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Investigation of twin screw granulation: integrating experimental and computational approaches

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IFPAC® Annual Meeting 2015

Session: QbD – Applications and Tools

LABORATORY OF PHARMACEUTICAL PROCESS ANALYTICAL TECHNOLOGY

FACULTY OF PHARMACEUTICAL SCIENCES

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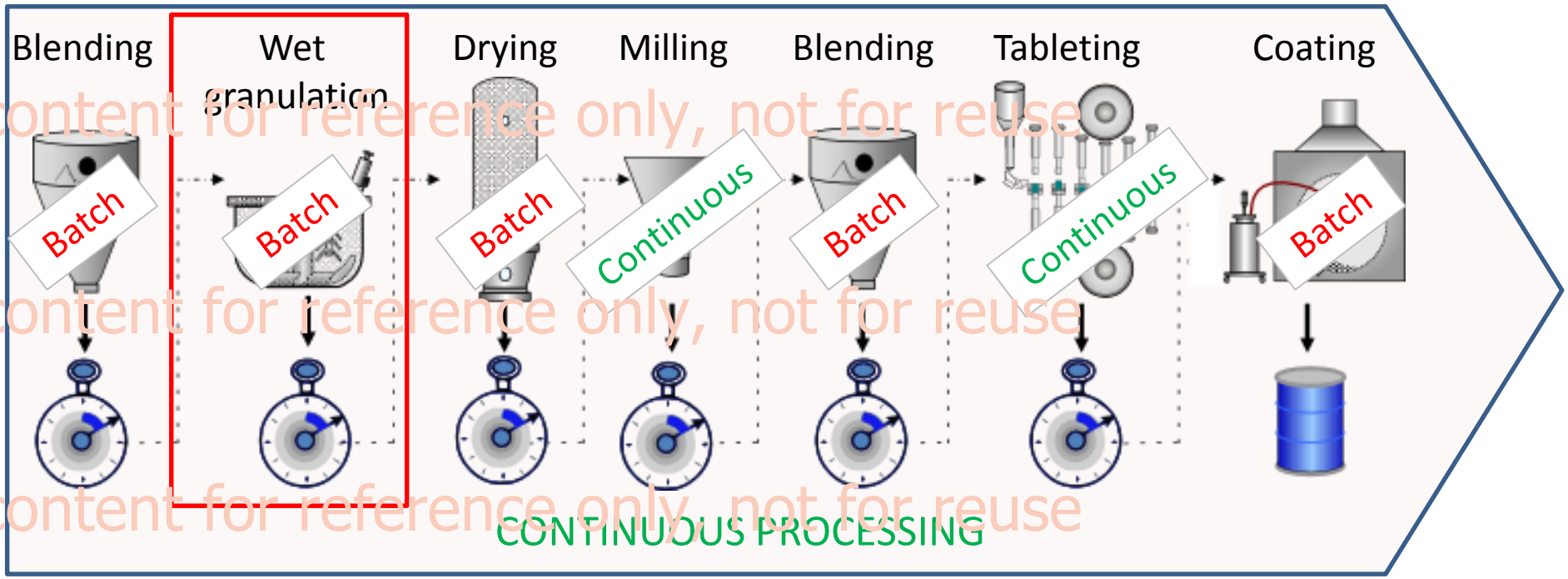
Current solid-dosage manufacturing is slow and expensive



Product collected after each unit operation

Actual processing time = days to weeks

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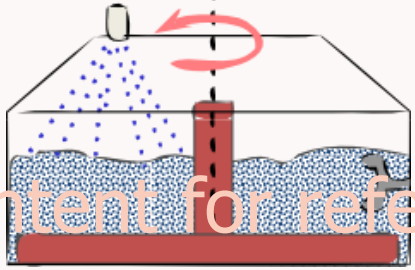
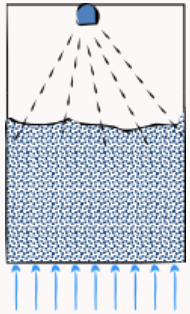
Traditional to new granulation method

High-shear mixer



Drum

Fluidised-bed

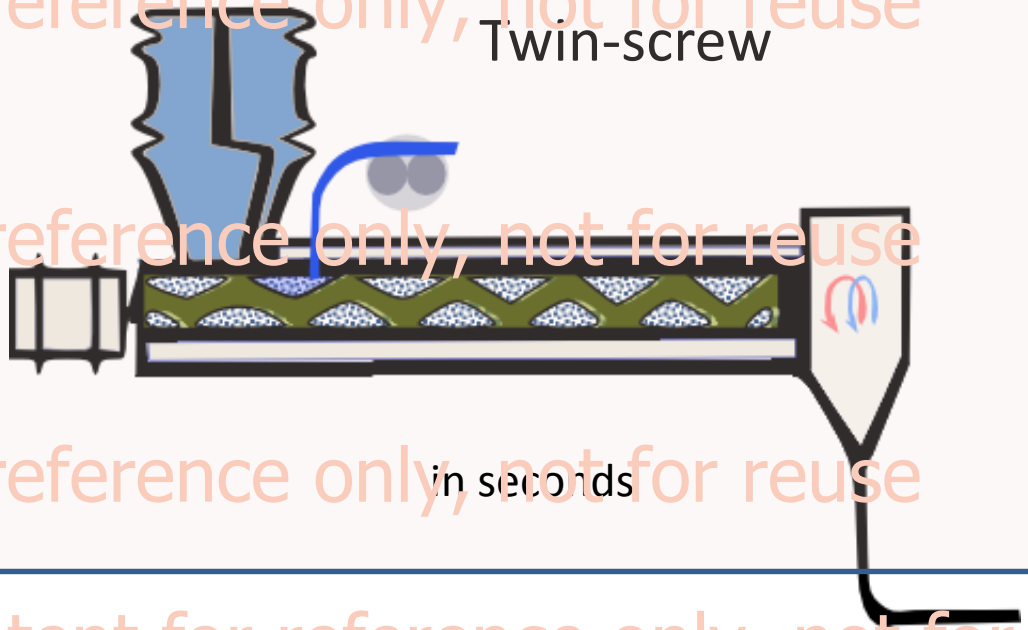


From minutes to hours

Batch

Continuous

Twin-screw



in seconds

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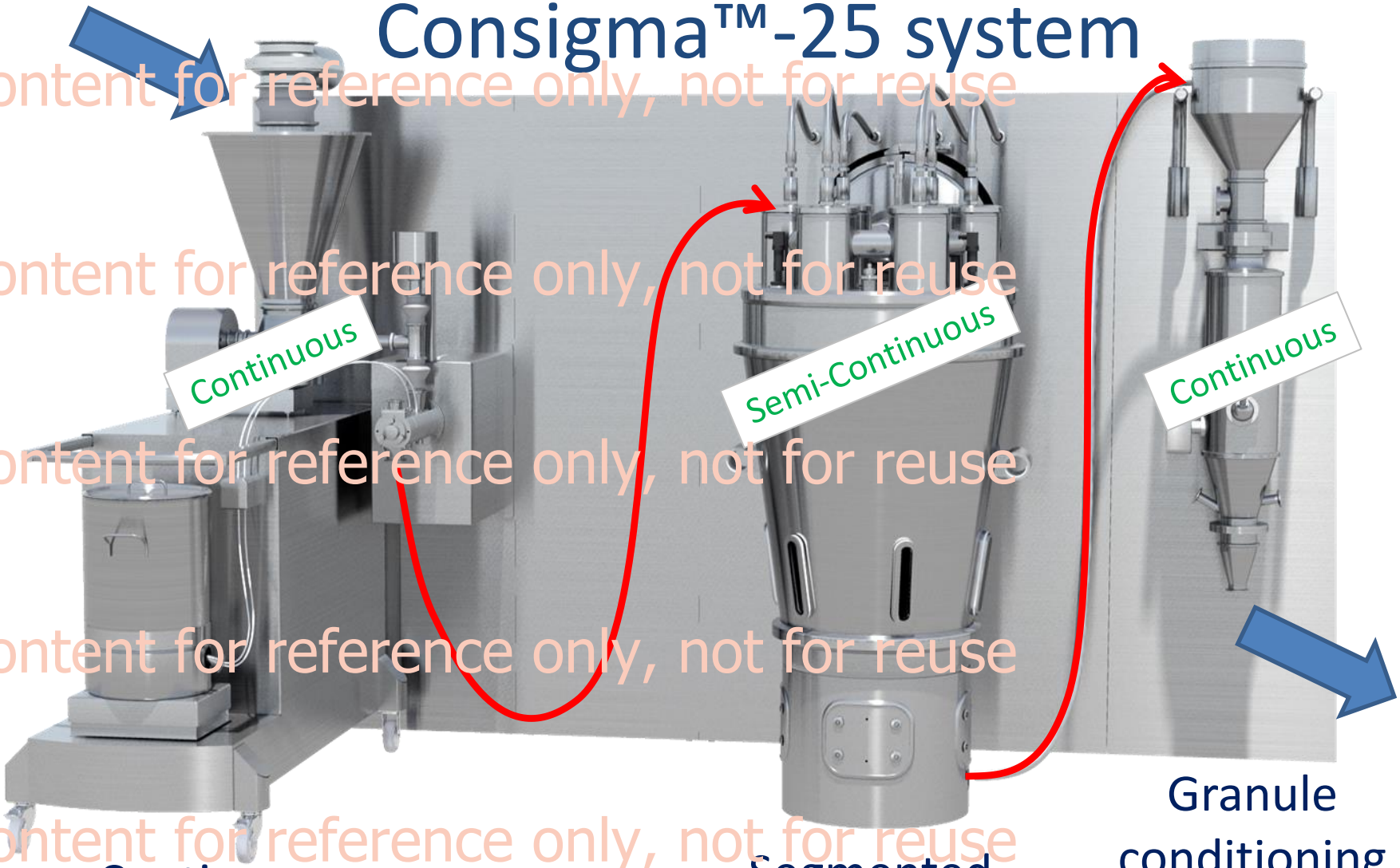
Continuous manufacturing line Consigma™-25 system

