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Experimental investigation of residence time distribution in twin-screw granulation

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IFPAC Annual Meeting

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Arlington, 22 January 2014
Ashish Kumar

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BIMATH, Ghent University, Belgium.

Laboratory of Pharmaceutical Process Analytical Technology,

Ghent University, Belgium.

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- **Background**

Consigma™-25 system

Twin-Screw Granulator

High shear wet granulation

- **Experiments**

Objective – factors and responses

Set-up: CI System

Results

- **Conclusions**

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Consigma™-25 system
(GEA pharma systems, Collette)



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Continuous twin screw
granulator

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Segmented Fluid bed dryer

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Granule conditioning
module

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Twin-Screw Granulation

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Loss-in-weight
powder feeder(s)

Liquid
addition



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Setpoints (logged):

Powder mass flow (g/min) - powder feeder

Liquid mass flow (g/min) - liquid addition

Screw speed (rpm)

Barrel temperature (°C)

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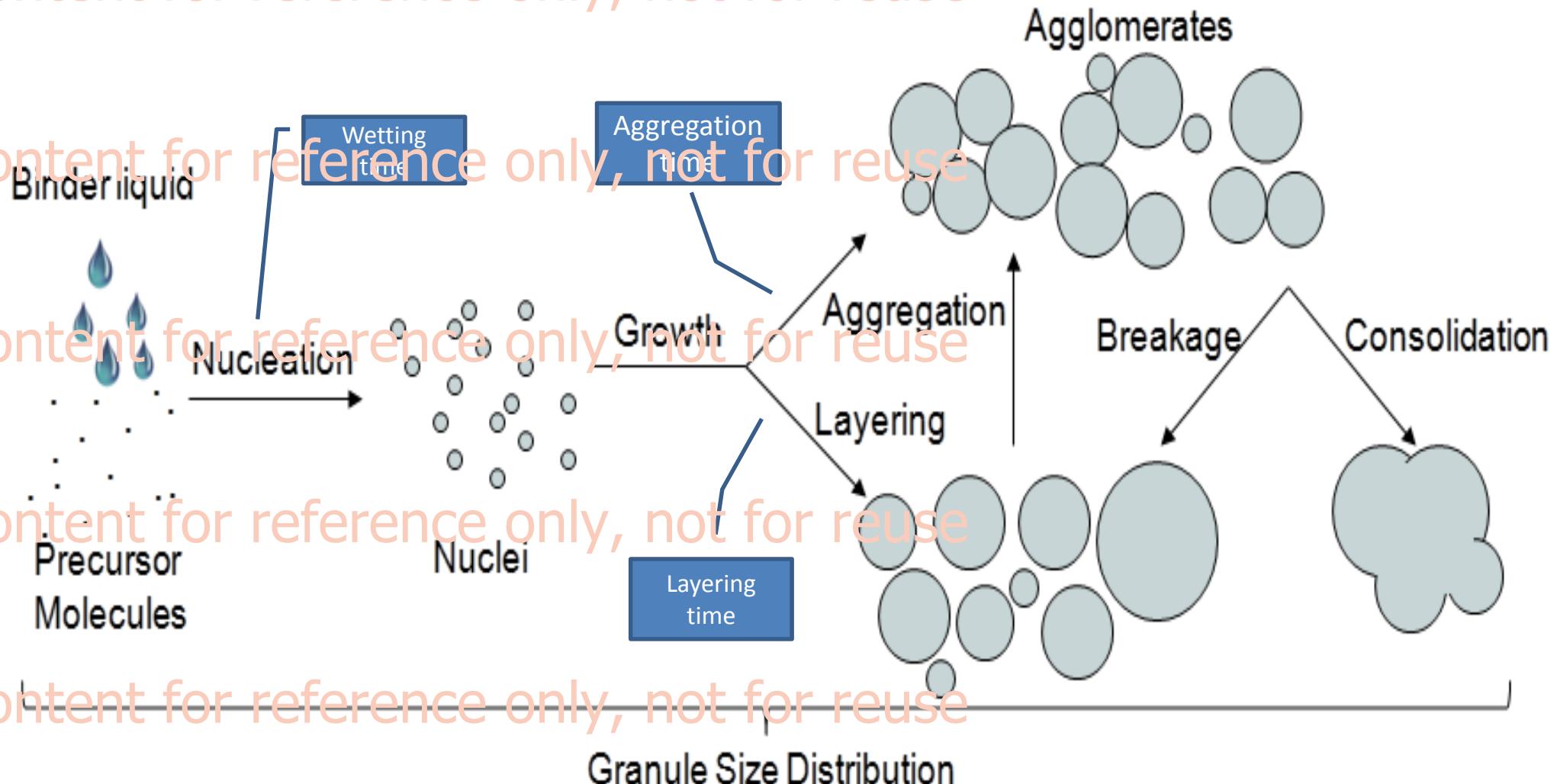
Granulation steady state criterion:

Torque granulator (N·m)



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Need for enhanced mechanistic understanding of the process through experiments and mathematical modelling for prediction and future control of product quality

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- number of kneading elements (2, 6, 12)
- screw speed (500, 700, 900 rpm)
- powder feed rate (10, 17.5, 25 kg/h)
- stagger angle (30, 60, 90°)

