

Battery Integrated Modular Multilevel Converters for Automotive Applications

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Contributions

Design optimization Loss minimization, dc-link capacitor size vs switching frequency.

Experimental validation Harmonic allocations and loss distribution within a submodule.

Compaitive analysis BI-MMC topologies with 2-level inverter.

DC charging Maximum DC charging power for BI-MMC topologies.

Topology overview

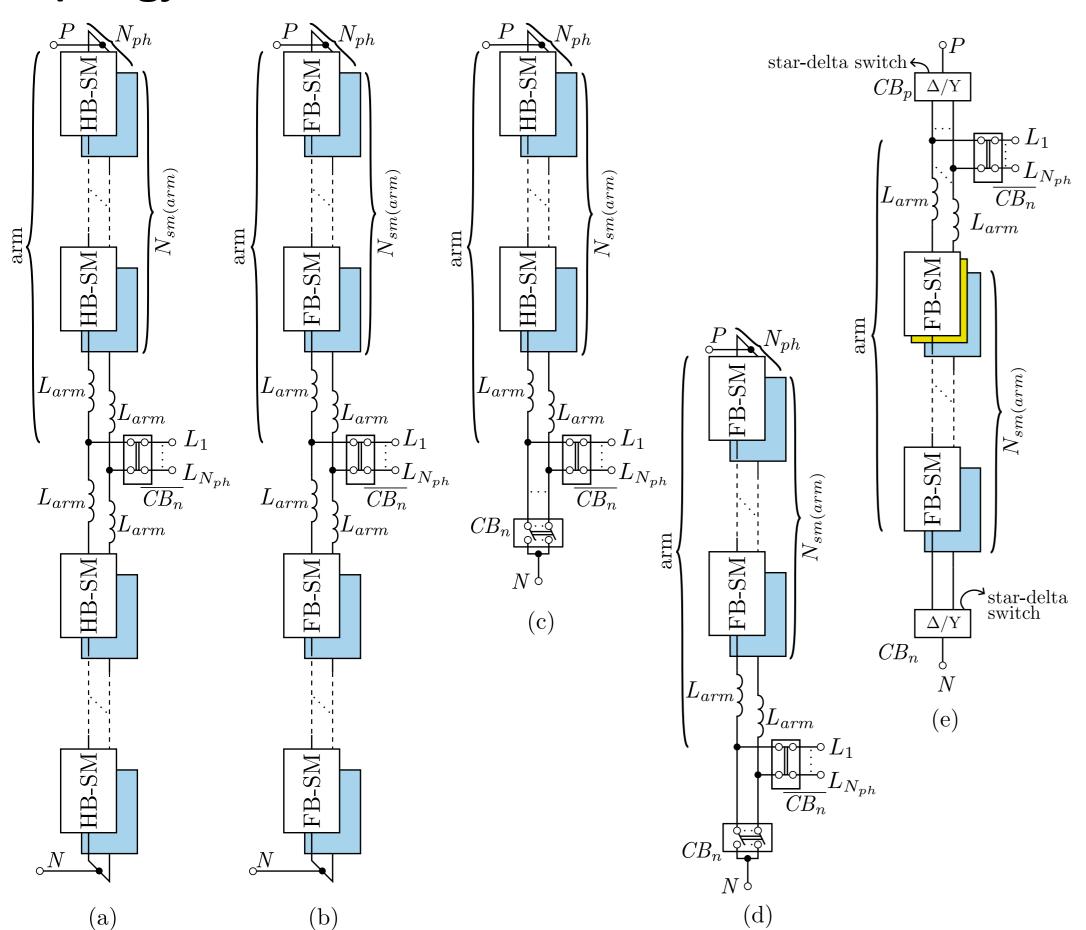
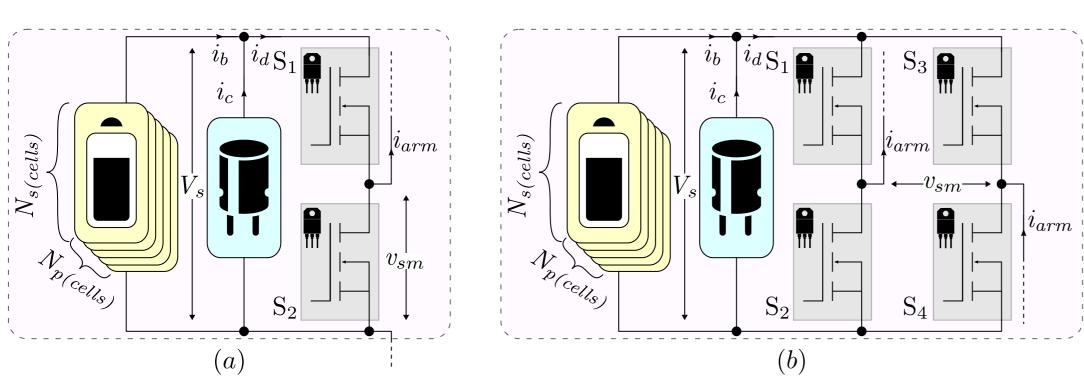
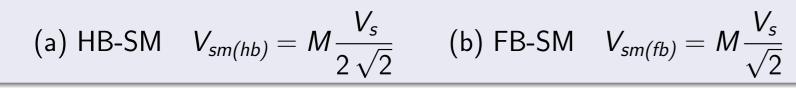