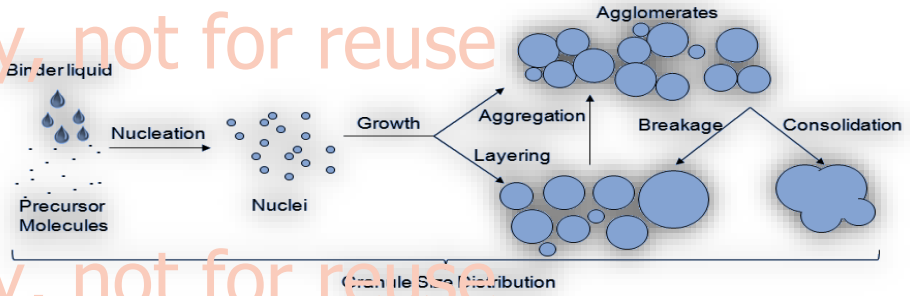


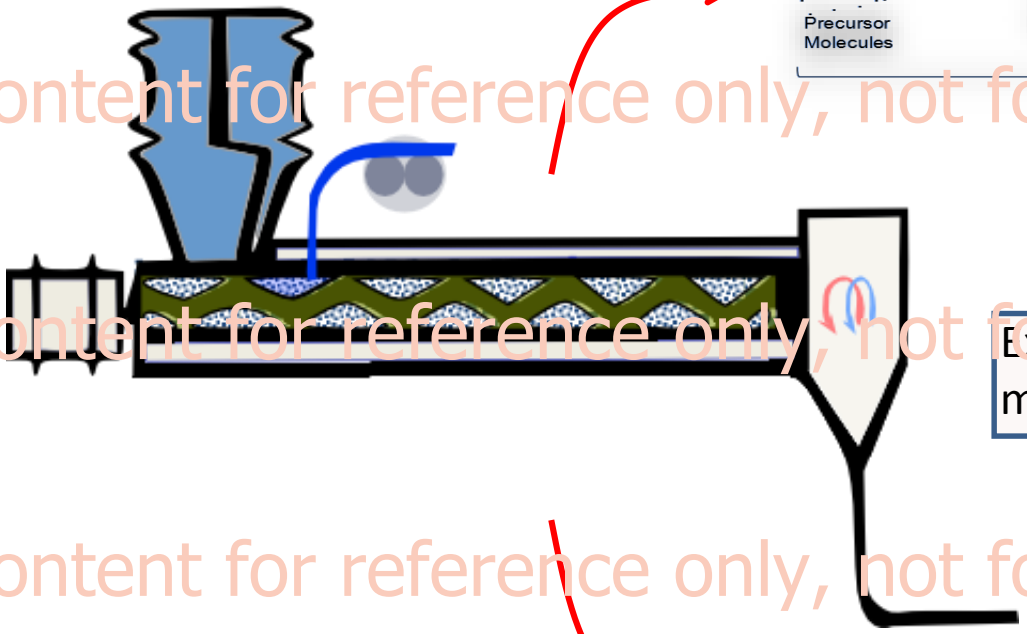
Continuous twin-screw granulator

Segmented Fluid bed dryer

Granule conditioning module

Both geometry and process conditions drive constitutive mechanisms





Experimental measurement

PBM

DEM

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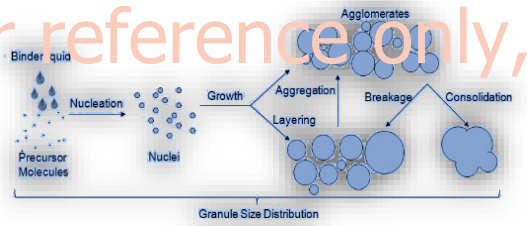
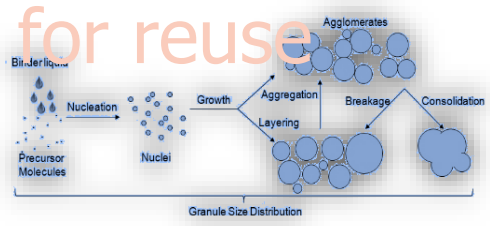
Understanding the role of screw design





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Consigma™-1 system

(GEA pharma systems, Collette)

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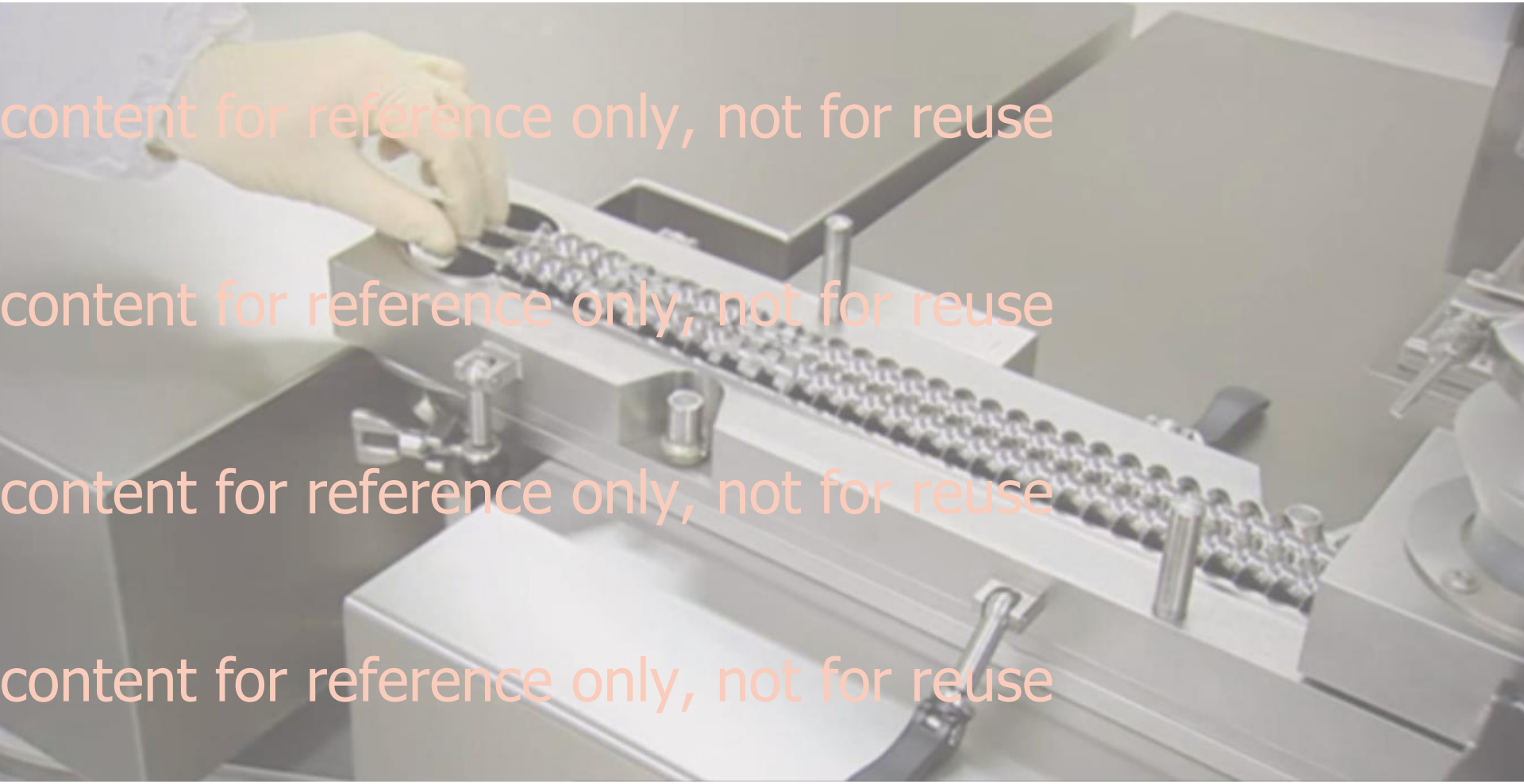
Open barrel of a twin screw granulator



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Consigma™- 1 experiments

Granulated Lactose monohydrate with distilled water

Factors:

Parameters	Low	High
Throughput	10 Kg/h	25 Kg/h
Liquid-solid ratio	4.58 %	6.52%
Screw speed	500 RPM	900 RPM

Responses: Particle characterization by Dynamic Image Analysis (Location 1, 3, 5)

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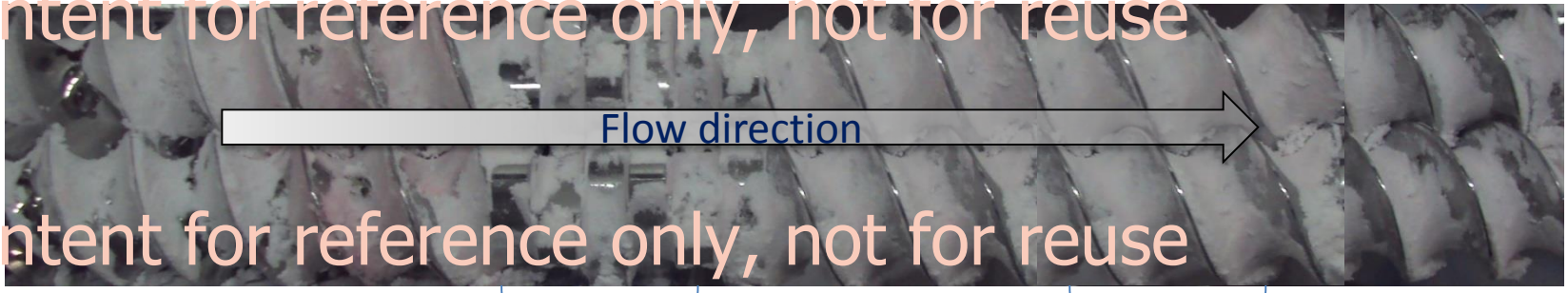
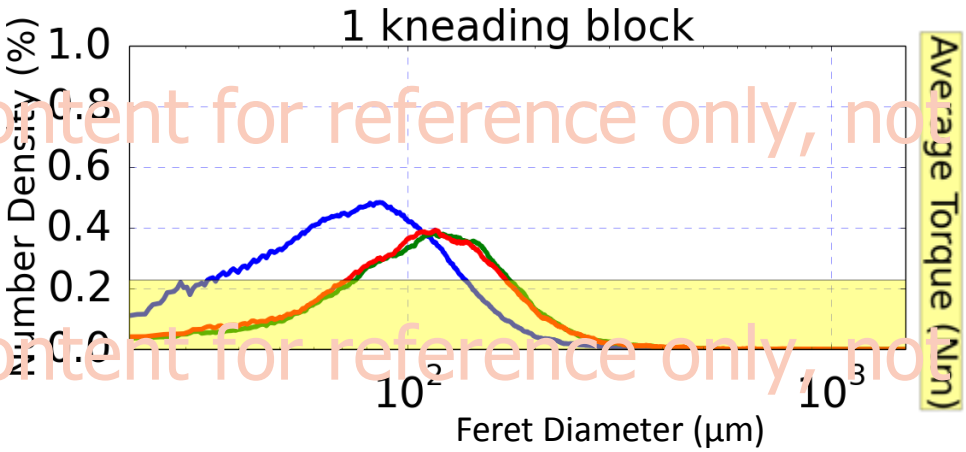
Consigma™-1 experiments



1 | 2 kneading block 1 | 3 | 4 kneading block 2 | 5

Throughput High	Liquid-solid ratio High	Screw speed Low



For details see: Kumar, et al. "Experimental investigation of granule size and shape dynamics in twin-screw granulation." *I J Pharma* 475.1 (2014): 485-495.