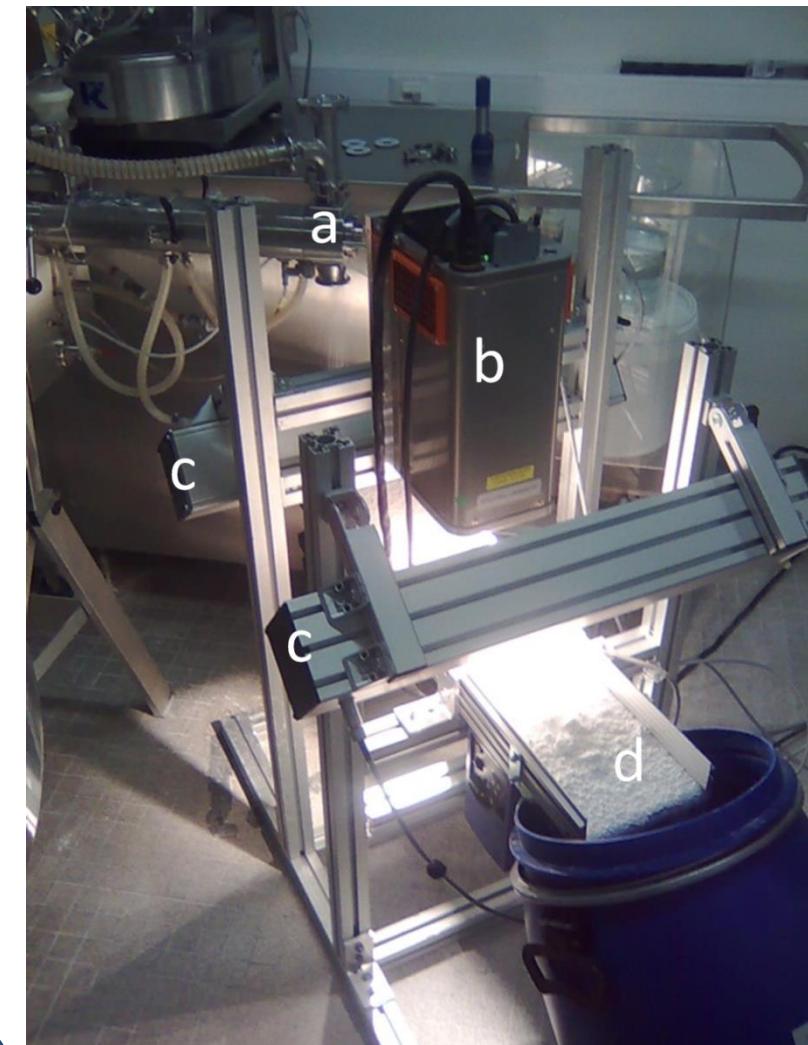
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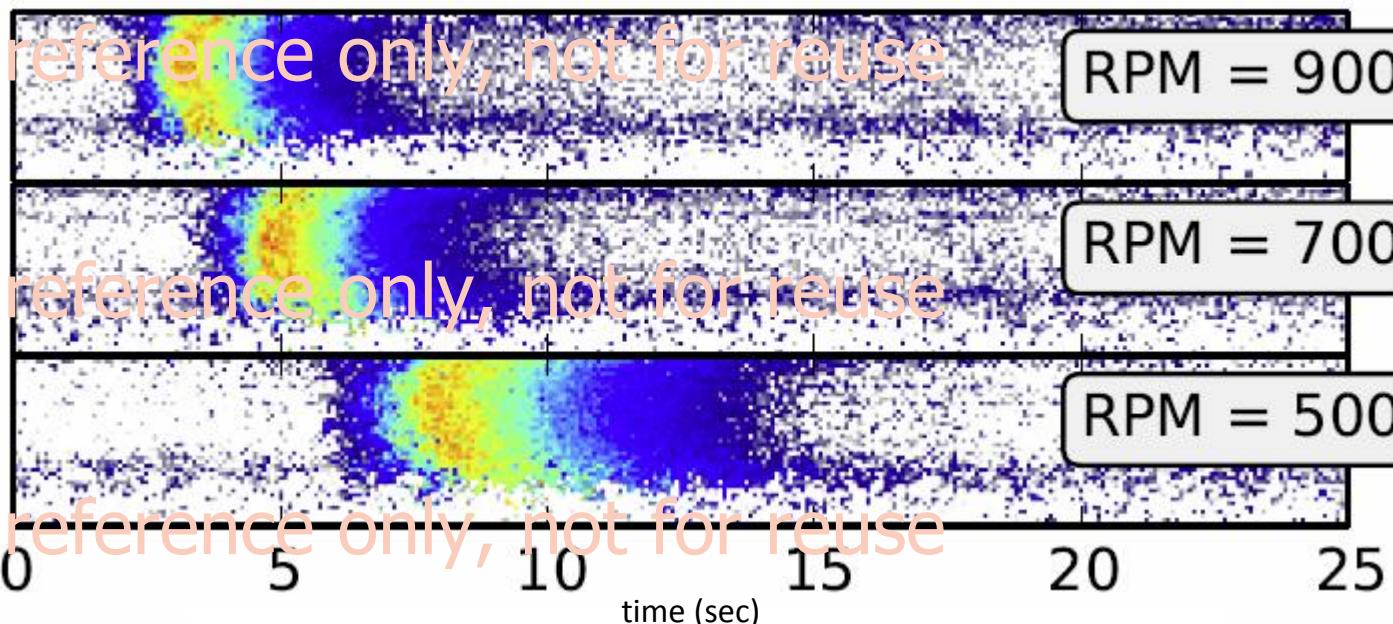
- a. CTSG
- b. Chemical Imaging-camera
- c. Uniform Light Source
- d. Conveyor Belt

