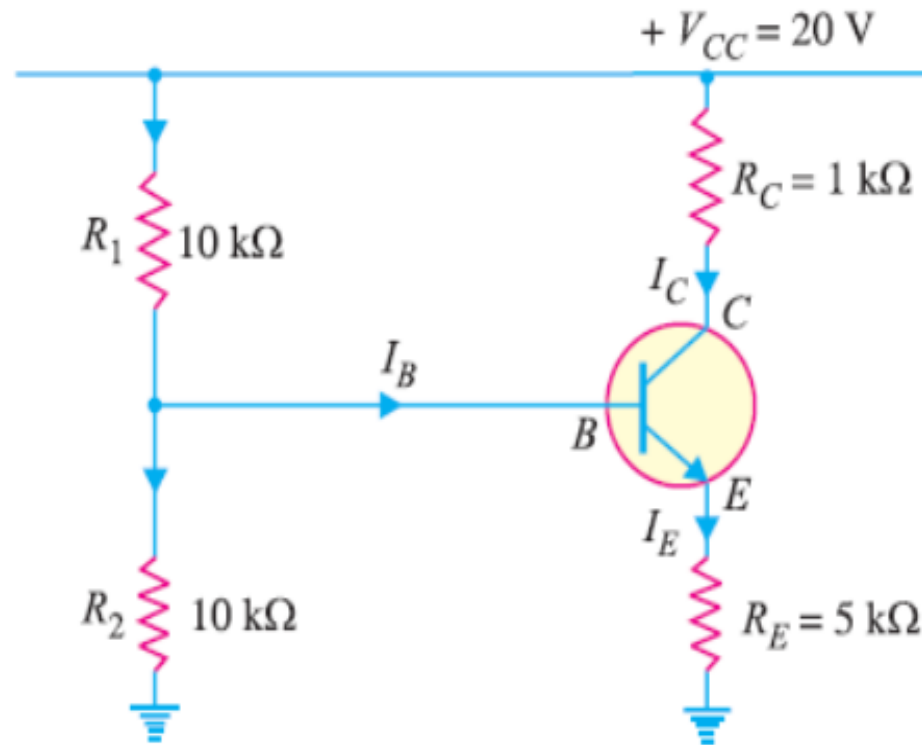
# Stability factor for Voltage Divider Bias Circuit



$$S = \frac{R_B}{R_E}$$

# **NUMERICAL PROBLEMS**

**QSTN: Calculate the emitter current in the voltage divider circuit shown in Fig**  
**Also find the value of  $V_{CE}$  and collector potential  $V_C$ .**



Thevenin's Voltage,  $V_2$

$$V_2 = \left( \frac{V_{CC}}{R_1 + R_2} \right) R_2 = \left( \frac{20}{10 + 10} \right) 10 = 10 \text{ V}$$

$$V_2 = V_{BE} + I_E R_E$$

As  $V_{BE}$  is generally small, therefore, it can be neglected.

$$\therefore I_E = \frac{V_2}{R_E} = \frac{10 \text{ V}}{5 \text{ k}\Omega} = 2 \text{ mA}$$