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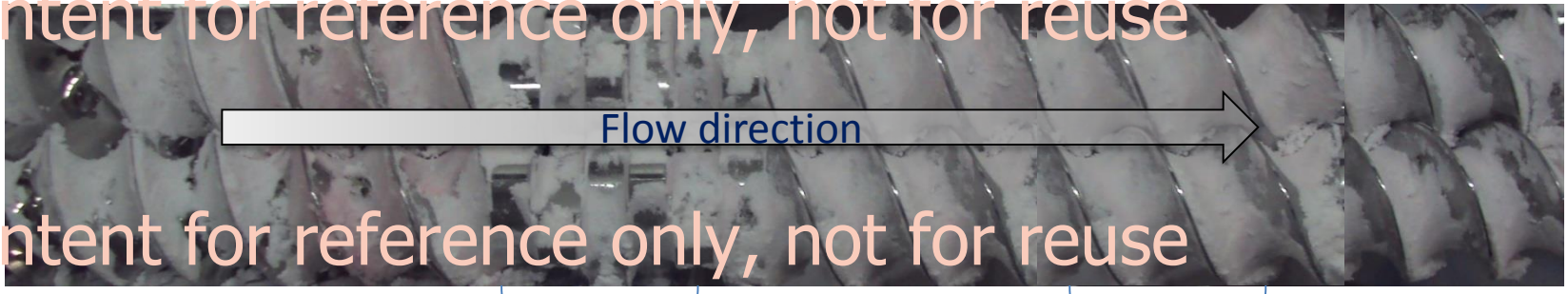
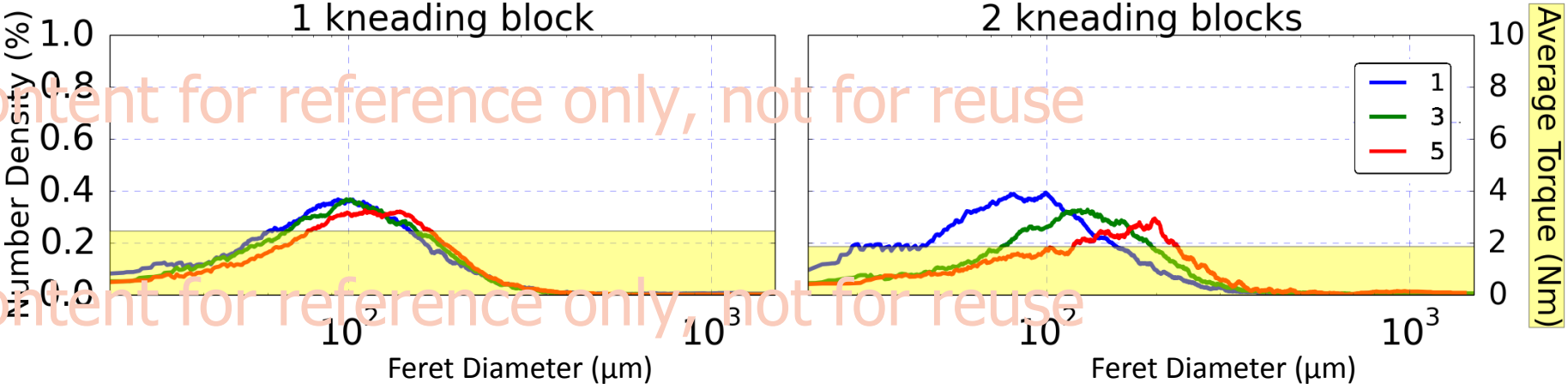
Consigma™-1 experiments

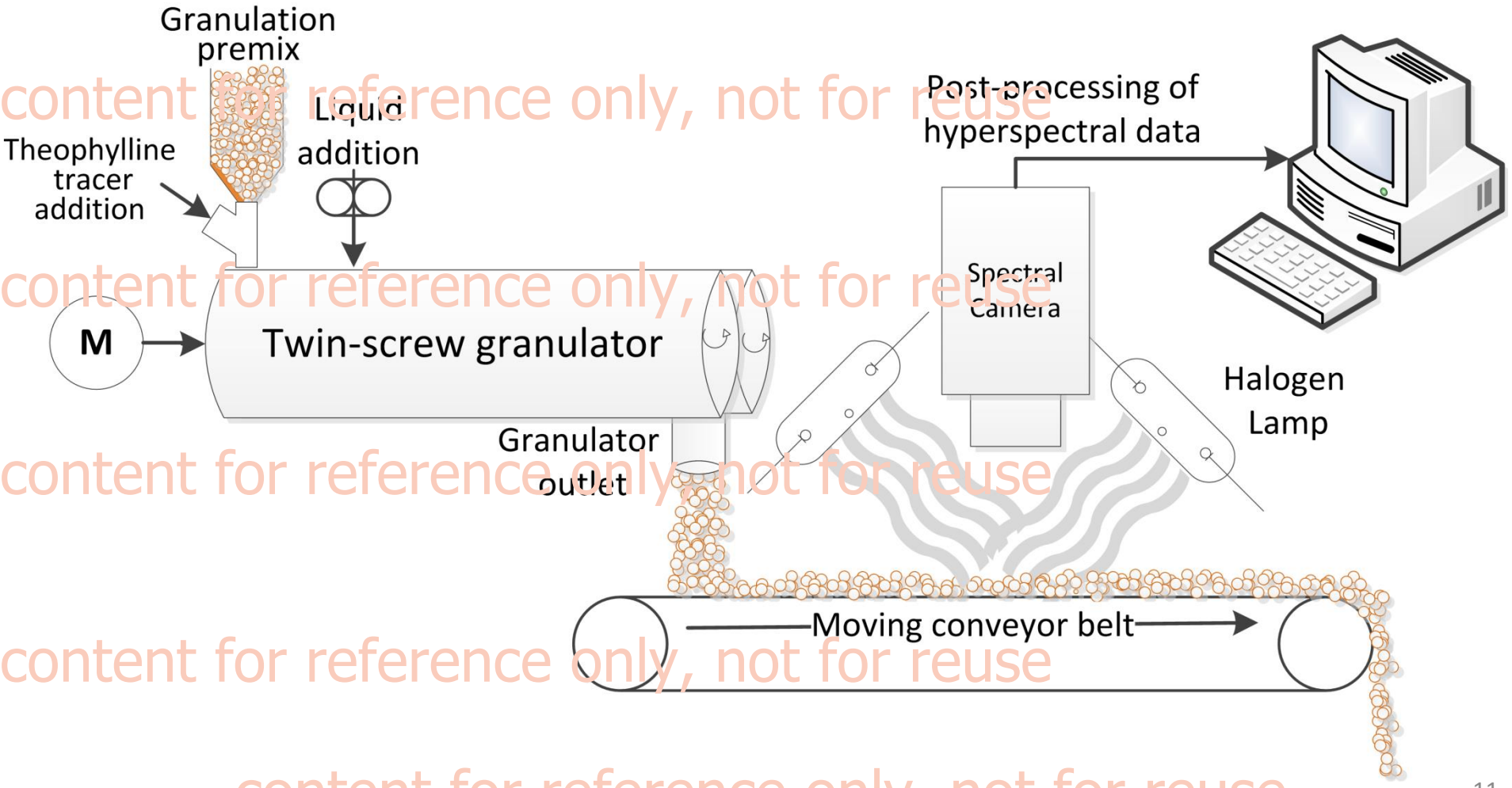


Throughput High	Liquid-solid ratio High	Screw speed High



For details see: Kumar, et al. "Experimental investigation of granule size and shape dynamics in twin-screw granulation." *I J Pharma* 475.1 (2014): 485-495.

Tracer concentration in granules produced was measured using NIR chemical imaging



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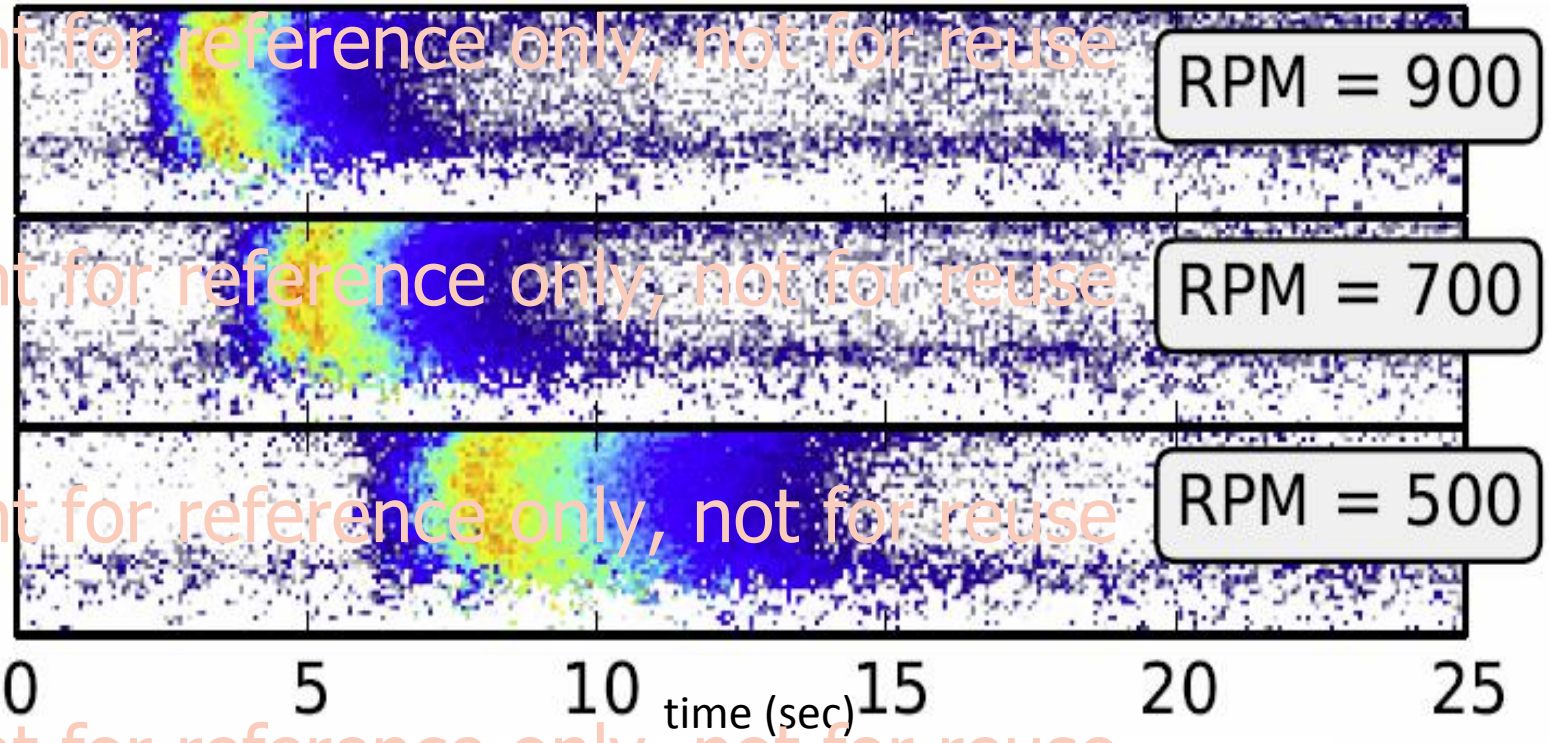
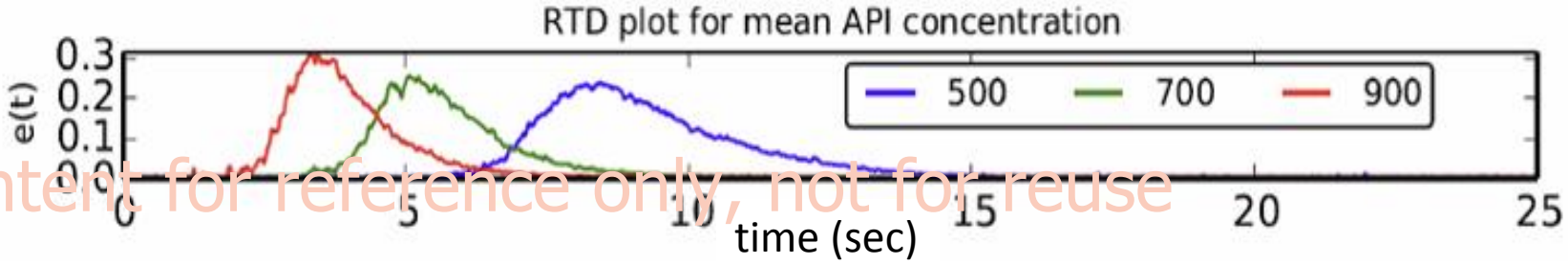
API Map was used to measure RTD





For details see: Kumar, et al. "Mixing and transport during pharmaceutical twin-screw wet granulation: Experimental analysis via chemical imaging." *Eur J Pharm Biopharm.* 87.2 (2014): 279-289.