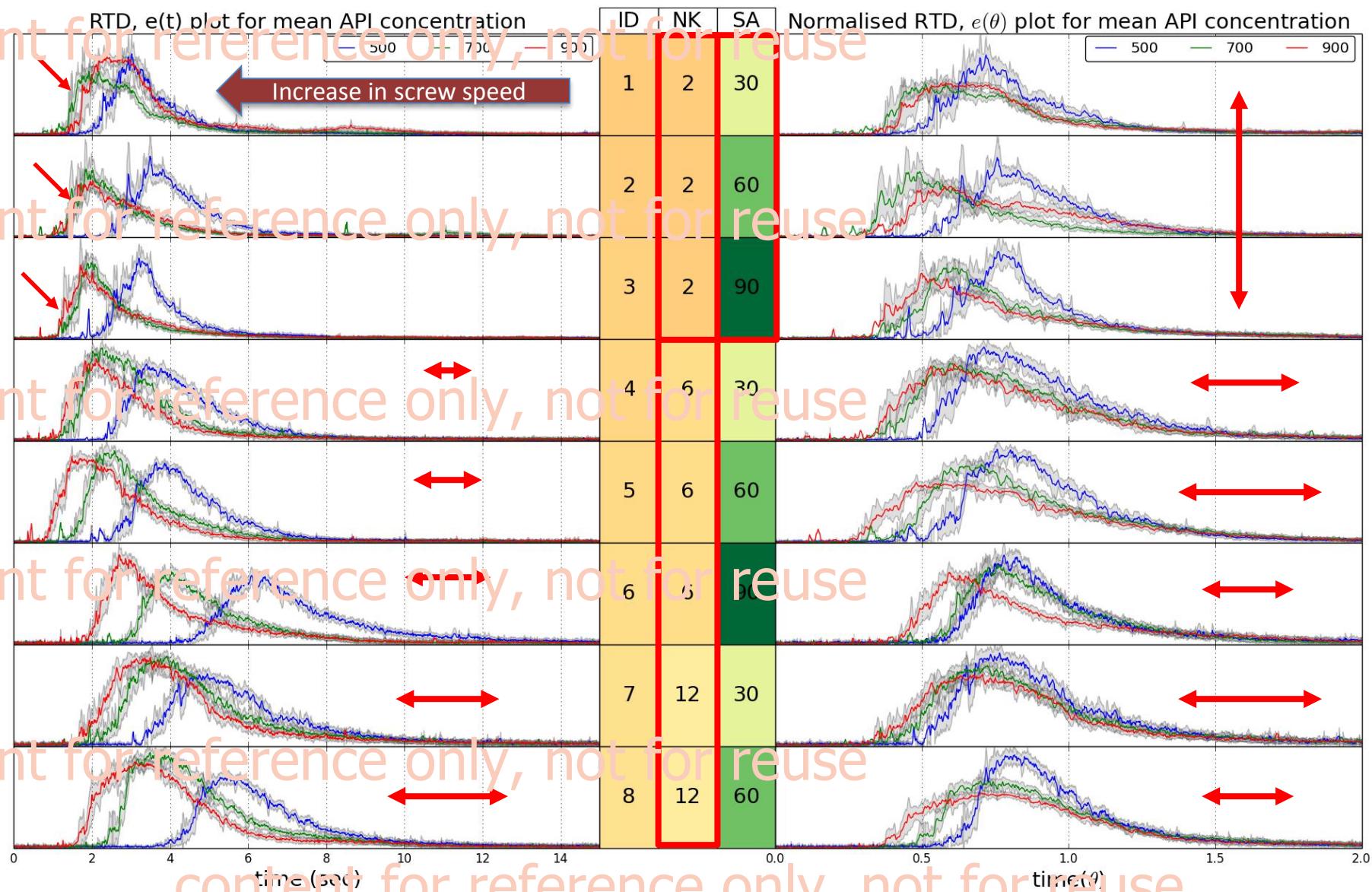
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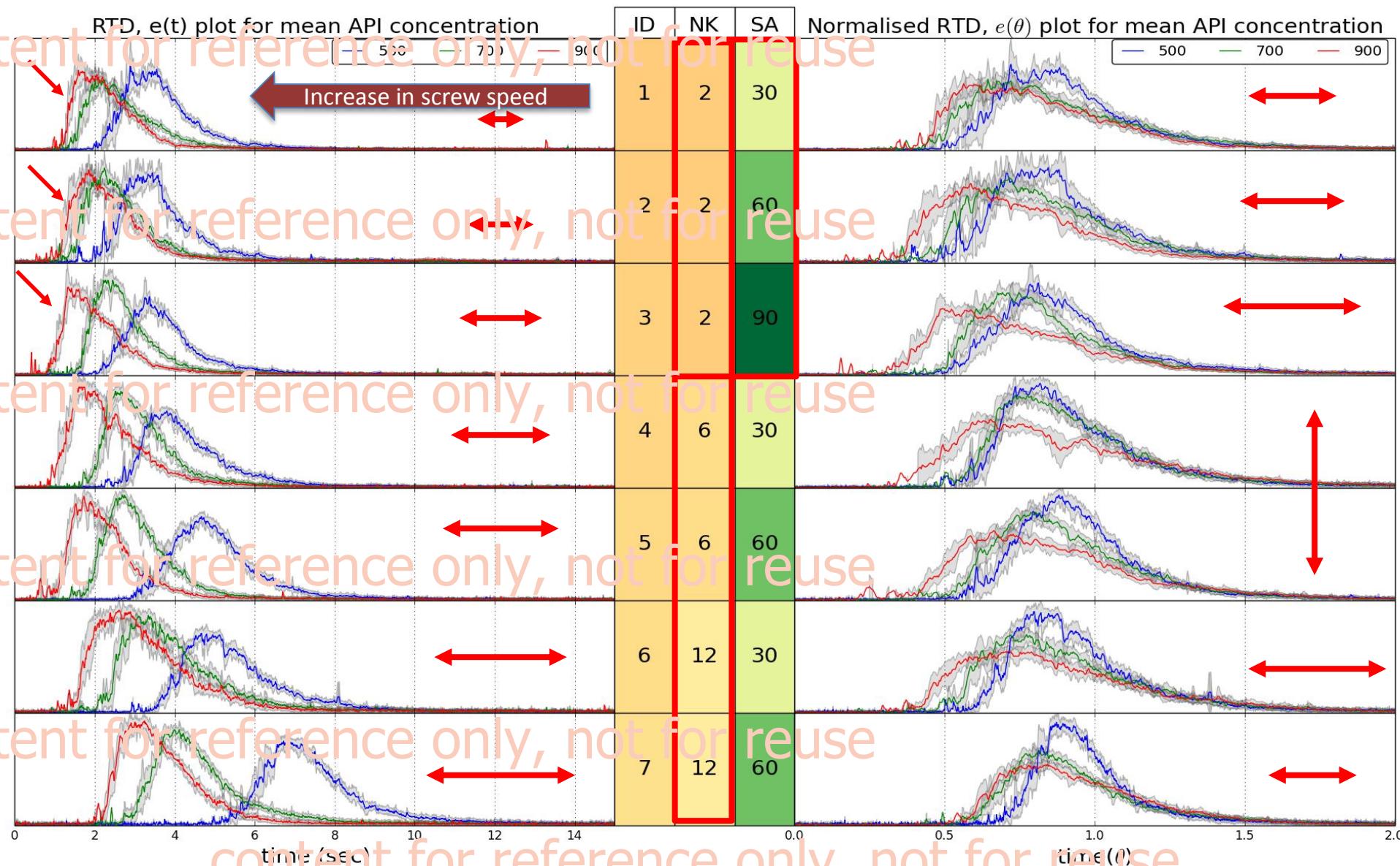
Lactose monohydrate granulated with distilled water (L/S = 10% (w/w)).