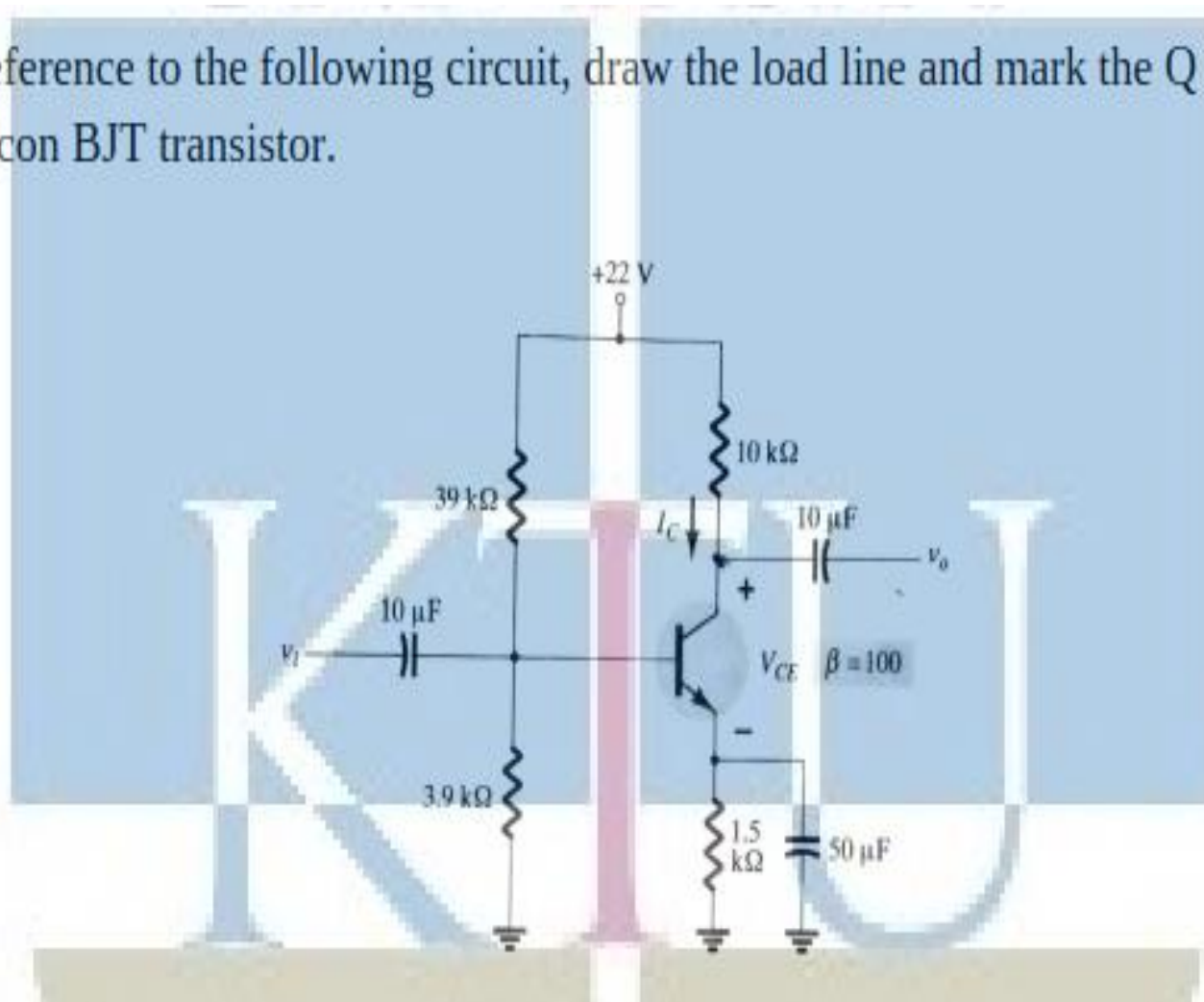
Now  $I_C \simeq I_E = 2 \text{ mA}$

$$\begin{aligned} \therefore V_{CE} &= V_{CC} - I_C (R_C + R_E) = 20 - 2 \text{ mA} (6 \text{ k}\Omega) \\ &= 20 - 12 = 8 \text{ V} \end{aligned}$$

$$\begin{aligned} \text{Collector potential, } V_C &= V_{CC} - I_C R_C = 20 - 2 \text{ mA} \times 1 \text{ k}\Omega \\ &= 20 - 2 = 18 \text{ V} \end{aligned}$$



**QSTN:** With reference to the following circuit, draw the load line and mark the Q point of the Silicon BJT transistor.