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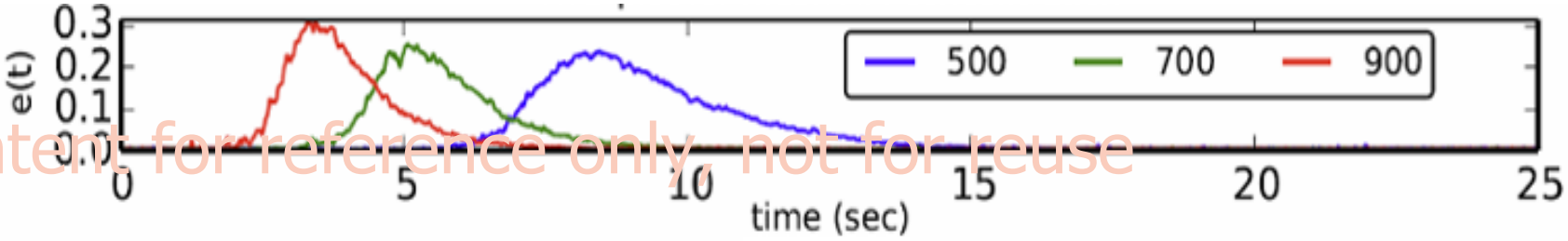
Measure of the mean of the distribution



$$\tau = \frac{\int_0^\infty t \cdot e(t)dt}{\int_0^\infty e(t)dt}$$

Mean residence time, τ

For details on results visit my presentation in Imaging Session of IPFAC 2015 on :
"Mixing and transport during pharmaceutical twin-screw wet granulation: Experimental analysis via chemical imaging"
or
Read: Kumar, et al. *E J Pharma. Biopharma.* 87.2 (2014): 279-289.

Population balance models can track granule attributes

$$\frac{\partial n(t,x)}{\partial t} = \frac{Q_{in}}{\tilde{V}} n_{in}(x) - \frac{Q_{out}}{\tilde{V}} n_{out}(x)$$

GSD balance

Aggregation term

$$+\frac{1}{2}\int_0^x \beta(t, x-\varepsilon, \varepsilon)\, n(t, x-\varepsilon)\, n(t,\varepsilon)\, d\varepsilon$$

aggregation rate

$$-n(t,x)\int_0^\infty \beta(t,x,\varepsilon)\, n(t,\varepsilon)\, d\varepsilon$$

aggregation rate

Breakage term

$$+\int_0^\infty b(x,\varepsilon) S(\varepsilon) n(t,\varepsilon)\, d\varepsilon$$

breakage fun. selection rate

$$-S(x) n(t,x)$$

selection rate

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Semi-empirical kernels

Aggregation Kernel

$$\beta(x, y) = \beta_0$$

(Constant kernel)

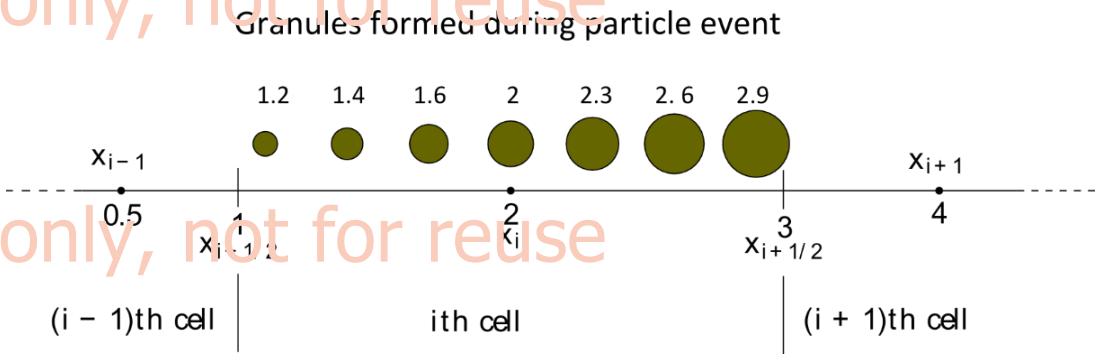
Breakage Kernel

$$S(y) = S_0 (y)^{\mu}$$

$$b(x, y) = \frac{\frac{\phi\gamma x^{\gamma-1}}{y^{\gamma}} + \frac{(1-\phi)\alpha x^{\alpha-1}}{y^{\alpha}}}{\frac{\phi\gamma}{\gamma+1} + \frac{(1-\phi)\alpha}{\alpha+1}}$$

(Austin, 2002)

Cell-average technique



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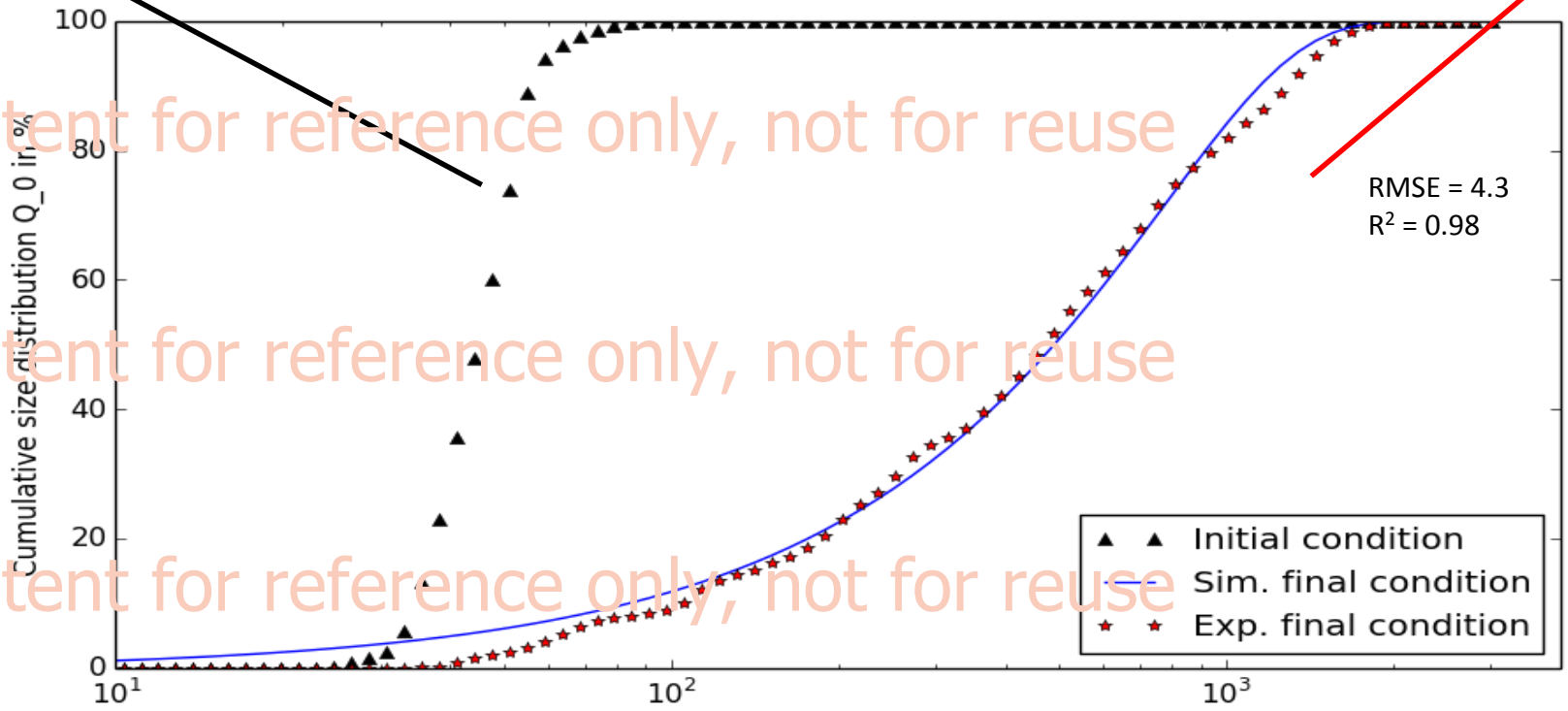
Experimental and simulated data have a good agreement



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Particle population dynamics during granulation

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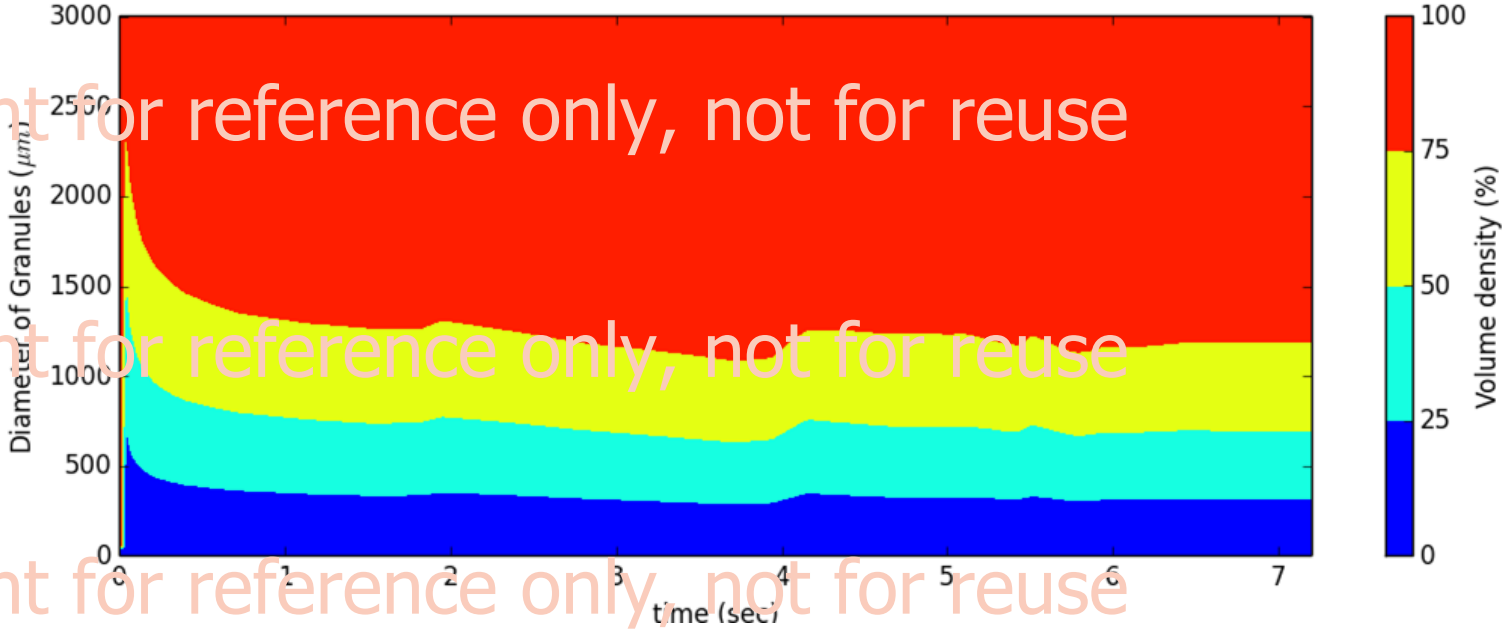