Theophylline anhydride (API) as tracer (2% (w/w)).









Mean residence time , τ

(a measure of the mean of the distribution)

$$\tau = \frac{\int_0^{\infty} t \cdot e(t) dt}{\int_0^{\infty} e(t) dt}$$

Variance, σ^2

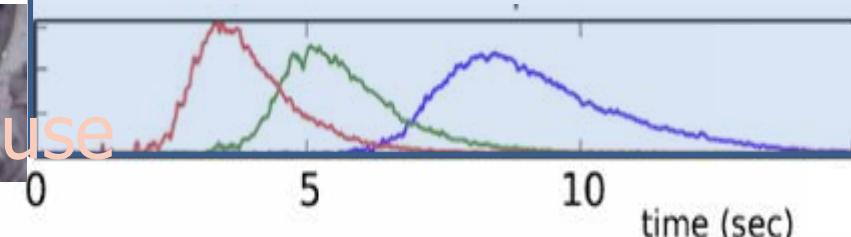
(width of the distribution)

$$\sigma^2 = \frac{\int_0^{\infty} (t - \tau)^2 \cdot e(t) dt}{\int_0^{\infty} e(t) dt}$$

Péclet Number, Pe

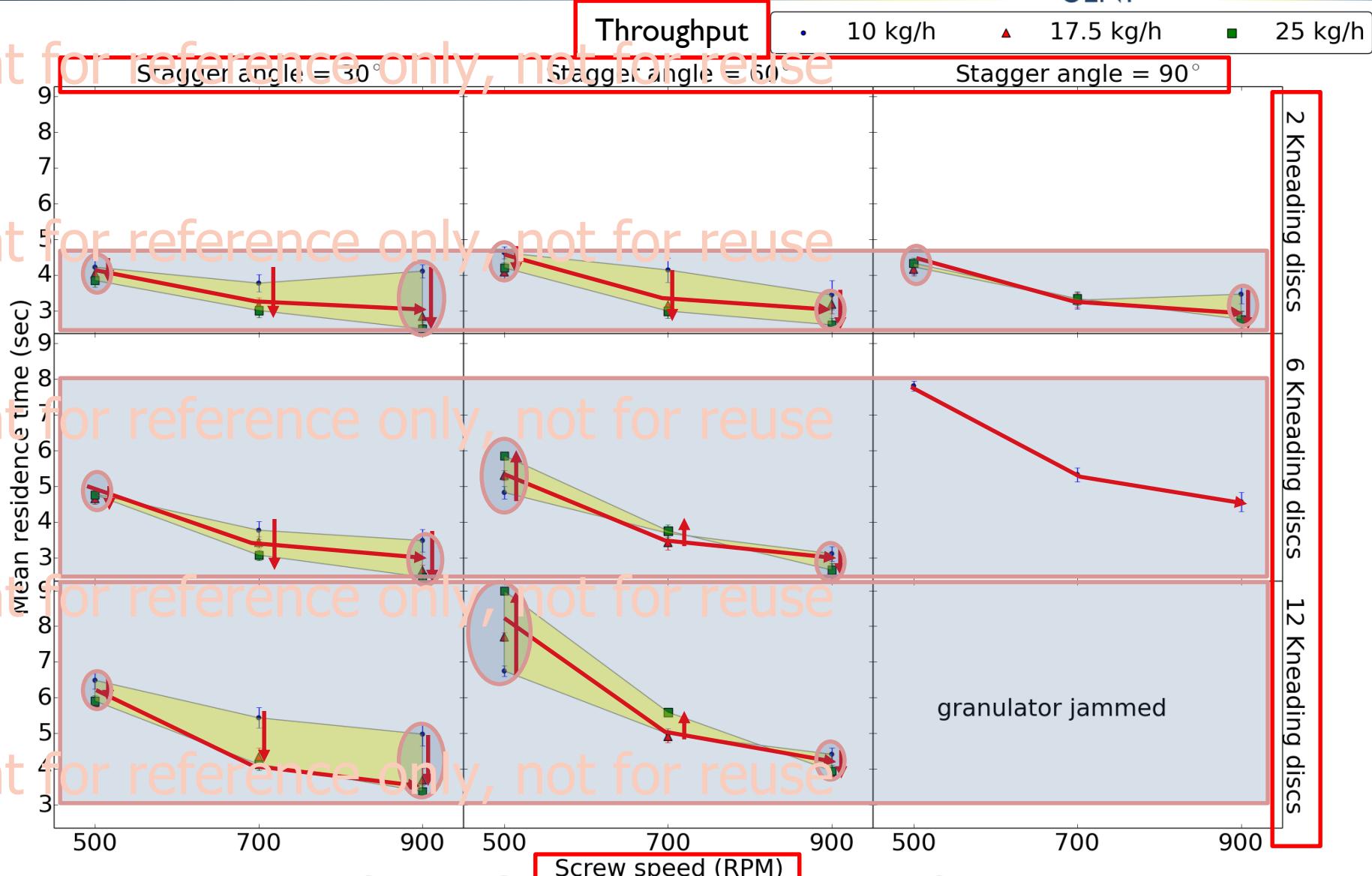
$\left(\frac{\text{Rate of axial transport by convection}}{\text{Rate of axial transport by dispersion}} \right)$