$R1 = 39\text{k}\Omega$   
 $R2 = 3.9\text{k}\Omega$   
 $RC = 10\text{k}\Omega$   
 $RE = 1.5\text{k}\Omega$   
 $V_{BE} = 0.7\text{V}$   
 $V_{CC} = 22\text{V}$   
 $\beta = 100$



$$R_{TH} = \frac{R_1 R_2}{R_1 + R_2}$$

$$V_{TH} = \frac{V_{CC} R_2}{R_1 + R_2}$$

$$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E}$$

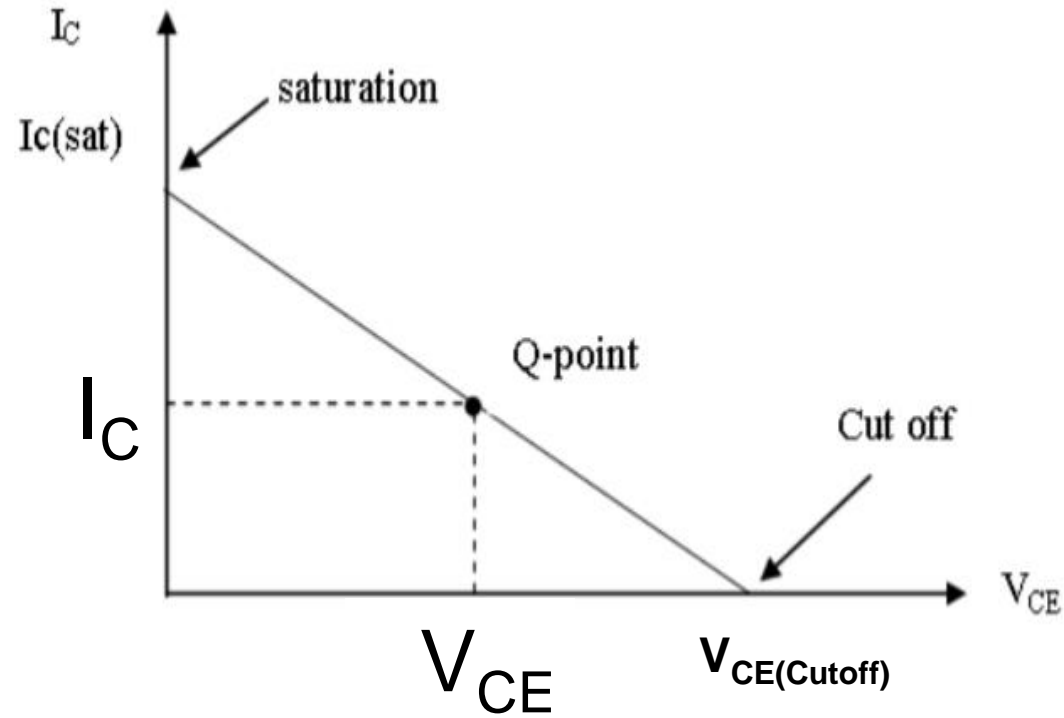
$$I_C = \beta I_B$$

$$I_E \approx I_C$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$V_{CE(\text{Cutoff})} = V_{CC}$$