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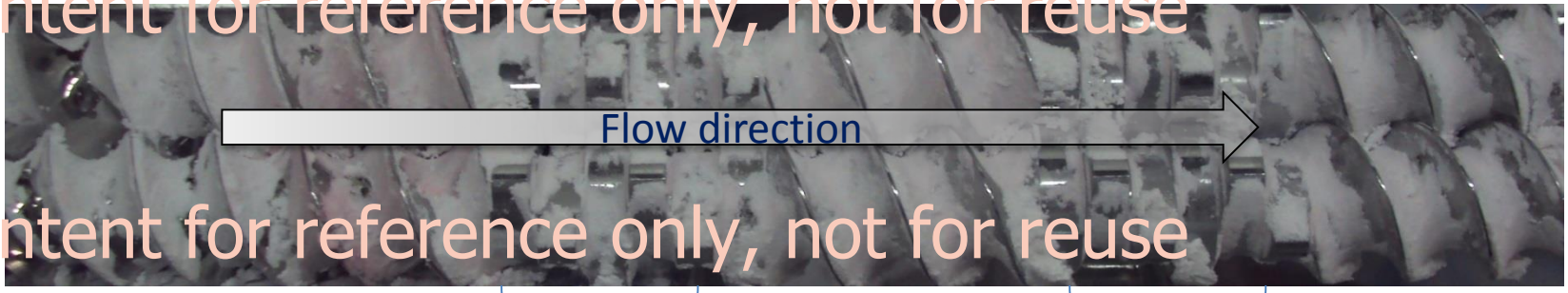
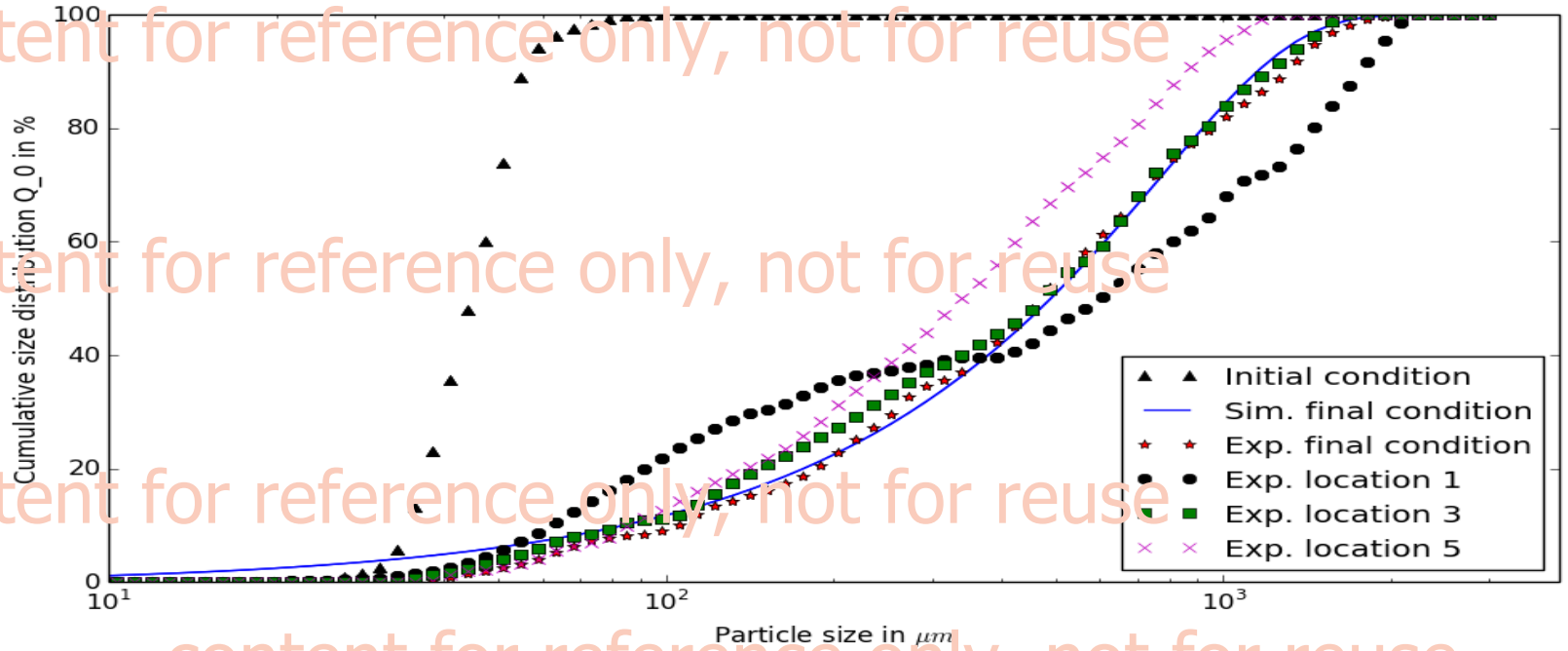
including effect of granulator design on granule size distribution



1 2 3 4 5



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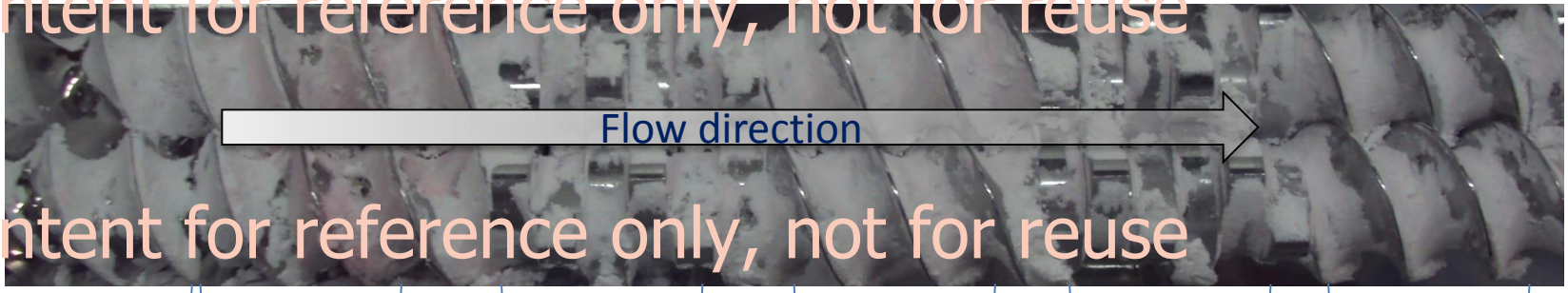
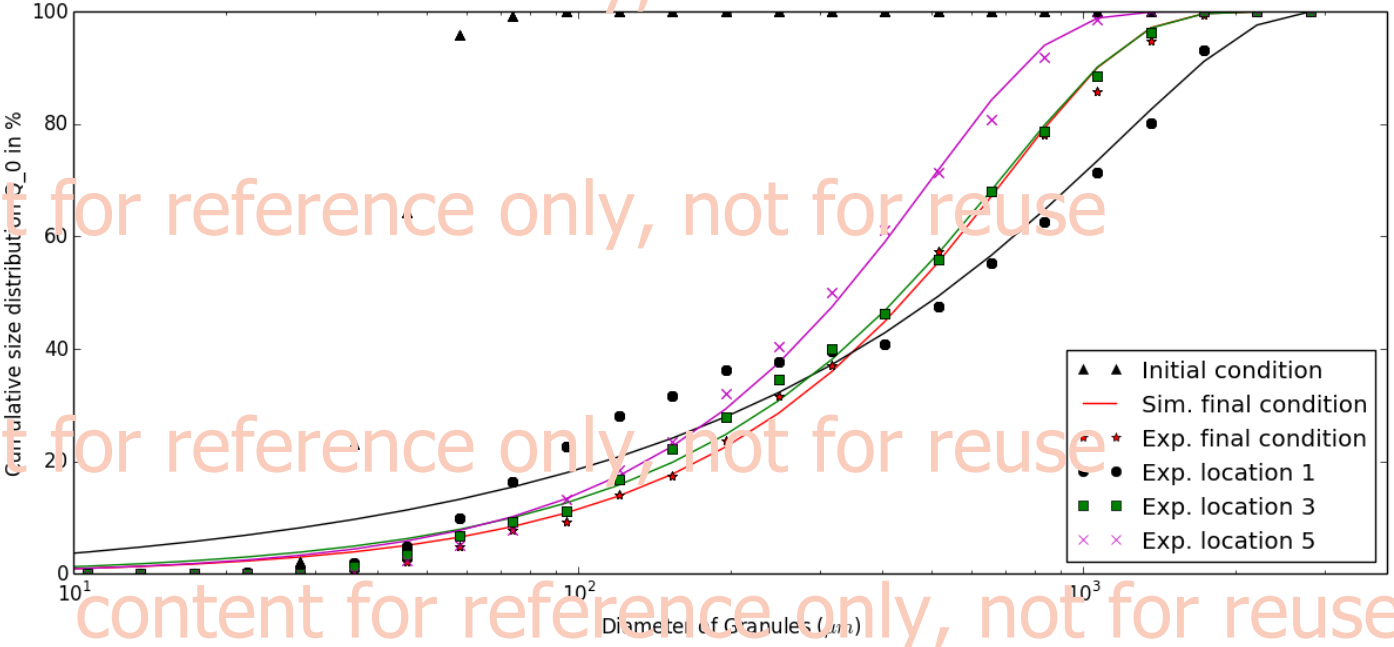
Including effect of granulator design on granule size distribution



	Start	1	2	3	4	5
PMSE		16.25		2.72		2.14



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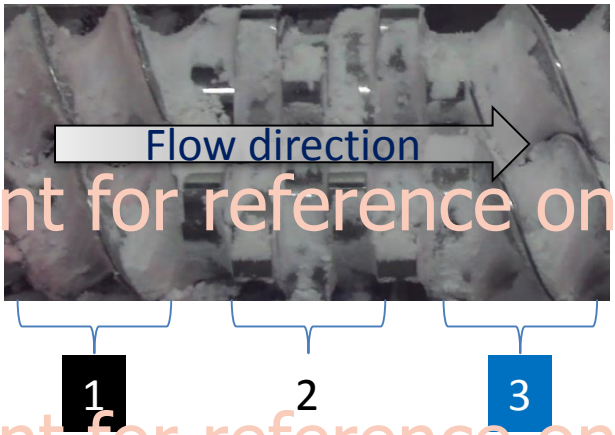
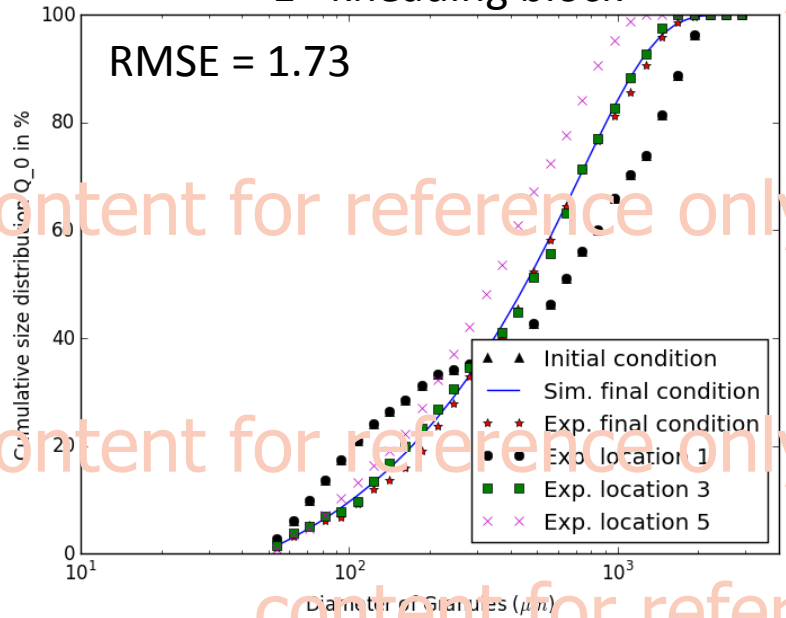
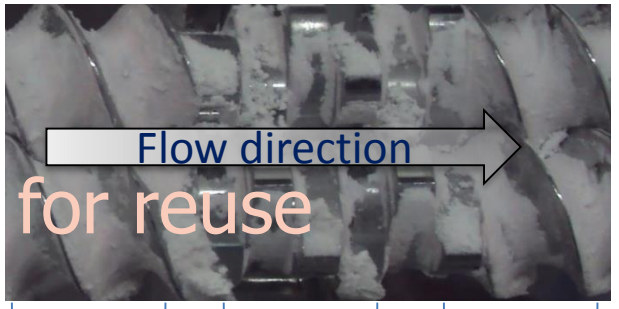
Including effect of granulator design on granule size distribution