$$Pe = \frac{UL}{D}$$



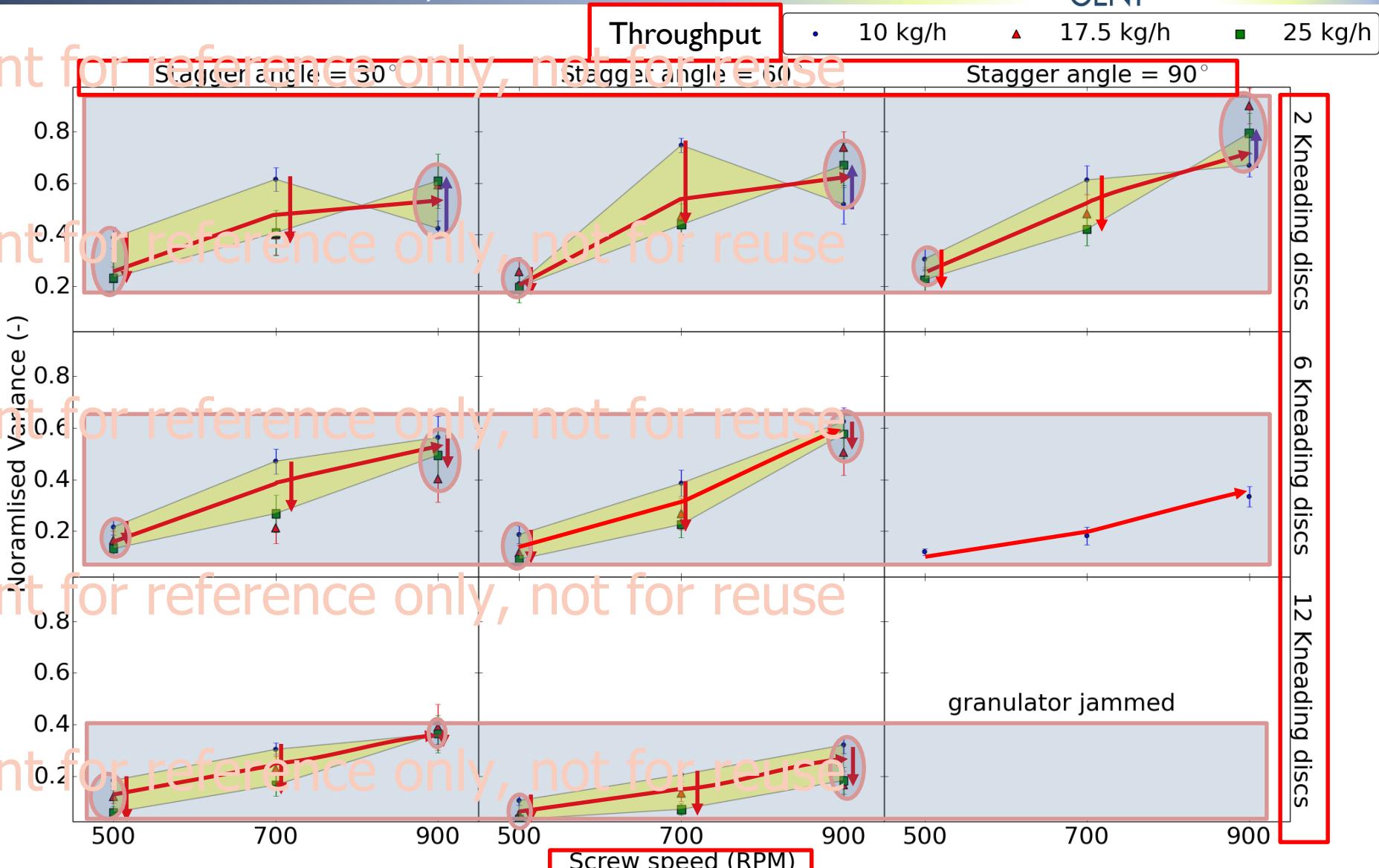
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Mean Residence Time (the mean of the distribution)