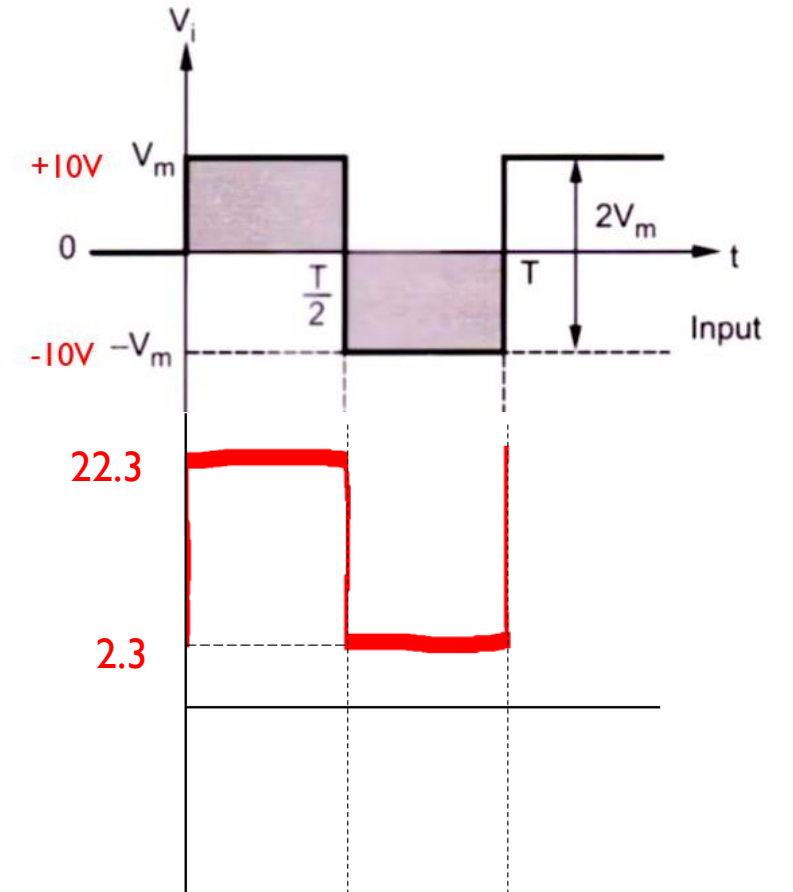
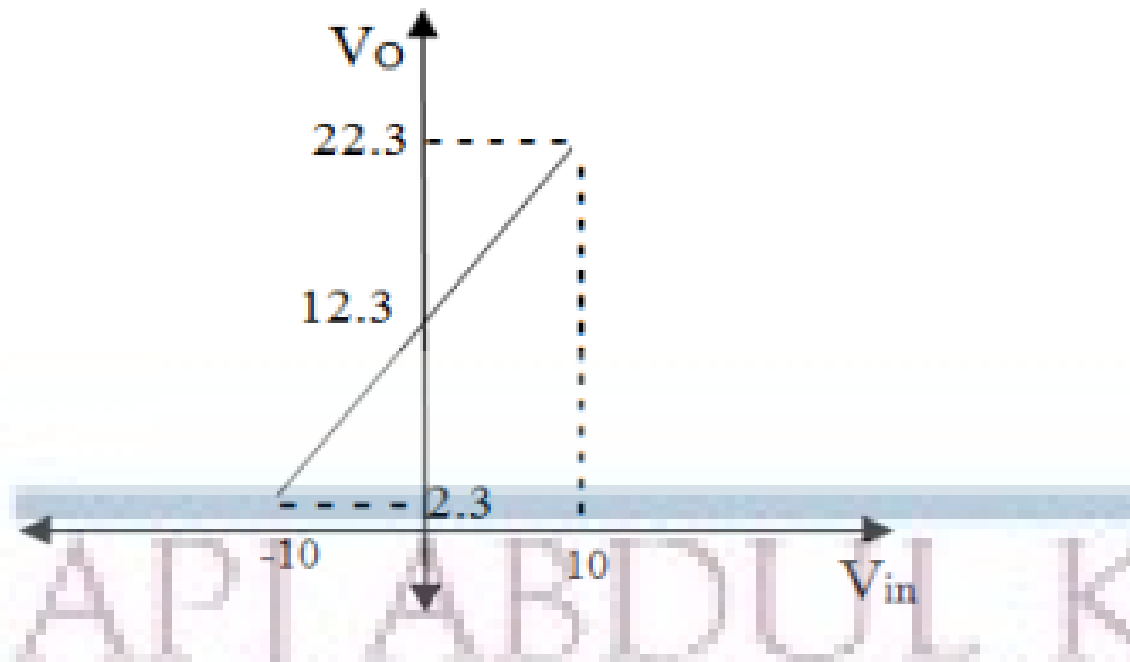
$$I_{C(\text{Sat})} = \frac{V_{CC}}{R_C + R_E}$$