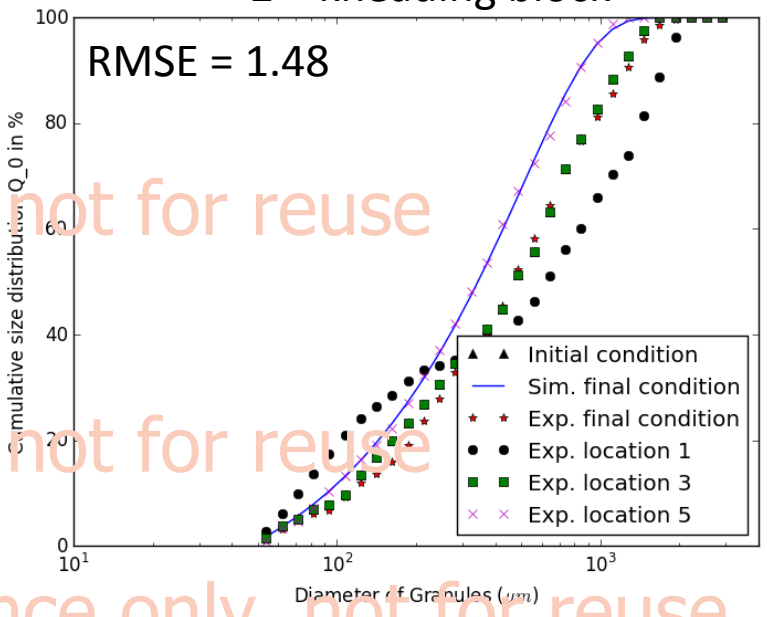


1st kneading block





2nd kneading block



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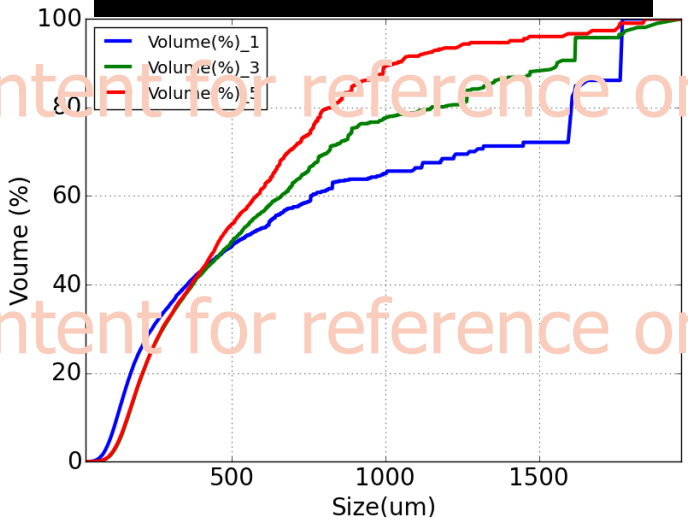
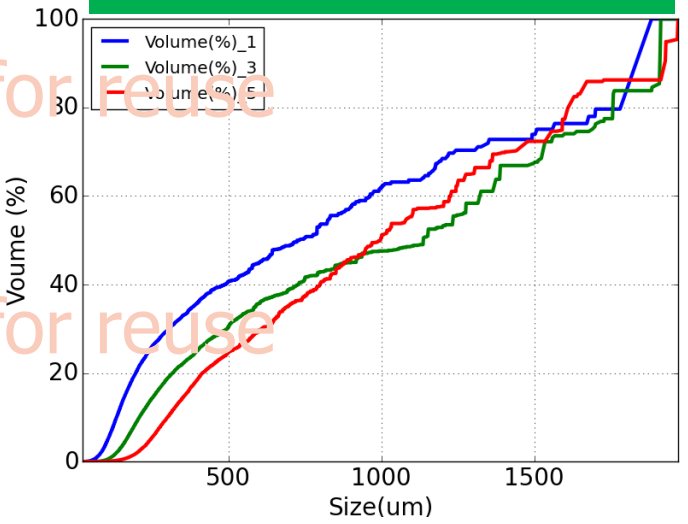
Throughput High | Liquid-solid ratio High | Screw speed Low

1 mixing zone

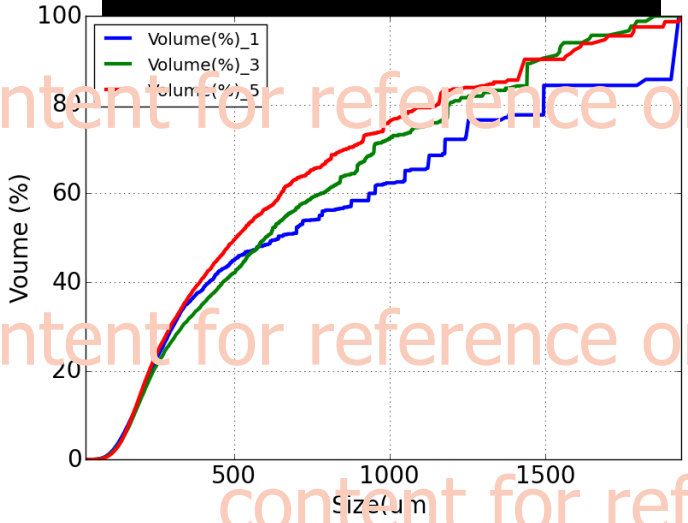


2 mixing zones

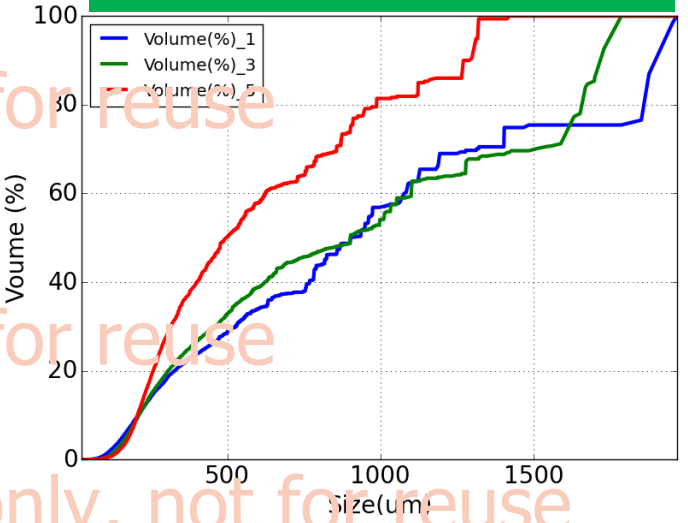


Throughput High | Liquid-solid ratio High | Screw speed High

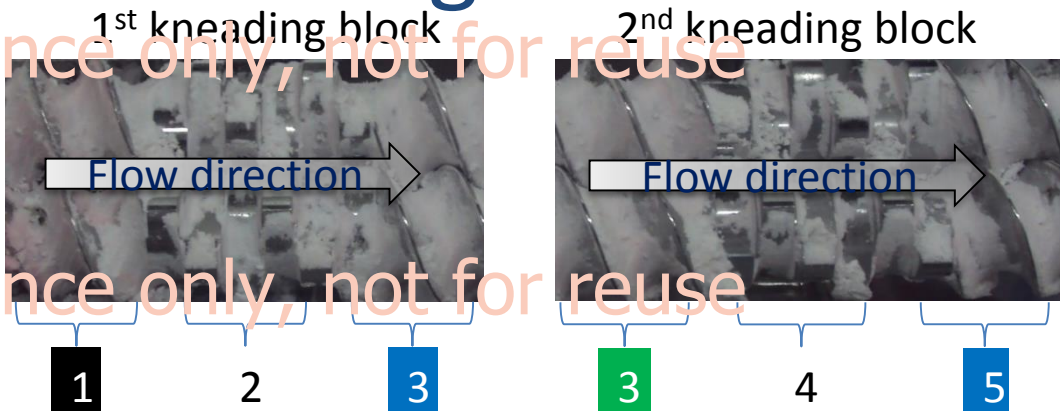
1 mixing zone



2 mixing zones



Investigating effect of screw speed and screw configuration



High throughput, high L/S

	Low Screw Speed				High Screw Speed			
	1 mixing zone		2 mixing zones		1 mixing zone		2 mixing zones	
Zone	1-3	3-5	1-3	3-5	1-3	3-5	1-3	3-5
RMSE	2.424	2.317	2.716	3.929	1.153	3.366	8.176	3.772
R^2	0.989	0.987	0.984	0.983	0.989	0.983	0.97	0.982

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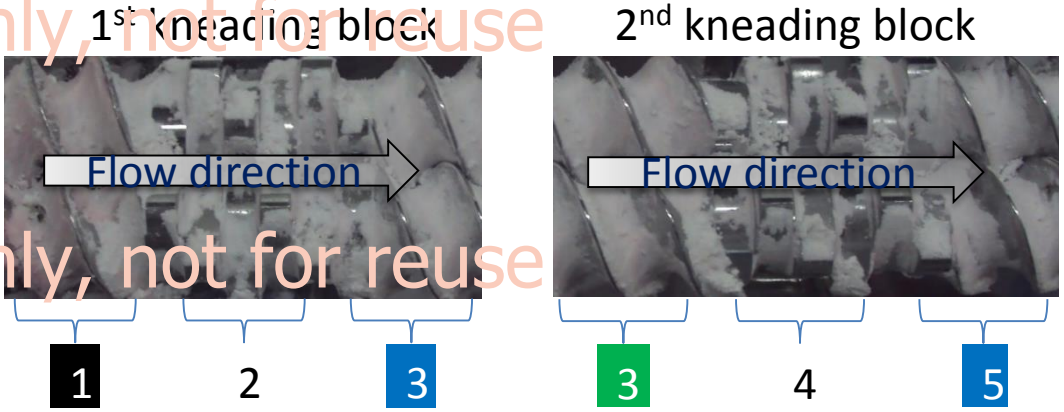

High throughput, high L/S

	Low Screw Speed				High Screw Speed			
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Zone	1-3	3-5	1-3	3-5	1-3	3-5	1-3	3-5
RMSE	2.424	2.317	2.716	3.929	1.153	3.366	8.176	3.772
R^2	0.989	0.987	0.984	0.983	0.989	0.983	0.97	0.982
β_0	1.05E-03	3.12E-01	3.11E-03	1.20E-02	2.36E-04	2.95E-01	8.97E-02	2.44E-01
S_0	0.030	3.304	0.023	0.062	0.051	1.180	0.030	3.340
α	6.01E-02	1.65E-07	1.47E-05	5.09E-04	1.86E-04	1.14E-06	1.39E-03	6.37E-07
γ	0.52	0.42	3.69	0.63	0.83	0.31	0.26	0.48
ϕ	0.97	0.72	0.93	0.98	0.41	0.53	1.00	0.48