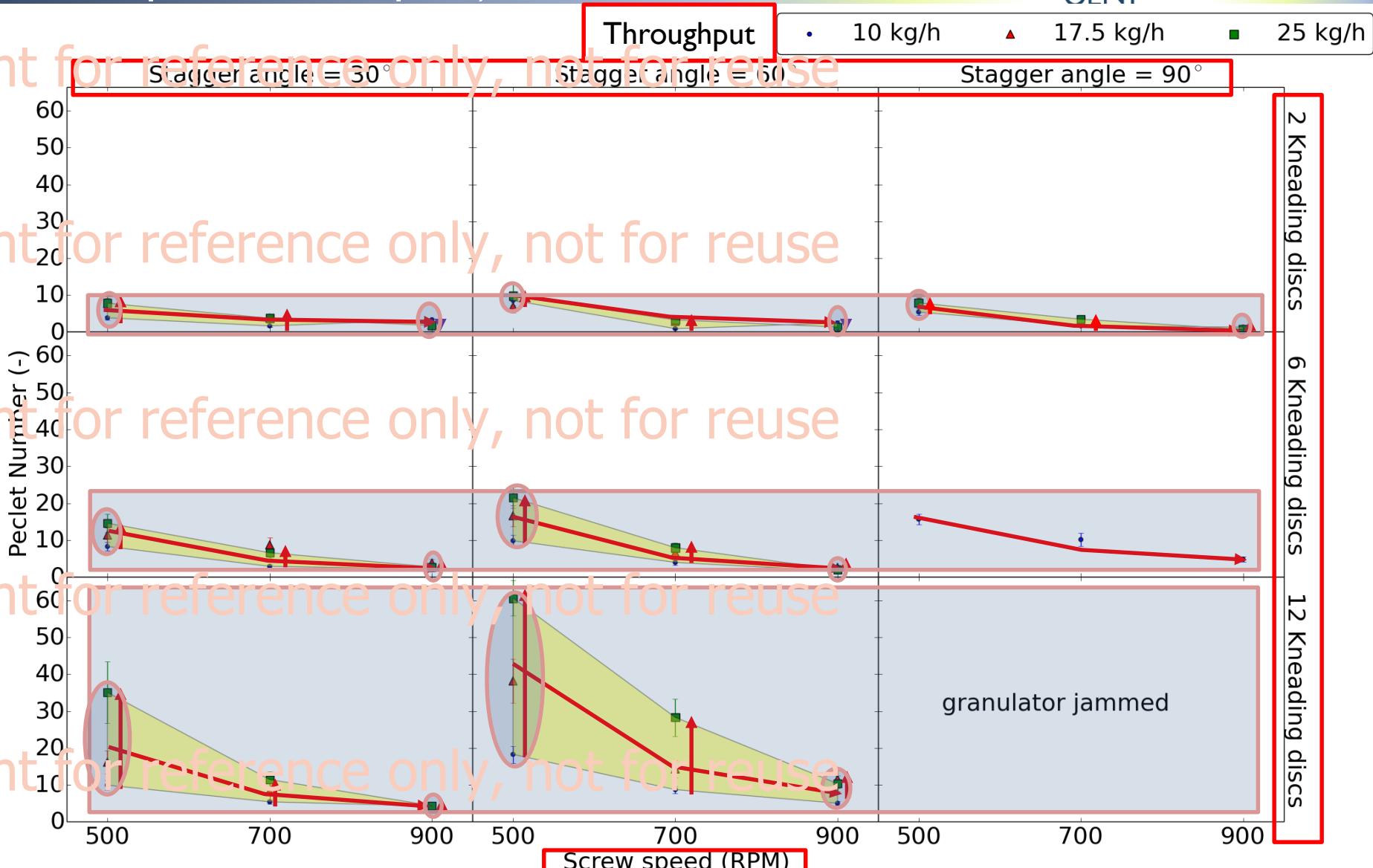
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Normalised Variance (the width of the distribution)



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Dispersion Model-Peclet Number (convective/dispersive transport)



It is not (always) true that, “the extent of axial mixing in the mixing zones of the granulator does not change for different configurations and process conditions (Lee et al. 2012)”. In fact they have a direct influence on both RTD and the axial mixing in TSG.

- Together with a PSD study it can be confirmed which mixing regime is most desirable for granulation purposes.
- In further study we will investigate material properties influence on the RTD and mixing.
- The results obtained will be used in our future work on mechanistic modeling of the granulation process in TSG.