Figure: Double-star (DS), single-star (SS) with half-bridge (HB) and full-bridge (FB), and single-delta with FB.





Submodule Loss distribution

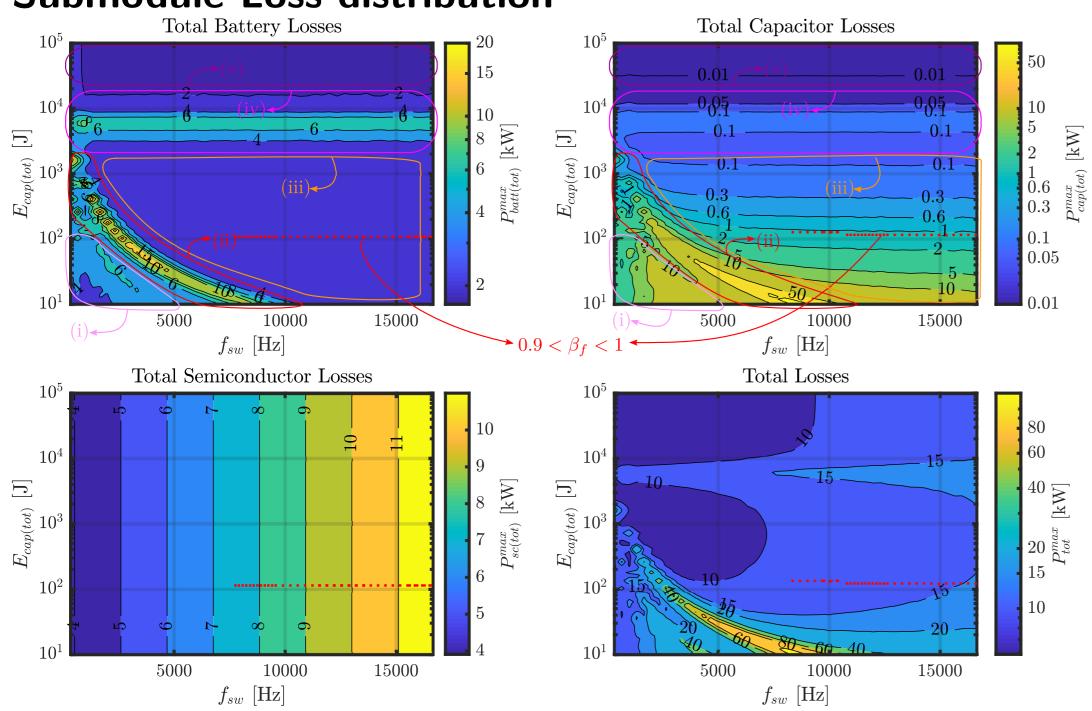


Figure: Losses for a 5- $N_{s(cells)}$, DSFB BI-MMC topology at a rated power of 400 kW.

region(i): region(ii): region(iii): region(iv): region(v): $f_{sw} < f_{res}$ $f_{sw} \approx f_{res}$ $f_{sw} > f_{res}$ $f_{sw} \approx 2 f_1$ $f_{sw} > 2 f_1$