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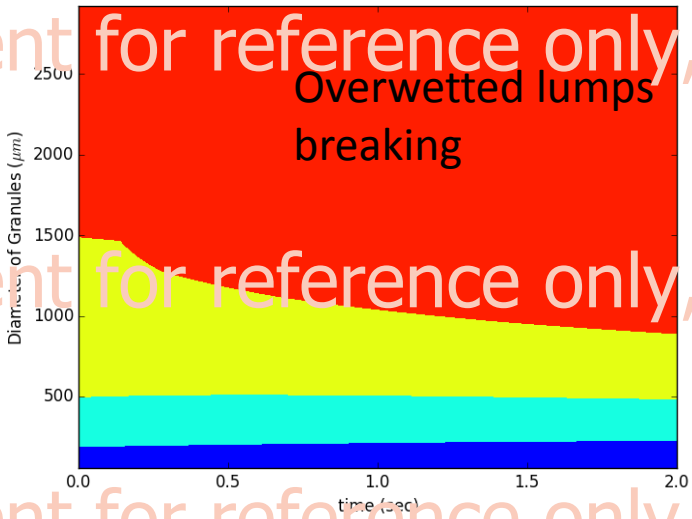
Throughput High

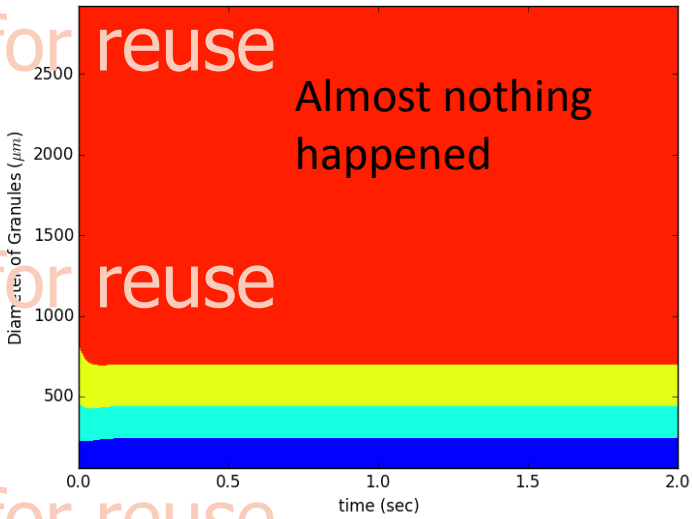
Liquid-solid ratio High

Screw speed Low

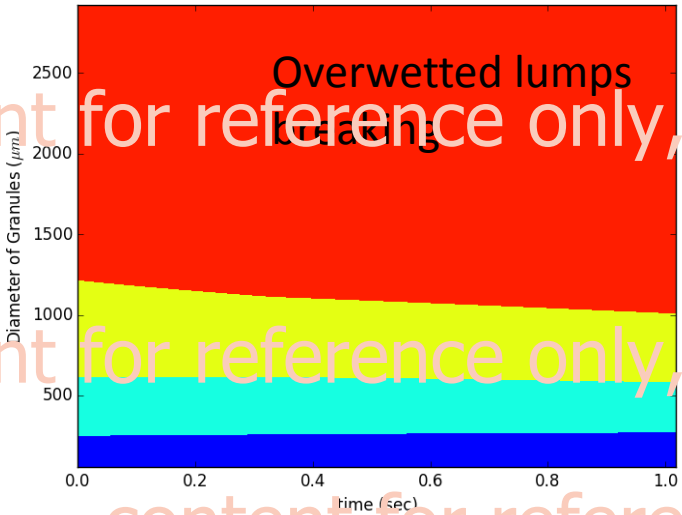
Location 1-3

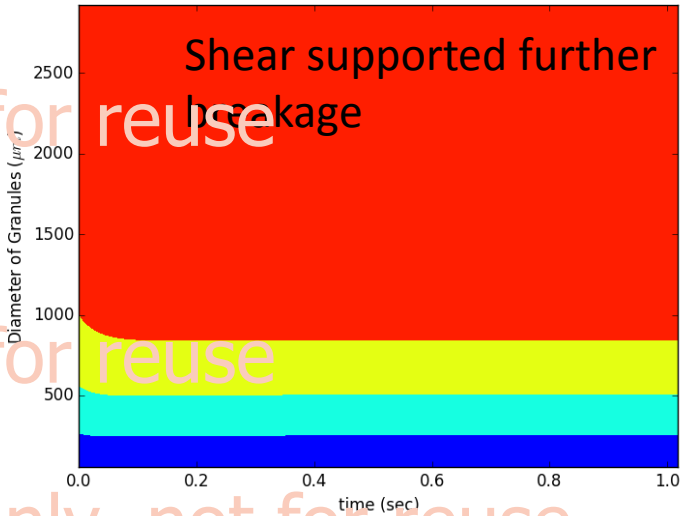
Location 3-5



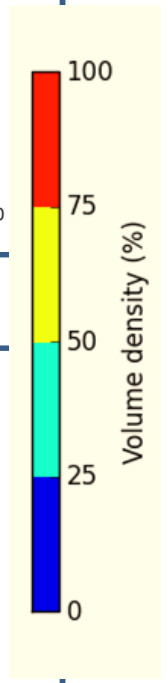


Screw speed High





1 mixing zone



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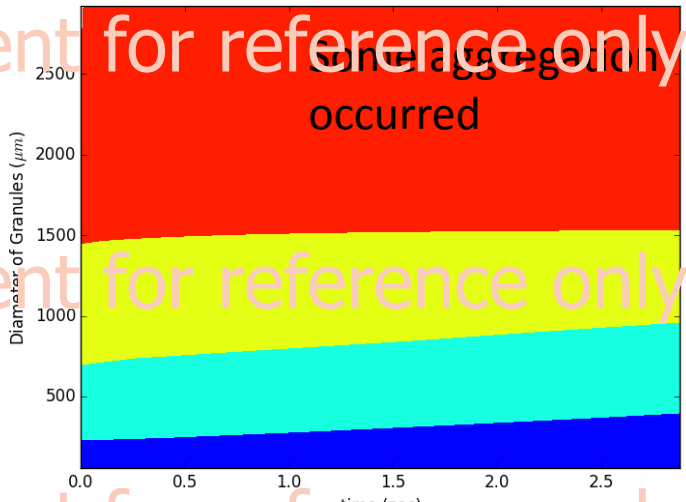
Throughput High

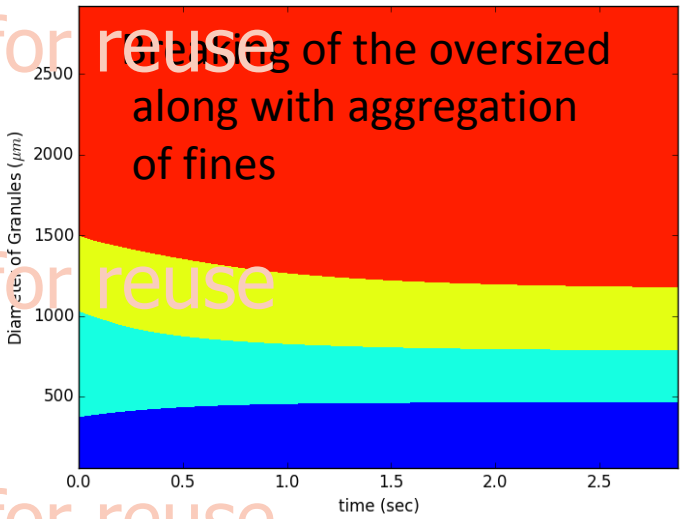
Liquid-solid ratio High

Screw speed Low

Location 1-3

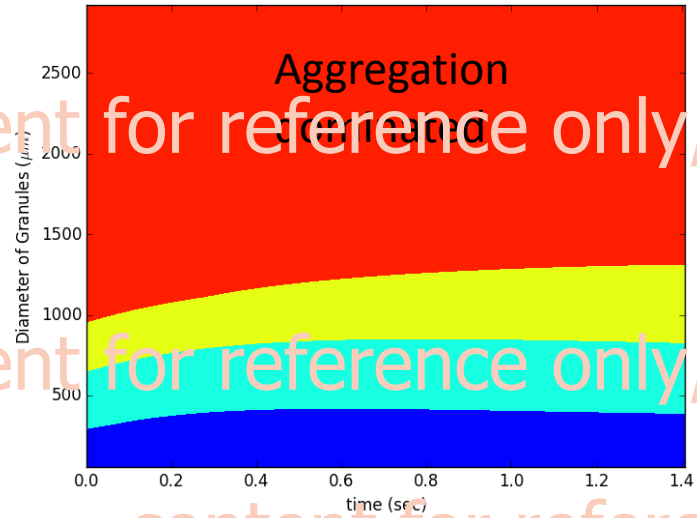
Location 3-5

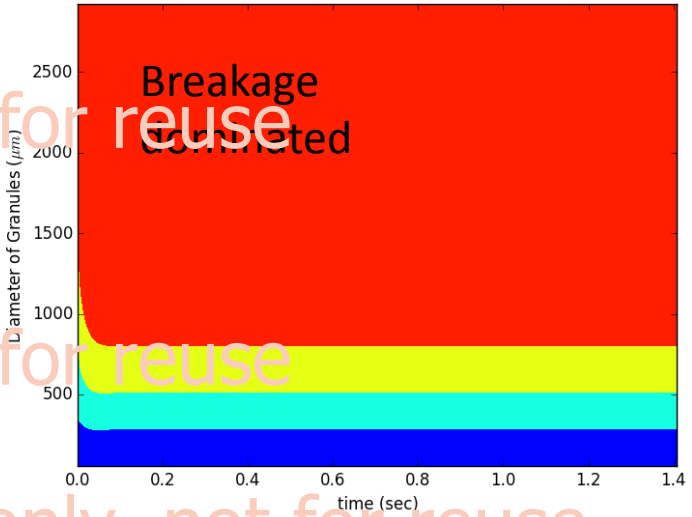


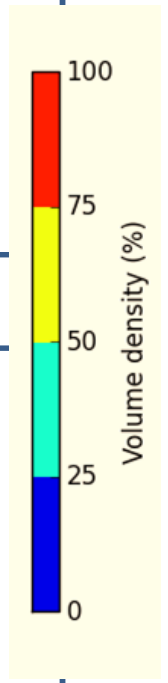


mixing zones

Screw speed High







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Conclusions

Along with experimental study, an improved insight can be obtained by model-based analysis.

Wetting kinetics requires a separate explanation in the twin-screw granulation modelling.

Aggregation and breakage are most dominant phenomena in the twin-screw granulation.

Particle population dynamics and screw geometry effect can be better understood by compartmental PBM, and can ultimately be used for predictive modelling of twin-screw granulation.