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Acknowledgements



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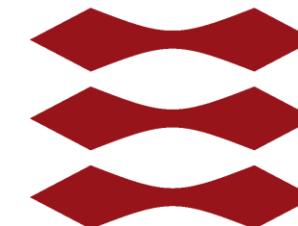
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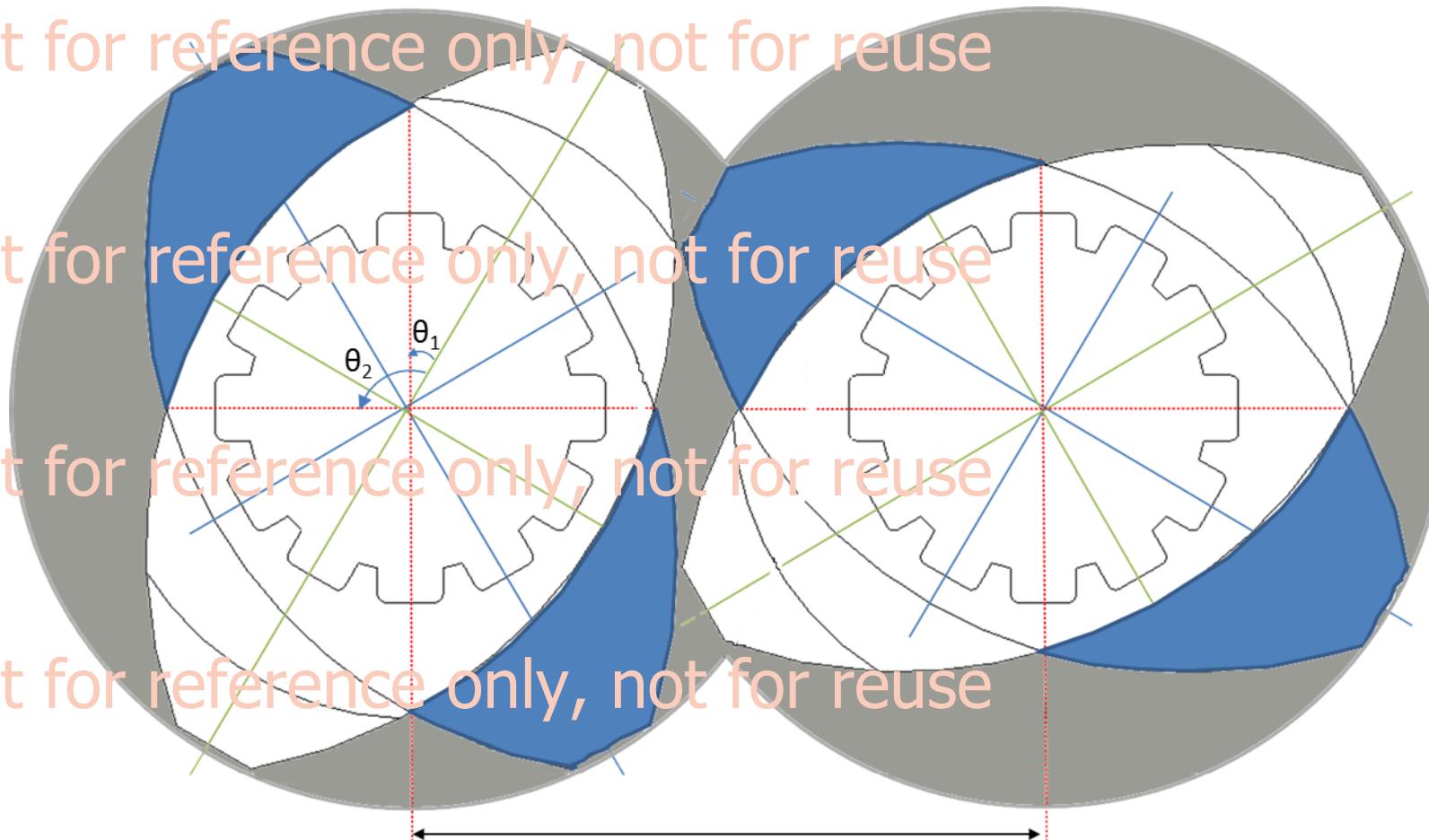
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Q & A

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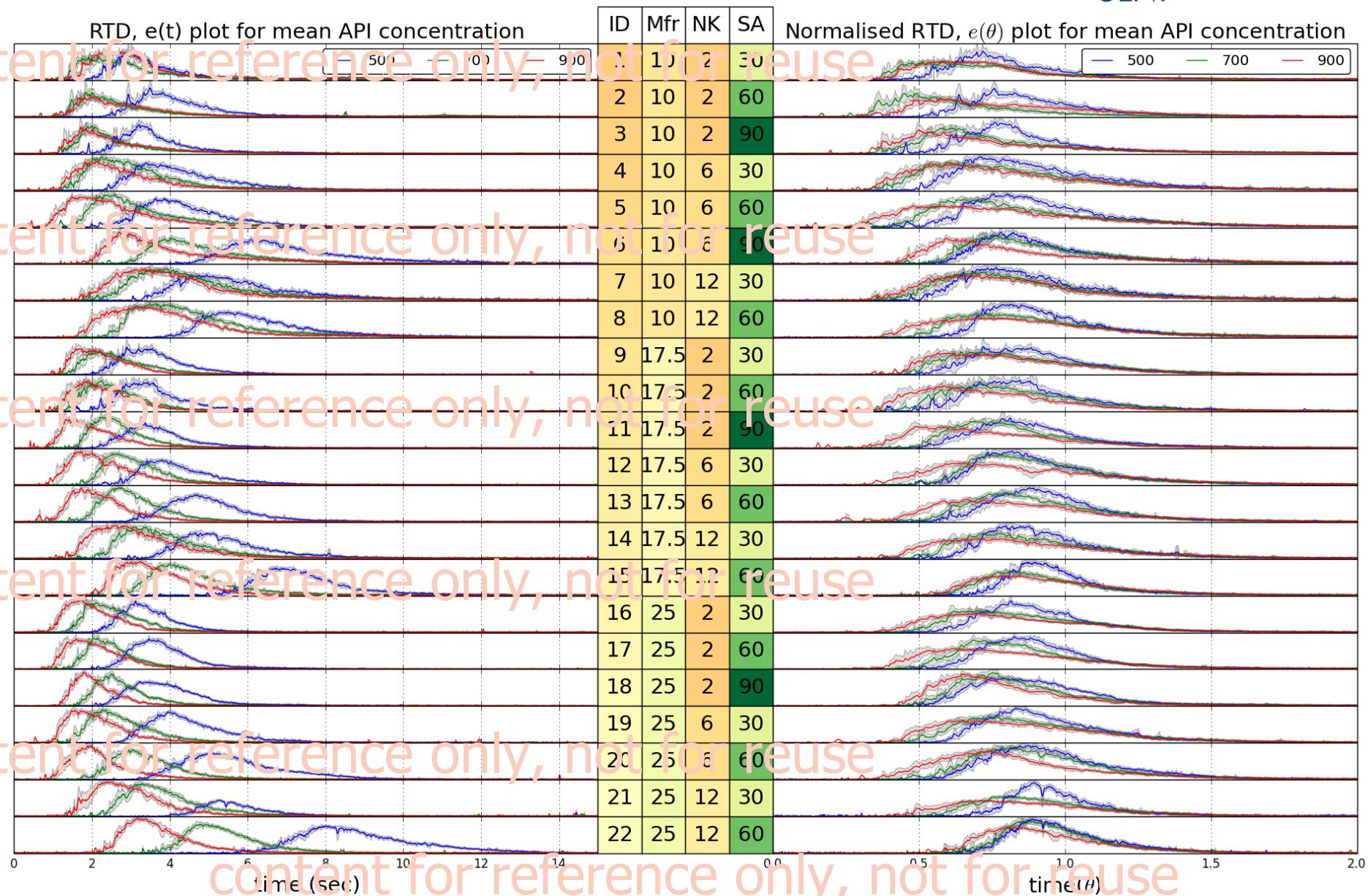