 $f_{res} = \frac{1}{2\pi \sqrt{I_{P}C_{res}}}$ $P_{tot}^{max} = P_{batt(tot)}^{max} + P_{cap(tot)}^{max} + P_{sc(tot)}^{max}$

Battery and capacitor currents in a submodule

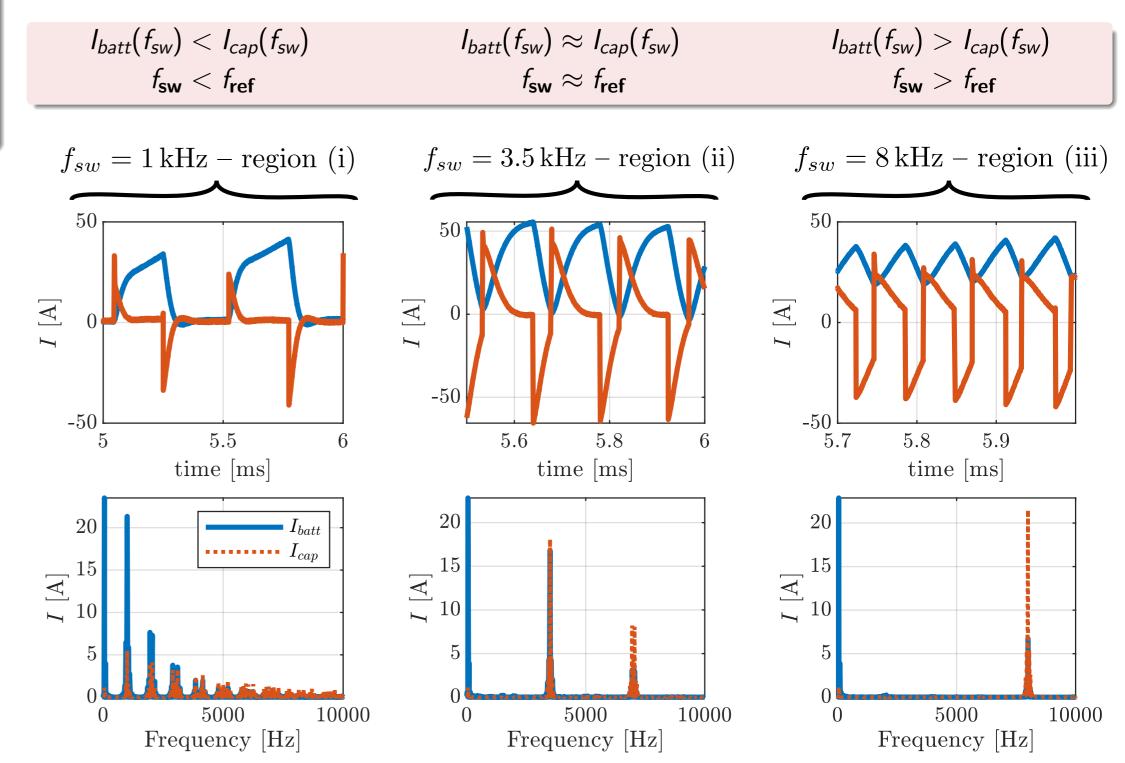
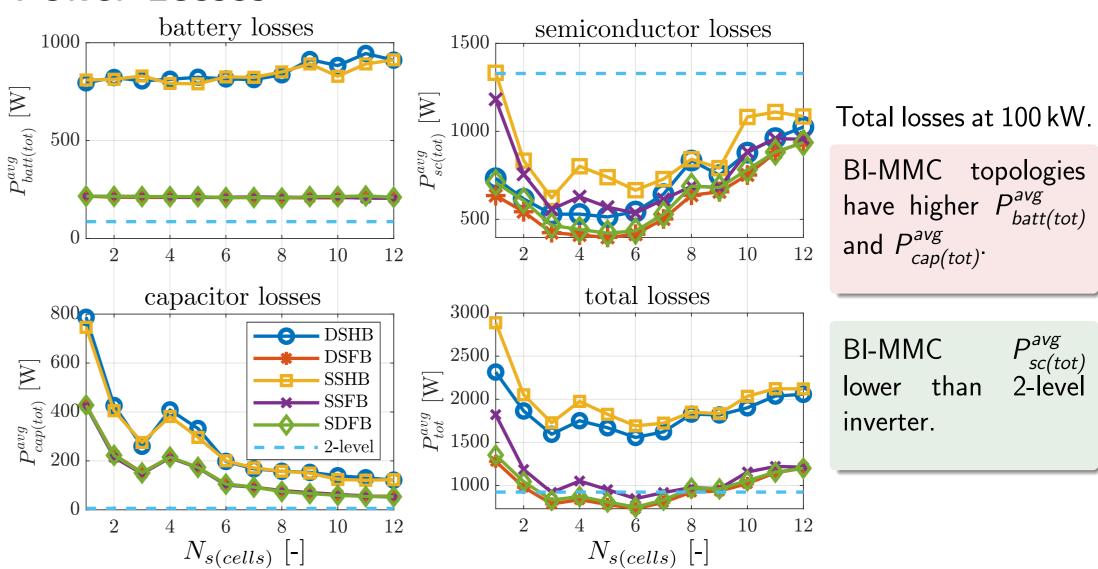
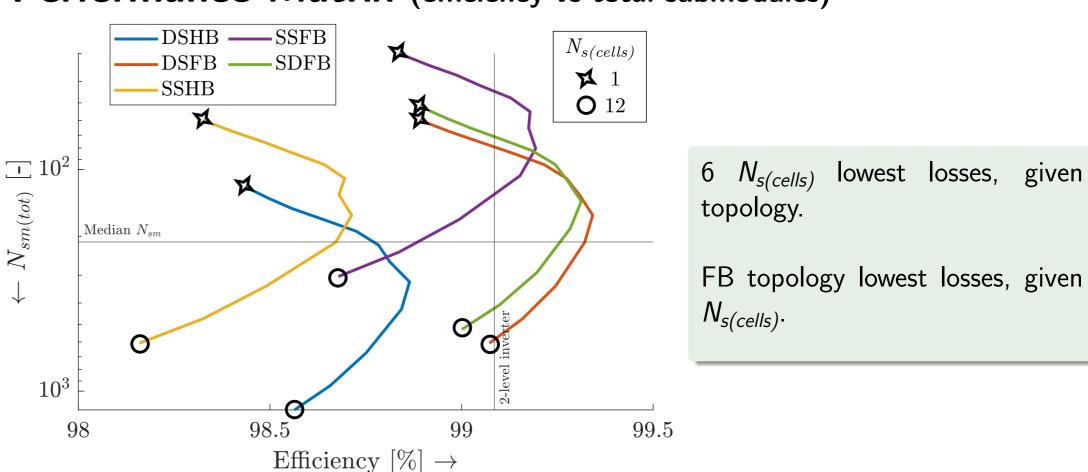