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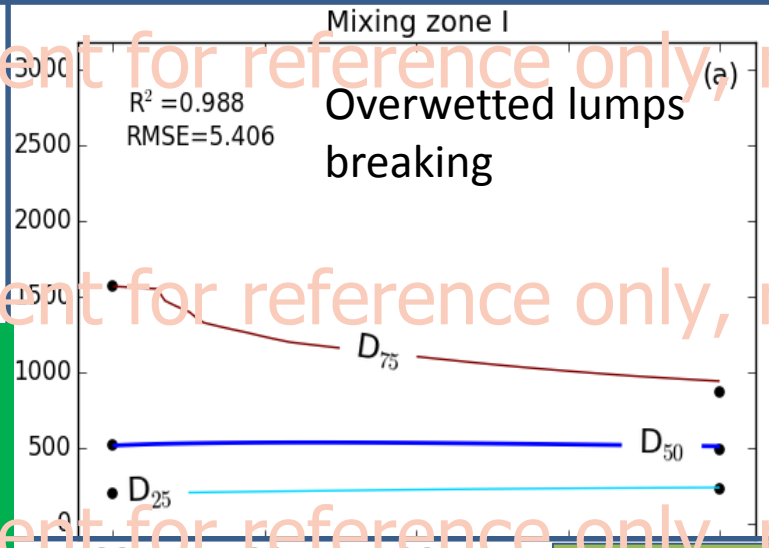
Throughput High

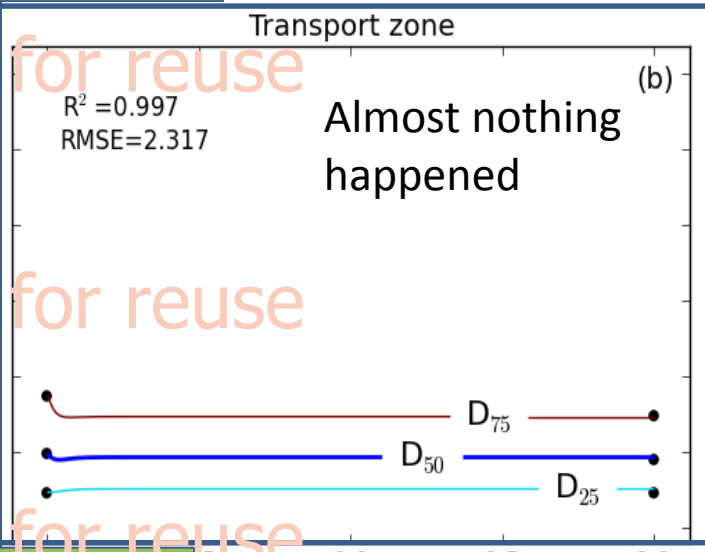
Liquid-solid ratio High

Screw speed Low

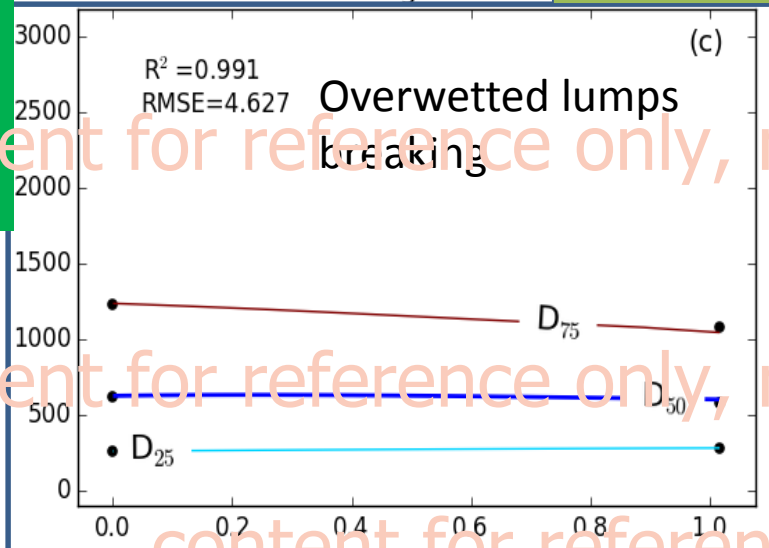
Location 1-3

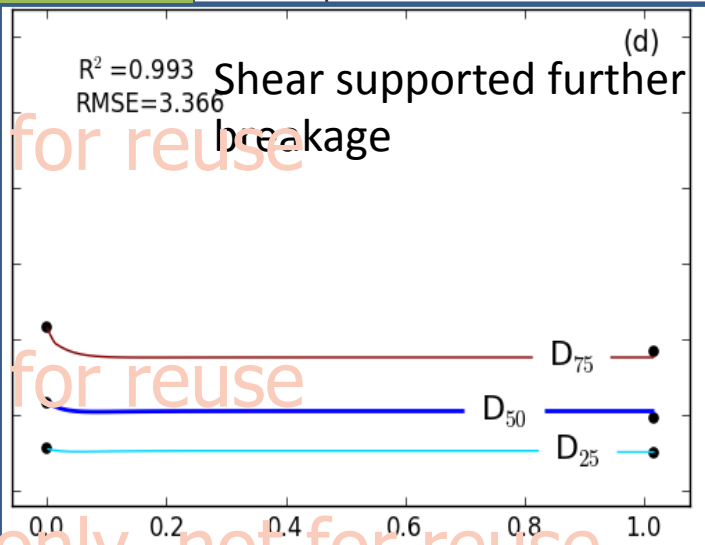
Location 3-5



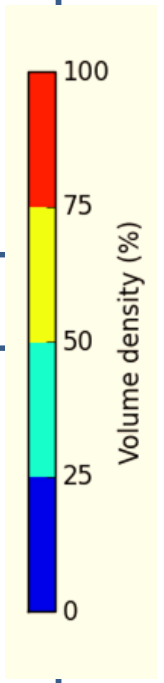


Screw speed High





1 mixing zone



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Throughput High

Liquid-solid ratio High

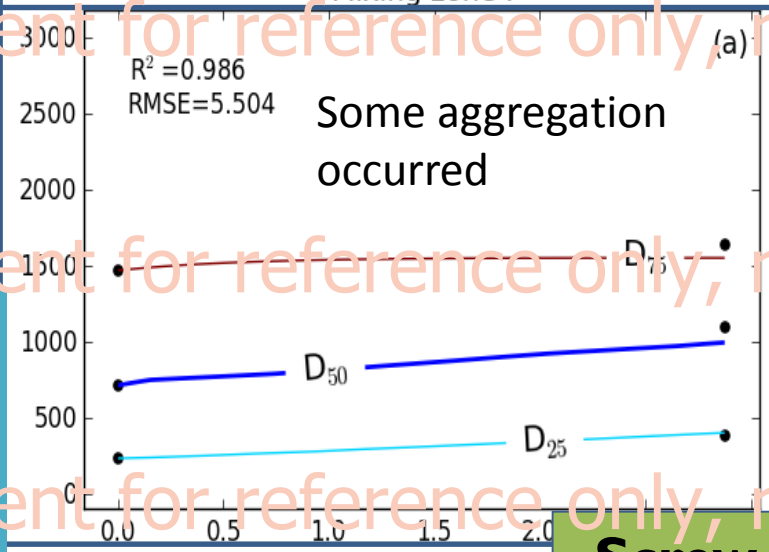
Screw speed Low

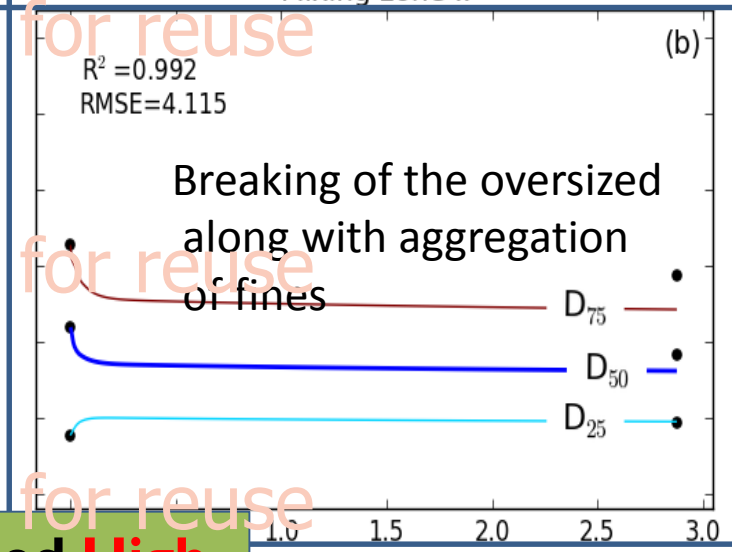
Location 1-3

Location 3-5

Mixing zone I

Mixing zone II

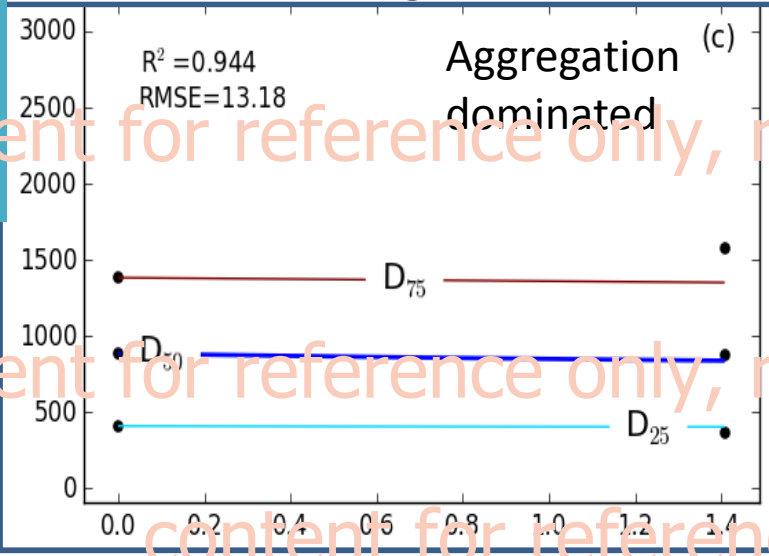


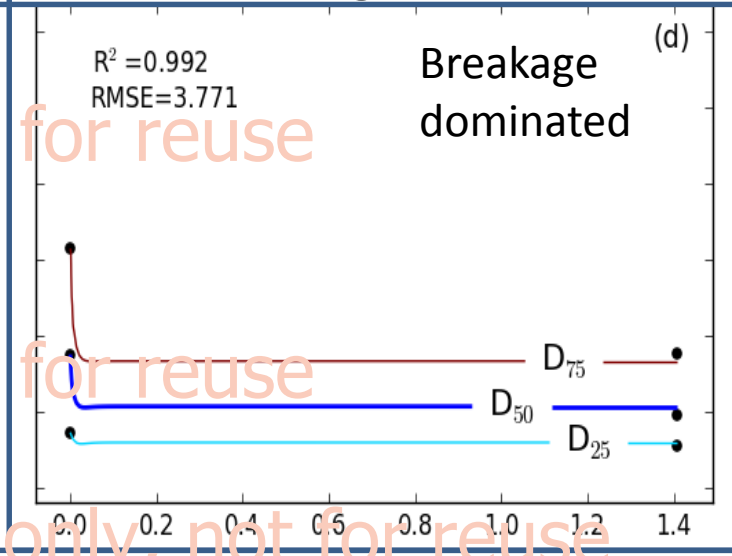
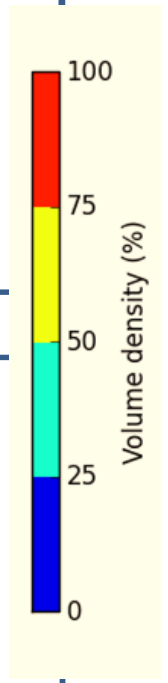


Screw speed High

Mixing zone I

Mixing zone II





Mixing zones