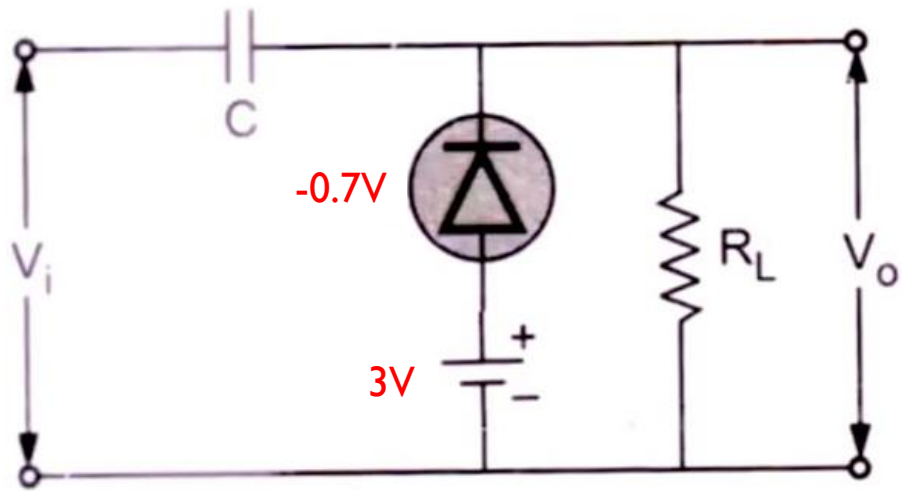


$R_1 = 39k\Omega$   
 $R_2 = 3.9k\Omega$   
 $R_C = 10k\Omega$   
 $R_E = 1.5k\Omega$   
 $V_{BE} = 0.7V$   
 $V_{CC} = 22V$   
 $\beta = 100$



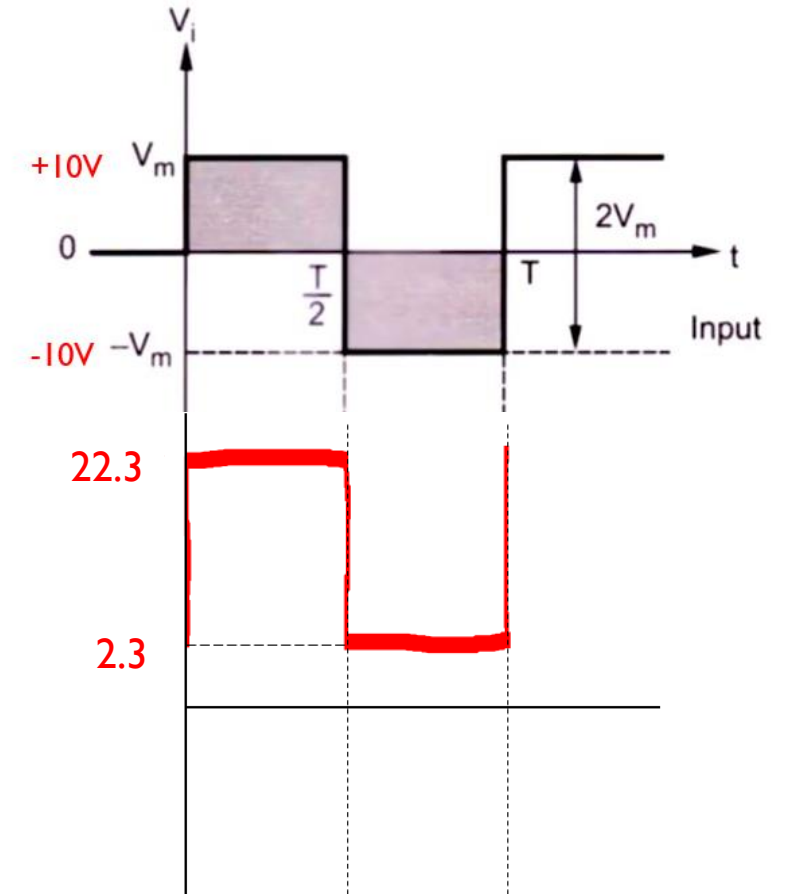
**QSTN:** Design a clamper circuit to get the following transfer characteristics, assuming voltage drop across the diodes 0.7V.





$$-0.7 + X = 2.3$$

$$X = 2.3 + 0.7 = 3V$$







# DC LOAD LINE