- Flow channel in the granulator barrel
- Area Restricted by successive kneading disc

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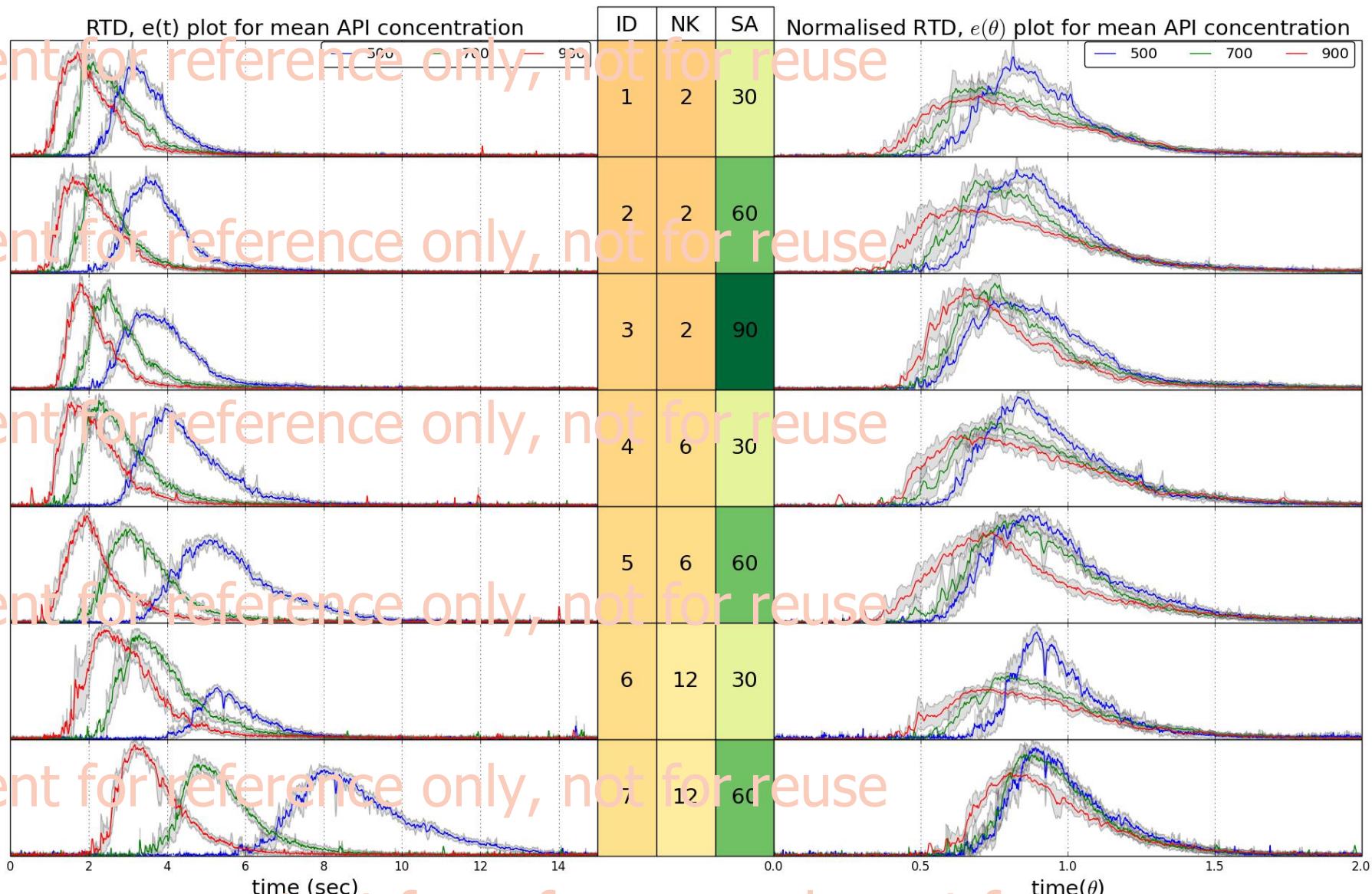
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API map- qualitative assesment



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API map- Powder feed rate 17.5 kg/h



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