Figure: Current measurements on a 1- $N_{s(cells)}$, 15 V SSFB BI-MMC topology.

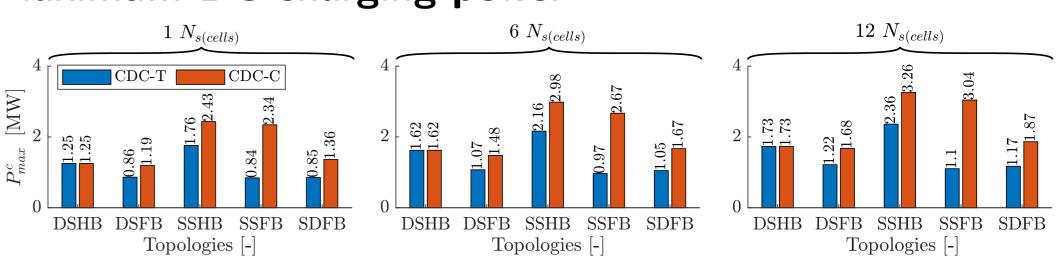
Power Losses



Performance Matrix (efficiency vs total submodules)



Maximum DC charging power



 $N_{sm(tot)}$ based on traction voltage (CDC-T) and based on charger voltage (CDC-C).

Conclusions

Design optimization: DC-link capacitor and switching frequency choice such that $f_{sw} \neq f_{res}$.

Comparative analysis: BI-MMC topologies vs 2-level inverter:

Higher battery and capacitor losses, but Lower submodule capacitor losses. Lower total losses for FB topologies with 5-6 $N_{s(cells)}$.

DC charging: maximum DC charging power for BI-MMCs is between 800 W to 3.26 MW with the same losses as traction.